

# Signal Processing - 1 by One

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- Previous Week: Shannon Sampling Theorem
- Previous Class: Systems and Circuits
- Today: Laplace Transform



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Notice that

$$\int_{k\frac{T}{2}}^{(k+1)\frac{T}{2}} \cos(2\pi ft) \sin(2\pi ft) dt = 0 \text{ for } T = \frac{1}{f}, k \in \mathbb{Z}.$$

Furthermore

$$\lim_{T_s \rightarrow \infty} \int_{-T_s}^{T_s} \cos(2\pi ft) \sin(2\pi ft) dt = 0 \text{ (In a generalized sense)}$$

$$\lim_{T_s \rightarrow \infty} \int_{-T_s}^{T_s} \cos(2\pi f_1 t) \sin(2\pi f_2 t) dt = 0 \text{ (as a generalized integral) .}$$



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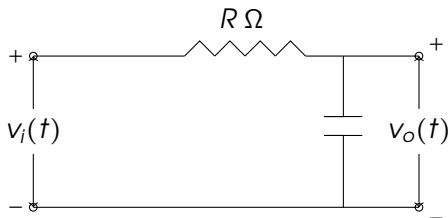
For  $f > 0$ , if the component  $\exp(-j2\pi f t)$  corresponds to positive frequency, then  $\exp(j2\pi f t)$  corresponds to negative frequency

Notice that  $\exp(-j2\pi f t)$  and  $\exp(j2\pi f t)$  are orthogonal for  $f > 0$ .



# Complex Circuits

Complex numbers in electrical circuits suggest the presence of both  $\cos(2\pi ft)$  and  $\sin(2\pi ft)$  inside, even when  $\cos(2\pi ft)$  is input.



Generalizing the Fourier Transform: For  $s = \sigma + j2\pi f$ ,

$$X(s) = \int_{\mathbb{R}} x(t) \exp(-st) dt \quad (\text{Two-sided Laplace Transform}).$$

Region of Convergence (ROC) :  $\{ \text{Real}(s) \}$  s.t. Integral exists.

$$\lim_{\sigma \rightarrow 0} X(s) = X(f).$$



# Circuits and Systems

Kirchoff's Voltage Law:

$$v_i(t) = i(t) R + \frac{1}{C} \int_{-\infty}^t i(\tau) d\tau.$$



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$$V_i(s) = I(s) R + \frac{1}{C} \frac{I(s)}{s} \quad \text{and} \quad V_o(s) = \frac{1}{C} \frac{I(s)}{s}.$$



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At  $s = j2\pi f$ ,

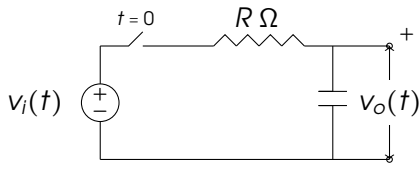
$$V_o(f) = H(f) V_i(f) \quad \text{where} \quad H(f) = \frac{1}{1 + j2\pi fRC}$$

$$v_o(t) = h(t) * v_i(t) \quad \text{where} \quad h(t) = \frac{1}{RC} \exp\left(-\frac{t}{RC}\right), t \geq 0.$$





# Laplace with Initial Conditions



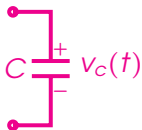
$$X(s) = \int_0^{\infty} x(t) \exp(-jst) dt$$

$$v_i(t) = i(t)R + \frac{1}{C} \int_{-\infty}^t i(\tau) d\tau.$$

Tool: One-sided or Unilateral Laplace Transform for  $t \geq 0$ .



# A Charged Capacitor

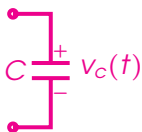


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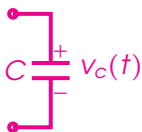
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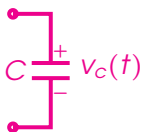
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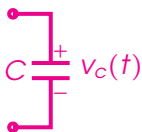
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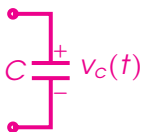


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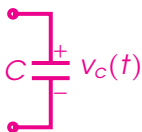


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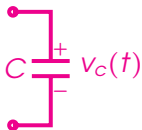
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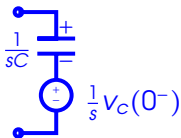




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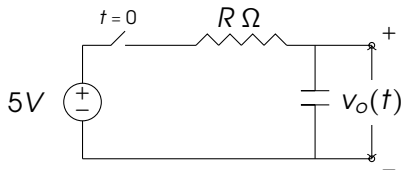
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## RC Circuit Example



$$X(s) = \int_0^{\infty} x(t) \exp(-st) dt$$

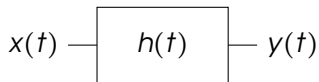
$$V_i(s) = I(s)R + \frac{v_c(0^-)}{s} + \frac{1}{sC}I(s).$$

$$I(s) = \frac{\frac{5}{s} - \frac{v_c(0^-)}{s}}{R + \frac{1}{sC}}$$

$$v_c(t) = v_c(0^-)u(t) + [5 - v_c(0^-)](1 - e^{-\frac{t}{RC}})u(t), \quad t \geq 0.$$



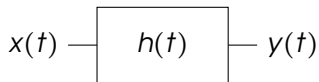
# Impulse Response



**Q1)** With unit step as the input  $x(t)$ , it is given that  $Y(s) = \frac{1}{s(s+\alpha)}$ , where  $\alpha \in \mathbb{R}^+$ . Find the impulse response  $h(t)$ .



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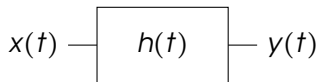


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$$Y(s) = H(s)X(s) \text{ (Convolution-Multiplication Theorem)}$$



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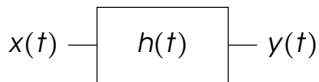


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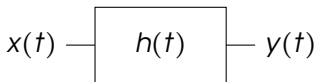
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Finding the Inverse Laplace Transform gives

$$h(t) = \exp(-at)u(t).$$



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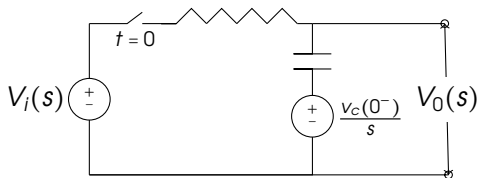
$$h(t) = \exp(-\alpha t)u(t).$$

GNURADIO: Showing the step response and identify the RC ckt.



## Superposition

**Q2)** Apply super-position theorem and Laplace Transform to find the output voltage  $v_0(t)$ , if the input is  $5u(t)$ . The resistor is  $R$  ohms and capacitor is  $C$  Farads.



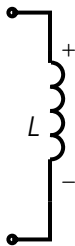


## Output to Bounded Inputs

**Q3)** Consider an LTI system with impulse response  $h(t)$ , which is integrable, i.e.  $\int_{\mathbb{R}} |h(t)| dt < \infty$ . If the input is bounded, i.e.  $\max_{t \in \mathbb{R}} |x(t)| = v_m < \infty$ , show that the output is also bounded (this is called **BIBO** stability).

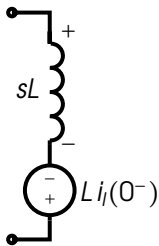


# Inertial Inductor

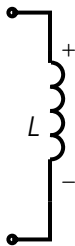


$$v_l(t) = L \frac{d}{dt} i_l(t)$$

$$V_l(s) = sL I_l(s) - L i_l(0^-).$$

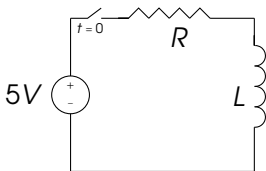
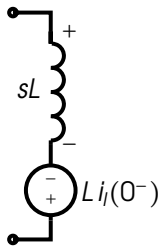


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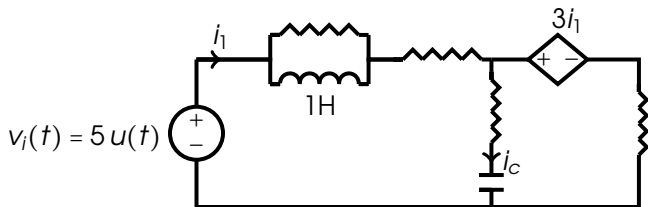
$$\begin{aligned} I_l(s) &= \frac{V_i(s) + L i_l(0^-)}{sL + R} = \frac{\frac{V_m}{s} + L i_l(0^-)}{sL + R} \\ &= \frac{V_m}{L s(s + \frac{R}{L})} + \frac{i_l(0^-)}{s + \frac{R}{L}} \\ &= \frac{V_m}{R} \left( \frac{1}{s} - \frac{1}{s + \frac{R}{L}} \right) + \frac{i_l(0^-)}{s + \frac{R}{L}}. \end{aligned}$$

$$V_i(s) = R I_l(s) + sL I_l(s) - L i_l(0^-)$$

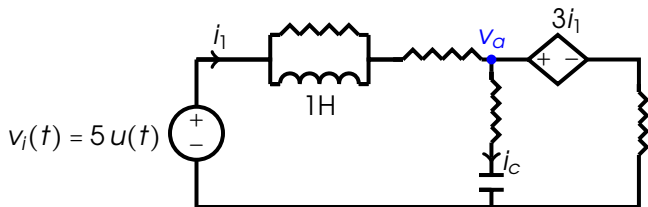
$$i_l(t) = i_{dc} - [i_{dc} - i_l(0^-)] e^{-\frac{R}{L}t}, \quad t \geq 0.$$



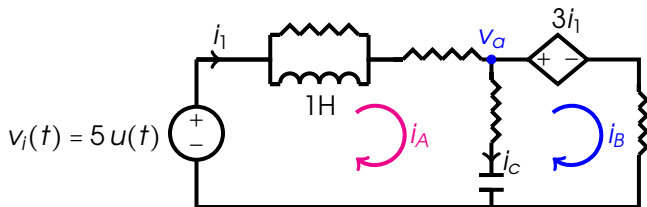
# Mesh Analysis



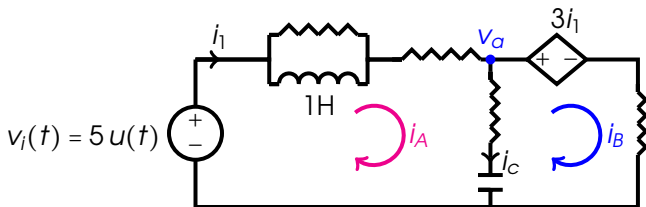
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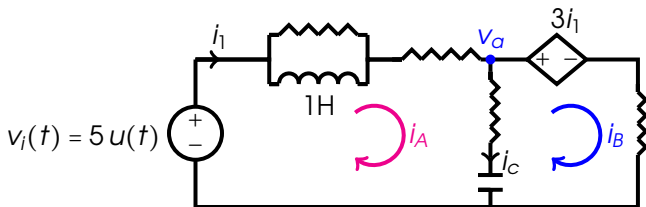


$$V_i(s) = \frac{s}{1+s} I_A(s) + I_A(s) + [I_A(s) - I_B(s)] \left(1 + \frac{1}{s}\right)$$

$$3I_A(s) = [I_A(s) - I_B(s)] \left(1 + \frac{1}{s}\right) - I_B(s)$$



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$$\begin{bmatrix} \frac{s}{s+1} + 2 + \frac{1}{s} & 1 + \frac{1}{s} \\ -2 + \frac{1}{s} & 2 + \frac{1}{s} \end{bmatrix} \begin{bmatrix} I_A \\ -I_B \end{bmatrix} = \begin{bmatrix} V_i(s) \\ 0 \end{bmatrix}$$

$$\text{Det} = \frac{8s^2 + 12s + 5}{s(s+1)}$$





# Matrix Inversion

$$\begin{bmatrix} a & b \\ c & d \end{bmatrix}^{-1} = \begin{bmatrix} d & -b \\ -c & a \end{bmatrix}^{-1} \frac{1}{ad-bc}.$$

$$A = \begin{bmatrix} \frac{s}{s+1} + 2 + \frac{1}{s} & 1 + \frac{1}{s} \\ -2 + \frac{1}{s} & 2 + \frac{1}{s} \end{bmatrix} \Rightarrow A^{-1} = \frac{1}{\text{Det}} \begin{bmatrix} 2 + \frac{1}{s} & -1 - \frac{1}{s} \\ \frac{s}{s+1} + 2 + \frac{1}{s} & 2 + \frac{1}{s} \end{bmatrix}.$$

$$A^{-1} \begin{bmatrix} V_i(s) \\ 0 \end{bmatrix} = \frac{1}{\text{Det}} \begin{bmatrix} 2 + \frac{1}{s} \\ 2 - \frac{1}{s} \end{bmatrix}$$

$$\text{Det} = \frac{8s^2 + 12s + 5}{s(s+1)}$$



## Mesh Solution

$$\begin{bmatrix} I_A \\ -I_B \end{bmatrix} = A^{-1} \begin{bmatrix} V_i(s) \\ 0 \end{bmatrix} = \frac{1}{\text{Det}} \begin{bmatrix} 2 + \frac{1}{s} \\ 2 - \frac{1}{s} \end{bmatrix} V_i(s) = \frac{1}{\text{Det}} \begin{bmatrix} 2 + \frac{1}{s} \\ 2 - \frac{1}{s} \end{bmatrix} \frac{5}{s}.$$



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Let us invert the first term



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$$\exp(-at)u(t) \xLeftrightarrow{L.T.} \frac{1}{s+a}, \text{ Real}(s+a) \geq 0. \quad (*)$$



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Clearly if  $\text{Real}(\alpha_i) \leq 0, \forall i, \Rightarrow h(t)$  stays bounded & integrable.

Thus,  $\alpha_i < 0, \forall i$  will imply BIBO stability.



# Oscillatory Responses

Second order circuits may have poles  $\alpha_i$  complex

$$\int_0^{\infty} \exp(-at) \cos(\omega t) dt = \frac{s + a}{(s + a)^2 + \omega^2}, \text{ Real}(s + a) > 0$$

$$\int_0^{\infty} \exp(-at) \sin(\omega t) dt = \frac{\omega}{(s + a)^2 + \omega^2}, \text{ Real}(s + a) > 0$$



## RLC Solution

$$V_C(s) = \frac{5}{2} \frac{1}{s^2 + \frac{3}{2}s + \frac{5}{8}} + \frac{5}{2} \frac{1}{s(s^2 + \frac{3}{2}s + \frac{5}{8})}$$



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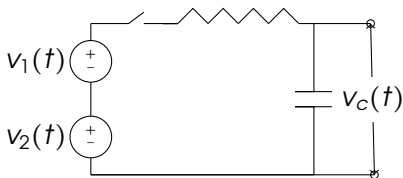
$$V_C(s) = \frac{20}{2} \frac{\frac{1}{4}}{(s + \frac{3}{4})^2 + \frac{1}{4^2}} + \frac{5}{2} \left( \frac{1}{s} - \frac{s + \frac{3}{2}}{(s + \frac{3}{4})^2 + \frac{1}{4^2}} \right) \frac{8}{5}$$

$$v_C(t) = 4u(t) - 4e^{-\frac{3}{4}t} \cos\left(\frac{t}{4}\right) - 2e^{-\frac{3}{4}t} \sin\left(\frac{t}{4}\right), t \geq 0.$$



## Not-So Linear Initial Conditions

**Q4)** Can you apply superposition theorem on the two voltage sources to find  $v_c(t)$ . The resistor is  $R$  ohms and capacitor is  $C$  Farads, which has an initial charge of 0.3V.



## RLC Circuit

**Q5)** For the serial RLC circuit find the voltage across C.

