



Stark Industries Pvt. Ltd.

## PROBLEM STATEMENT – PS2: THE VOLATILE CARGO

### 1. Overview

STARK autonomous convoys carrying fragile Stark lab cargo must maintain comfort, stability, and safety over uneven roads. In this problem, you will design an Active Suspension controller for a 2-DOF quarter-car model and evaluate its performance on a set of pre-generated road profiles.

During this challenge, you are required to:

Load the provided dataset (road displacement vs. time) along with accelerometer signals from both the sprung and unsprung masses.

Implement or reuse a 2-DOF quarter-car dynamic model for a single wheel station using the given parameters.

Design your own Active Suspension controller that outputs the command  $c(t)$  within the given limits using only the accelerometer measurements and vehicle constraints (plus any causal internal memory).

Include a 20 ms actuator delay between the commanded  $c(t)$  and the applied  $c(t)$  in the dynamics.

Run the closed-loop model on all five road profiles and record the displacement responses of the sprung mass (required) and unsprung mass (bonus).

Compute and submit the required per-profile metrics in the specified format and include displacement plots in your report.

This problem tests your understanding of control systems, dynamic modelling, numerical simulation, and performance evaluation in a realistic automotive context.

## 2. Quarter-Car System Description

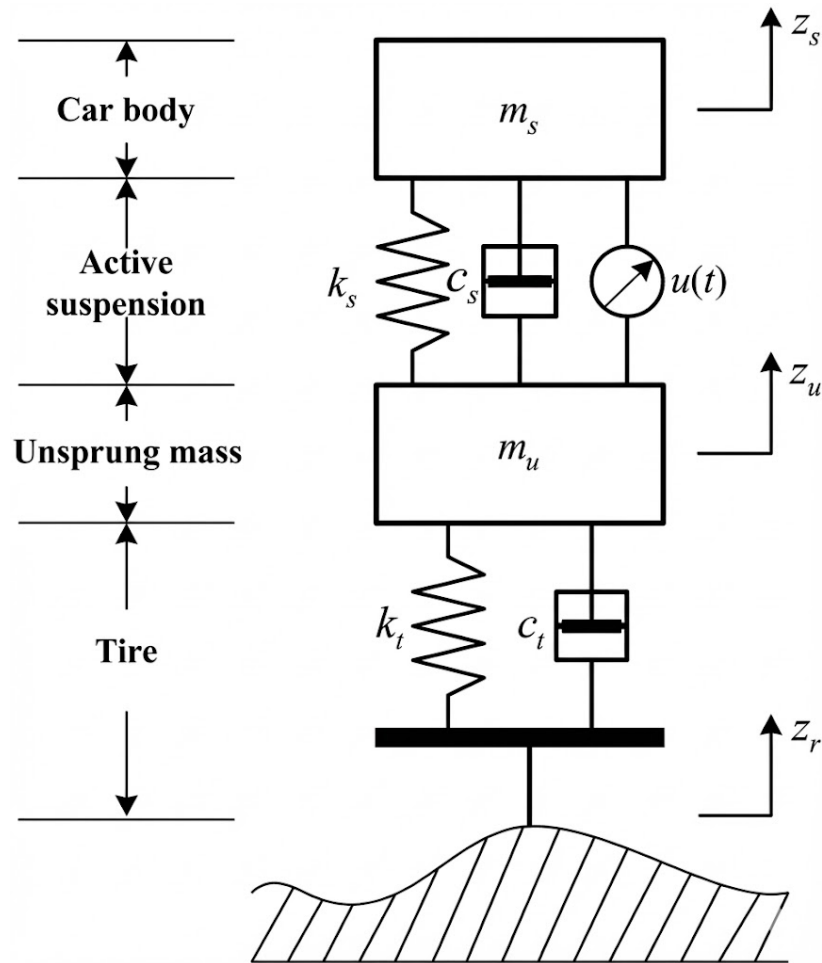
You will simulate a standard 2-DOF quarter-car model, representing one corner of a vehicle (one wheel and the associated body mass above it). The physical structure consists of:

- **Sprung mass ( $m_s$ ):** portion of vehicle body mass supported by the suspension (cabin + cargo).
- **Unsprung mass ( $m_u$ ):** wheel, hub, and associated suspension components.
- **Suspension spring ( $k_s$ ):** elastic element between sprung and unsprung mass.
- **Active suspension actuator command ( $c(t)$ ):** controllable suspension command applied between sprung and unsprung mass (you choose  $c(t)$  within limits).

- **Tire stiffness ( $k_t$ ):** vertical stiffness between unsprung mass and road surface.
- **Road displacement  $r(t)$ :** vertical motion of the road at the tire contact patch (given in the dataset).

Sprung-mass accelerometer  $a_s(t)$ : measured vertical acceleration of the body/cargo mass (provided in the dataset).

Unsprung-mass accelerometer  $a_u(t)$ : measured vertical acceleration of the wheel assembly (provided in the dataset).



You are free to choose the exact state-space representation and integration scheme, as long as it is physically consistent (for example: avoid negative damping, respect the command bounds, and ensure numerical stability).

## 2.1 Quarter-Car Parameters (Use These Values)

Use the following nominal parameters in all your simulations.

Parameter	Value	Description
<b>m<sub>s</sub></b>	290 kg	Sprung mass (vehicle body above suspension)
<b>m<sub>u</sub></b>	59 kg	Unsprung mass (wheel + hub + part of suspension)
<b>k<sub>s</sub></b>	16 000 N/m	Suspension spring stiffness
<b>k<sub>t</sub></b>	190 000 N/m	Tire vertical stiffness
<b>c<sub>min</sub></b>	800 N·s/m	Minimum damping coefficient (fully soft)
<b>c<sub>max</sub></b>	3 500 N·s/m	Maximum damping coefficient (fully stiff)

Your controller must always output a damping command  $c(t)$  that satisfies:

$$c_{\min} \leq c(t) \leq c_{\max}.$$

Any strategy that violates these bounds will be considered physically invalid.

## 2.2 Actuator Delay

In reality, dampers and their control valves do not react instantaneously. To reflect this, you must model a finite actuator delay between the damping value requested by your controller and the damping actually applied in the dynamics.

For this problem, assume:

- Sampling time  $\Delta t = 0.005$  s (200 Hz)
  - Actuator delay = 20 ms
- ⇒ Effective delay = 4 simulation steps

One simple way to implement this is to maintain a FIFO buffer of length 4 for the damping command:

1. At each time step  $k$ , compute  $c_{\text{request}}(k)$  using your controller and the current state.
2. Clip  $c_{\text{request}}(k)$  into  $[c_{\text{min}}, c_{\text{max}}]$ .
3. Push  $c_{\text{request}}(k)$  into the back of a list.
4. Pop the oldest value from the front of the list and apply it as  $c_{\text{applied}}(k)$  in the dynamics.

You may use any equivalent discrete-time implementation that produces an effective 20 ms delay between the commanded and applied damping values.

### 3. Road Profile Dataset

You are given a CSV file containing five pre-generated road profiles. Each profile is a vertical road displacement signal  $r(t)$  describing how the road moves under the tire as the vehicle travels forward.

Profile 1: Two half-sine bumps (isolated obstacles).

Profile 2: Smooth wavy road (low-frequency undulations).

Profile 3: Rough asphalt (noise-like high-frequency content).

Profile 4: Speed breaker followed by a sharp dip.

Profile 5: "The coffee run" - mixed sine waves, noise, and a pothole around  $t \approx 15$  s.



All profiles are sampled at a fixed rate and stored together in a single CSV file:

File: road\_profiles.csv

Columns (exact header format):

- $t$  – time in seconds (0 to 20 s)
- For each  $k \in \{1..5\}$ , the dataset includes:
  - profile\_ $k$  – road displacement  $r_k(t)$  in meters

NOTE: You must evaluate the accelerometer's data for both sprung and unsprung mass by yourself to generate inputs for the controller. Refer to the diagram provided.

Header:

$t, \text{profile}_i$

Sampling frequency: 200 Hz ( $\Delta t = 0.005$  s)

Duration: 20 s per profile  $\Rightarrow$  4,000 samples per profile.

#### 4. Your Task

You must complete the following steps:

Step 1 — Load Dataset: Read `road_profiles.csv`, extract the time vector `t` and, for each profile, the road displacement `profile_k` and both accelerometer signals `acc_s_profile_k` and `acc_u_profile_k`.

Step 2 — Implement Quarter-Car Dynamics: Set up your 2-DOF quarter-car model using the given parameters. Choose a suitable numerical integrator (e.g., explicit Euler, semi-implicit Euler, or 4th-order Runge-Kutta).

Step 3 — Design an Active Suspension Controller: Implement a control law that outputs a command `c_request(t)` in `[c_min, c_max]`. The controller may use the sprung and unsprung accelerometer measurements (`a_s(t)`, `a_u(t)`), vehicle constraints/parameters, and any causal internal memory/state you maintain.

Step 4 — Implement Actuator Delay: Convert `c_request(t)` into the applied command `c_applied(t)` using a 20 ms (4-step) delay as described in Section 2.2.



Step 5 — Simulate on All Road Profiles: For each of the five profiles, simulate the full time horizon and record the sprung-mass displacement  $z_s(t)$  (required) and unsprung-mass displacement  $z_u(t)$  (bonus), along with any signals needed for metric computation (e.g.,  $a_s(t)$  and jerk).

Step 6 — Compute Metrics: From each simulation, compute the performance metrics defined in Section 5.

Step 7 — Generate submission.csv: Write one row per profile with the required metrics in the specified format and submit this file to Kaggle.

Mandatory report: For each profile, include displacement plots of  $z_s(t)$  versus time. Include  $z_u(t)$  versus time as well (bonus points if you also keep the unsprung motion well-behaved).

## 5. Metrics and Cost Function

For each profile, you must compute the following metrics from your simulation results:

- RMS sprung-mass displacement —  $\text{rms\_zs}$  (cargo/body motion)
- Maximum sprung-mass displacement —  $\text{max\_zs}$  (peak cargo/body excursion)
- RMS jerk (sprung mass) —  $\text{rms\_jerk}$  (how rapidly acceleration changes; linked to discomfort/coffee spill)
- Comfort score —  $\text{comfort\_score}$  (a combined index based on displacement and jerk)

Let  $z_s(t)$  and  $z_u(t)$  be the sprung and unsprung vertical displacements, and let  $a_s(t)$  be the sprung-mass vertical acceleration signal used for jerk (typically the same signal your controller observes as the sprung accelerometer). Define displacement relative to the initial value to avoid offset effects:

- Relative sprung displacement:  $z_{s\_rel}(t) = z_s(t) - z_s(0)$

Then compute:

- $rms_{zs} = \text{RMS}(z_{s\_rel})$
- $max_{zs} = \max_t |z_{s\_rel}(t)|$

Define jerk using a finite-difference approximation ( $\Delta t = 0.005$  s):

- $rms_{jerk} = \text{RMS}(jerk)$
- $jerk_{max} = \max_t |jerk(t)|$

The comfort score is defined as:

$$\text{comfort\_score} = 0.5 \cdot \text{rms\_zs} + \text{max\_zs} + 0.5 \cdot \text{rms\_jerk} + \text{jerk\_max}$$

Additional reporting requirement (displacement):

- Compute and record displacement at every time step: For each simulation, record  $z_s(t)$  and  $z_u(t)$  for all  $t$ .
- Include displacement plots in the report: Plot  $z_s(t)$  and  $z_u(t)$  versus time for each road profile and include these graphs in the report submission.
- Design objective note: The controller should aim to keep the sprung-mass displacement response as steady (low-variation) as practical while also avoiding sharp changes in motion (low jerk).

## 6. Submission Format

You must submit a CSV file named `submission.csv`, with one row per profile and the following columns:

Header: `profile,rms_zs,max_zs,rms_jerk,comfort_score`



Example rows:

profile\_1, ..., ..., ..., ...

profile\_2, ..., ..., ..., ...

...

profile\_5, ..., ..., ..., ...

The profile column must exactly match the identifiers used in the evaluation (profile\_1 to profile\_5). All metric columns must be numeric and use the same units as defined above. Any missing or malformed values may result in your submission being rejected or scored as zero.

## 7. Evaluation (Kaggle Leaderboard)

On the backend, the evaluation system has a hidden file `reference_metrics.csv` containing the metrics produced by Stark's reference controller for each profile.



For each metric  $m \in \{\text{rms\_zs}, \text{max\_zs}, \text{rms\_jerk}, \text{comfort\_score}\}$ , an accuracy score is computed as:

$$\text{Accuracy}_m = (1 - |\text{pred}_m - \text{ref}_m| / |\text{ref}_m|) \times 100\%$$

Perfect match gives 100% accuracy. A 10% relative error yields 90% accuracy. Negative accuracies (from extreme errors) are clamped to 0 before aggregation.

Per-profile accuracies are combined into a single overall score per profile using fixed weights:

$\text{overall\_accuracy}(\text{profile}) =$

$$0.35 \times \text{Accuracy}_{\text{rms\_zs}}$$

$$+ 0.30 \times \text{Accuracy}_{\text{max\_zs}}$$

$$+ 0.20 \times \text{Accuracy}_{\text{rms\_jerk}}$$

$$+ 0.15 \times \text{Accuracy}_{\text{comfort\_score}}$$



## 8. Final Deliverables

In addition to your Kaggle submission, you are asked to submit the following through a separate form at the end of the hackathon:

- Python source file(s) implementing your controller, quarter-car model, and metric computation.
- Your final submission.csv file (profile,rms\_zs,max\_zs,rms\_jerk,comfort\_score).
- A short report (2–4 pages) describing your approach, including: modelling choices, controller design, tuning strategy, and key observations.

The report must include displacement plots of  $z_s(t)$  and  $z_u(t)$  versus time for each road profile (sprung mass is required; unsprung mass handling is evaluated as a bonus).



Include the following details on the cover of your report:

NAME: \_\_\_\_\_

ENROLMENT NUMBER: \_\_\_\_\_

BRANCH: \_\_\_\_\_

YEAR: \_\_\_\_\_

APPROACH (short summary): \_\_\_\_\_

GIT REPOSITORY LINK: \_\_\_\_\_