

# Computational Design of Crack-Resistant W-Nb-C Alloy for LPBF

Analysis Based on “Near crack free additive manufacturing of a  
novel W-Nb-C alloy”

# Overview

- 1 Question 1: Composition Re-optimization for Higher Nb
- 2 Question 2: Oxygen Segregation & Embrittlement
- 3 Question 3: Non-equilibrium Solidification Modeling
- 4 Summary & Conclusions

# Q1: Thermodynamic Strategy for Crack Resistance

## Primary Objective

Maintain “crack-healing” mechanism in W-15Nb-C alloy through controlled eutectic solidification

## Key Challenge

Ensure liquid phase availability during critical solidification stages to prevent hot tearing and enable crack backfilling

# Governing Thermodynamic Parameters (Part 1)

## 1. Solid Fraction at Eutectic Onset ( $F_{s,eutectic}$ )

- **Role:** Timing of crack-healing liquid availability
- **Target:**  $F_{s,eutectic} > 0.65$
- **Effect:** Liquid must appear AFTER stress development

## 2. Dendritic Coherency Point ( $F_{s,DCP}$ )

- **Role:** Stress initiation point
- **Critical Condition:**  
 $F_{s,eutectic} > F_{s,DCP}$
- **Effect:** Liquid reservoir remains after stress buildup

# Governing Thermodynamic Parameters (Part 2)

## 3. Eutectic Temperature Range ( $\Delta T_{\text{eutectic}}$ )

- **Role:** Duration of healing process
- **Target:** Wide temperature plateau
- **Effect:** Prolonged stress relaxation window

## 4. Terminal Solidification Slope ( $dT/df_s$ )

- **Role:** Final-stage healing effectiveness
- **Target:** Shallow slope near  $F_s = 1$
- **Effect:** Maximum time for liquid backfilling

# Optimization Strategy Summary

## Target Solidification Profile

- 1 **Rapid initial solidification** to form dendritic skeleton
- 2 **Late eutectic onset** ( $F_s \sim 0.7$ ) after coherency
- 3 **Wide, flat eutectic plateau** for prolonged healing
- 4 **Shallow terminal slope** for final crack sealing

## Success Criteria for W-15Nb-C

Scheil simulation must show eutectic reaction beginning after dendritic coherency and persisting with minimal temperature change until complete solidification

# Q2: Computational Workflow Overview

## Primary Objective

Quantify oxygen segregation tendency and embrittlement effect at critical interfaces using first-principles methods

## Target Interfaces

- 1 W-rich SS / NbC interphase boundary
- 2 W-rich SS grain boundaries

## Primary Method

Density Functional Theory (DFT)

- Software: VASP
- Pseudopotentials: PAW
- Functional: PBE

# Three-Step DFT Workflow

## Step 1: Interface Structure Modeling

- Construct atomic supercells of target interfaces
- Find most stable configurations via energy minimization
- Model both coherent and semi-coherent interfaces

## Step 2: Oxygen Segregation Energy

$$E_{seg} = E_{\text{interface}+\text{O}} - E_{\text{interface}} - \mu_{\text{O}}$$

- Negative value indicates favorable segregation
- Compare multiple interface sites
- Reference  $\mu_{\text{O}}$  to  $\text{O}_2$  molecule or bulk W



## Step 3: Work of Separation

$$\gamma_{sep} = \frac{E_{slab1} + E_{slab2} - E_{interface}}{2 \times Area}$$

- Quantifies interfacial cohesion strength
- Compare  $\gamma_{sep}^{clean}$  vs  $\gamma_{sep}^{with\ O}$
- Large reduction indicates severe embrittlement

# Validation & Databases

## Computational Resources

- **VASP** with PAW pseudopotentials
- **Materials Project** database
- **NIST** reference data for benchmarking

## Validation Methods

- **XPS:** Core-level binding energy shifts
- **STEM-EELS:** Direct interface chemistry
- **SEM Fractography:** Fracture path analysis

## Predicted Correlation

Strong oxygen segregation at W/NbC interface + reduced  $\gamma_{sep}$   $\rightarrow$  SEM shows interphase fracture along segregation channels

# Q3: Multi-scale Modeling Approach

## LPBF Challenge

Extreme cooling rates ( $10^5$ - $10^7$  K/s) cause:

- Severe microsegregation
- Solute trapping
- Metastable phase formation
- Retained supersaturation

## Standard CALPHAD Limitation

Equilibrium assumptions invalid under LPBF conditions - requires kinetic coupling

# Hierarchical Computational Framework

## 1. DICTRA Simulations

### Inputs:

- CALPHAD thermodynamic database
- Mobility database
- Initial composition
- Cooling rate ( $10^6$  K/s)

### Outputs:

- Phase fractions vs. time
- Composition profiles
- Solute trapping extent

## 2. Phase-Field Modeling

### Coupled with CALPHAD:

- Dendritic morphology
- Eutectic structure
- Metastable phases

**Output:** Microstructure evolution

## 3. Advanced Scheil Model

- Clyne-Kurz back-diffusion
- Quick microsegregation estimate
- Screening tool

# Heat-Treatment Design Guidance

## Homogenization Treatment

### Using DICTRA:

- Input: Microsegregation profiles from LPBF simulation
- Simulate annealing (1200-1400°C)
- Optimize time to achieve homogeneity
- Prevent excessive grain growth

## Precipitation Hardening

### Using CALPHAD:

- Calculate TTT/CCT diagrams
- Identify solvus temperatures
- Design aging treatments
- Control carbide precipitation

## Integrated Workflow

LPBF Process → Non-equilibrium Simulation →  
Optimized Heat Treatment → Enhanced  
Properties

## Multi-scale Approach Success

- **CALPHAD:** Thermodynamic-guided alloy design
- **DFT:** Fundamental interface properties
- **DICTRA/Phase-Field:** Process simulation
- **Complementary methods** for comprehensive understanding

## Impact on Additive Manufacturing

This framework enables **rational design** of crack-resistant refractory alloys, significantly reducing trial-and-error experimentation and accelerating development of high-performance materials for extreme environments.

# Thank You