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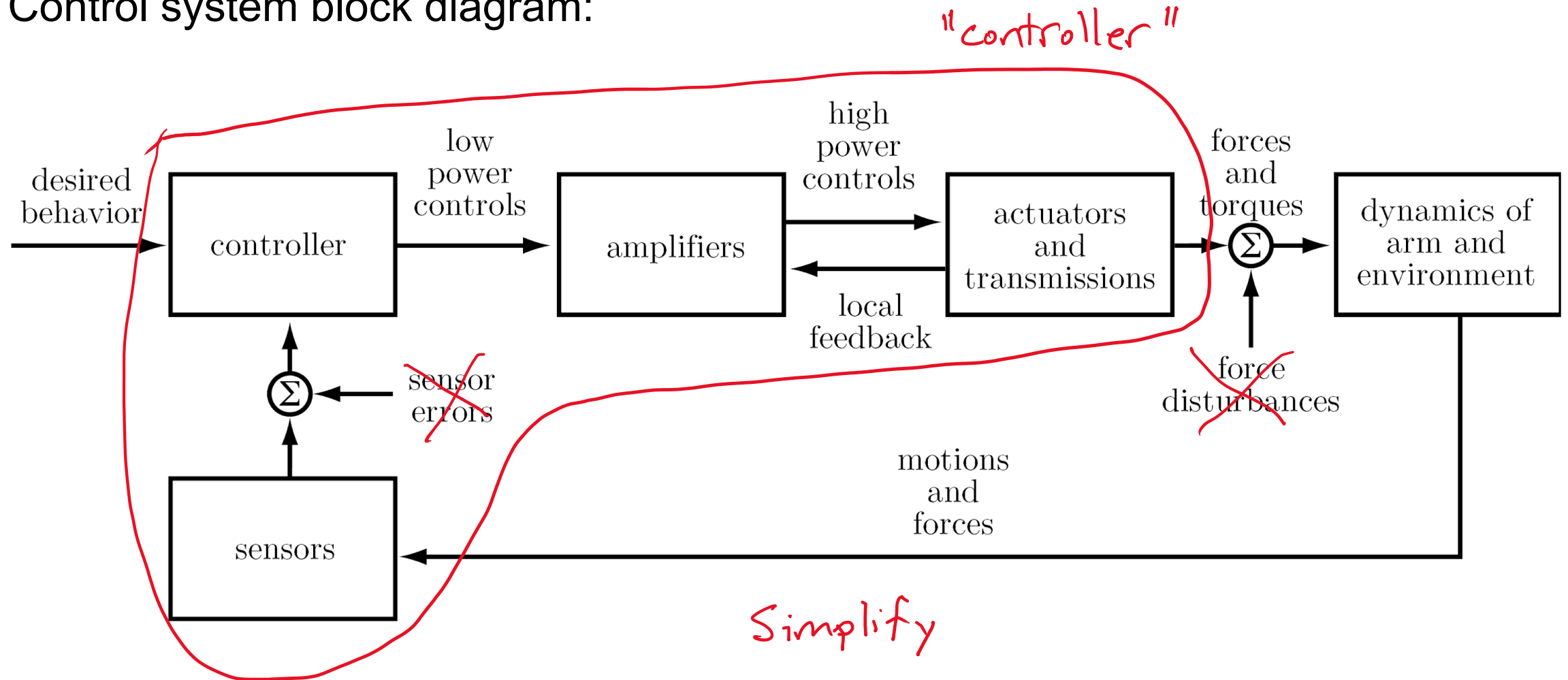
## Important concepts, symbols, and equations

Example control objectives:

- **motion control**
- **force control**
- **hybrid motion-force control**
- **impedance control**

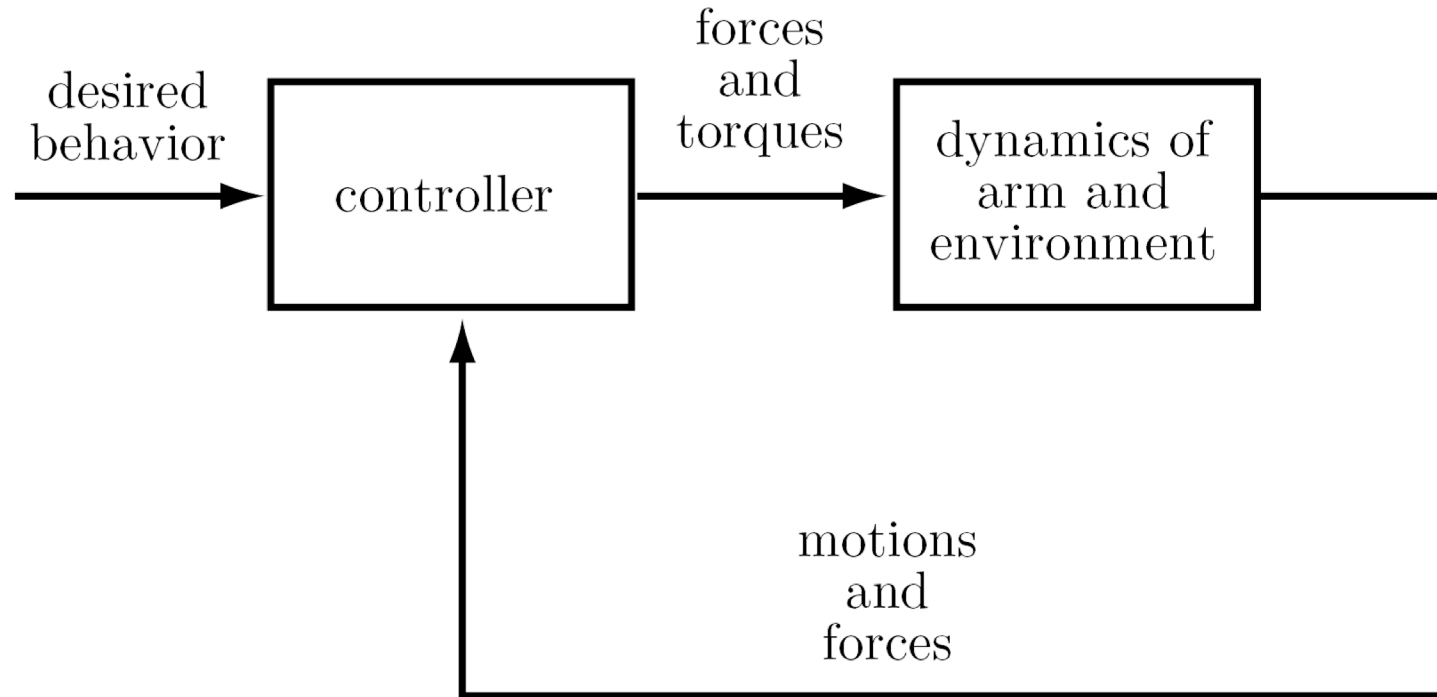
## Important concepts, symbols, and equations (cont.)

Control system block diagram:



## Important concepts, symbols, and equations (cont.)

Simplified block diagram:



Also assuming continuous-time (not discrete-time) control.

## Important concepts, symbols, and equations (cont.)

For motion control,

**reference:**  $\theta_d(t)$

**actual:**  $\theta(t)$

**error:**  $\theta_e(t) = \theta_d(t) - \theta(t)$

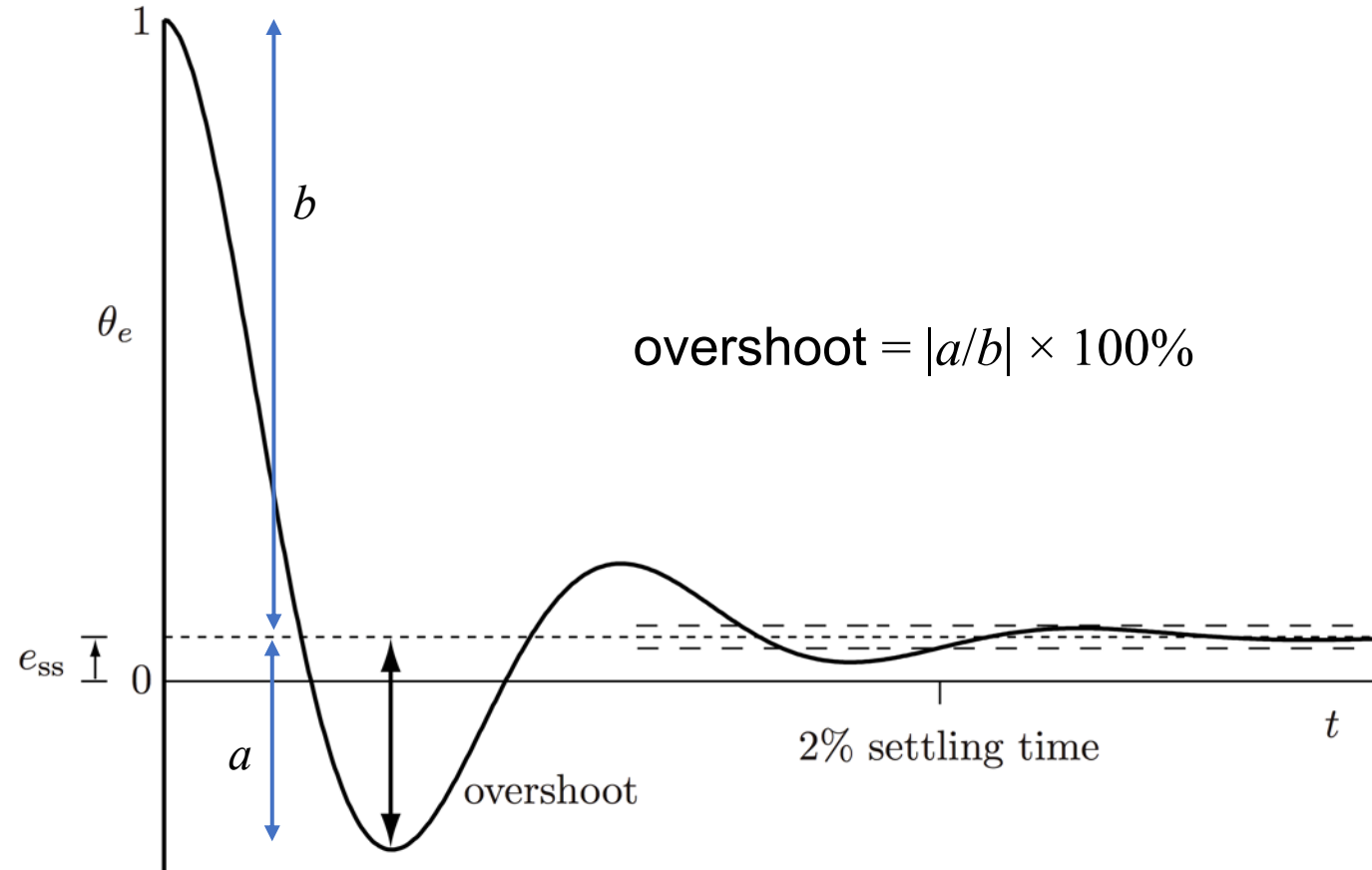
**Unit step error response:**

$\theta_e(t)$  starting from  $\theta_e(0) = 1$

**Steady-state error response:**  $e_{ss}$

**Transient error response:**

overshoot, settling time



## Important concepts, symbols, and equations (cont.)

System dynamics, feedback controllers, and error response are often modeled by **linear ordinary differential equations**.

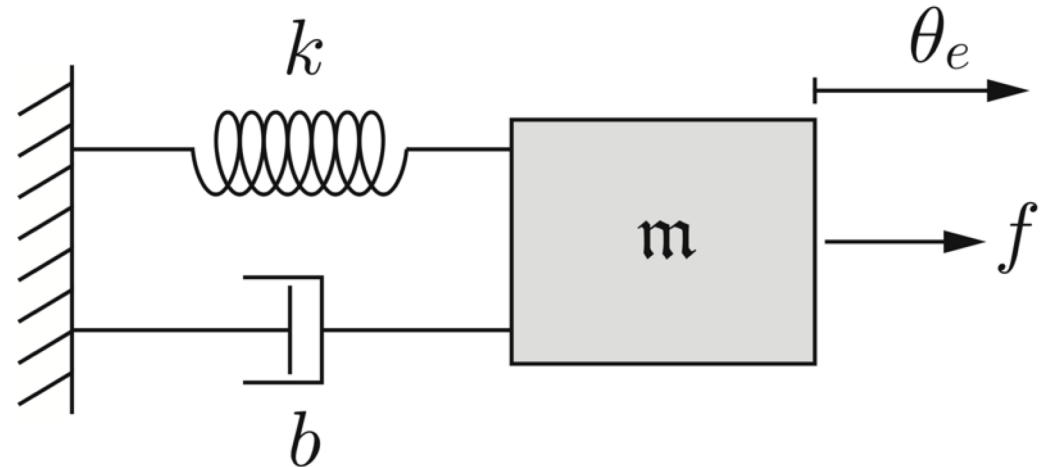
The simplest linear ODE exhibiting overshoot is second order, e.g.,

$$m\ddot{\theta}_e + b\dot{\theta}_e + k\theta_e = f$$

or, if  $f=0$ ,

$$\ddot{\theta}_e + \frac{b}{m}\dot{\theta}_e + \frac{k}{m}\theta_e = 0$$

*mbk model of error dynamics*



$k$  and  $b$  depend on the control law

## Important concepts, symbols, and equations (cont.)

A more general  $p^{\text{th}}$ -order linear ODE:

$$a_p \theta_e^{(p)} + a_{p-1} \theta_e^{(p-1)} + \dots + a_2 \ddot{\theta}_e + a_1 \dot{\theta}_e + a_0 \theta_e = c \quad \text{nonhomogenous}$$

$$a_p \theta_e^{(p)} + a_{p-1} \theta_e^{(p-1)} + \dots + a_2 \ddot{\theta}_e + a_1 \dot{\theta}_e + a_0 \theta_e = 0 \quad \text{homogeneous}$$

$$\theta_e^{(p)} + a'_{p-1} \theta_e^{(p-1)} + \dots + a'_2 \ddot{\theta}_e + a'_1 \dot{\theta}_e + a'_0 \theta_e = 0$$

$$\theta_e^{(p)} = -a'_{p-1} \theta_e^{(p-1)} - \dots - a'_2 \ddot{\theta}_e - a'_1 \dot{\theta}_e - a'_0 \theta_e$$

## Important concepts, symbols, and equations (cont.)

Defining a state vector  $x = (x_1, x_2, \dots, x_p)$ , you can write the  $p^{\text{th}}$ -order ODE as  $p$  first-order ODEs (a vector ODE).

$$x_1 = \theta_e,$$

$$x_2 = \dot{x}_1 = \dot{\theta}_e,$$

$$\vdots \quad \vdots$$

$$x_p = \dot{x}_{p-1} = \dot{\theta}_e^{(p-1)}$$

$$\dot{x}(t) = Ax(t) \rightarrow x(t) = e^{At}x(0)$$

$$A = \begin{bmatrix} 0 & 1 & 0 & \cdots & 0 & 0 \\ 0 & 0 & 1 & \cdots & 0 & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & 0 & 0 & \cdots & 1 & 0 \\ 0 & 0 & 0 & \cdots & 0 & 1 \\ -a'_0 & -a'_1 & -a'_2 & \cdots & -a'_{p-2} & -a'_{p-1} \end{bmatrix} \in \mathbb{R}^{p \times p}$$



## Important concepts, symbols, and equations (cont.)

$$\dot{x}(t) = Ax(t) \rightarrow x(t) = e^{At}x(0)$$

If  $\text{Re}(s) < 0$  for all eigenvalues  $s$  of  $A$ , then the error dynamics are **stable** (the error decays to zero).

The eigenvalues are the roots of the **characteristic equation**

$$\det(sI - A) = s^p + a'_{p-1}s^{p-1} + \dots + a'_2s^2 + a'_1s + a'_0 = 0$$

**Necessary conditions** for stability: each  $a'_i > 0$ .

*↳ the  $p^{\text{th}}$ -order ODE with  $s^k$  replacing  $\Theta^{(k)}$  for  $k=1 \dots p$ .*

These necessary conditions are also **sufficient** for first- and second-order systems.

*Higher-order systems: use Routh-Hurwitz criterion.*

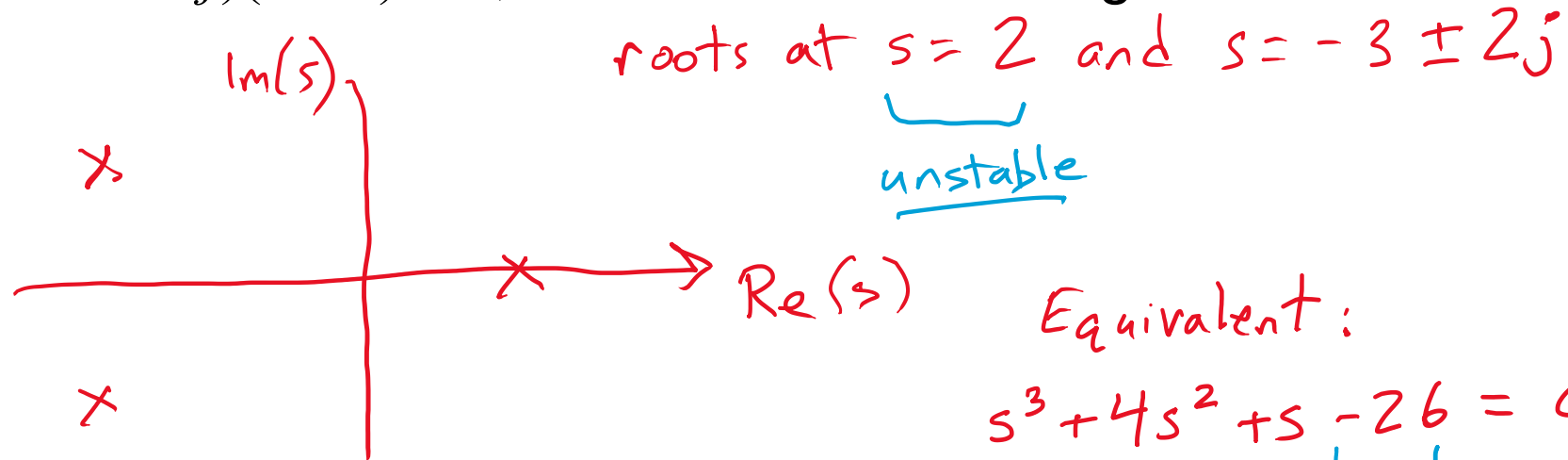
## Types of control for the following tasks:

- Shaking hands with a human *impedance + "soft" motion control?*
- Erasing a whiteboard *hybrid*
- Spray painting *motion*
- Back massage *hybrid*
- Pushing an object across the floor with a mobile robot *motion*
- Opening a refrigerator door *hybrid*
- Inserting a peg in a hole *impedance (compliance) + motion*
- Polishing with a polishing wheel *force, maybe*
- Folding laundry *motion*

*No single "correct" answer for most.*

If the error dynamics characteristic equation is

$(s + 3 + 2j)(s + 3 - 2j)(s - 2) = 0$ , does the error converge to zero?



Equivalent:

$$s^3 + 4s^2 + s - 26 = 0$$

does not satisfy  
necessary condition

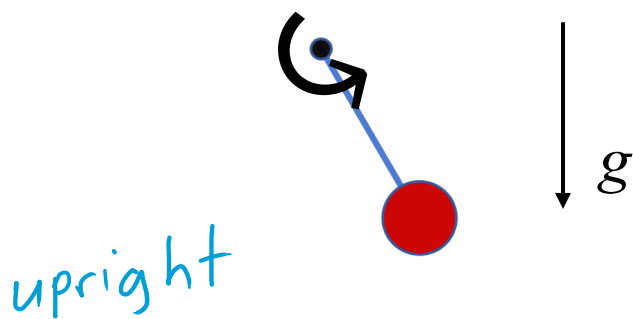
Note: if  $x_1 = \text{error}$  and  $x = (x_1, x_2, x_3)$ , then  $\dot{x} = Ax$ , where

$$\begin{aligned}x_2 &= \dot{x}_1 \\x_3 &= \dot{x}_2 \\\dot{x}_3 &= 26x_1 - x_2 - 4x_3\end{aligned}$$

$$A = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 26 & -1 & -4 \end{bmatrix}$$

eigenvalues are  $2, -3 \pm 2j$

You can choose a control law to be a virtual spring, a virtual damper, a virtual spring plus damper, or nothing. Which of these could stabilize an actuated pendulum with viscous friction to the upright configuration? To a horizontal configuration? To the downward configuration? Describe the transient and steady-state error response for each.



Need P or PD  
P has to overcome destabilizing "spring" of gravity.

spring: P control  
damper: D control  
both: PD

Natural viscous damping provides stabilization, but D term can allow better trans response.  
 $e_{ss} = 0$

horizontal  
Need P or PD. Will have  $e_{ss} \neq 0$  if spring set point is exactly horizontal (due to gravity).

no controller is needed, but can improve trans response.  $e_{ss} = 0$   
downward