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Chapter 4	Forward Kinematics
Chapter 5	Velocity Kinematics and Statics
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Chapter 13	Wheeled Mobile Robots
	13.1 Types of Wheeled Mobile Robots
	13.2 Omnidirectional Wheeled Mobile Robots

Important concepts, symbols, and equations

Types of wheels



conventional

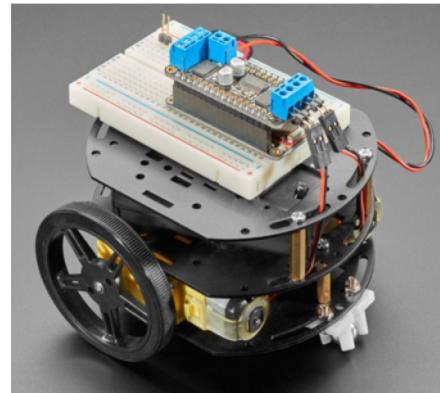


omniwheel



mecanum wheel

Kinematic wheeled
mobile robots
(no skidding, slipping)



differential drive

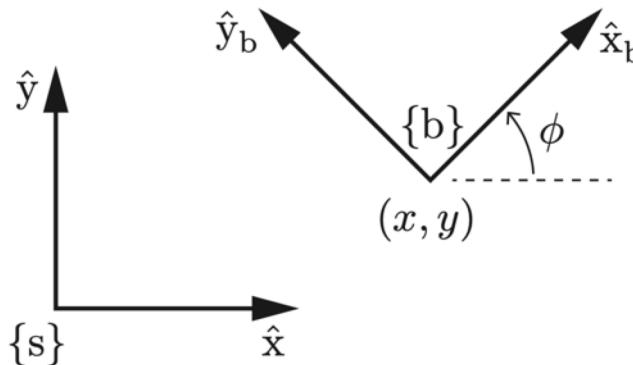


car-like
Ackermann steering



omnidirectional

Important concepts, symbols, and equations (cont.)



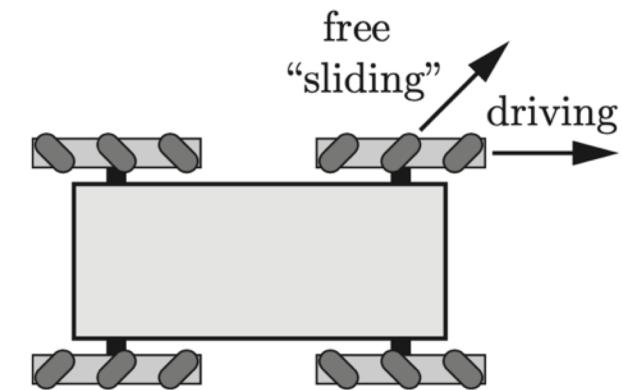
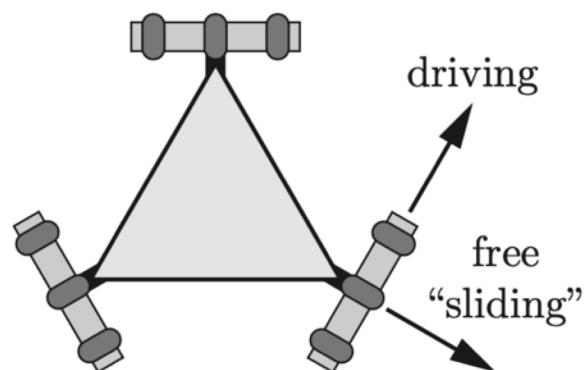
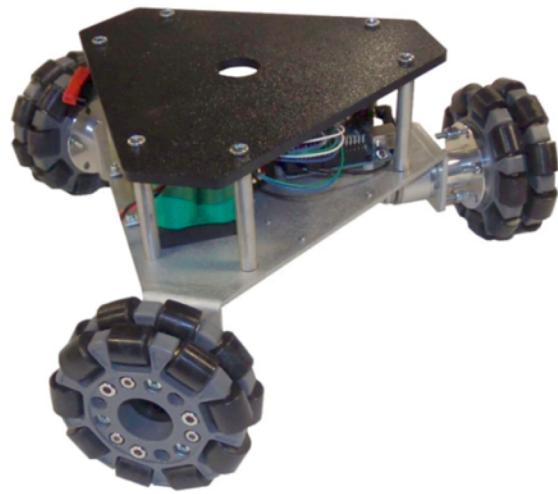
Configuration of the mobile base

$$T_{sb} = \begin{bmatrix} r_{11} & r_{12} & r_{13} & p_1 \\ r_{21} & r_{22} & r_{23} & p_2 \\ \cancel{r_{31}} & \cancel{r_{32}} & \cancel{r_{33}} & p_3 \\ 0 & 0 & 0 & 1 \end{bmatrix} \in SE(2) \text{ or } q = (\phi, x, y) \in \mathbb{R}^3$$

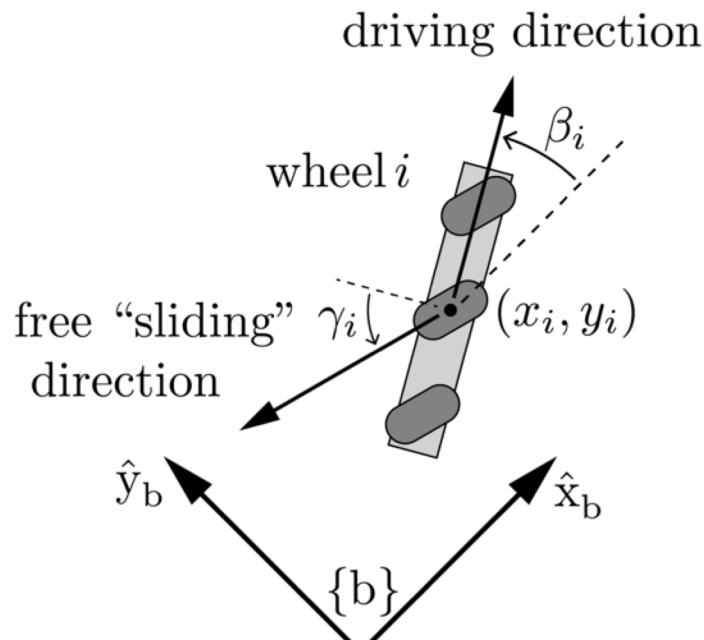
Velocity of the mobile base: $\mathcal{V}_b = (\cancel{\omega}_{bx}, \cancel{\omega}_{by}, \boxed{\omega_{bz}, v_{bx}, v_{by}, \cancel{v_{bz}}})$ or $\dot{q} \in \mathbb{R}^3$

Important concepts, symbols, and equations (cont.)

Examples of omnidirectional wheeled mobile robots



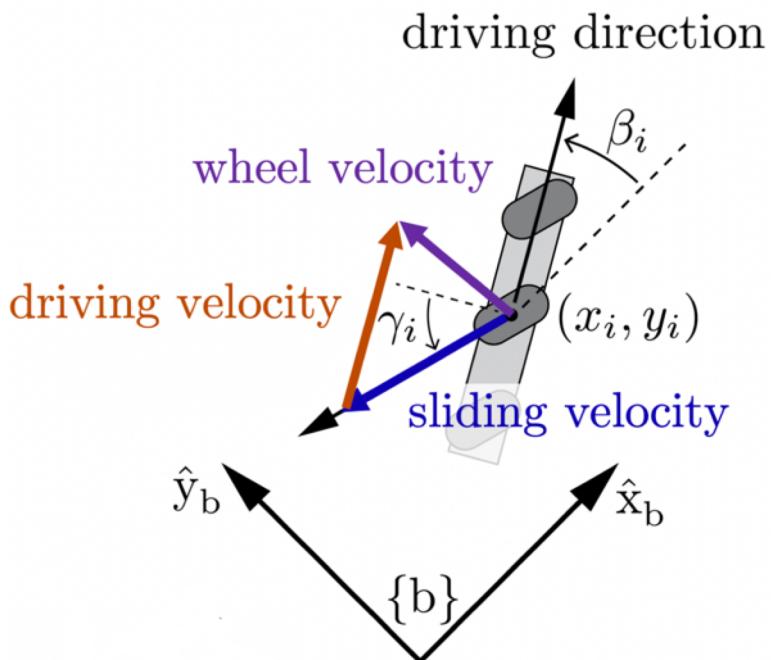
Important concepts, symbols, and equations (cont.)



wheel driving speed:

$$u_i = \frac{1}{r_i} [1 \ tan \gamma_i] \begin{bmatrix} \cos \beta_i & \sin \beta_i \\ -\sin \beta_i & \cos \beta_i \end{bmatrix} \begin{bmatrix} -y_i & 1 & 0 \\ x_i & 0 & 1 \end{bmatrix} \mathcal{V}_b$$

wheel radius
component in driving direction
linear velocity at wheel, in wheel frame
linear velocity at wheel, in {b}



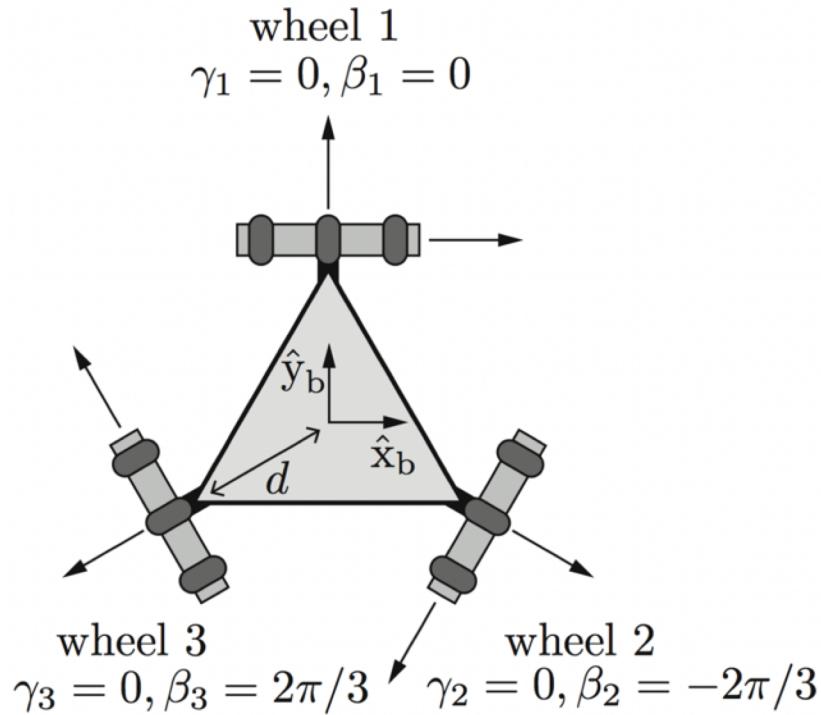
$$u_i = h_i(0)v_b$$

$$H(0) = \begin{bmatrix} h_1(0) \\ \vdots \\ h_m(0) \end{bmatrix} \in \mathbb{R}^{m \times 3}$$

m wheels

wheel speed vector

Important concepts, symbols, and equations (cont.)



spin in place

right

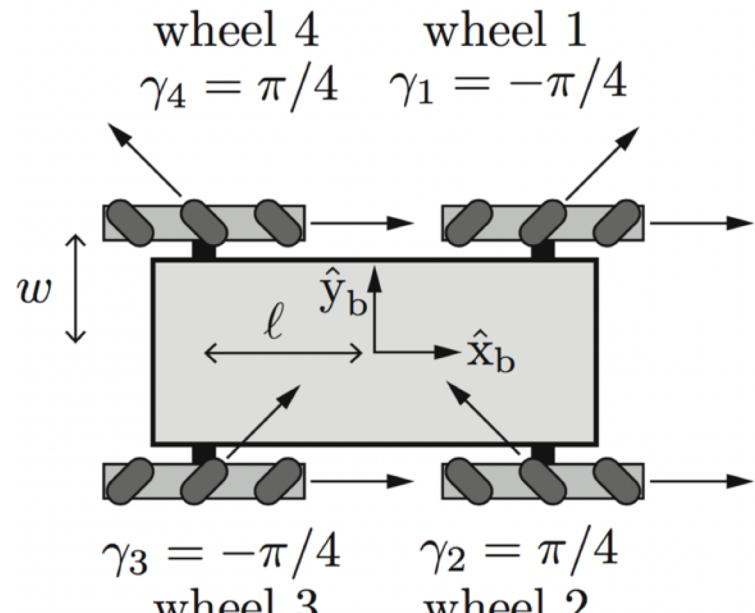
up

Why are at least three wheels required for omnidirectional motion?

Need at least 3 controls
(wheel speeds) to map to
all of the 3d twist space

$$u = \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix} = H(0)\mathcal{V}_b = \frac{1}{r} \begin{bmatrix} -d & 1 & 0 \\ -d & -1/2 & -\sin(\pi/3) \\ -d & -1/2 & \sin(\pi/3) \end{bmatrix} \begin{bmatrix} \omega_{bz} \\ v_{bx} \\ v_{by} \end{bmatrix}$$

Important concepts, symbols, and equations (cont.)



Wheel velocities are 4d.
Chassis twist is 3d.
Implications?

spin in place	forward	sideways	All u not in the 3d space $\{ H(0) \mathcal{V}_b \text{ for all } \mathcal{V}_b \}$ mean that the wheels must be skidding
$-l - w$	1	-1	
$l + w$	1	1	
$l + w$	1	-1	
$-l - w$	1	1	

$$u = \begin{bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \end{bmatrix} = H(0)\mathcal{V}_b = \frac{1}{r} \begin{bmatrix} -l - w & 1 & -1 \\ l + w & 1 & 1 \\ l + w & 1 & -1 \\ -l - w & 1 & 1 \end{bmatrix} \begin{bmatrix} \omega_{bz} \\ v_{bx} \\ v_{by} \end{bmatrix}$$

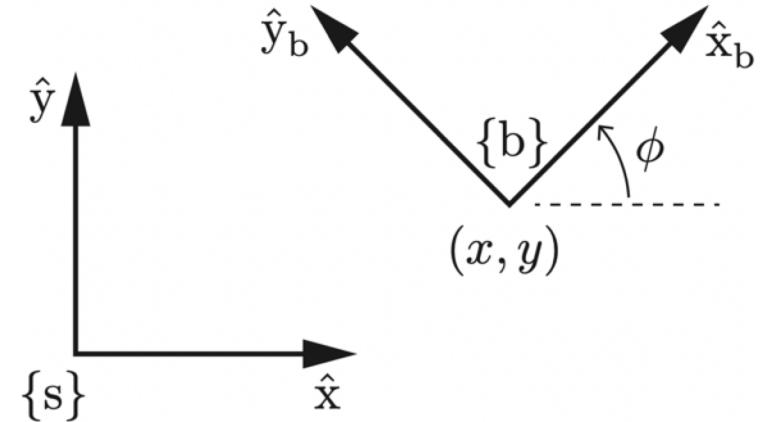
Important concepts, symbols, and equations (cont.)

Wheel speeds in terms of \dot{q} :

$$u = H(0)\mathcal{V}_b, \quad H(0) \in \mathbb{R}^{m \times 3}$$

$$u = H(0) \underbrace{\begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \phi & \sin \phi \\ 0 & -\sin \phi & \cos \phi \end{bmatrix}}_{H(\phi)} \begin{bmatrix} \dot{\phi} \\ \dot{x} \\ \dot{y} \end{bmatrix}$$

$$u = H(\phi)\dot{q}$$



Important concepts, symbols, and equations (cont.)

Feedforward + PI feedback stabilization of a planned trajectory:

$$\dot{q}(t) = \dot{q}_d(t) + K_p(q_d(t) - q(t)) + K_i \int_0^t (q_d(t) - q(t)) dt$$

$$u = H(\phi)\dot{q}$$

$K_p, K_i > 0$
for stability

Stability and steady-state error
for different control laws and
desired trajectories?

Setpoint control:
 $e_{ss} = 0$ for P, PI

Constant velocity reference:
 $e_{ss} = 0$ for PI

Important concepts, symbols, and equations (cont.)

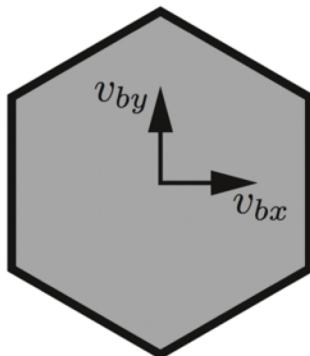
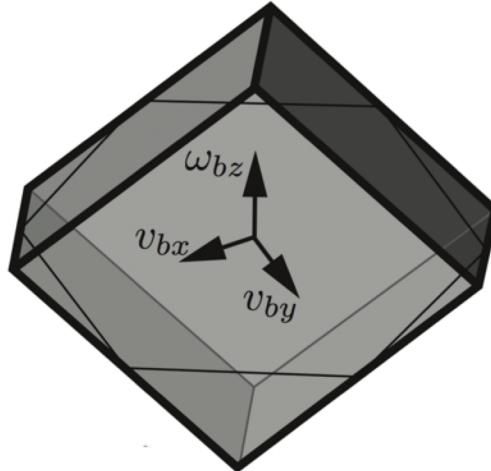
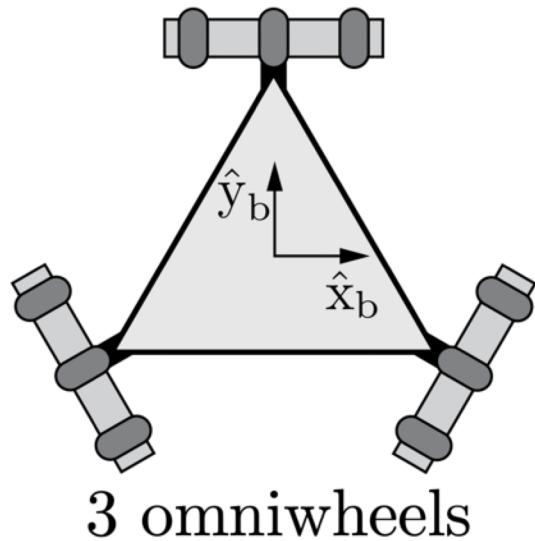
Given wheel velocity limits, the chassis' feasible twists lie inside a $2m$ -sided convex polyhedron:

$$\begin{bmatrix} u_1 \\ \vdots \\ u_m \end{bmatrix} = H(0)\mathcal{V}_b = \begin{bmatrix} h_1(0) \\ \vdots \\ h_m(0) \end{bmatrix} \mathcal{V}_b$$

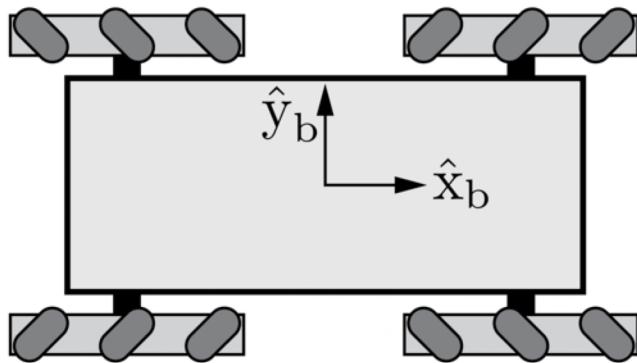
$$-u_{i,\max} \leq u_i = h_i(0)\mathcal{V}_b \leq u_{i,\max}$$

$\left. \begin{array}{l} -u_{i,\max} = h_i(0)\mathcal{V}_b \\ u_{i,\max} = h_i(0)\mathcal{V}_b \end{array} \right\}$ define two parallel bounding planes in twist space

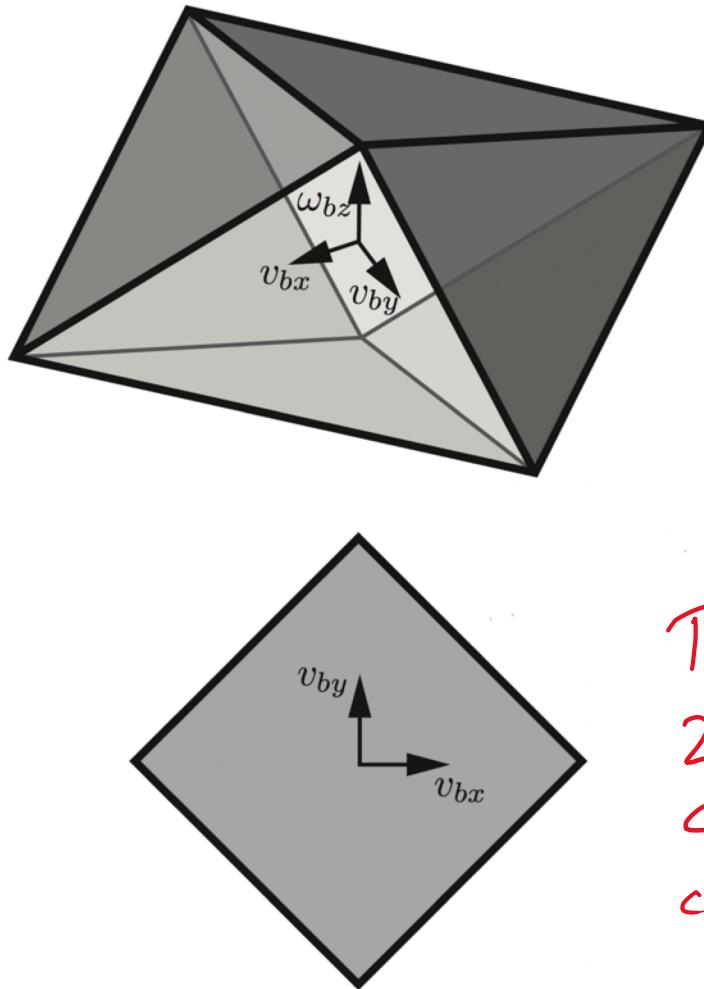
Important concepts, symbols, and equations (cont.)



Important concepts, symbols, and equations (cont.)

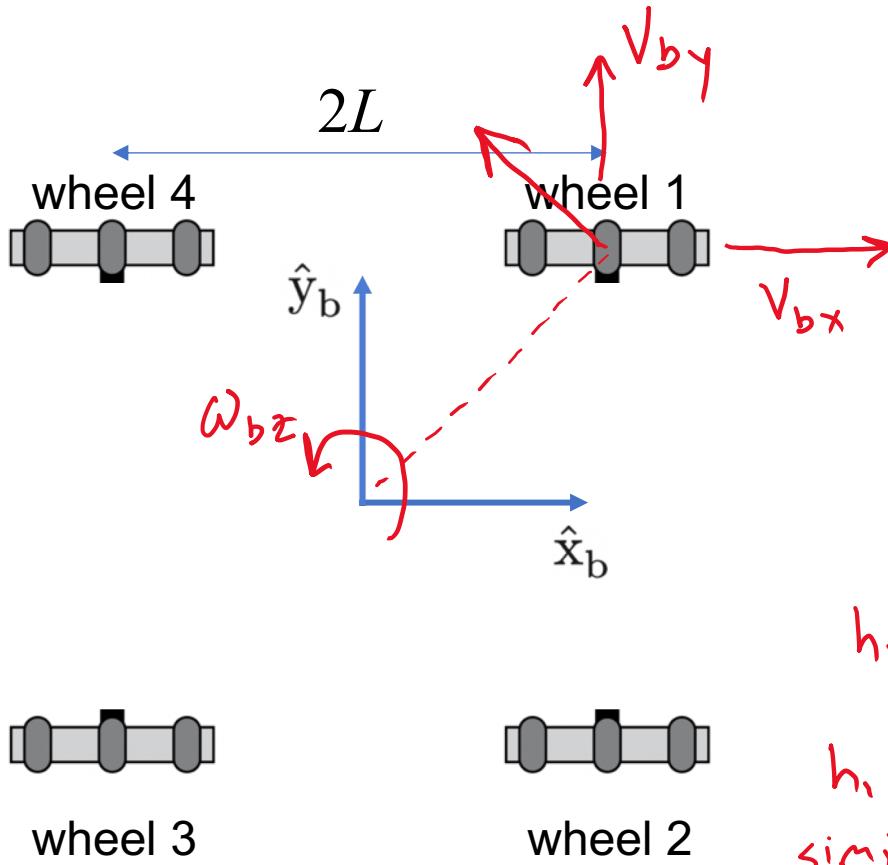


4 mecanum wheels



What does it mean
if the convex
polyhedron is
unbounded?

The $H(\omega)$ matrix has rank 2 or less. Some twists cannot be obtained by controlling wheel speeds.



The centers of the omniwheels of a mobile robot are at the corners of a square a distance $2L$ from each other. The radius of the wheels is r , and the forward driving direction for each wheel is to the right. What is $H(0)$?

$h_1(0)$ first. Find driving speed for

$$\begin{bmatrix} \omega_{bz} \\ v_{bx} \\ v_{by} \end{bmatrix} = \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix}$$

$$\begin{bmatrix} \omega_{bz} \\ v_{bx} \\ v_{by} \end{bmatrix} = \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix}$$

$$\begin{bmatrix} \omega_{bz} \\ v_{bx} \\ v_{by} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$

$$h_1(0) = (-L, 1, 0)$$

similarly

$$H(0) = \begin{bmatrix} h_1(0) \\ h_2(0) \\ h_3(0) \\ h_4(0) \end{bmatrix} = \frac{1}{r} \begin{bmatrix} -L & 1 & 0 \\ L & 1 & 0 \\ L & 1 & 0 \\ -L & 1 & 0 \end{bmatrix}$$

only rank 2
no way to achieve

$$\begin{bmatrix} 0 \\ 0 \\ v_{by} \end{bmatrix} = \mathbf{v}_b$$