

# **EL2520 Control Theory and Practice**

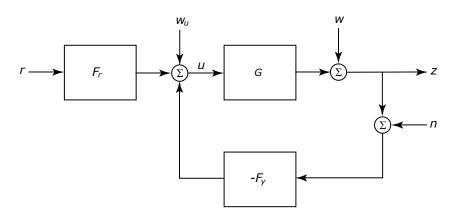
#### Fundamental Limitations in MIMO Control

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## Today's Lecture

- Performance specifications for MIMO systems
- Performance limitations in MIMO systems
  - S+T=I
  - Generalized Bode sensitivity integral
  - RHP zeros and poles
  - Disturbances and RHP zeros

## Performance Objectives



We have

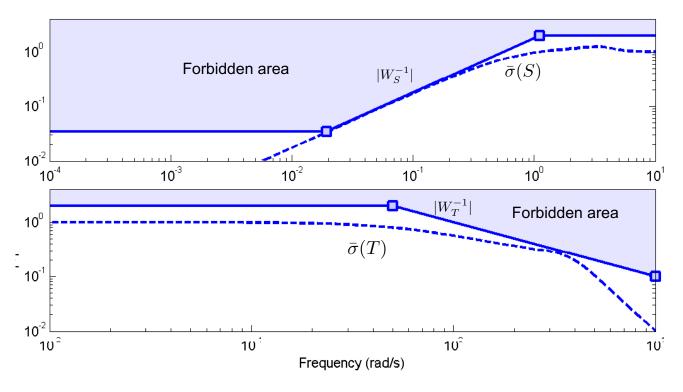
$$z = (I + GF_y)^{-1}w - (I + GF_y)^{-1}GF_yn = Sw - Tn$$

- Thus, make S "small" for disturbance attenuation and T "small" for noise damping
- At each frequency we have

$$\underline{\sigma}(S(i\omega)) \le \frac{|z|}{|w|} \le \bar{\sigma}(S(i\omega)) \; ; \quad \underline{\sigma}(T(i\omega)) \le \frac{|z|}{|n|} \le \bar{\sigma}(T(i\omega))$$

 $-\;\;$  Thus, to bound |z|, need to bound  $ar{\sigma}(S)$  and  $ar{\sigma}(T)$ 

## Frequency Domain Specifications



$$\bar{\sigma}(S) \le |W_S^{-1}| \ \forall \omega \iff \|W_S S\|_{\infty} \le 1 \ ; \ \bar{\sigma}(T) \le |W_T^{-1}| \ \forall \omega \iff \|W_T T\|_{\infty} \le 1$$

- What limits the choices for  $W_S$  and  $W_T$  ?
- Note: we assume scalar weights throughout

## A Note on Scaling

- Before considering performance specifications and limitations it is useful to scale the problem so that the expected or allowed size of any signal is 1
- See Lecture notes 6 on how to scale.

### Trade-off 1: S+T=I

$$\underbrace{(I+GF_y)^{-1}}_{S} + \underbrace{(I+GF_y)^{-1}GF_y}_{T} = I$$

Fan's Theorem:

$$\sigma_i(A+B) \ge \sigma_i(A) - \bar{\sigma}(B) \quad \forall i$$

Thus,

$$|1 - \bar{\sigma}(T)| \le \bar{\sigma}(S) \le 1 + \bar{\sigma}(T)$$

- Hence, at any frequency
  - can not make both  $\bar{\sigma}(S)$  and  $\bar{\sigma}(T)$  small (at the same frequency)
  - peak in S implies peak in T:

$$\bar{\sigma}(S) >> 1 \iff \bar{\sigma}(T) >> 1$$

• Hence, we can not choose  $|W_S|$  and  $|W_T|$  large at the same frequency

## Trade-off 2: (Bode) Sensitivity Integral

 Extension of the Bode Sensitivity Integral (see lec 4) to MIMO systems yields

$$\int_0^\infty \ln|\det(S(i\omega))| d\omega = \sum_j \int_0^\infty \ln \sigma_j(S(i\omega)) d\omega = \pi \sum_i \operatorname{Re}(p_i)$$

- proof based on Cauchy integral formula.
  - $\det(S)$  is essentially a sensitivity function and  $\det(S) = \prod_j \sigma_j(S)$
- trade-off between frequencies as well as between directions
- cannot make  $|W_S|$  large at all frequencies and in all directions (note that a scalar weight usually is preferred and then all directions are weighted equal)

### **Limitation 1: RHP Zeros**

**Thm:** Assume G(s) has a RHP zero at s=z>0. Then

$$||W_S S||_{\infty} \ge |W_S(z)|$$

generalization of result for SISO case (see video/lec notes 4)

**Proof:** By definition G(z) is rank deficient, i.e.,

$$y_z^H G(z) = 0 \Rightarrow y_z^H T(z) = 0$$

Since T=S-I we get

$$y_z^H S(z) = y_z^H \Rightarrow S^H(z) y_z = y_z$$

and since  $\bar{\sigma}(S) = \bar{\sigma}(S^H)$ 

$$\bar{\sigma}(S(z)) \ge 1$$

#### RHP Zeros cont'd

Then, by Maximum Modulus Thm

$$||W_S S||_{\infty} \geq \bar{\sigma}(W_S(z)S(z)) \geq |W_S(z)|$$

where we have assumed the weight  $W_S$  is scalar

– same restriction on  $\bar{\sigma}(S)$  as on |S| in SISO case (see lec notes 4)

### **Limitation 2: RHP Poles**

**Thm:** Assume G(s) has a RHP pole at s=p>0, then

$$||W_T T||_{\infty} \ge |W_T(p)|$$

**Proof:** as above for RHP zeros, but with  $S(p)y_p = 0 \implies T(p)y_p = y_p$ 

- same restriction on  $\bar{\sigma}(T)$  as on |T| in SISO case (see lec notes 4)

#### Requirements for Disturbance Attenuation

Consider a scalar disturbance d such that

$$w = g_d(s)d \Rightarrow z = S(s)g_d(s)d, \quad |d| < 1 \ \forall \omega$$

• Requirement  $|z| < 1 \ \forall \omega$  implies

$$\bar{\sigma}(Sg_d) < 1 \ \forall \omega \ \Rightarrow \ \|Sg_d\|_{\infty} < 1$$

Define the disturbance direction

$$y_d(i\omega) = \frac{g_d(i\omega)}{|g_d(i\omega)|}$$

Then, requirement is

$$\bar{\sigma}(Sy_d) < \frac{1}{|g_d|} \ \forall \omega$$

- note: requirement on S is only in direction  $y_d$ 

#### Requirements cont'd

 Consider high-gain and low-gain directions of sensitivity S (from SVD of S)

$$S\bar{v} = \bar{\sigma}(S)\bar{u} \; ; \quad S\underline{v} = \underline{\sigma}(S)\underline{u}$$

- If 
$$y_d = \bar{u} \Rightarrow \bar{\sigma}(S) < \frac{1}{|g_d|}$$
 ('worst' direction)

- if 
$$y_d = \underline{u} \Rightarrow \underline{\sigma}(S) < \frac{1}{|g_d|}$$
 ('best' direction)

#### Disturbances and RHP Zeros

Assume G(s) has a RHP zero at s=z, then

$$y_z^H S(z) = y_z^H \Rightarrow y_z^H S(z)g_d(z) = y_z^H g_d(z)$$

From Maximum Modulus Thm we get

$$||Sg_d||_{\infty} \ge |y_z^H g_d(z)|$$

Thus, we get requirement

$$|y_z^H g_d(z)| < 1$$

- otherwise no controller exists that will provide acceptable performance corresponding to keeping  $\vert z \vert < 1$  in the presence of disturbances  $\vert d \vert < 1$
- note that this depends on the system only

### Disturbances and RHP Zeros

- "Extreme" cases
  - If  $y_z \perp y_d \Rightarrow y_z^H g_d(z) = 0$  (RHP zero has no impact on disturbance attenuation)
  - if  $y_z \parallel y_d \Rightarrow y_z^H g_d(z) = |g_d(z)|$  ("worst-case" alignment)
- Example:

$$G(s) = \begin{pmatrix} \frac{2}{s+1} & \frac{1}{s+2} \\ \frac{2}{s+3} & \frac{2}{s+2} \end{pmatrix} \; ; \quad \det G(s) = \frac{1-s}{(s+1)(s+2)} \; \Rightarrow \; z = 1$$

$$\downarrow \downarrow$$

$$G(1) = \begin{pmatrix} 1 & 1/3 \\ 2 & 2/3 \end{pmatrix} \; \Rightarrow \; y_z^H = \frac{1}{\sqrt{5}} \begin{pmatrix} -2 & 1 \end{pmatrix}$$

## Example cont'd

1. Disturbance  $d_1$ 

$$g_{d1}(s) = \frac{2}{s+1} \begin{pmatrix} 1 \\ 1 \end{pmatrix} \Rightarrow |y_z^H g_{d1}(1)| = \frac{1}{\sqrt{5}} < 1$$

2. Disturbance  $d_2$ 

$$g_{d2}(s) = \frac{2}{s+1} \begin{pmatrix} -1\\1 \end{pmatrix} \Rightarrow |y_z^H g_{d2}(1)| = \frac{3}{\sqrt{5}} > 1$$

- Thus, can attenuate disturbance  $d_1$  but not  $d_2$  such that |z| < 1 when |d| < 1 (with any controller!)

## Summary

- Results on performance requirements and limitations carry more or less directly over from SISO to MIMO by considering the maximum singular values of the transfer-matrices we want to make small, e.g., S and T
- By using scalar weights  $W_S, W_T$  we impose same bound on sensitivity in all directions
- Disturbances have specific directions and therefore impose requirements on the sensitivity only in these directions
- To what extent a RHP zero imposes a limitation for disturbance attenuation depends on how the disturbance direction is aligned with the zero output direction
- Multivariable systems: directions matter!
- Next time: controller design