

Homework 5

Shaobo Wang

Question 1.

```
clear;clc
```

(a)

Assume $a = 100$, the system plant model is:

$$G(s) = \frac{1}{s^2 + 2s + 10000} \begin{bmatrix} s - 10000 & 100(s + 1) \\ -100(s + 1) & s - 10000 \end{bmatrix}$$

```
s = tf('s');  
a = 100;  
G = (1/(s^2+a/50*s+a^2))*[s-a^2,a*(s+1);-a*(s+1),s-a^2];
```

Find the poles of the system:

```
p = roots([1,a/50,a^2])
```

```
p = 2×1 complex  
-1.0000 +99.9950i  
-1.0000 -99.9950i
```

Find the directions with SVD by choosing the vector corresponding to $\bar{\sigma}$:

```
Gp1 = evalfr(G,p(1));  
[Up1,Sp1,Vp1] = svd(Gp1);
```

Output direction of the first pole:

```
outdirp1 = Up1(:,1)
```

```
outdir1 = 2×1 complex  
-0.7071 + 0.0035i  
-0.0035 - 0.7071i
```

Input direction of the first pole:

```
indirp1 = Vp1(:,1)
```

```
indir1 = 2×1 complex  
0.7071 + 0.0000i  
0.0000 + 0.7071i
```

```
Gp2 = evalfr(G,p(2));  
[Up2,Sp2,Vp2] = svd(Gp2);
```

Output direction of the second pole:

```
outdirp2 = Up2(:,1)
```

```
outdir2 = 2×1 complex
-0.7071 - 0.0035i
-0.0035 + 0.7071i
```

Input direction of the second pole:

```
indirp2 = Vp2(:,1)
```

```
indir2 = 2×1 complex
0.7071 + 0.0000i
0.0000 - 0.7071i
```

Find the zeros of the system:

```
z = tzero(minreal(G))
```

```
z = 2×1 complex
0.0000 +100.0000i
0.0000 -100.0000i
```

Find the directions with SVD by choosing the vector corresponding to $\underline{\sigma}$:

```
Gz1 = evalfr(G,z(1));
[Uz1,Sz1,Vz1] = svd(Gz1);
```

```
Uz1 = 2×2 complex
-0.0071 - 0.7071i -0.2315 - 0.6682i
0.7071 - 0.0071i -0.6682 + 0.2315i
Sz1 = 2×2
100.0050 0
0 0.0000
Vz1 = 2×2 complex
-0.7071 + 0.0000i -0.7071 + 0.0000i
0.0000 - 0.7071i 0.0000 + 0.7071i
```

Output direction of the first zero:

```
outdirz1 = Uz1(:,1)
```

Input direction of the first zero:

```
indirz1 = Vz1(:,1)
Gz2 = evalfr(G,z(2));
[Uz2,Sz2,Vz2] = svd(Gz2)
```

```
Uz2 = 2×2 complex
-0.0071 + 0.7071i -0.2315 + 0.6682i
0.7071 + 0.0071i -0.6682 - 0.2315i
Sz2 = 2×2
100.0050 0
0 0.0000
Vz2 = 2×2 complex
-0.7071 + 0.0000i -0.7071 + 0.0000i
0.0000 + 0.7071i 0.0000 - 0.7071i
```

Output direction of the second zero:

```
outdirz2 = Uz2(:,1)
```

Input direction of the second zero:

```
indirz2 = Vz2(:,1)
```

(b) The rank of a matrix will not change if a full rank matrix is multiplied to original matrix:

$$\begin{bmatrix} A - sI + BK & B \\ C + DK & D \end{bmatrix} = \begin{bmatrix} A - sI & B \\ C & D \end{bmatrix} \begin{bmatrix} I & O \\ K & I \end{bmatrix}$$

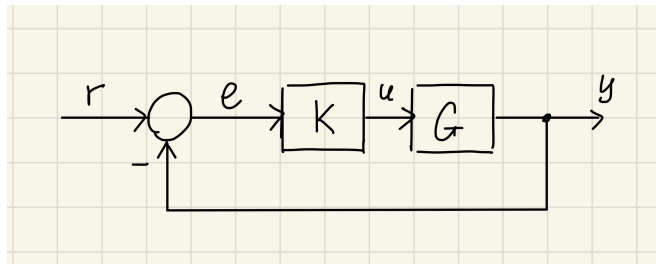
The matrix $\begin{bmatrix} I & O \\ K & I \end{bmatrix}$ is always full rank because of its diagonal entries are all ones.

Therefore, the rank of system matrix will not be affected by the state feedback:

$$\text{rank}\left(\begin{bmatrix} A - sI + BK & B \\ C + DK & D \end{bmatrix}\right) = \text{rank}\left(\begin{bmatrix} A - sI & B \\ C & D \end{bmatrix}\right)$$

Problem 2

(a) Define signal $e = r - y$, the equivalent system block diagram is:



Assume $d_y = 0$, derive the TF of K

$$\begin{cases} e = r - y = r - GQr \\ u = Qr \end{cases} \Rightarrow u = Q(I - GQ)^{-1}e \Rightarrow K = Q(I - GQ)^{-1}$$

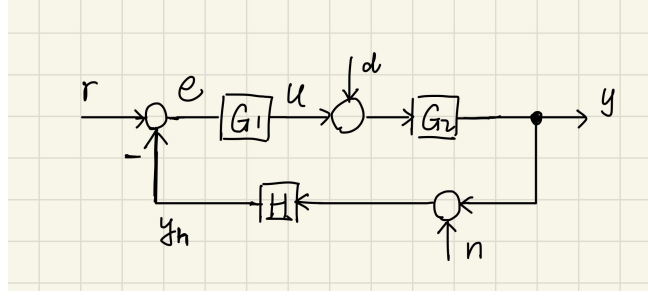
Solve for Q in terms of K :

$$Q = (I + KG)^{-1}K = K(I + GK)^{-1}$$

A system is internally stable if and only if $K(I + GK)^{-1}$ is stable.

Therefore, if Q is unstable, the IMC structure is internally unstable.

(b) Write out all the output signal in terms of input signal of the following system:



$$\begin{aligned}
 y &= (I + G_2 G_1 H)^{-1} G_2 d + (I + G_2 G_1 H)^{-1} G_2 G_1 r - (I + G_2 G_1 H)^{-1} G_2 G_1 H n \\
 u &= (I + G_1 H G_2)^{-1} G_1 r - (I + G_1 H G_2)^{-1} G_1 H n - (I + G_1 H G_2)^{-1} G_1 H G_2 d \\
 y_h &= (I + H G_2 G_1)^{-1} H n + (I + H G_2 G_1)^{-1} H G_2 d + (I + H G_2 G_1)^{-1} H G_2 G_1 r
 \end{aligned}$$

Therefore, there are nine conditions in total to meet in order for the system to be internally stable:

$$\left\{ \begin{array}{l}
 (I + G_2 G_1 H)^{-1} G_2 = G_2 (I + G_1 H G_2)^{-1} \\
 (I + G_2 G_1 H)^{-1} G_2 G_1 = G_2 (I + G_1 H G_2)^{-1} G_1 \\
 (I + G_2 G_1 H)^{-1} G_2 G_1 H = G_2 (I + G_1 H G_2)^{-1} G_1 H \\
 (I + G_1 H G_2)^{-1} G_1 \\
 (I + G_1 H G_2)^{-1} G_1 H \\
 (I + G_1 H G_2)^{-1} G_1 H G_2 \\
 (I + H G_2 G_1)^{-1} H = H (I + G_1 H G_2)^{-1} \\
 (I + H G_2 G_1)^{-1} H G_2 = H (I + G_1 H G_2)^{-1} G_2 \\
 (I + H G_2 G_1)^{-1} H G_2 G_1 = H (I + G_1 H G_2)^{-1} G_2 G_1
 \end{array} \right.$$

Define $Q = G_2 (I + G_1 H G_2)^{-1}$, we can proof: $\begin{cases} (I + G_1 H G_2)^{-1} = I - G_1 H Q \\ (I + G_2 G_1 H)^{-1} = I - Q G_1 H \end{cases}$

$$\left\{ \begin{array}{l}
 (I + G_2 G_1 H)^{-1} G_2 = G_2 (I + G_1 H G_2)^{-1} = Q \\
 (I + G_2 G_1 H)^{-1} G_2 G_1 = G_2 (I + G_1 H G_2)^{-1} G_1 = Q G_1 \\
 (I + G_2 G_1 H)^{-1} G_2 G_1 H = G_2 (I + G_1 H G_2)^{-1} G_1 H = Q G_1 H \\
 (I + G_1 H G_2)^{-1} G_1 = (I - G_1 H Q) G_1 \\
 (I + G_1 H G_2)^{-1} G_1 H = (I - G_1 H Q) G_1 H \\
 (I + G_1 H G_2)^{-1} G_1 H G_2 = I - (I + G_1 H G_2)^{-1} = G_1 H Q \\
 (I + H G_2 G_1)^{-1} H = H (I + G_2 G_1 H)^{-1} = H (I - Q G_1 H) \\
 (I + H G_2 G_1)^{-1} H G_2 = H G_2 (I + G_1 H G_2)^{-1} = H Q \\
 (I + H G_2 G_1)^{-1} H G_2 G_1 = I - (I + H G_2 G_1)^{-1} = Q G_1 H
 \end{array} \right.$$

All nine conditions can be written in terms of Q, G_1, H .

Therefore, if $H(s), G_1(s)$ are both stable, the condition for internal stability of the feedback system is $Q(s)$ stable.

Problem 3

The RHP zero and pole of the plant model are:

$$\begin{cases} z = 1 \\ p = 2 \end{cases}$$

Design the weight shape for a conventional loop shape.

Since we already know it's impossible to maintain conventions with those RHP zeros and poles, just boldly assume $M = 3, A = 0, M_T = 3$.

(1) bandwidth limitations

For sensitivity bandwidth, since $|S| = 1$ at the RHP zero,

$$1 > \|W_p S\|_\infty \geq \frac{|1+2|}{|1-2|} |W_p(1)| = 3|W_p(1)| \Rightarrow |W_p(1)| < \frac{1}{3}$$

The sensitivity weight is:

$$W_p(s) = \frac{s/M + \omega_{BW}}{s + \omega_{BW}A} = 1/3 + \omega_{BW}/s$$

Therefore, the S bandwidth limit is:

$$|1/3 + \omega_{BW}| < 1/3 \Rightarrow \omega_{BW} < 0$$

For complementary sensitivity bandwidth, since $|T| = 1$ at the RHP pole,

$$1 > \|W_T T\|_\infty \geq \frac{|1+2|}{|1-2|} |W_T(2)| = 3|W_T(2)| \Rightarrow |W_T(2)| < \frac{1}{3}$$

The complementary sensitivity weight is:

$$W_T(s) = s/\omega_{BT} + 1/M_T = s/\omega_{BT} + 1/3$$

Therefore, the T bandwidth limit is:

$$|2/\omega_{BW} + 1/3| < 1/3 \Rightarrow \omega_{BW} > \infty$$

This contradictory result basically means the desired loopshape cannot be met with RHP poles and zeros.

(2) minimum peak

Since we only have one RHP zero and one RHP pole, the sensitivity peak is:

$$\min_K \|S\|_\infty = \sqrt{\frac{|z+p|^2}{|z-p|^2}} = \sqrt{\frac{|1+2|^2}{|1-2|^2}} = 3$$