

CHEMICAL KINETIC REACTION MECHANISM STUDY FOR AUTOIGNITION OF N-HEPTANE BLEND WITH TOLUENE AND 1,3-CYCLOHEPTADIENE

Speaker: Shenghui Qin

Advisor: Richard West

Promoting cleaner fuel combustion requires kinetic mechanisms

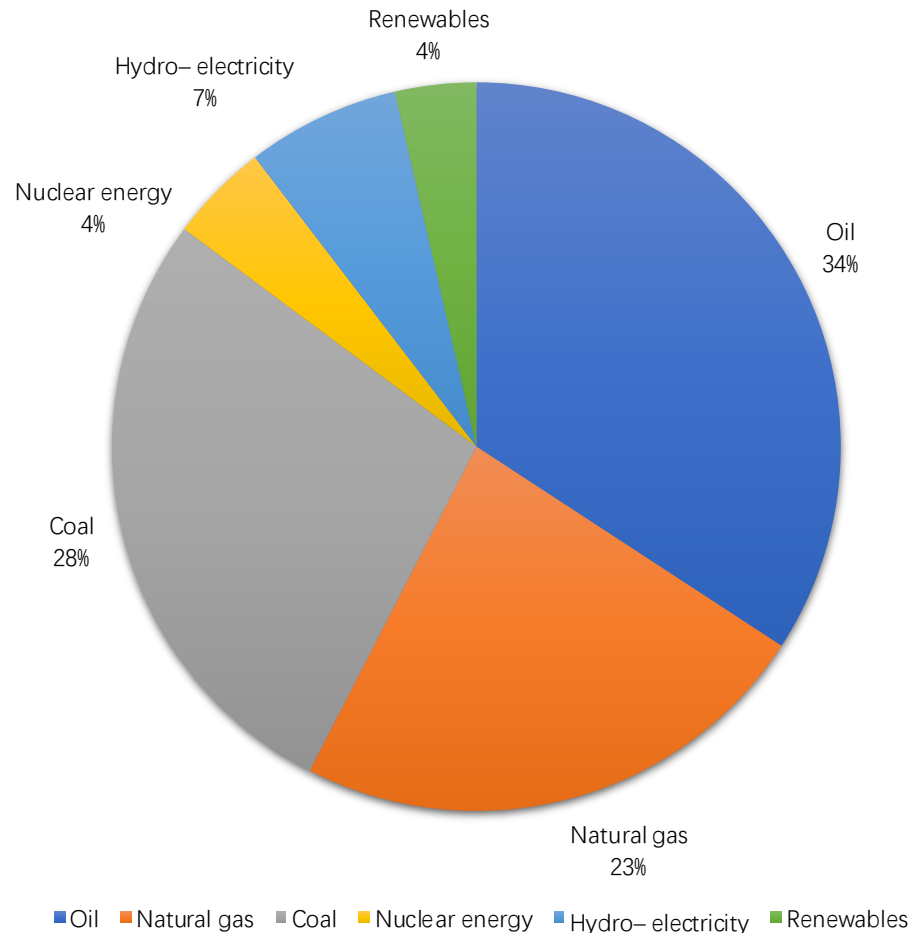


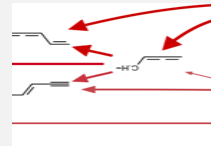
Figure 1. 2018 World Energy Consumption[1]



Energy consumption keeps growing, and fossil fuels will continue to be the primary energy source until 2040[1]



Engine combustion study promotes the design of efficient and clean combustion of hydrocarbons



Detailed kinetic reaction mechanism are needed to study combustion chemistry during fuel oxidation.

Brief glance of kinetic reaction mechanisms

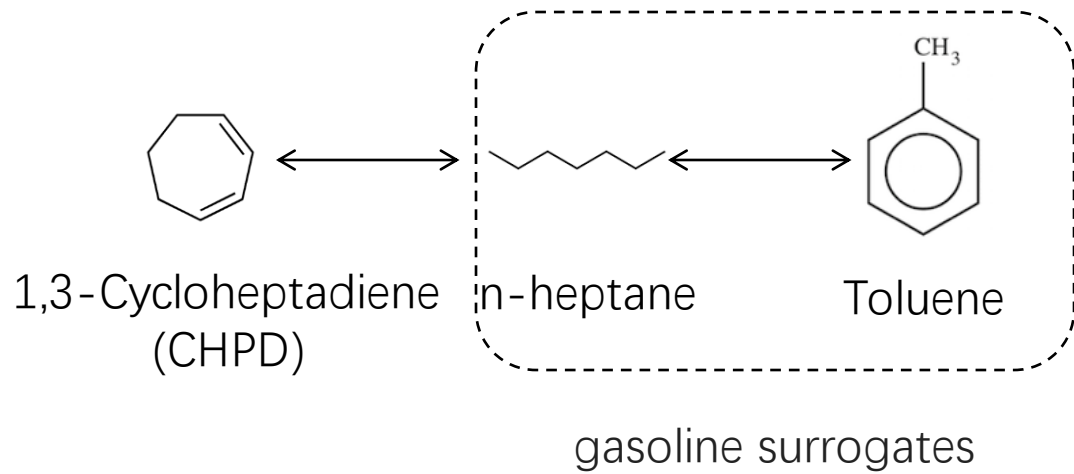
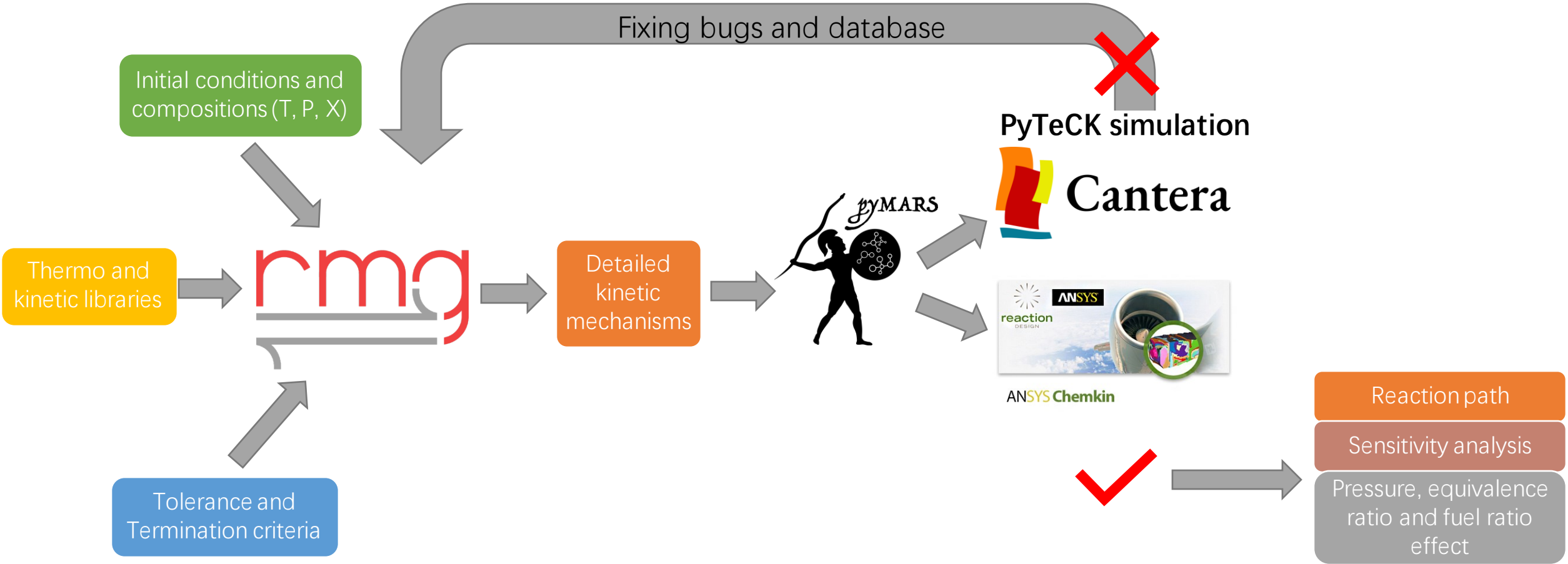


Table 1. RMG kinetic models' information

RMG model	Details
CHPD	870 species and 17120 reactions.
n-Heptane	708 species and 23059 reactions.
Toluene	998 species and 11571 reactions.
Blend of CHPD & n-Heptane	1734 species and 15096 reactions.
Blend of Toluene & n-Heptane	1937 species and 33995 reactions.

Workflow of proposing a kinetic mechanism



Model generation	Model reduction	Model validation	Model analysis
------------------	-----------------	------------------	----------------

Detailed kinetic mechanisms are bigger over time

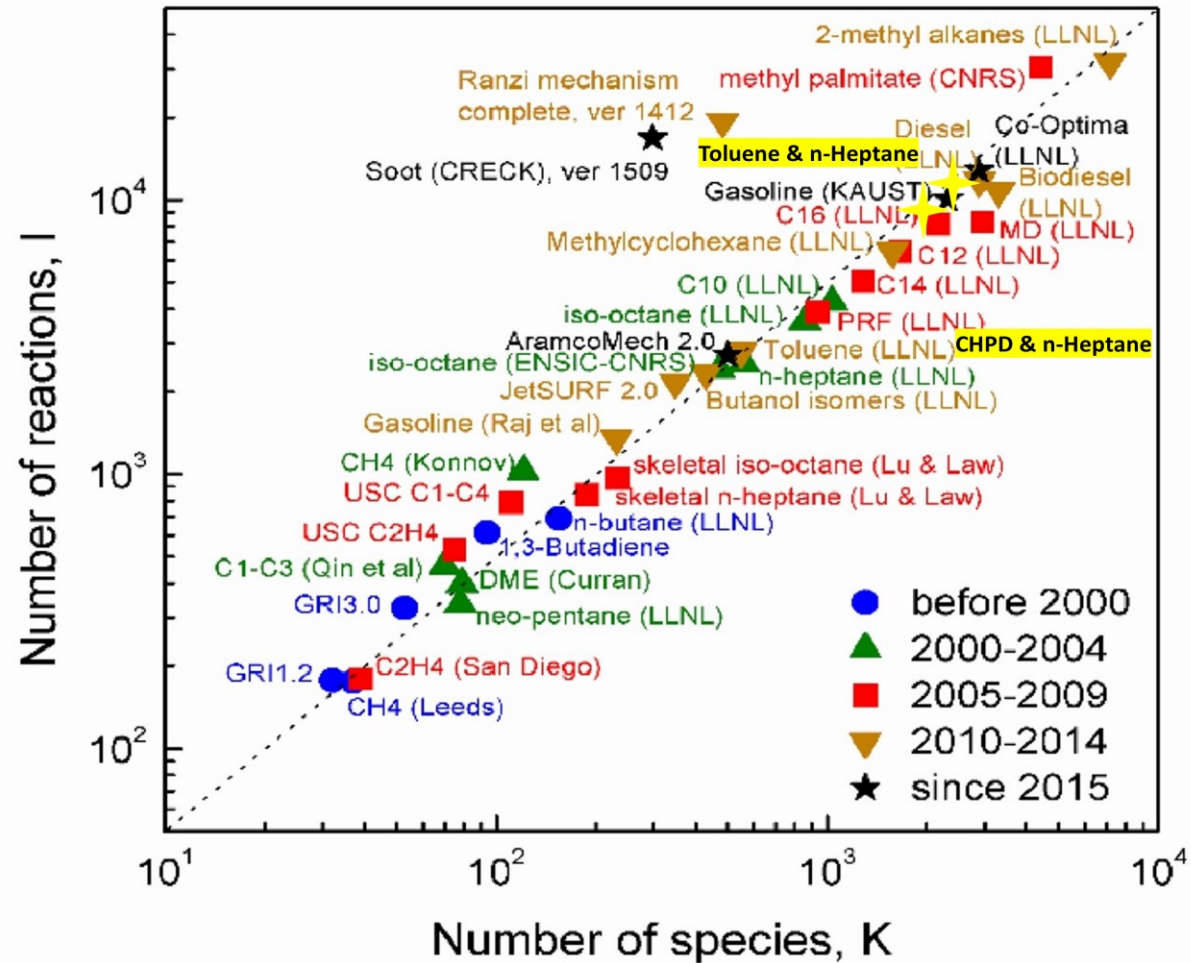
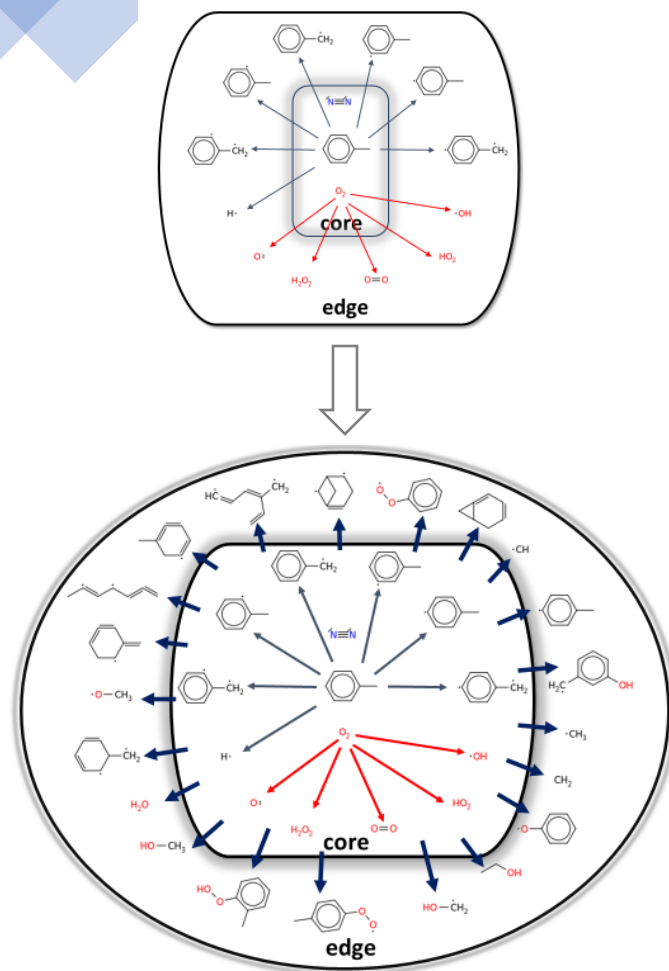


Figure 2. Increasing in size of kinetic mechanisms for hydrocarbon fuels[2]

- GRI-Mech 3.0 developed more than two decades ago (1999) and still in use, it contains 53 species and 325 reactions.
- Larger mechanisms construction are plausible as computation ability increases over the years
- Although it is possible to produce large mechanisms of thousands of reactions by hand, automatic generation of kinetic mechanisms can be more efficient, more systematic and less error-prone.

Reaction Mechanism Generator (RMG) generates combustion models automatically!



pyMARS reduces detailed kinetic mechanisms for computation concerns



pyMARS (Python-based Model Automatic Reduction) is a Python package for reducing the size of blend mechanism. Directed relation graph with error propagation (DRGEP) method[3] is applied in our application. In this study, we propose detailed kinetic reaction mechanisms of 1,3-Cycloheptadiene(CHPD), toluene, n-Heptane, and their blends using Reaction Mechanism Generator (RMG).

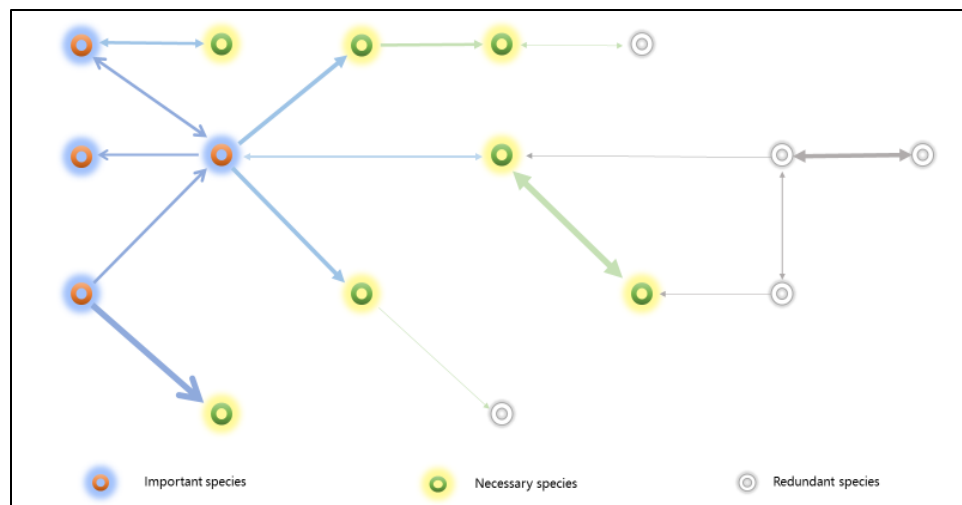


Figure 4. Relationships between species

Blend of CHPD & n-Heptane

Reduced CHPD & n-Heptane

1734 species and 15096 reactions.

470 species and 8970 reactions.

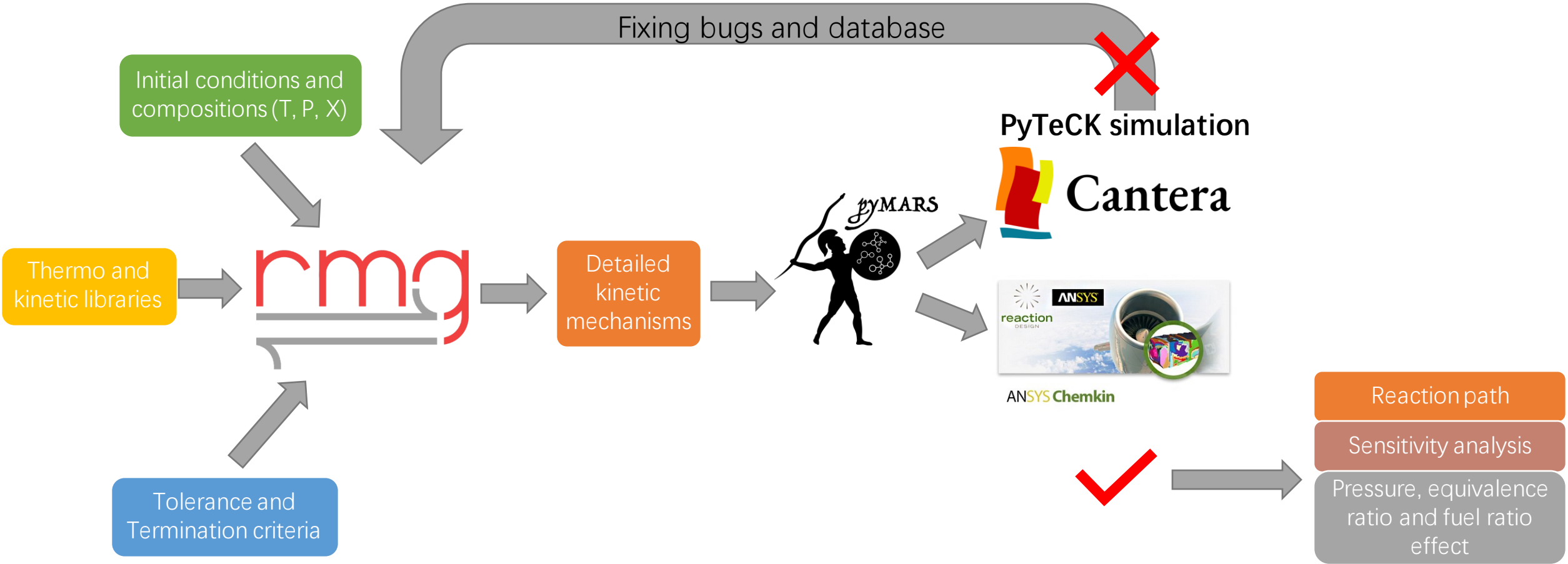
Blend of Toluene & n-Heptane

Reduced Toluene & n-Heptane

1937 species and 33995 reactions.

723 species and 20515 reactions.

Workflow of proposing a kinetic mechanism

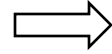


Model generation	Model reduction	Model validation	Model analysis
------------------	-----------------	------------------	----------------

PyTeCK simulation calculates ignition delay time

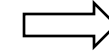
Ignition Delay Time

(IDT) experimental results at various temperature, pressure and fuel ratio conditions



ChemKED

Chemical Kinetics Experiment Data
YAML format datasets contains experimental IDT results



PyTeCK

Python tool for Testing Chemical Kinetics

Need: proposed kinetic mechanism

Output: all simulation results from ChemKED datasets

Rapid Compression Machine Shock Tube

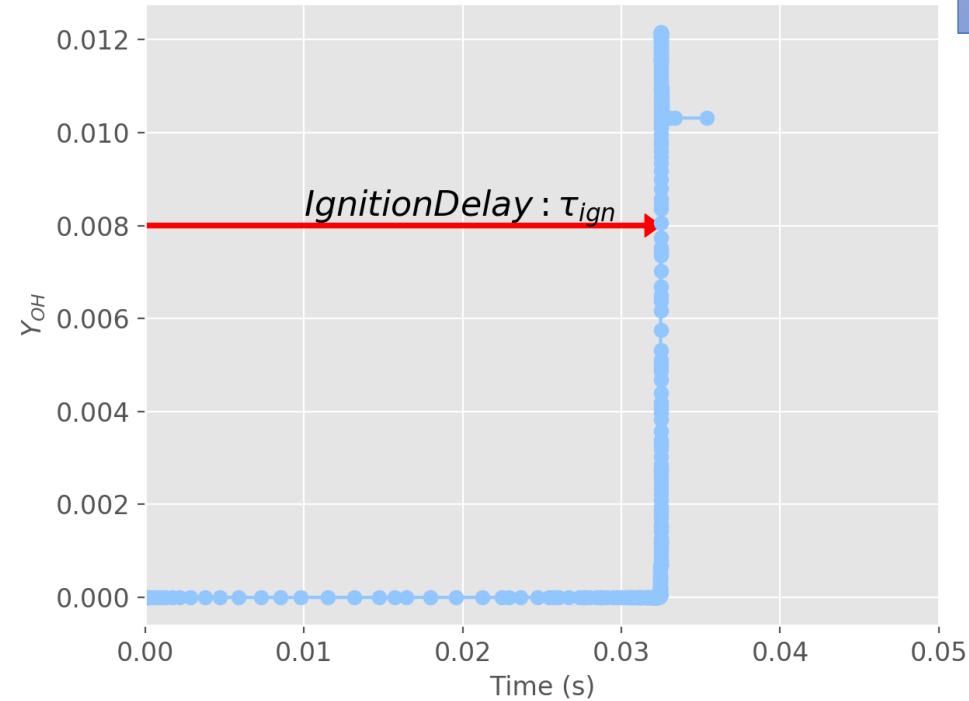
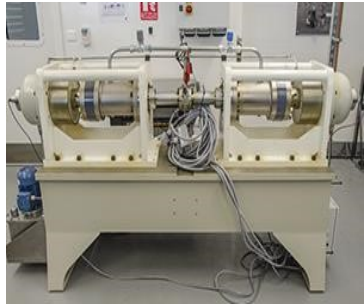


Figure 5. Illustration of ignition delay using OH radical

How ChemKED datasets are created

Table2. References with detailed experimental conditions[4 - 15]

Literature	Experimental conditions
Darshan M.A.Karwat RCM	Pressure: 9 atm Temperatures: 660–710 K Phi: 1
Alexander Burcat ST	Pressure: 2 to 12 atm Temperatures: 1100-1700 K Phi: 0.5-2
H.K.Ciezki ST	Pressure: 3.2 to 42 bar Temperatures: 660–1350 K Phi: 0.5-3

Listed left are 3 references with detailed experimental conditions when testing n-Heptane IDTs. These data were recompiled into 56 ChemKED datasets, and ready for PyTeCK comparison

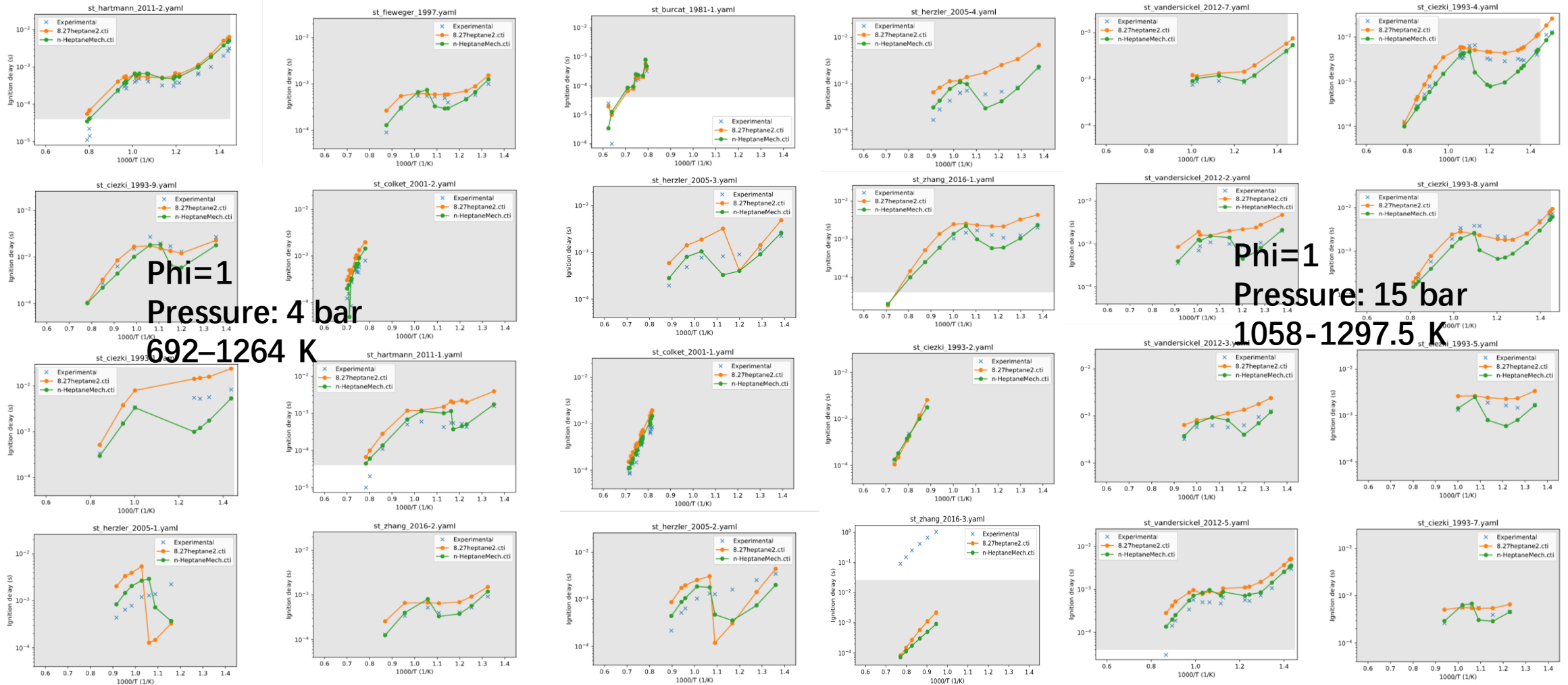
..... (12 references in total)

NO.	Pressure(bar)	phi
1	3.2	1
2	6.5	1
3	13.5	1
4	13.5	0.5
5	13.5	2
6	13.5	3
7	19.3	1
8	30	1
9	42	1

- [4] DM Karwat et al., Combustion and flame **160** (12), 2693 (2013).
- [5] A Burcat et al., 1971.
- [6] H Ciezki and G Adomeit, Combustion and flame **93** (4), 421 (1993).
- [7] MB Colket III and LJ Spadaccini, Journal of propulsion and power **17** (2), 315 (2001).
- [8] K Fieweger et al., Combustion and Flame **109** (4), 599 (1997).
- [9] M Hartmann et al., Combustion and Flame **158** (1), 172 (2011).
- [10] J Herzler et al., Proceedings of the Combustion Institute **30** (1), 1147 (2005).
- [11] DC Horning et al., Journal of Propulsion and Power **18** (2), 363 (2002).
- [12] JM Smith et al., International journal of chemical kinetics **37** (12), 728 (2005).
- [13] A Vandersickel et al., Fuel **93**, 492 (2012).
- [14] D Vermeer et al., Combustion and Flame **18** (3), 327 (1972).
- [15] K Zhang et al., Combustion and Flame **172**, 116 (2016).

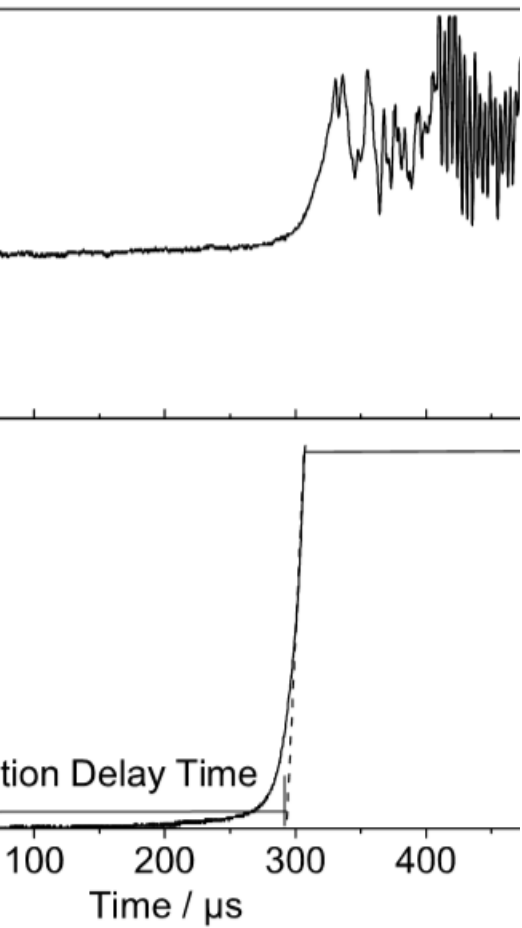
n-Heptane experiments and simulation IDT comparison over a wide range conditions

Qin-n-Heptane
LLNL-n-Heptane



..... (56 subfigures in total)

Figure 6. PyTeCK results of n-Heptane



ure (upper part) and CH* emis
indicating ignition delay in a lean
Reaction conditions: $\Phi =$
= 51.5 bar.

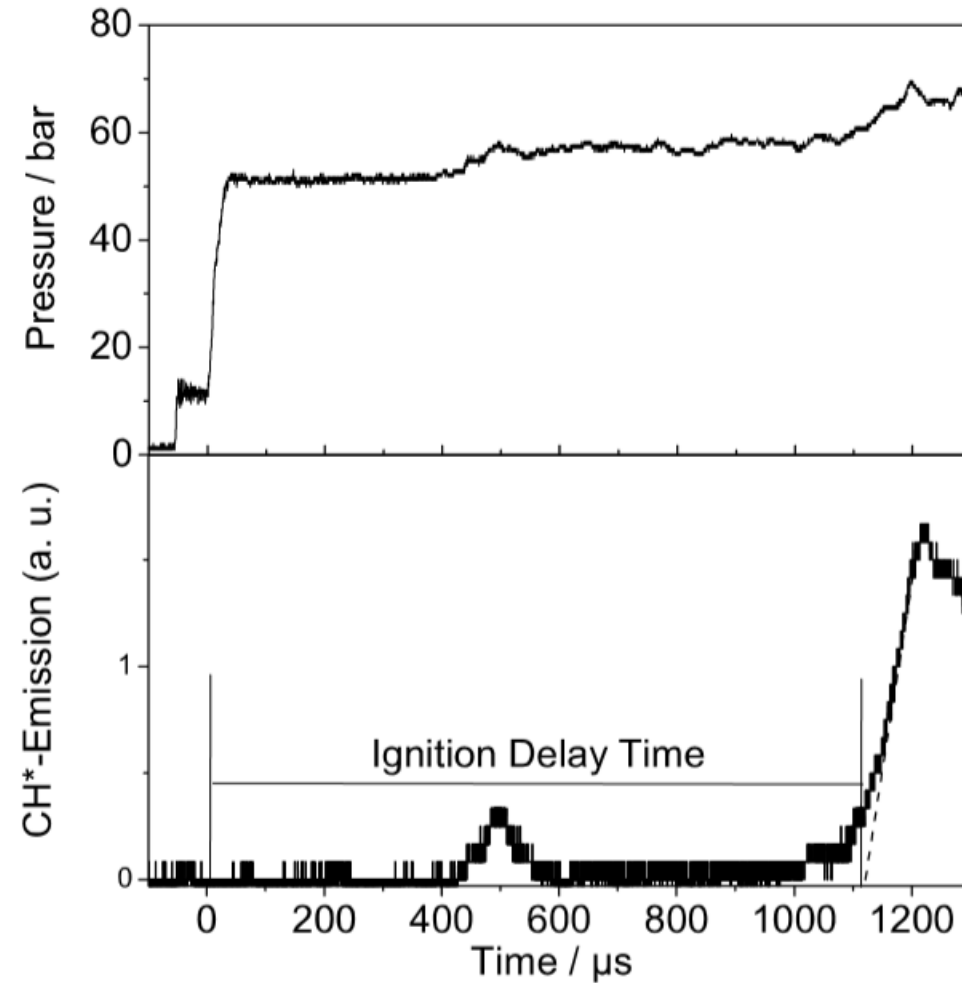


Fig. 3. Typical pressure (upper part) and CH* emission (lower part) profiles indicating two-stage ignition delay in a lean n-heptane/air mixture. Reaction conditions:

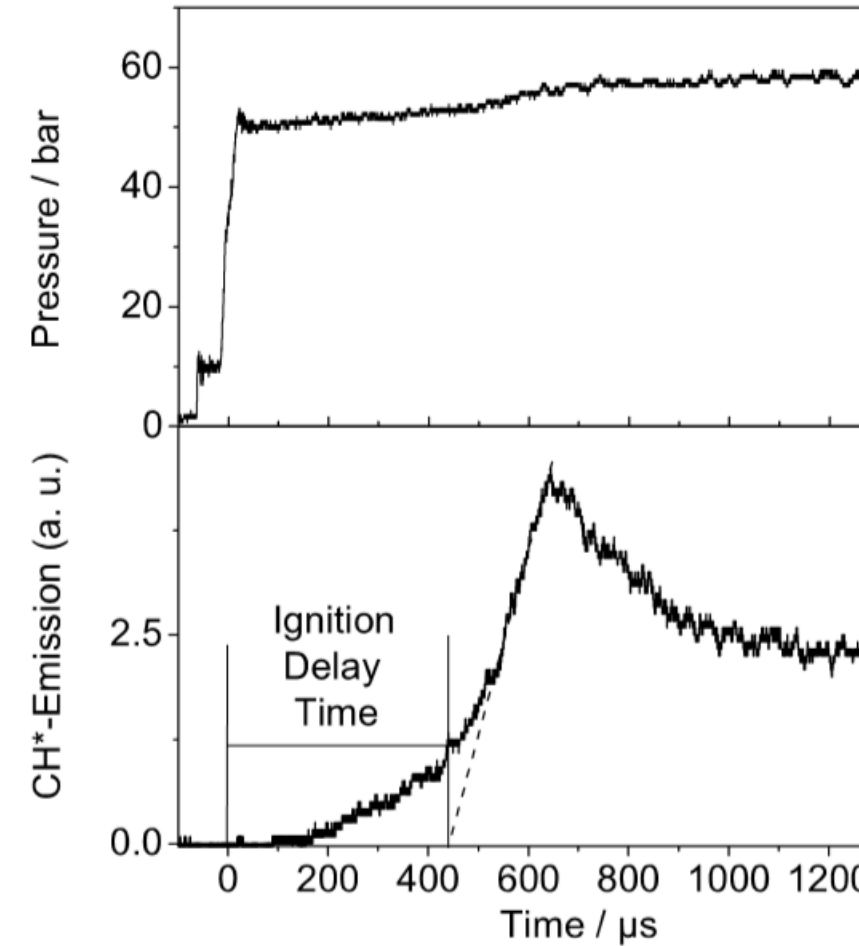


Fig. 5. Typical pressure (upper part) and CH* emission (lower part) profiles indicating ignition delay in a heptane/air mixture. Reaction conditions:

n-Heptane IDT simulation show large errors due to wrong stage of IDTs

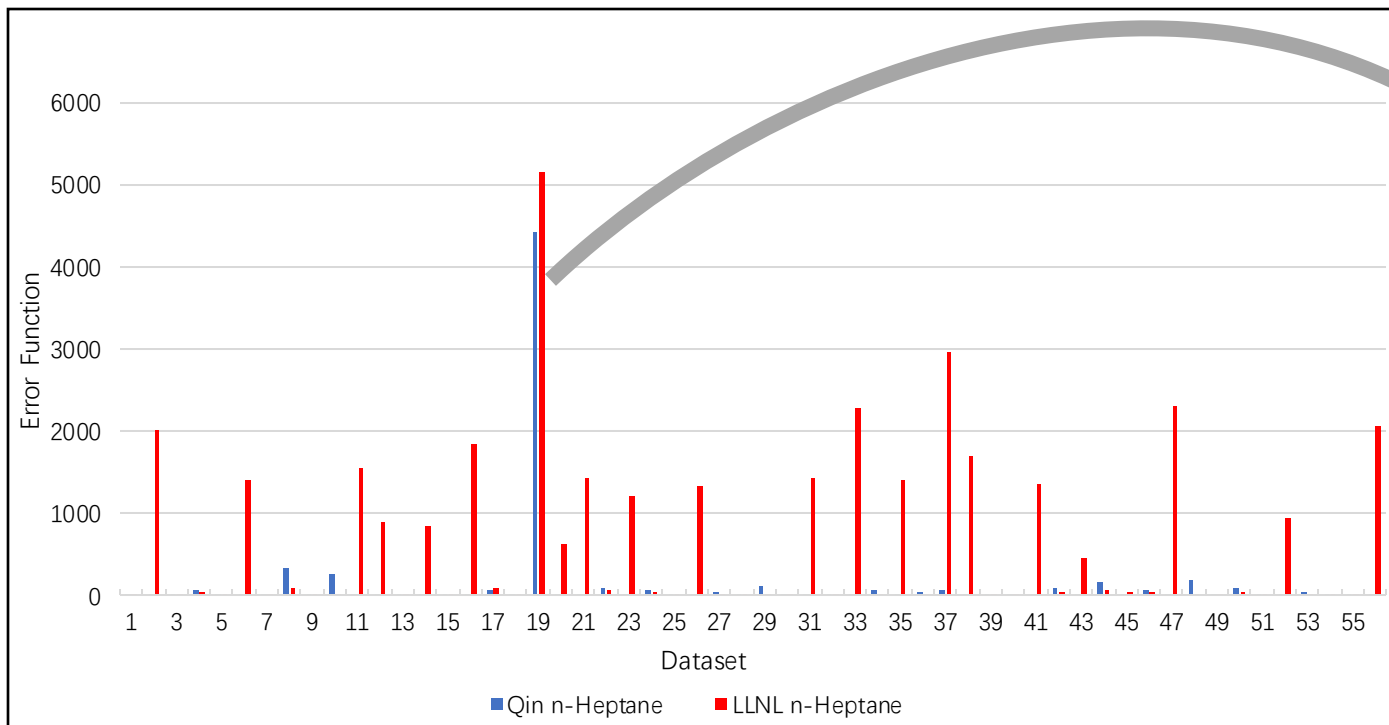


Figure 7. Error function of two tested models for n-Heptane IDT simulation

$$\text{Error function} = \left(\frac{\log(\text{ignition_delays_sim})}{\log(\text{ignition_delays_exp}) / \text{standard_deviation}} \right)^2$$

Where `standard_deviation` is defined as the standard deviation of the difference between data and best-fit line, and it is explained in the “eval_model” file in the PyTeCK website.

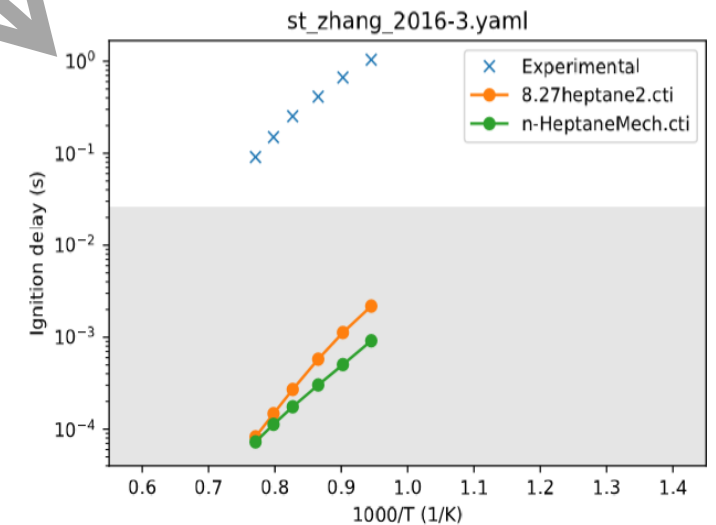


Figure 8. experimental and situational IDTs over 1000/K Phi=1 15 bar

In dataset 19, there is a 3-magnitude error between experimental and simulation IDTs. Two model did not correctly predict IDT and we attribute this to wrong IDT selection.

Ignition delay time selection is tricky

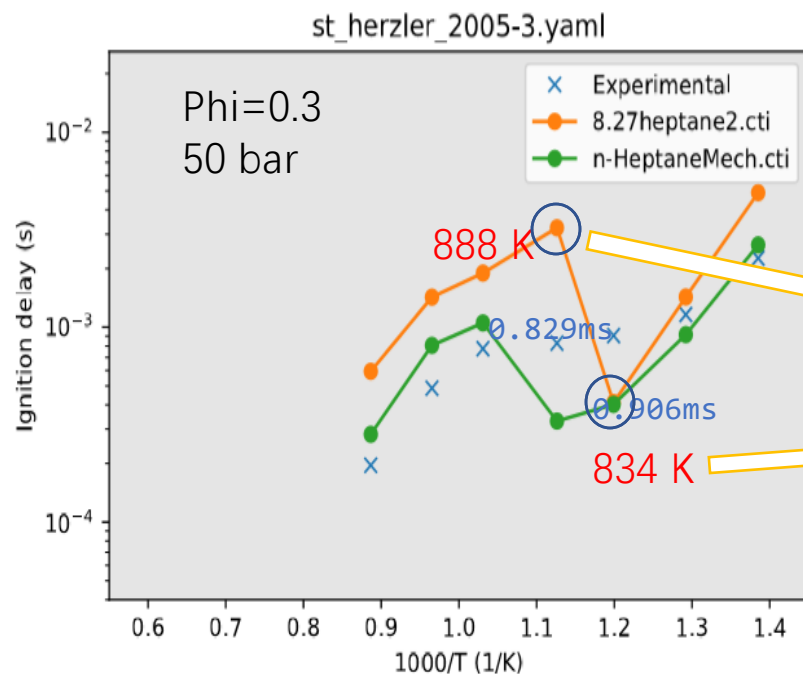


Figure 9. experimental and situational IDTs over 1000/K

Some experiments measure pressure rise; some monitor the concentration of an intermediate like OH via laser absorption; but other studies monitor the luminescence of excited OH* decaying to ground state OH (which it does by emitting a photon).

In herzler's experiments, all ignition delay time values were determined by extrapolating the highest increase of the emission signal to its zero level at the time axis. In short, **d(CH*)/dt max** as IDT signal.

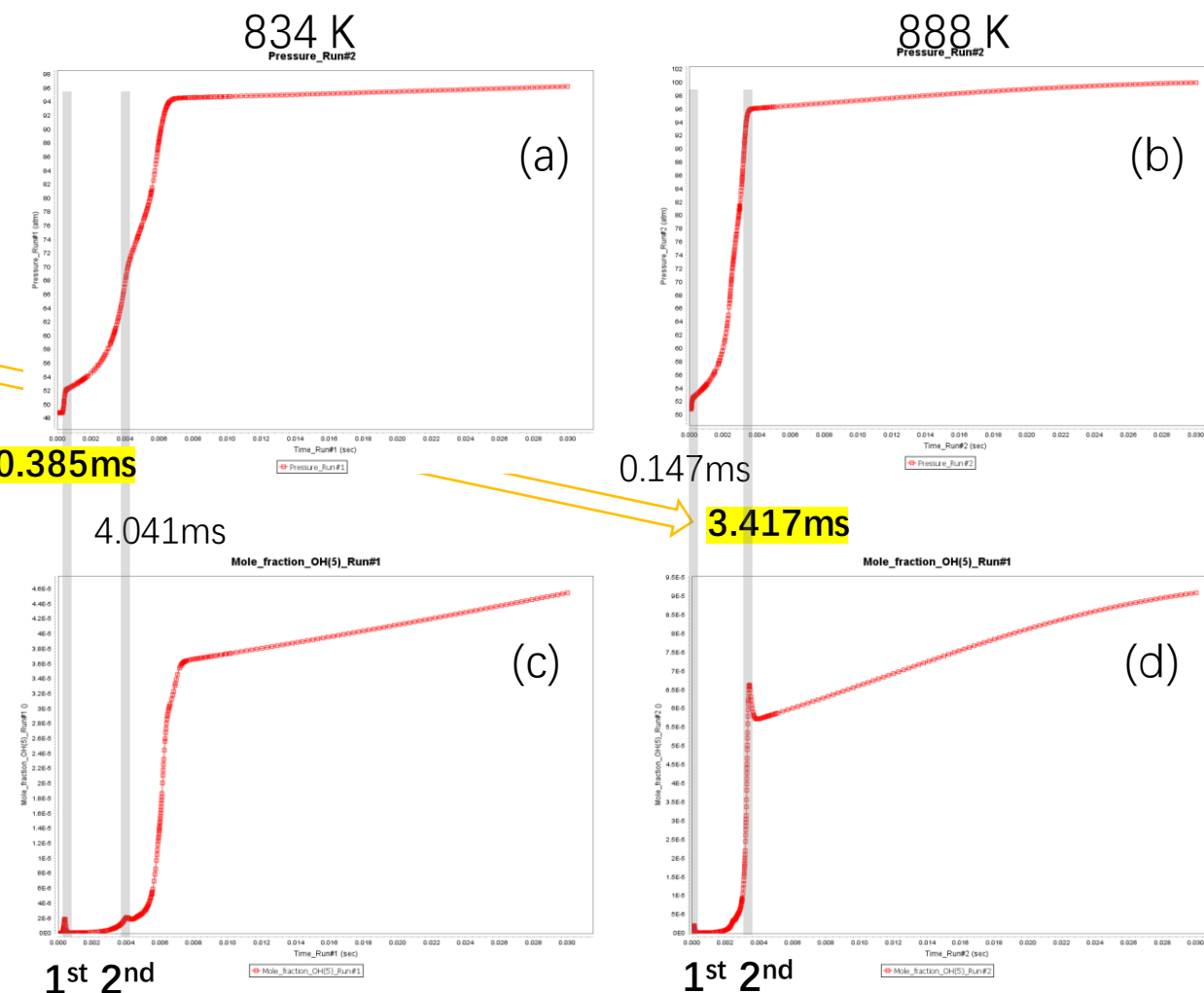


Figure 10. Pressure and OH mole fraction variation over time

In simulation, we use dP/dt max as the IDT signal. At 834 K, the simulation use 0.385 ms as IDT, while at 888 K, it consider 3.417 ms as IDT.

Blend model of n-Heptane&Toluene validation using same process above

Table2. References with detailed experimental conditions[16 - 20]

Literature	Experimental conditions
R Di Sante RCM	Pressure: 11 bar Temperatures: 710–790 K Phi: 1 Toluene ratio: 25-60 %vol
M Hartmann ST	Pressure: 40 bar Temperatures: 710-1184 K Phi: 0.5-1 Toluene/n-Heptane: 10/90 %vol
J Herzler ST	Pressure: 10-50 bar Temperatures: 640–1180 K Phi: 0.3-1 Toluene/n-Heptane: 65/35 %vol
Z Malliotakis ST RCM	Pressure: 10-30 bar Temperatures: 690–1480 K Phi: 0.5-2 Toluene ratio: 50-90 %vol
S Goldsborough RCM	Pressure: 20-40 bar Temperatures: 715-870 K Phi: 0.5-2 Toluene ratio: 25-50 %vol

Pressure ranging from 10-50 bar

Temperature ranging from 640-1480 K

Equivalence ration ranging from 0.3-2

Toluene volume fraction in fuels from 25-90 %

[16] R Di Sante, Combustion and flame **159** (1), 55 (2012).
[17] M Hartmann et al., Combustion and Flame **158** (1), 172 (2011).
[18] J Herzler et al., Combustion and flame **149** (1-2), 25 (2007).
[19] Z Malliotakis et al., Combustion and Flame **199**, 241 (2019).
[20] S Goldsborough, unpublished.

Three blended models' performance expressed using error function

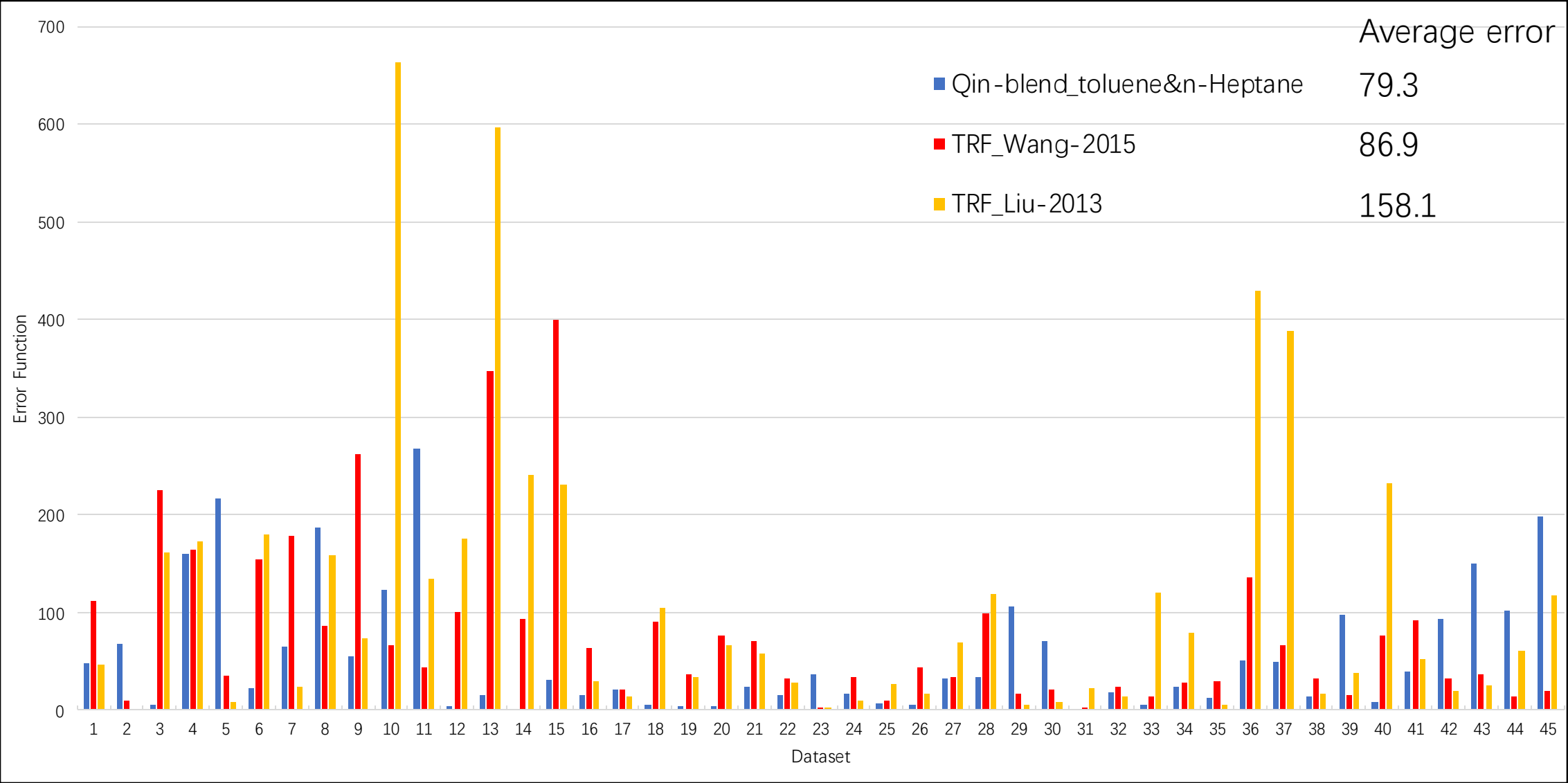
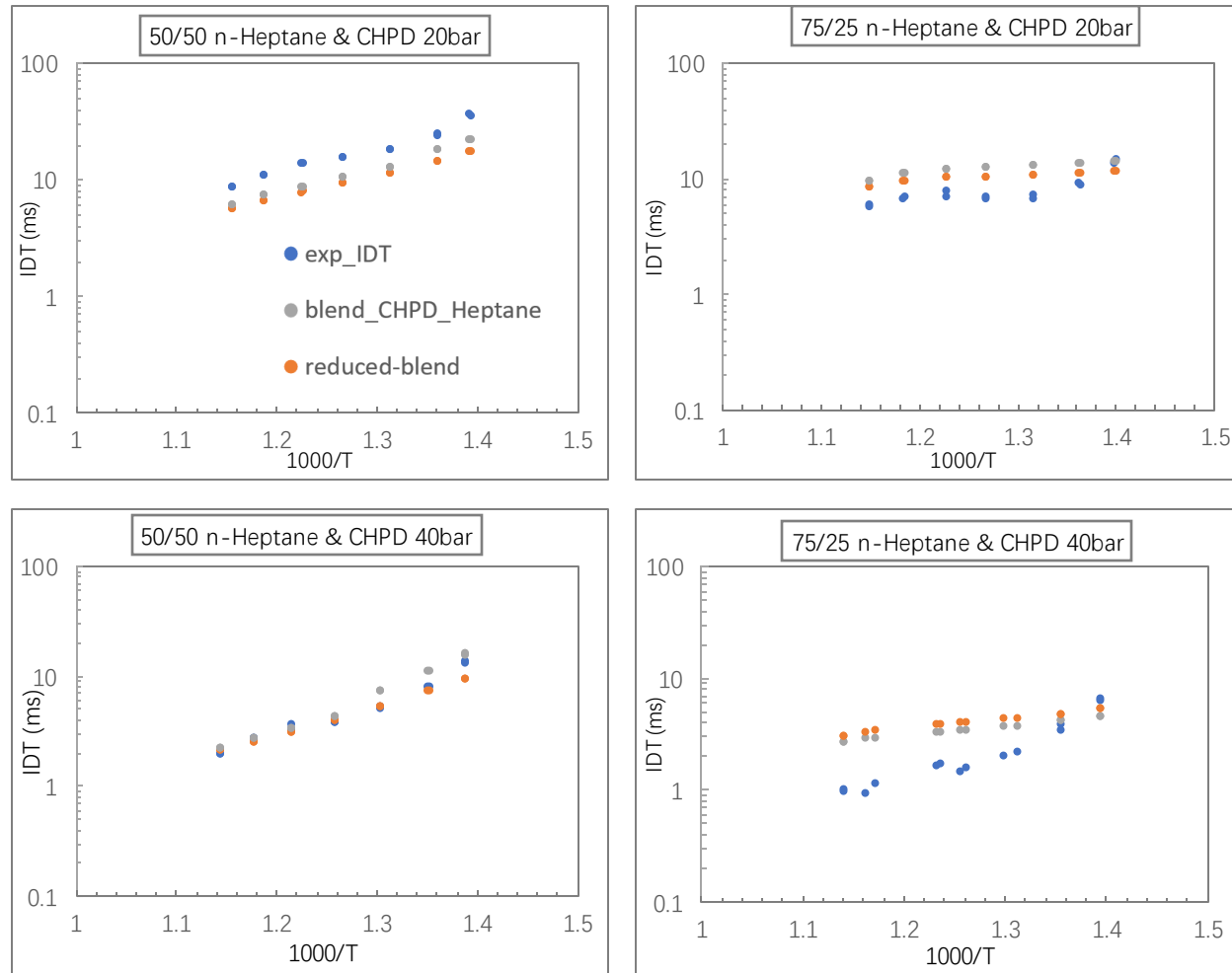


Figure 11. Error function of three tested models for toluene & n-heptane blend IDT simulation

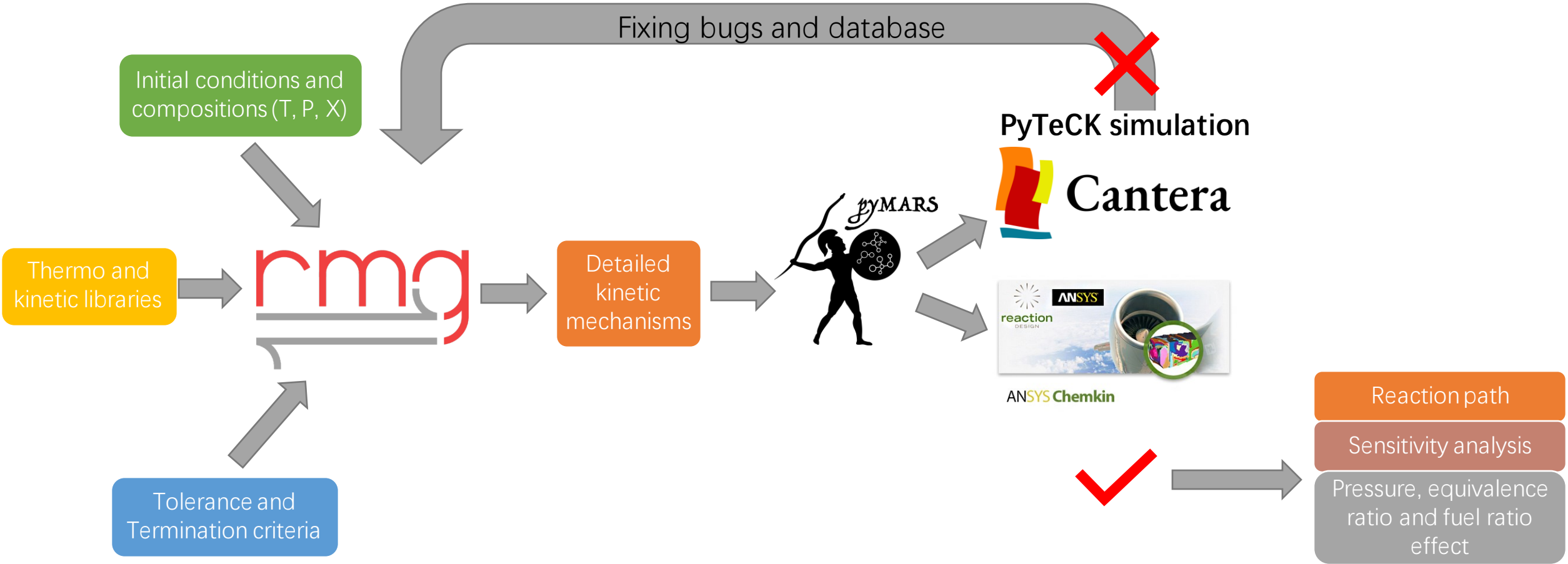
Blend model IDT simulations show acceptable discrepancy with exp data



- The experimental data are from Scott's RCM experimentation, and as far as we know, these are the only IDT experimentation about CHPD and n-Heptane blends.
- The simulation IDT results of the blend model and reduced blend model shows good uniformity, and this can help prove our reduced model does capture the core pathways of a detailed kinetic reaction model.
- Similarly, original model VS reduced model of toluene & n-Heptane blend is attached in Appendix B.

Figure 12. Comparison between experimental data and simulation results of CHPD & n-Heptane blend models

Workflow of proposing a kinetic mechanism



Model generation	Model reduction	Model validation	Model analysis
------------------	-----------------	------------------	----------------

Reaction pathway for n-Heptane

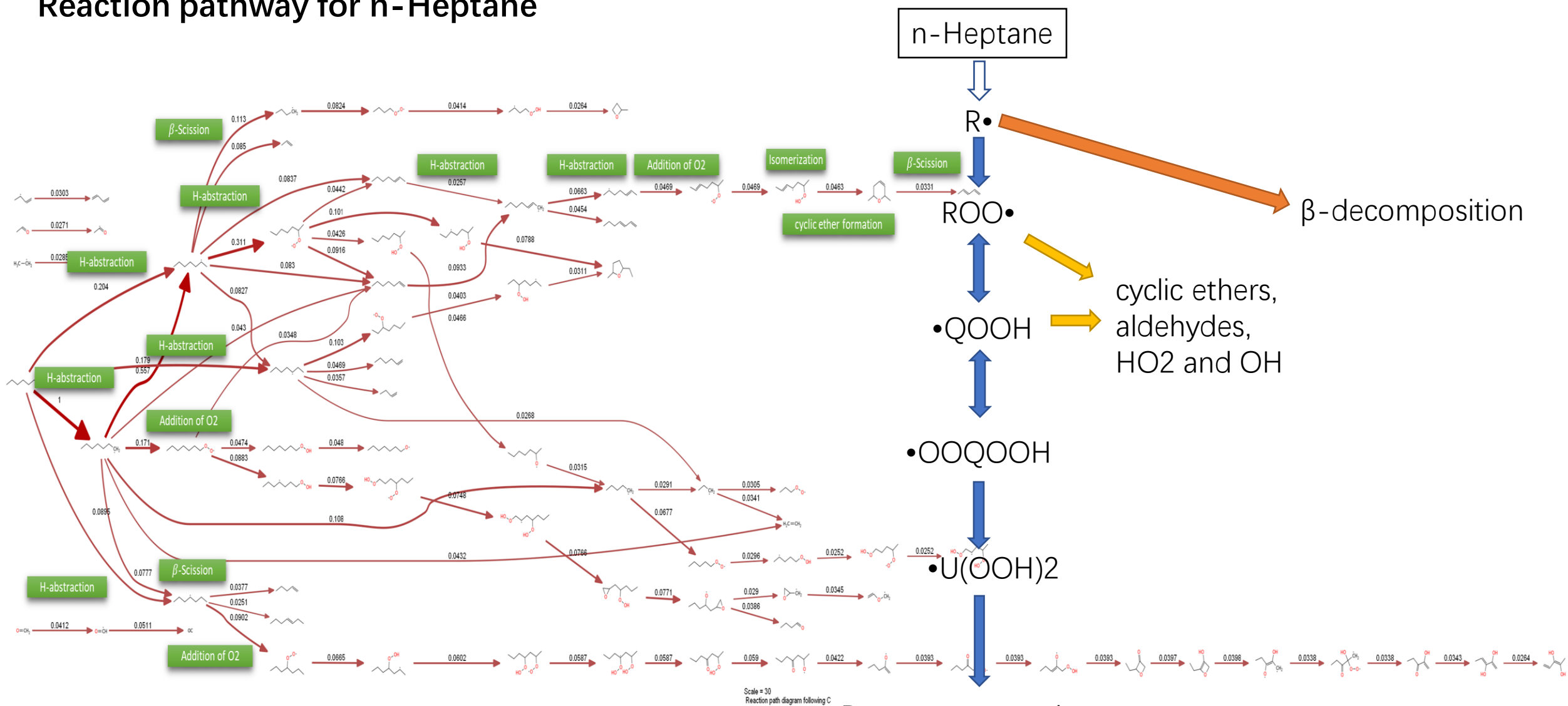


Figure 13. Reaction path for n-Heptane at 950 K

Degenerate products

Low temperature

Intermediate

High temperature

Reaction pathway for toluene in blend of toluene & n-Heptane

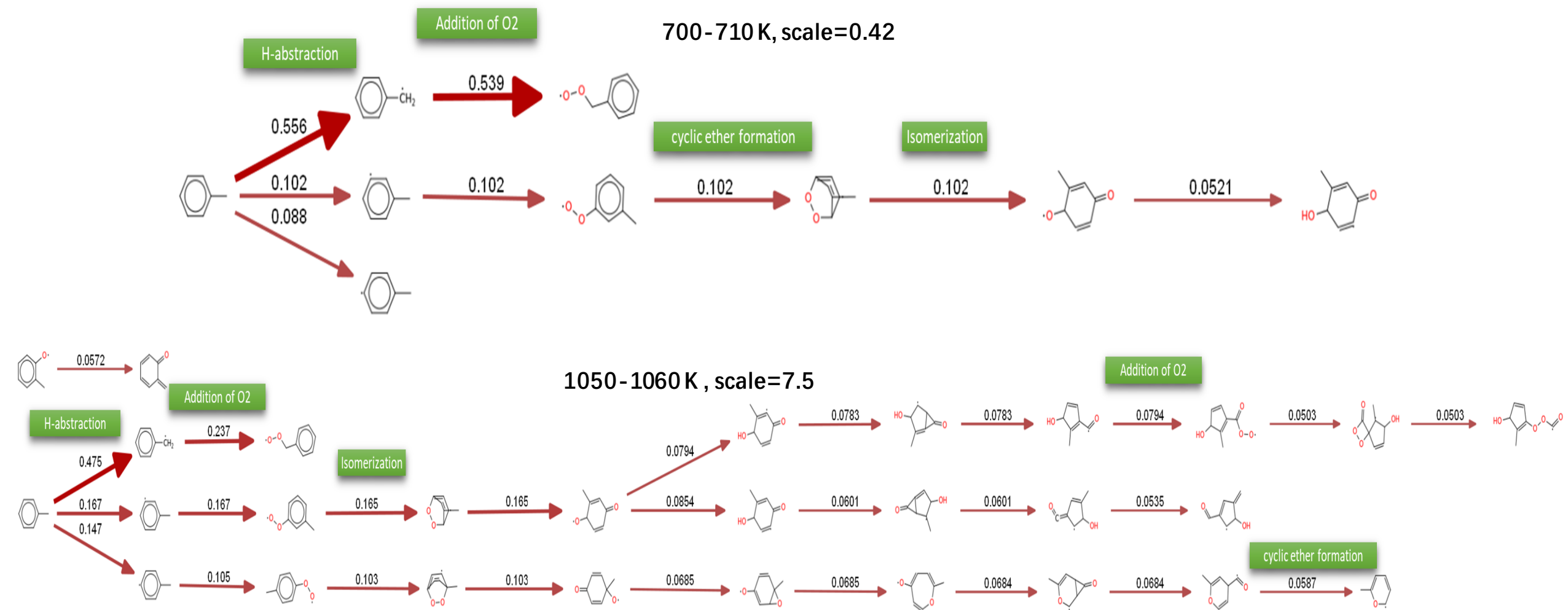


Figure 14. Reaction path for toluene at different initial temperatures

OH sensitivity for toluene & n-Heptane blend over NTC region

This paper we compute normalized OH radical concentration sensitivity against rate constant for reaction i below:

$$\frac{\partial \ln[OH]}{\partial \ln k_i} = \frac{\partial [OH]}{[OH]} \cdot \frac{k_i}{\partial k_i}$$

$$= \frac{k_i}{[OH]} \cdot \frac{\partial [OH]}{\partial k_i}$$

A positive sensitivity result means the increase in the reaction rate will favor the production of OH radicals and speed up the reaction chain and vice versa.

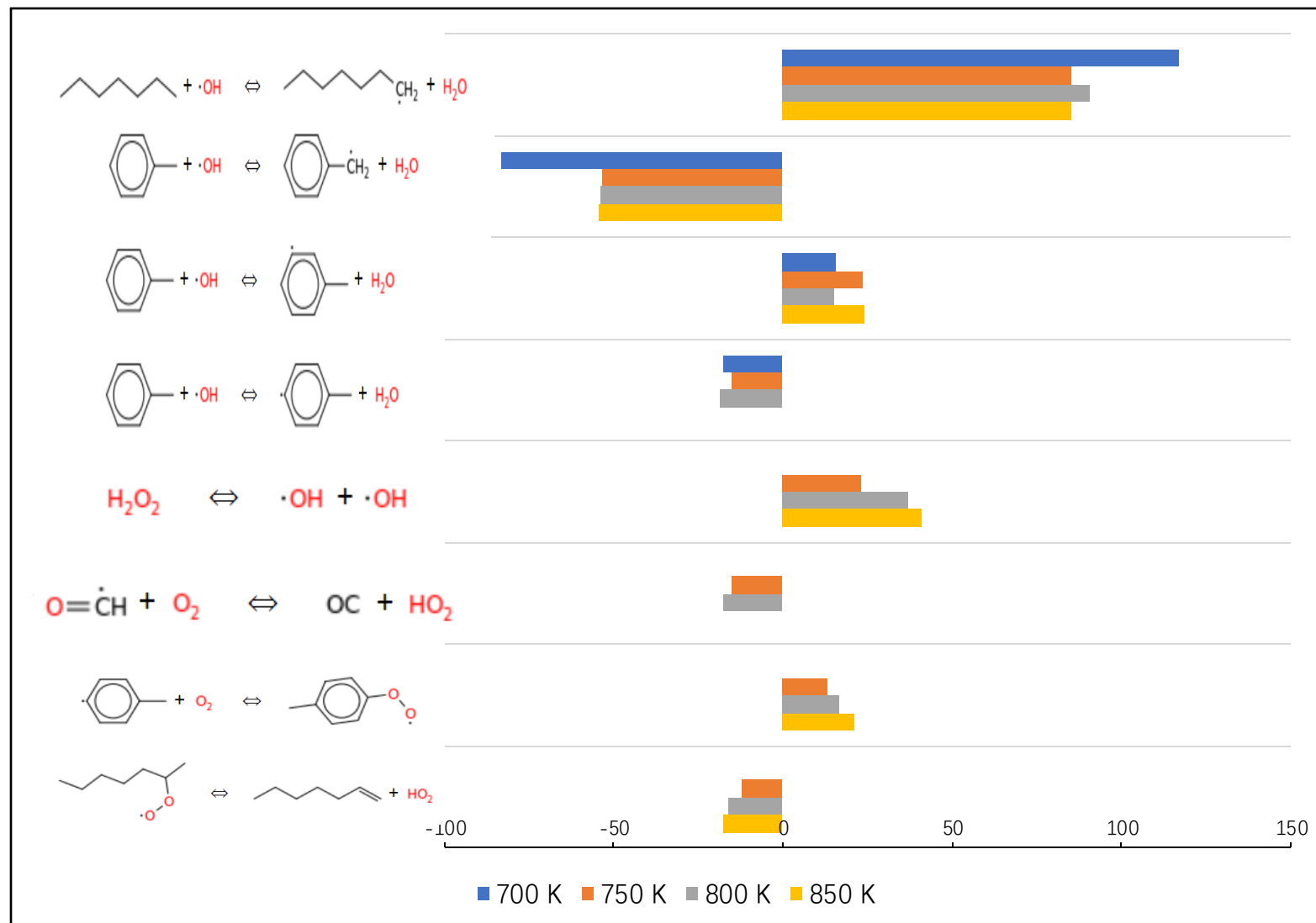


Figure 15. OH sensitivity for Toluene & n-Heptane blend at 700-850 K and 40 atm

Reaction pathway for CHPD & n-Heptane blend

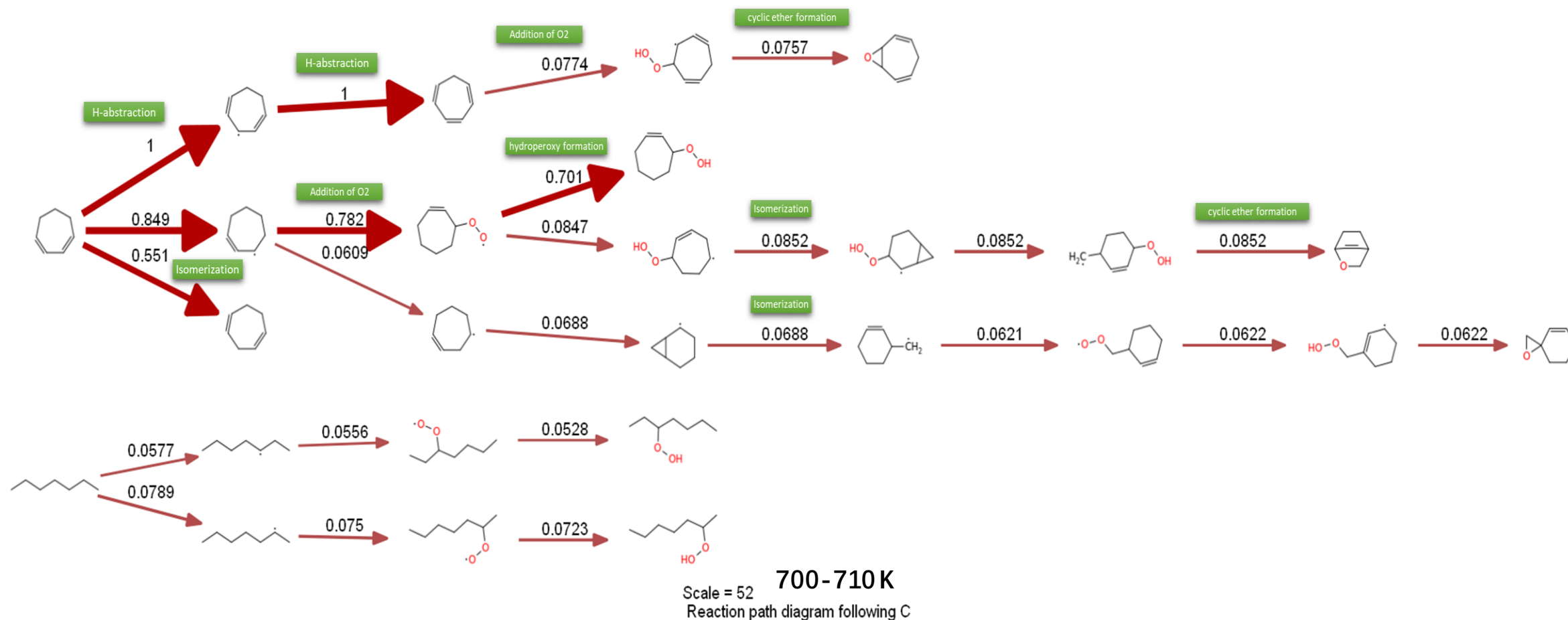


Figure 16. Reaction path for the blend fuel of CHPD and n-Heptane at different initial temperatures

OH sensitivity for CHPD & n-Heptane blend

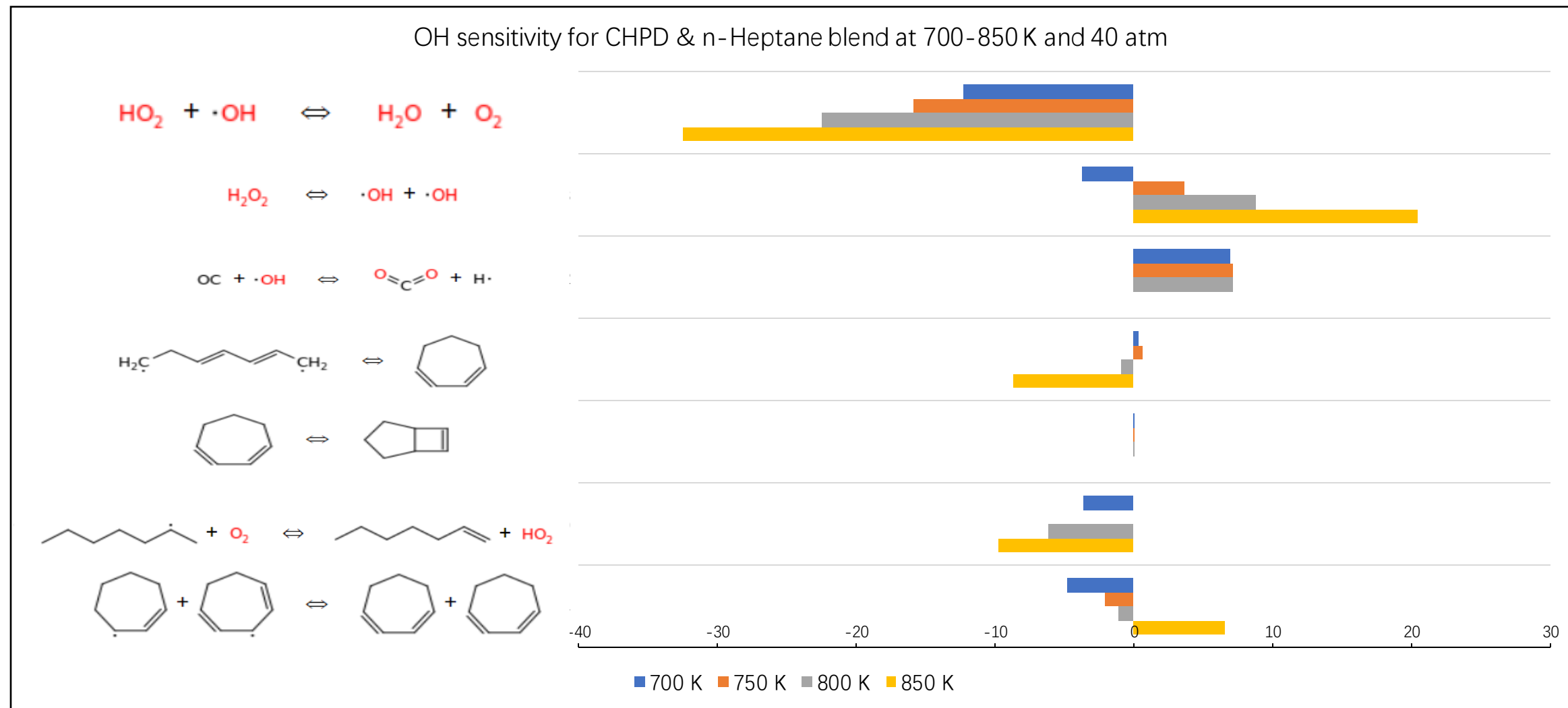


Figure 17. OH sensitivity for CHPD & n-Heptane blend at 700-850 K and 40 atm

Model performance of fuel X from lean to rich in volume ratio

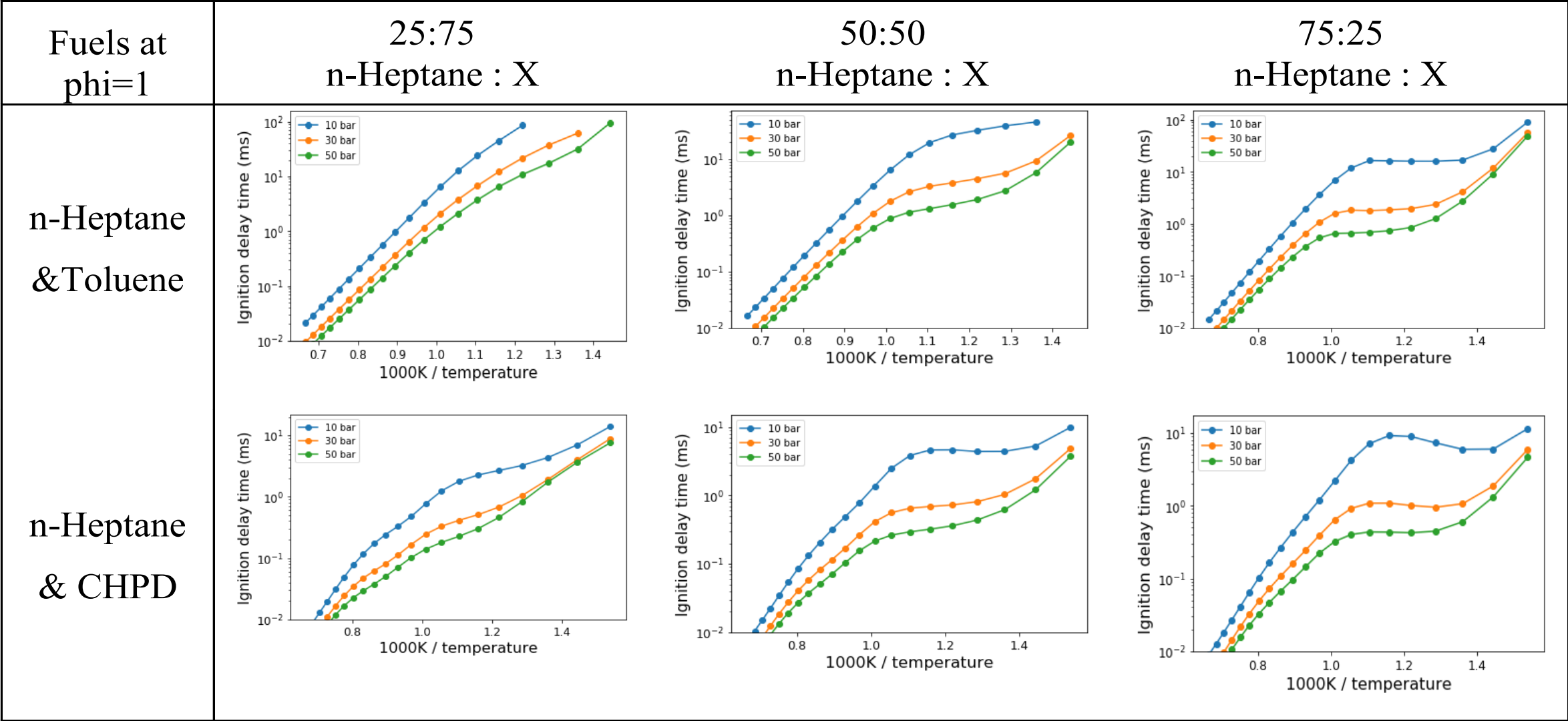
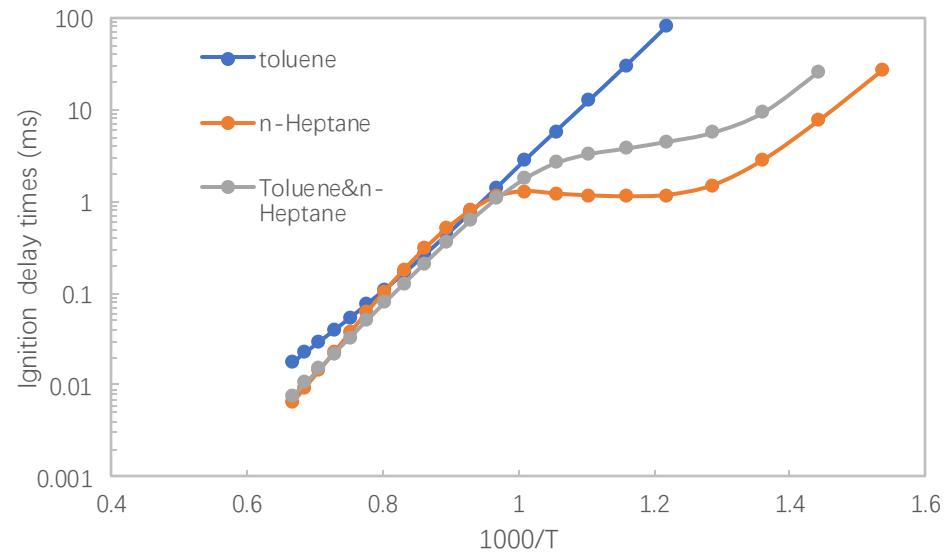
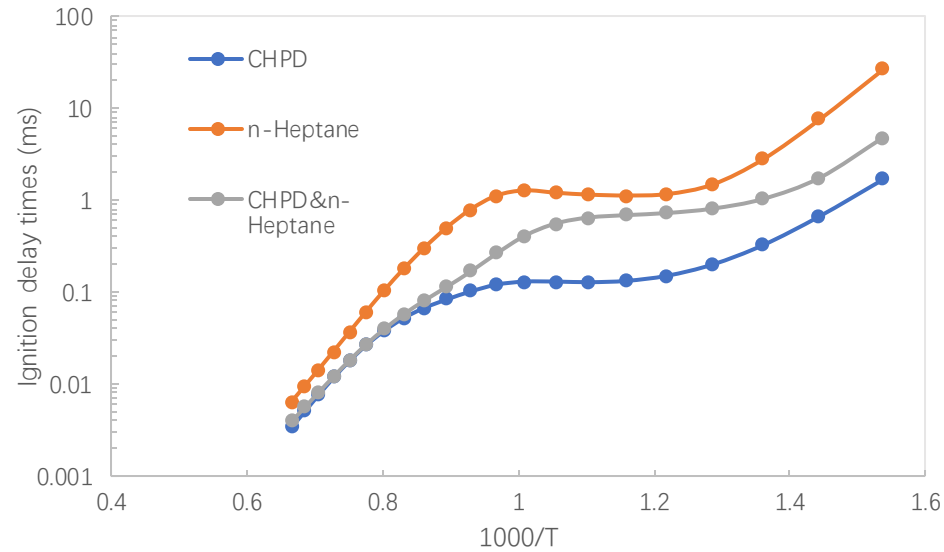


Figure 18. Simulated IDT of fuels at various equivalence ratio and pressures

CHPD and toluene performance when blended with n-Heptane



- The blend of CHPD & n-Heptane shows a similar ignition curve to n-Heptane and CHPD, but the blend NTC region moves to lower temperature than the two fuels alone.
- Toluene oxidation is a line, while blended with n-Heptane, a relatively slightly NTC region shows.
- Toluene delays blend of toluene & n-Heptane IDT. E.g., at 30 bar, and ϕ equals 1, the blend is about 3 ms higher than n-Heptane for temperature range from 730 to 900 K.

Figure 19. Simulated IDT of fuel blends at 30 bar and $\phi=1$

Thank you!

Richard and all the members in Computational Modeling in Chemical Engineering(CoMoChEng) Group,

Committee members: Scott Goldsborough and Benjamin Woolston.

Department of Chemical Engineering at Northeastern University

And all my family members
