# Computational Design of Crack-Resistant W-Nb-C Alloy for LPBF

Analysis Based on "Near crack free additive manufacturing of a novel W-Nb-C alloy"

#### Overview

- 1 Question 1: Composition Re-optimization for Higher Nb
- Question 2: Oxygen Segregation & Embrittlement
- Question 3: Non-equilibrium Solidification Modeling
- 4 Summary & Conclusions

## Q1: Thermodynamic Strategy for Crack Resistance

#### Primary Objective

Maintain "crack-healing" mechanism in W-15Nb-C alloy through controlled eutectic solidification

#### Key Challenge

Ensure liquid phase availability during critical solidification stages to prevent hot tearing and enable crack backfilling

## Governing Thermodynamic Parameters (Part 1)

#### Solid Fraction at Eutectic Onset (F<sub>s,eutectic</sub>)

- Role: Timing of crack-healing liquid availability
- Target:  $F_{s,eutectic} > 0.65$
- Effect: Liquid must appear AFTER stress development

## 2. Dendritic Coherency Point $(F_{s,DCP})$

- Role: Stress initiation point
- Critical Condition:  $F_{s,eutectic} > F_{s,DCP}$
- Effect: Liquid reservoir remains after stress buildup

## Governing Thermodynamic Parameters (Part 2)

## 3. Eutectic Temperature Range ( $\Delta T_{eutectic}$ )

- Role: Duration of healing process
- Target: Wide temperature plateau
- **Effect:** Prolonged stress relaxation window

## 4. Terminal Solidification Slope $(dT/df_s)$

- Role: Final-stage healing effectiveness
- Target: Shallow slope near  $F_s = 1$
- Effect: Maximum time for liquid backfilling

## Optimization Strategy Summary

#### Target Solidification Profile

- Rapid initial solidification to form dendritic skeleton
- ② Late eutectic onset  $(F_s \sim 0.7)$  after coherency
- Wide, flat eutectic plateau for prolonged healing
- Shallow terminal slope for final crack sealing

#### Success Criteria for W-15Nb-C

Scheil simulation must show eutectic reaction beginning after dendritic coherency and persisting with minimal temperature change until complete solidification

## Q2: Computational Workflow Overview

#### Primary Objective

Quantify oxygen segregation tendency and embrittlement effect at critical interfaces using first-principles methods

#### Target Interfaces

- W-rich SS / NbC interphase boundary
- W-rich SS grain boundaries

#### Primary Method

Density Functional Theory (DFT)

- Software: VASP
- Pseudopotentials: PAW
- Functional: PBE

### Three-Step DFT Workflow

#### Step 1: Interface Structure Modeling

- Construct atomic supercells of target interfaces
- Find most stable configurations via energy minimization
- Model both coherent and semi-coherent interfaces

#### Step 2: Oxygen Segregation Energy

$$E_{seg} = E_{interface+O} - E_{interface} - \mu_O$$

- Negative value indicates favorable segregation
- Compare multiple interface sites
- Reference  $\mu_O$  to  $O_2$  molecule or bulk W



#### Step 3: Work of Separation

$$\gamma_{\textit{sep}} = \frac{\textit{E}_{\textit{slab1}} + \textit{E}_{\textit{slab2}} - \textit{E}_{\textit{interface}}}{2 \times \textit{Area}}$$

- Quantifies interfacial cohesion strength
- Compare  $\gamma_{sep}^{clean}$  vs  $\gamma_{sep}^{with O}$
- Large reduction indicates severe embrittlement

#### Validation & Databases

#### Computational Resources

- VASP with PAW pseudopotentials
- Materials Project database
- NIST reference data for benchmarking

#### Validation Methods

- **XPS**: Core-level binding energy shifts
- **STEM-EELS:** Direct interface chemistry
- **SEM Fractography:** Fracture path analysis

#### Predicted Correlation

Strong oxygen segregation at W/NbC interface + reduced  $\gamma_{\it sep} \to {\rm SEM}$  shows interphase fracture along segregation channels

## Q3: Multi-scale Modeling Approach

#### LPBF Challenge

Extreme cooling rates ( $10^5$ - $10^7$  K/s) cause:

- Severe microsegregation
- Solute trapping
- Metastable phase formation
- Retained supersaturation

#### Standard CALPHAD Limitation

Equilibrium assumptions invalid under LPBF conditions - requires kinetic coupling

### Hierarchical Computational Framework

#### 1. DICTRA Simulations

#### Inputs:

- CALPHAD thermodynamic database
- Mobility database
- Initial composition
- Cooling rate  $(10^6 \text{ K/s})$

#### **Outputs:**

- Phase fractions vs. time
- Composition profiles
- Solute trapping extent

#### 2. Phase-Field Modeling

#### Coupled with CALPHAD:

- Dendritic morphology
- Eutectic structure
- Metastable phases

**Output:** Microstructure evolution

#### 3. Advanced Scheil Model

- Clyne-Kurz back-diffusion
- Quick microsegregation estimate
- Screening tool

## Heat-Treatment Design Guidance

#### Homogenization Treatment

#### **Using DICTRA:**

- Input: Microsegregation profiles from LPBF simulation
- Simulate annealing (1200-1400°C)
- Optimize time to achieve homogeneity
- Prevent excessive grain growth

#### Precipitation Hardening

#### **Using CALPHAD:**

- Calculate TTT/CCT diagrams
- Identify solvus temperatures
- Design aging treatments
- Control carbide precipitation

#### Integrated Workflow

 $\begin{array}{c} \mathsf{LPBF\ Process} \to \mathsf{Non\text{-}equilibrium\ Simulation} \to \\ \mathsf{Optimized\ Heat\ Treatment} \to \mathsf{Enhanced} \\ \mathsf{Properties} \end{array}$ 

## Integrated Computational Materials Engineering

#### Multi-scale Approach Success

- CALPHAD: Thermodynamic-guided alloy design
- **DFT:** Fundamental interface properties
- DICTRA/Phase-Field: Process simulation
- Complementary methods for comprehensive understanding

#### Impact on Additive Manufacturing

This framework enables **rational design** of crack-resistant refractory alloys, significantly reducing trial-and-error experimentation and accelerating development of high-performance materials for extreme environments.

## Thank You

Questions