

Superheterodyne Receiver, Sampling, PCM, Transmission of FM and AM Signals over Non-Linear Channels: Examples

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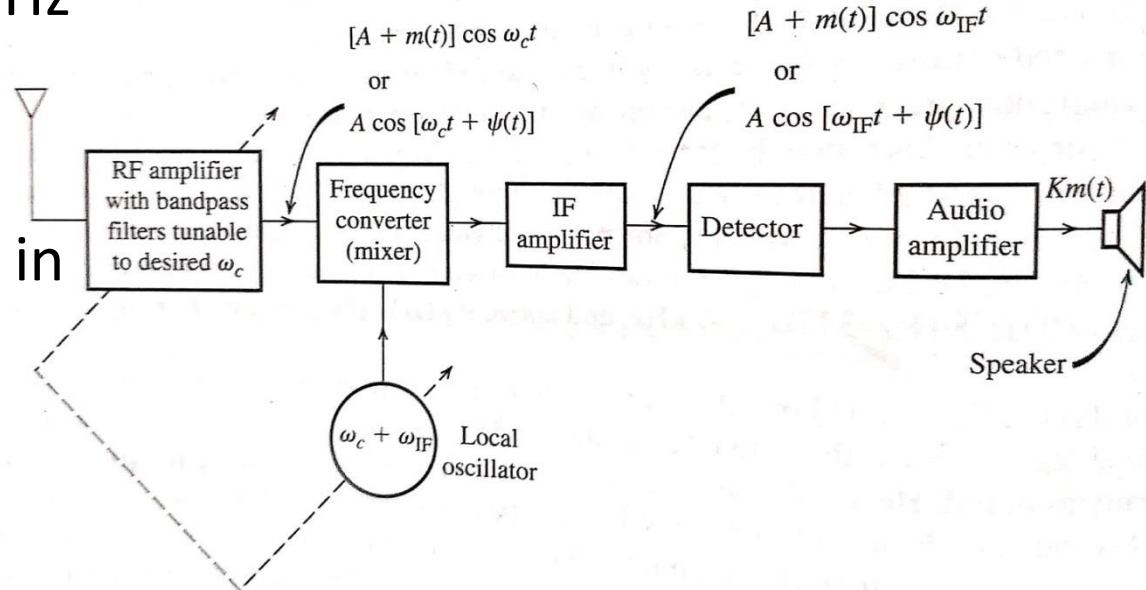
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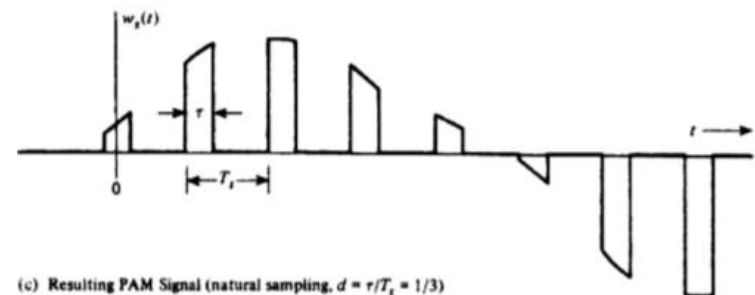
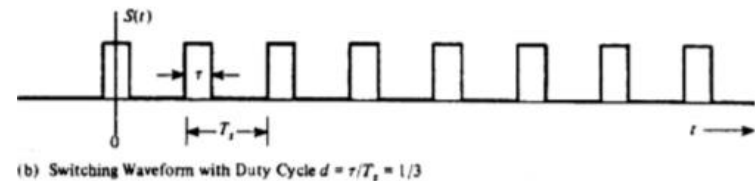
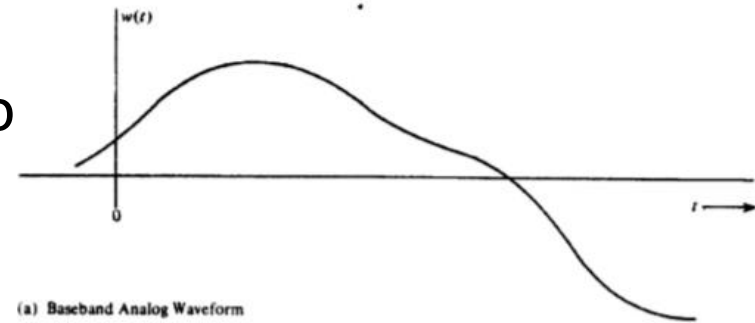
Example: Superheterodyne Receiver

- A superheterodyne FM receiver operates in the frequency range: $f_c \in [88 \text{ MHz}, 108 \text{ MHz}]$
- We require that image frequency f_c' lie outside $[88 \text{ MHz}, 108 \text{ MHz}]$ for every f_c
- Want minimum required f_{IF}
- Recall: $f_c' = f_c + 2f_{IF}$
- So $f_c + 2f_{IF} \geq 108 \text{ MHz}$ for every f_c
- So $f_{IF} \geq \frac{108-88}{2} = 10 \text{ MHz}$
- Next, assume that $f_{IF} = 10 \text{ MHz}$
- Want range of variations in f_{LO}
- Recall: $f_{LO} = f_c + f_{IF} = f_c + 10$
- So required range:
□ $[98 \text{ MHz}, 118 \text{ MHz}]$



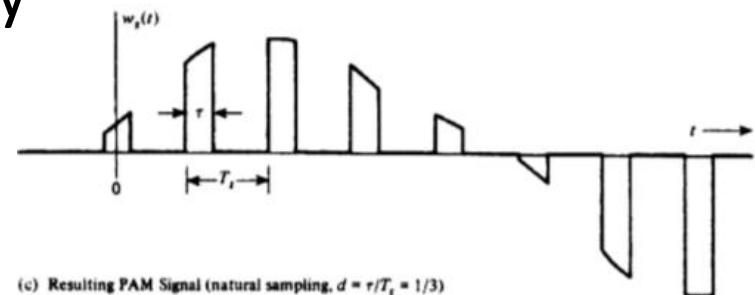
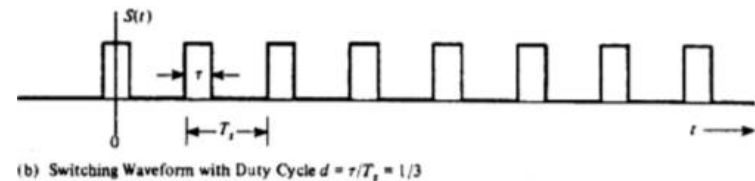
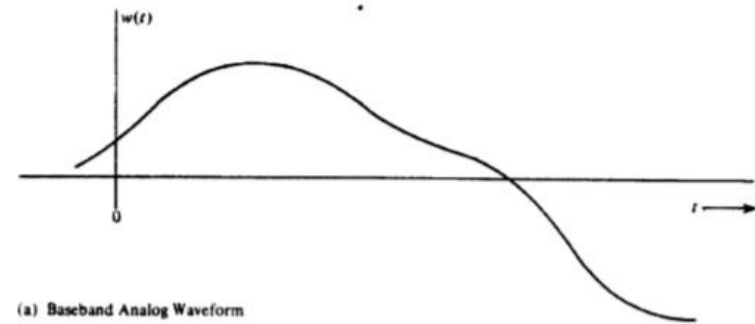
Example: Natural Sampling

- In *natural sampling*, an analog signal $g(t)$ is multiplied by a periodic train of rectangular pulses $c(t)$
 - pulse repetition frequency of periodic train: f_s
 - duration (respectively, amplitude) of each rectangular pulse: T (respectively, $1/T$)
- Assume that time $t = 0$ corresponds to midpoint of a rectangular pulse in $c(t)$
- Want spectrum of signal $s(t)$ that results from the use of natural sampling
- Fourier series expansion of $c(t)$:
 - $c(t) = \sum_{n=-\infty}^{\infty} f_s \text{sinc}(nf_s T) e^{j2\pi n f_s t}$
- $s(t)$:
 - $c(t)g(t) = \sum_{n=-\infty}^{\infty} f_s \text{sinc}(nf_s T) g(t) e^{j2\pi n f_s t}$
- $S(f)$:
 - $\sum_{n=-\infty}^{\infty} f_s \text{sinc}(nf_s T) G(f - nf_s)$



Example: Natural Sampling (contd.)

- 1) Recall: $S(f) = \sum_{n=-\infty}^{\infty} f_s \text{sinc}(nf_s T) G(f - nf_s)$
- Under what conditions can $g(t)$ be recovered exactly from its naturally sampled version?
 - Assume that $g(t)$ is bandlimited with $G(f) = 0$ for $f \notin (-W, W)$; also, $f_s > 2W$
 - Then by 1), the different frequency-shifted replicas of $G(f)$ in the spectrum $S(f)$ will not overlap
 - Hence, $G(f)$, and therefore the signal $g(t)$, can be recovered exactly by passing $s(t)$ through a low-pass filter of bandwidth W



Example: PCM

- A PCM system uses a uniform quantizer and represents each quantized value using 7 bits
- Bit rate of system equals 50×10^6 bps
- Want maximum message bandwidth for which system operates satisfactorily
- Nyquist rate:
 - $2W$, where W is message bandwidth
- So $2W \times 7 \leq 50 \times 10^6$
- Hence, $W \leq 3.57$ Mbps
- Suppose a sinusoidal modulating wave of amplitude A_m and frequency 1 MHz is applied to input
- Assume that quantizer divides the range $[-A_m, A_m]$ into intervals of equal sizes
- Output signal-to-quantization noise ratio:
 - $\left(\frac{3P}{m_{max}^2}\right) 2^{2R}$
- P :
 - $\frac{A_m^2}{2}$
- m_{max} :
 - A_m
- Substituting above values of P and m_{max} , and $R = 7$, we get the above ratio to be:
 - $1.5 \times 2^{14} = 43.91$ dB

Effect of Sending FM Signal over Non-linear Channel

- Consider FM signal:
 - ❑ $s(t) = A_c \cos[2\pi f_c t + \phi(t)]$
 - ❑ where $\phi(t) = 2\pi k_f \int_0^t m(\tau) d\tau$
- Sent over a channel with following input-output characteristic:
 - ❑ $v_o(t) = a_1 v_i(t) + a_2 v_i^2(t) + a_3 v_i^3(t)$
 - ❑ where a_1 , a_2 and a_3 are constants
- Recall the trigonometric identity: $\cos^3 \theta = \frac{1}{4} (3\cos(\theta) + \cos(3\theta))$
- Output of channel:
 - ❑ $v_o(t) = \frac{1}{2} a_2 A_c^2 + \left(a_1 A_c + \frac{3}{4} a_3 A_c^3\right) \cos[2\pi f_c t + \phi(t)] + \frac{1}{2} a_2 A_c^2 \cos[4\pi f_c t + 2\phi(t)] + \frac{1}{4} a_3 A_c^3 \cos[6\pi f_c t + 3\phi(t)]$
- Can message signal $m(t)$ be recovered from $v_o(t)$?
 - ❑ Yes, assuming that f_c is much larger than bandwidth of FM signal
- Recovery:
 - ❑ Input $v_o(t)$ to band-pass filter with mid-band frequency f_c
- Output:
 - ❑ $v_o'(t) = \left(a_1 A_c + \frac{3}{4} a_3 A_c^3\right) \cos[2\pi f_c t + \phi(t)]$
- $v_o'(t)$ is scaled version of $s(t)$
- Thus, FM signals robust to transmission over non-linear channels of above type
- So FM widely used in satellite communication systems
 - ❑ permits the use of highly non-linear amplifiers, which are required for producing a high-power output at radio frequencies

Effect of Sending AM Signal over Non-linear Channel

- Consider AM signal:
 - $s(t) = A_c[1 + k_a m(t)]\cos[2\pi f_c t]$
- Sent over a channel with following input-output characteristic:
 - $v_o(t) = a_1 v_i(t) + a_2 v_i^2(t) + a_3 v_i^3(t)$
 - where a_1, a_2 and a_3 are constants
- Output of channel:
 - $v_o(t) =$
 $\frac{1}{2}a_2A_c^2[1 + k_a m(t)]^2 +$
 $\left(a_1A_c[1 + k_a m(t)] + \frac{3}{4}a_3A_c^3[1 + k_a m(t)]^3\right)\cos[2\pi f_c t] +$
 $\frac{1}{2}a_2A_c^2[1 + k_a m(t)]^2\cos[4\pi f_c t] + \frac{1}{4}a_3A_c^3[1 + k_a m(t)]^3\cos[6\pi f_c t]$
- Can message signal $m(t)$ be recovered from $v_o(t)$?
 - Difficult to recover it; cannot be recovered using envelope detection
- Thus, AM signal gets distorted when transmitted over non-linear channels of above type