

# EE240: Power Engineering LAB

## **Characteristics of Separately Excited DC Motor**

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# DC Motor

⇒ input is electrical energy

⇒ armature is connected to the source

⇒ 'V' induced in the armature is also known as back emf

$$I_a = \frac{V_a - E_b}{R_a}$$

⇒ power input to the armature =  $V_a I_a$

⇒ power input to the motor =  $V_a I_a + V_f I_f$

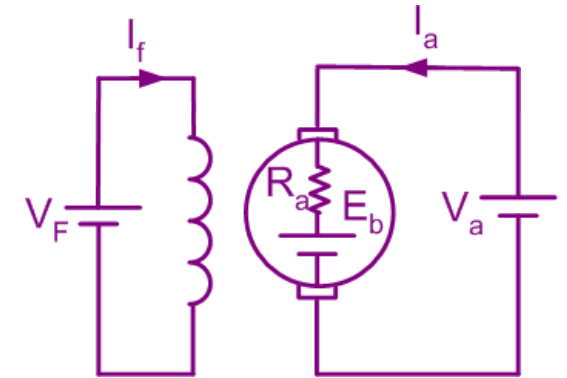
⇒  $V_a = E_b + I_a R_a$  multiplying by  $I_a$

$$V_a I_a = \underbrace{E_b I_a}_{\text{power developed in the armature}} + I_a^2 R_a$$

*power developed in the armature*

$$E_b I_a = T \omega$$

If frictional loss is neglected



$$T\omega = E_b I_a = (k\phi\omega)I_a$$

$$\therefore T = k\phi I_a$$

$$= kF_s F_r \sin\delta$$

$$\Rightarrow \delta = 90 \quad \phi \rightarrow F_s \quad I_a \rightarrow F_r$$

$$\Rightarrow \frac{T}{I_a} \text{ or } \frac{T}{A} \text{ when } \delta = 90 > \frac{T}{A} \text{ when } \delta < 90$$

$\therefore$  DC machine has maximum  $\frac{T}{A}$  ratio

In other machine to achieve this condition extra control is needed.

$\Rightarrow$  Mmf produced by the field coil and the armature coil are in quadrature hence provide wide and smooth range of speed control.



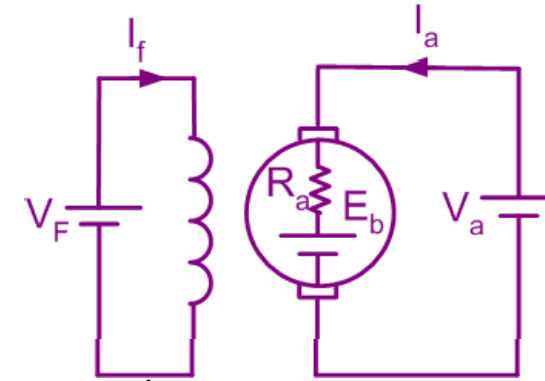
# Speed Control

⇒ The basic equations governing the steady state operation of DC machine are:

$$V_a = E_b + I_a R_a \qquad E_b = k\omega\phi \qquad I_F = \frac{V_F}{R_F}$$

$$\Rightarrow E_b = V_a - I_a R_a \qquad I_a = \frac{T}{k\phi}$$

$$\Rightarrow \omega = \frac{V_a}{k\phi} - \frac{TR_a}{(k\phi)^2}$$



If armature voltage  $V_a$  and air gap flux  $\phi$  is held constant then above equation can be written as:

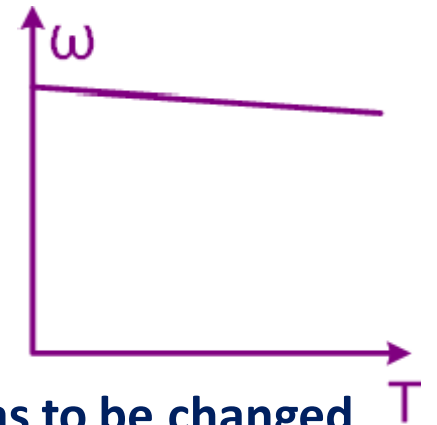
$$\omega = A + BT \quad \text{where } A = \frac{V_a}{k\phi} \text{ and } B = -\frac{TR_a}{(k\phi)^2}$$

$A \Rightarrow Y$  axis intercept (no load speed) and  $B \Rightarrow$  slope

$R_a$ : armature resistance  $\rightarrow$  very small

$\therefore$  for all practical purposes, S.E. dc motor is a constant speed motor

$\therefore \Rightarrow$  if application requires **wide variation in speed** (fan or pump), **Y-axis intercept has to be changed**



- ⇒ Armature reaction helps in maintain the speed constant.
- ⇒ For wide range of speed variation Y axis intercept has to be changed

$$A = \frac{V_a}{k\phi}$$

- ⇒ This can be achieved by
  1. controlling the voltage applied to the armature terminal ( $V_a$ )
  2. controlling the flux produced by the field winding ( $\phi$ )
- ⇒ Speed can be controlled in two range
  1. below the rated speed ( $0 < \omega < \omega_{rated}$ )
  2. above the rated speed ( $\omega > \omega_{rated}$ )

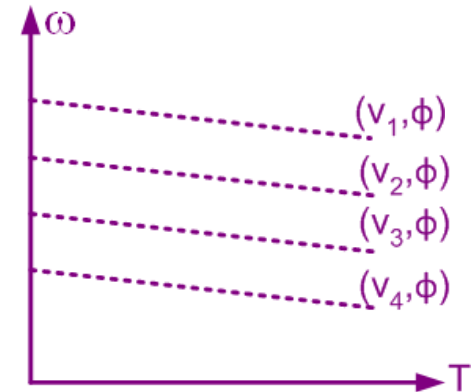
⇒ **Controlling speed below base speed ( $0 < \omega < \omega_{rated}$ ):**

either  $\uparrow \phi$  or  $\downarrow V_a$

' $\phi$ ' can not be  $\uparrow$  (saturation)

∴ as  $V_a \downarrow$ , 'A' will  $\downarrow$

∴ For  $0 < \omega < \omega_{rated}$ , ' $\phi$ ' held constant at its rated value &  $V_a$  is  $\downarrow$ ,  $A \propto V_t$



⇒ ' $\phi$ ' is held constant → constant flux operation

⇒ If  $I_a$  is held constant →  $T$  remains constant

(at low speeds ' $T$ ' required is high, eg., train, scooter.....)

→ **constant torque region**

⇒ By varying the armature voltage from 0 to rated value speed can be varied from upto rated speed.

⇒ This method is known as "**Armature Voltage Control**"

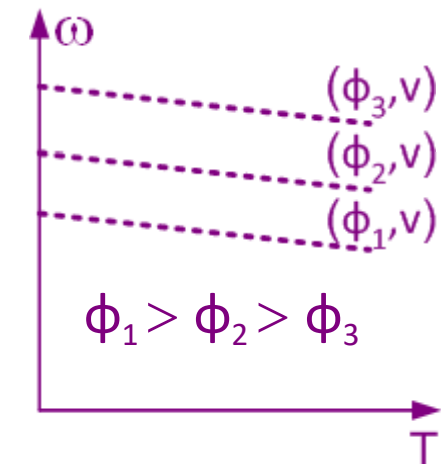
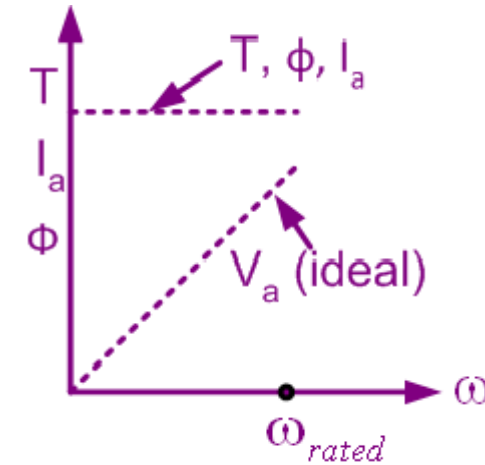
⇒ **Controlling speed above base speed ( $\omega > \omega_{rated}$ ):**

$$A = \frac{V_a}{k\phi}$$

→ either  $\uparrow V_a$  &  $\downarrow \phi$

⇒ not a good engineering practice to  $\uparrow V_a$  beyond  $V_{rated}$

→ keep  $V_a = V_{rated}$  &  $\downarrow \phi$



⇒ field is weakened → **field weakening mode**

⇒ as  $\phi \downarrow$ ,  $A \uparrow$

⇒ If 'I' is held constant, power input to the armature remains constant

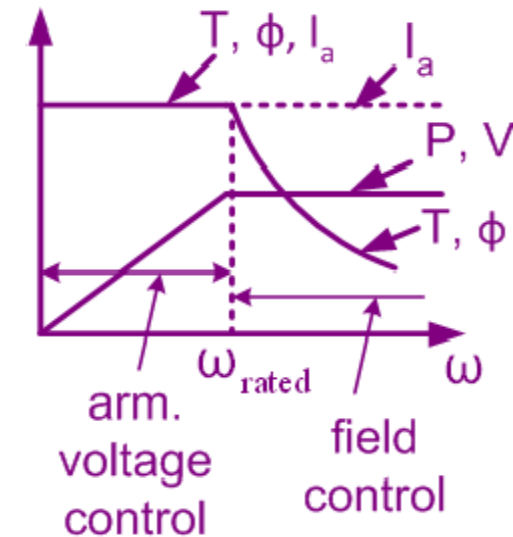
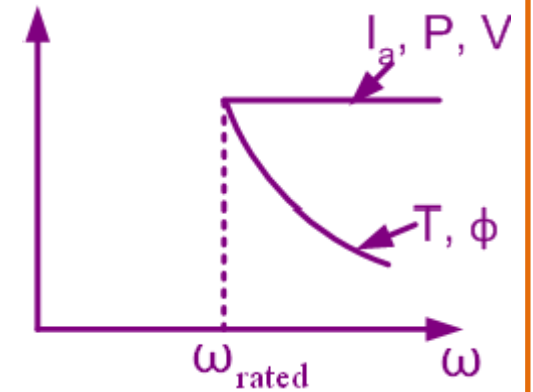
$$V_a I_a$$

⇒ power o/p =  $V_a I_a - I_a^2 R_a$  - friction loss

as  $I_a$  is constant →  $I_a^2 R_a$  remains constant

⇒ loss due to friction varies with speed

⇒ If this change is neglected → power o/p remains constant  
→ constant HP mode



# Starting of DC Motor

$$I_a = \frac{V_a - k\phi\omega}{R_a}$$

$$T = k\phi I_a$$

- ☐ Starting torque is utilised to
  - ☐ Overcome friction
  - ☐ Accelerating the armature
  - ☐ Accelerating the load
- ☐ At standstill  $E_b = 0$ , hence small armature voltage is required to flow full rated current
- ☐ The starting current can be limited by two methods:
  - ☐ Add external resistance in the armature circuit (helps in developing necessary starting torque but should be cut off once back emf has developed)
  - ☐ Applying low voltage by using variable DC power supply. This voltage can be increased if machine accelerates
- ☐ The developed torque and rate at which back emf is generated depends on air gap flux.

