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# GATE 2019

## Electronics Engineering

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Questions and Solutions

**Date of Exam : 9/2/2019**

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## **SECTION A : GENERAL APTITUDE**



Ans. (d)

When he did not come home, she pictured him lying dead on the roadside somewhere. "pictured" is the most appropriate option in this situation as she is imagining or creating an image of somebody/something in her mind.

- • • • End of Solution



Ans. (b)

"Company" is singular, hence, "uses" would be the correct option in blank 1. "products" is plural, hence, "include" would be the correct option in blank 2.

- • • • End of Solution



Ans. (d)

Machine X = 4 hours

Machine Y = 2 hours

In 1 hour  $X$  can work =  $\frac{1}{4}$

In 1 hour  $Y$  can work =  $\frac{1}{2}$

$$\text{In 1 hour } (X + Y) \text{ can work} = \frac{1}{4} + \frac{1}{2} = \frac{3}{4}$$

$$(X + Y) \text{ together} = \frac{4}{3} \text{ hours}$$

- • • • End of Solution



# ESE 2019

## Mains Classroom Program

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at **Delhi Centre**.

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Batch Details	Course Duration	Class Duration	Test Series
	90 days   300 - 350 hours	5-6 days a week and 6-7 hours a day	Every Sunday

Streams	Batch Code	Batch Commencing Date	Venue (Delhi)	Timing
ME	A	20-Feb-2019	Ghitorni Centre	7:30 AM to 1:30 PM
ME	B	20-Feb-2019	Ghitorni Centre	3:00 PM to 9:00 PM
ME	C	20-Feb-2019	Saket Centre	7:30 AM to 1:30 PM
CE	A	21-Feb-2019	Ignou Road Centre	7:30 AM to 1:30 PM
CE	B	21-Feb-2019	Kalu Sarai Centre	3:00 PM to 9:00 PM
EE	A	22-Feb-2019	Lado Sarai Centre	7:30 AM to 1:30 PM
EE	B	22-Feb-2019	Kalu Sarai Centre	3:00 PM to 9:00 PM
EC	A	22-Feb-2019	Lado Sarai Centre	7:30 AM to 1:30 PM

Fee Structure	Program (Inclusive of ESE-2019 Mains Offline Test Series)	Ex. MADE EASY Students Enrolled in Postal, Rank Improvement, Mains, GS, Post-GATE, ESE+ GATE, GATE Batches	Non MADE EASY students
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facility  
will be  
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**Ans. (b)**

Option 1 i.e. "on" is used when one is talking about a day of the week e.g. on Thursday, or a particular part of a date e.g. on Sunday evening, or a particular date e.g. on 9th March.

Option 3 i.e. "in" is used when one is talking about a month e.g. in June, or a season e.g. in winter, or a specific year e.g. in 2019.

Option 4 i.e. "under" is absurd in this situation.

Option 2 i.e. "at" is used when one is referring to a particular time e.g. at dawn, or a calendar festival season e.g. at Christmas.

● ● ● End of Solution

**Q.5** Five different books (P, Q, R, S, T) are to be arranged on a shelf. The books R and S are to be arranged first and second, respectively from the right side of the shelf. The number of different orders in which P, Q and T may be arranged is \_\_\_\_.

- |         |       |
|---------|-------|
| (a) 12  | (b) 2 |
| (c) 120 | (d) 6 |

**Ans. (d)**

Here R and S are fixed in 1<sup>st</sup> and 2<sup>nd</sup> places from right.

P Q T [S] [R]

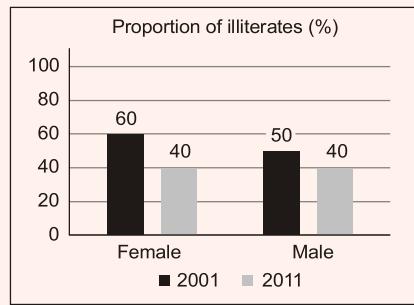
Therefore arrangement of

$$P, Q, T = {}^3P_3 = 3! = 6$$

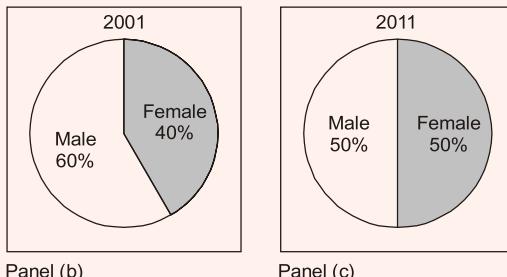
● ● ● End of Solution

**Q.6** The bar graph in Panel (a) shows the proportion of male and female illiterates in 2001 and 2011. The proportions of males and females in 2001 and 2011 are given in Panel (b) and (c), respectively. The total population did not change during this period.

The percentage increase in the total number of literates from 2001 to 2011 is \_\_\_\_.



Panel (a)



Panel (b)

Panel (c)

Ans. (c)

Let total population

in 2001 = 100

in 2011 = 100

In 2001, males = 60, females = 40  
illiterates,

$$50\% \text{ of } 60 = 30$$

$$50\% \text{ of } 60 = \underline{24}$$

54

$$\text{literate} = 100 - 54 = 46$$

In 2011, males = 50, females = 50  
illiterates,

$$40\% \text{ of } 50 = 20$$

$$40\% \text{ of } 50 = \underline{20}$$

40

$$\text{literates} = 100 - 40 = 60$$

$$\text{Percentage of increase literates from 2001 to 2011} = \frac{60 - 46}{46} \times 100 = 30.43\%.$$

- • • • End of Solution

**Q.7** Two design consultants, P and Q, started working from 8 AM For a client. The client budgeted a total of USD 3000 for the consultants. P stopped working when the hour hand moved by 210 degrees on the clock. Q stopped working when the hour hand moved by 240 degrees. P took two tea breaks of 15 minutes each during her shift, but took no lunch break. Q took only one lunch break for 20 minutes, but no tea breaks. The market rate for consultants is USD 200 per hour and breaks are not paid. After paying the consultants, the client shall have USD \_\_\_\_\_ remaining in the budget.



Ans. (d)

*P* and *Q* started 8 am

1 hour = 30

$$P = \frac{210}{30} = 7 \text{ hours}$$

$$Q = \frac{240}{30} = 8 \text{ hours}$$

After break time:  $P = 7:30 \text{ min} = 6 \text{ hours } 30 \text{ min}$

After break time:  $Q = 8:20 \text{ min} = 7 \text{ hours}40 \text{ min}$

$$\text{Total time} = 6 \text{ hours } 30 \text{ min} + 7 \text{ hour } 40 \text{ min} \\ = 14 \text{ hours } 10 \text{ min}$$



$$= 14 \text{ hour} + \frac{10}{16} \text{ hour}$$

$$= 14 \text{ hour} + \frac{1}{6} \text{ hour} = \frac{85}{6} \text{ hours}$$

In every 1 hour USD 200

$$\therefore \frac{85}{6} \text{ hours} = \frac{85}{6} \times 200 = 2833.33$$

$$\text{Remaining} = 3000 - 2833.33 = 166.666666 = 166.67$$

• • • **End of Solution**

- Q.8** Five people P, Q, R, S and T work in a bank. P and Q don't like each other but have to share an office till T gets a promotion and moves to the big office next to the garden. R, who is currently sharing an office with T wants to move to the adjacent office with S, the handsome new intern. Given the floor plan, what is the current location of Q, R and T?

(O = Office, WR = Washroom)

- (a) 

WR	O 1 P	O 2 Q	O 3 R	O 4 S
Manager		Teller 1	Teller 2	
Entry				
Garden				
- (b) 

WR	O 1 P, Q	O 2	O 3 T	O 4 R, S
Manager		Teller 1	Teller 2	
Entry				
Garden				
- (c) 

WR	O 1 P, Q	O 2	O 3 R, T	O 4 S
Manager		Teller 1	Teller 2	
Entry				
Garden				
- (d) 

WR	O 1 P, Q	O 2	O 3 R	O 4 S
Manager T		Teller 1	Teller 2	
Entry				
Garden				

**Ans. (c)**

Only option (c) shows P and Q in same office, R and T in same office with S being in the adjacent office. Thus, option (c) is correct.

● ● ● **End of Solution**

**Q.9** Four people are standing in a line facing you. They are Rahul, Mathew, Seema and Lohit. One is an engineer, one is a doctor, one a teacher and another a dancer. You are told that:

1. Mathew is not standing next to Seema.
2. There are two people standing between Lohit and the engineer.
3. Rahul is not a doctor.
4. The teacher and the dancer are standing next to each other.
5. Seema is turning to her right to speak to the doctor standing next to her.

Who among them is an engineer?

- |           |            |
|-----------|------------|
| (a) Lohit | (b) Rahul  |
| (c) Seema | (d) Mathew |

**Ans. (d)**

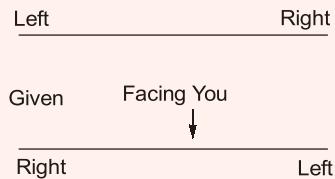
According to given conditions sequence is

Lohit, Seema, Rahul, Mathew,

↓                          ↓

Doctor                    Engineer

∴                         Engineer = Mathew



● ● ● **End of Solution**

**Q.10** "Indian history was written by British historians-extremely well documented and researched, but not always impartial. History had to serve its purpose: Everything was made subservient to the glory of the Union Jack. Latter-day Indian scholars presented a contrary picture."

From the text above, we can infer that:

Indian history written by British historians \_\_\_\_\_.

- (a) was well documented and researched but was sometimes biased
- (b) was well documented and not researched but was always biased
- (c) was not well documented and researched and was sometimes biased
- (d) was not well documented and researched and was always biased

**Ans. (a)**

The passage says "extremely well documented and researched, but not always impartial". This suggests that Indian history written by British historians was well documented and researched but was sometimes biased. hence option (a) is the correct answer.

● ● ● **End of Solution**

**SECTION B : TECHNICAL**

**Q.1** The families of curves represented by the solution of the equation

$$\frac{dy}{dx} = -\left(\frac{x}{y}\right)^n$$

for  $n = -1$  and  $n = +1$ , respectively, are

- |                              |                            |
|------------------------------|----------------------------|
| (a) Hyperbolas and Parabolas | (b) Hyperbolas and Circles |
| (c) Parabolas and Circles    | (d) Circles and Hyperbolas |

**Ans. (b)**

$$\frac{dy}{dx} = -\left(\frac{x}{y}\right)^n$$

$$n = -1,$$

$$\frac{dy}{dx} = -\frac{y}{x}$$

$$\frac{dy}{y} = -\frac{dx}{x}$$

$$\int \frac{1}{y} dy = - \int \frac{1}{x} dx$$

$$\ln y = -\ln x + \ln c$$

$$\ln(yx) = \ln c$$

$xy = c$  Represents rectangular hyperbola

$$n = 1,$$

$$\frac{dy}{dx} = -\frac{x}{y}$$

$$ydy = -xdx$$

$$\int ydy = - \int xdx$$

$$\frac{y^2}{2} = -\frac{x^2}{2} + c$$

$x^2 + y^2 = 2c$  Represents family of circles

● ● ● **End of Solution**

**Q.2** In the table shown, List-I and List-II, respectively, contain terms appearing on the left-hand side and the right-hand side of Maxwell's equations (in their standard form). Match the left-hand side with the corresponding right-hand side.

**List-I**

1.  $\nabla \cdot \vec{D}$

2.  $\nabla \times \vec{E}$

3.  $\nabla \cdot \vec{B}$

4.  $\nabla \times \vec{H}$

**List-II**

P. 0

Q.  $\rho$

R.  $-\frac{\partial \vec{B}}{\partial t}$

S.  $\bar{J} + \frac{\partial \vec{D}}{\partial t}$

- (a) 1-R, 2-Q, 3-S, 4-P
- (b) 1-Q, 2-S, 3-P, 4-R
- (c) 1-P, 2-R, 3-Q, 4-S
- (d) 1-Q, 2-R, 3-P, 4-S

Ans. (d)

$$\nabla \cdot \vec{D} = \rho_v$$

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$\nabla \cdot \vec{B} = 0$$

$$\nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t}$$

● ● ● End of Solution

**Q.3** Radiation resistance of a small dipole current element of length  $l$  at a frequency of 3 GHz is 3 ohms. If the length is changed by 1%, then the percentage change in the radiation resistance, rounded off to two decimal places, is \_\_\_\_\_ %.

Ans. (2.01)

Radiation resistance of a small dipole current element of length ' $l$ ' is

$$R_{\text{rad}} = 80\pi^2 \left(\frac{l}{\lambda}\right)^2 \Rightarrow R \propto l^2$$

$$\frac{R_2}{R_1} = \left(\frac{l_2}{l_1}\right)^2$$

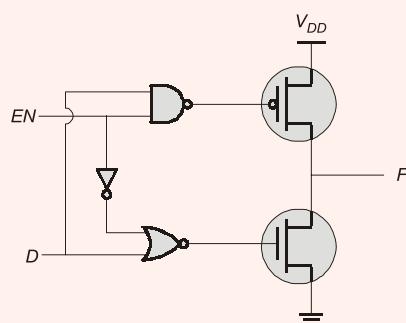
If length is changed by 1% then percentage change in the radiation resistance.

$$\frac{R_2}{R_1} = \left(\frac{1.01l}{l}\right)^2 = 1.0201$$

$$\text{Percentage change in radiation resistance} = \frac{R_2 - R_1}{R_1} \times 100 = 0.0201 \times 100 = 2.01\%$$

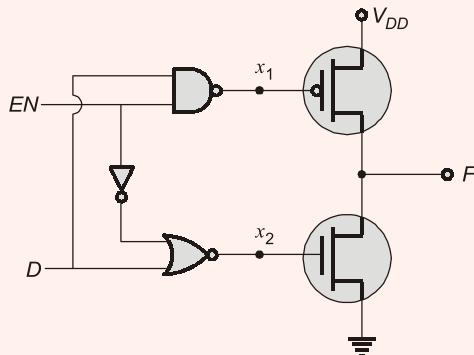
● ● ● End of Solution

**Q.4** In the circuit shown, what are the values of  $F$  for  $EN = 0$  and  $EN = 1$ , respectively?



- (a) 0 and 1
- (b) Hi-Z and  $D$
- (c) Hi-Z and  $\bar{D}$
- (d) 0 and  $D$

Ans. (b)



When  $EN = 0$ :  $x_1 = (\overline{D} \cdot \overline{0}) = 1 \Rightarrow$  PMOS is in OFF state

$$x_2 = (\overline{1} + \overline{D}) = 0 \Rightarrow$$
 NMOS is in OFF state

Both the transistors are in OFF state, which offers high impedance.

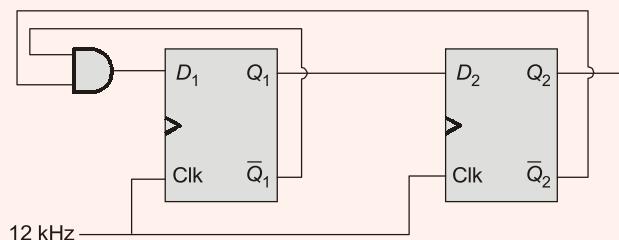
When  $EN = 1$ :  $x_1 = (\overline{D} \cdot \overline{1}) = \overline{D}$

$$x_2 = (\overline{0} + \overline{D}) = \overline{D}$$

$$F = D$$

● ● ● End of Solution

- Q.5** In the circuit shown, the clock frequency, i.e., the frequency of the Clk signal, is 12 kHz. The frequency of the signal at  $Q_2$  is \_\_\_\_\_ kHz.



Ans. (4)

$$D_1 = \overline{Q}_2 \overline{Q}_1 = \overline{Q}_2 + \overline{Q}_1$$

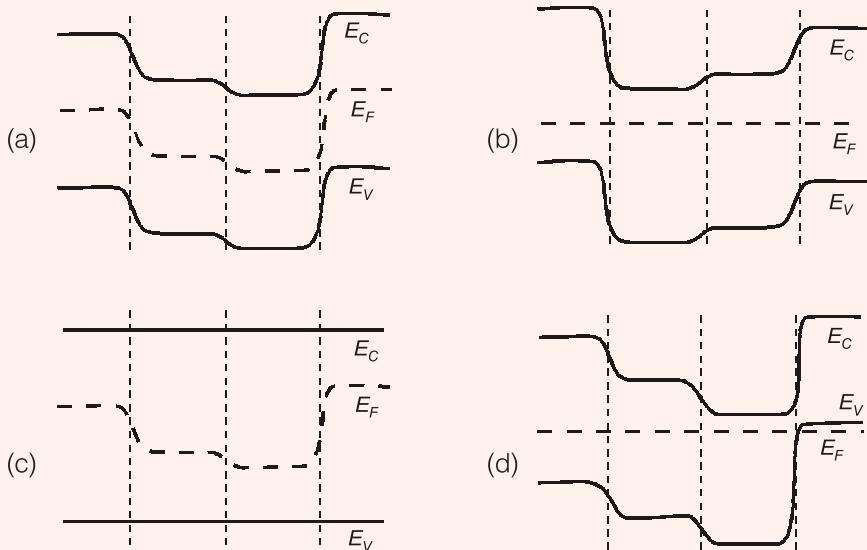
PS	D <sub>2</sub>	D <sub>1</sub>	NS
$Q_2 \quad Q_1$	X	X	$Q_2^+ \quad Q_1^+$
0 0	0	1	0 1
0 1	1	0	1 0
1 0	0	0	0 0

MOD = 3

$$f_{Q2} = \frac{f_{\text{clk}}}{3} = \frac{12}{3} \text{ kHz} = 4 \text{ kHz}$$

● ● ● End of Solution

- Q.6** Which one of the following options describes correctly the equilibrium band diagram at  $T = 300 \text{ K}$  of a Silicon  $pnn^+p^{++}$  configuration shown in the figure?



**Ans.** (d)

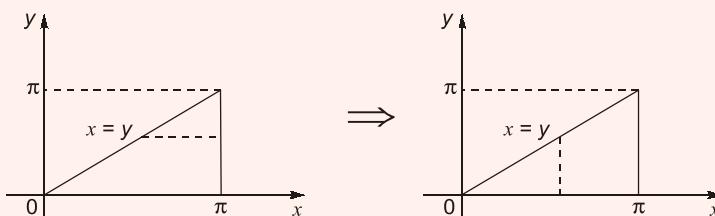


**End of Solution**

- Q.7** The value of integral  $\int_0^\pi \int_y^\pi \frac{\sin x}{x} dx dy$ , is equal to \_\_\_\_\_.

**Ans.** (2)

$$\begin{aligned} x &= y ; \quad x = \pi \\ y &= 0 ; \quad y = \pi \end{aligned}$$



∴

$$\begin{aligned} &= \int_0^\pi \int_y^\pi \frac{\sin x}{x} dx dy = \int_0^\pi \frac{\sin x}{x} (y)|_0^x dx \\ &= \int_0^\pi \frac{\sin x}{x} (x) dx = \int_0^\pi \sin x dx = (-\cos x)|_0^\pi \\ &= -\cos \pi + \cos 0 = 1 + 1 = 2 \end{aligned}$$



**End of Solution**



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**Q.8** If  $X$  and  $Y$  are random variables such that  $E[2X + Y] = 0$  and  $E[X + 2Y] = 33$ , then  $E[X] + E[Y] = \underline{\hspace{2cm}}$ .

**Ans.** (11)

$$\begin{aligned}E[2X + Y] &= 0 \text{ and } E[X + 2Y] = 33 \\ \text{then, } 2E[X] + E[Y] &= 0 \text{ and } E[X] + 2E[Y] = 33 \\ 3E[X] + 3E[Y] &= 0 + 33 = 33 \\ E[X] + E[Y] &= 11\end{aligned}$$

● ● ● **End of Solution**

**Q.9** A linear Hamming code is used to map 4-bit messages to 7-bit codewords. The encoder mapping is linear. If the message 0001 is mapped to the codeword 0000111, and the message 0011 is mapped to the codeword 1100110, then the message 0010 is mapped to

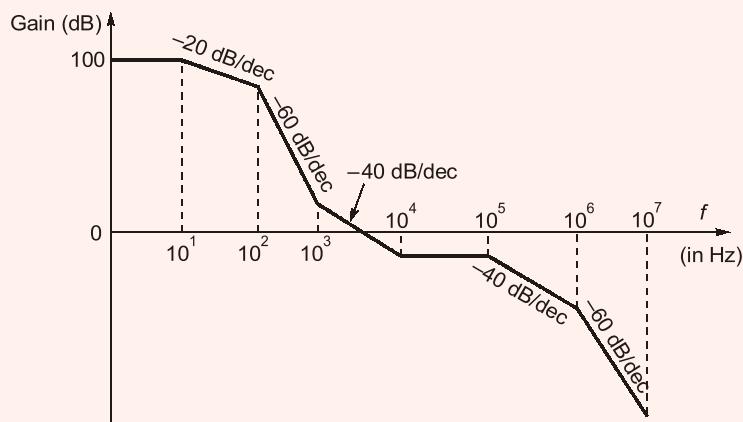
- |             |             |
|-------------|-------------|
| (a) 0010011 | (b) 1100001 |
| (c) 1111000 | (d) 1111111 |

**Ans.** (b)

$$\begin{array}{rcl} 0001 & \xrightarrow{\oplus} & 0000111 \\ + \\ 0011 & \xrightarrow{\oplus} & 1100110 \\ \hline 0010 & \xrightarrow{\oplus} & 1100001 \end{array}$$

● ● ● **End of Solution**

**Q.10** For an LTI system, the Bode plot for its gain is as illustrated in the figure shown. The number of system poles  $N_p$  and the number of system zeros  $N_z$  in the frequency range  $1 \text{ Hz} \leq f \leq 10^7 \text{ Hz}$  is



- |                        |                        |
|------------------------|------------------------|
| (a) $N_p = 6, N_z = 3$ | (b) $N_p = 7, N_z = 4$ |
| (c) $N_p = 5, N_z = 2$ | (d) $N_p = 4, N_z = 2$ |

Ans. (a)

Corner frequency (in Hz)	No. of poles (or) zeros
10	1 pole
$10^2$	2 poles
$10^3$	1 zero
$10^4$	2 zeros
$10^5$	2 poles
$10^6$	1 pole

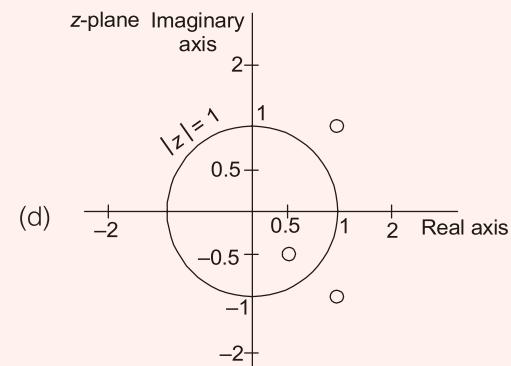
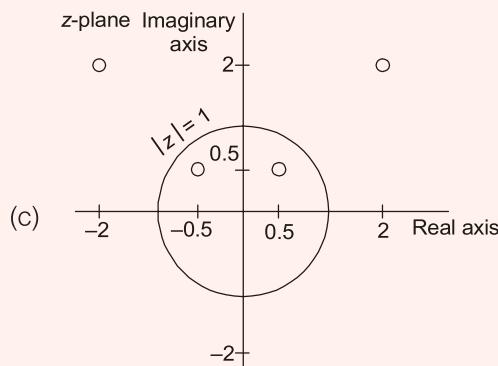
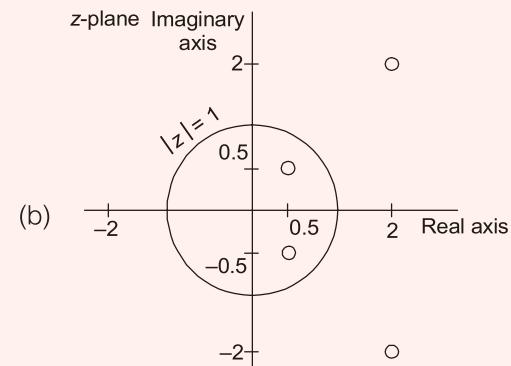
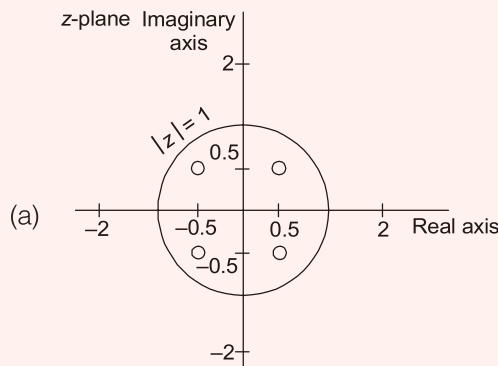
$$\text{Number of poles } (N_p) = 6$$

$$\text{Number of zeros } (N_z) = 3$$

• • • End of Solution

**Q.11** Let  $H(z)$  be the  $z$ -transform of a real-valued discrete-time signal  $h[n]$ . If  $P(z) = H(z)H\left(\frac{1}{z}\right)$

has a zero at  $z = \frac{1}{2} + \frac{1}{2}j$ , and  $P(z)$  has a total of four zeros, which one of the following plots represents all the zeros correctly?



Ans. (d)

$$P(z) = H(z)H\left(\frac{1}{z}\right)$$

- (i)  $h(n)$  is real. So,  $p(n)$  will be also real
- (ii)  $P(z) = P(z^{-1})$

**From (i):** If  $z_1$  is a zero of  $P(z)$ , then  $z_1^*$  will be also a zero of  $P(z)$ .

**From (ii):** If  $z_1$  is a zero of  $P(z)$ , then  $\frac{1}{z_1}$  will be also a zero of  $P(z)$ .

So, the 4 zeros are,

$$z_1 = \frac{1}{2} + \frac{1}{2}j$$

$$z_2 = z_1^* = \frac{1}{2} - \frac{1}{2}j$$

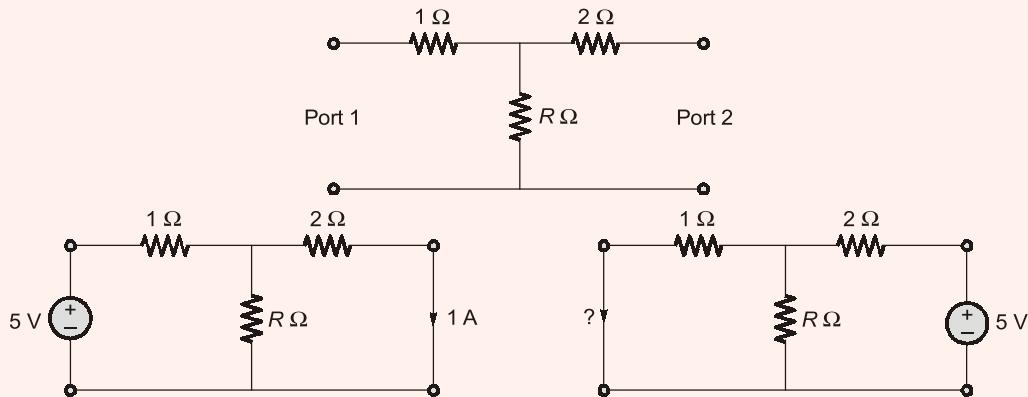
$$z_3 = \frac{1}{z_1} = \frac{1}{\frac{1}{2} + \frac{1}{2}j} = 1 - j$$

$$z_4 = \left(\frac{1}{z_1}\right)^* = z_3^* = 1 + j$$

So, option (d) is correct.

● ● ● End of Solution

- Q.12** Consider the two-port resistive network shown in the figure. When an excitation of 5 V is applied across Port 1, and Port 2 is shorted, the current through the short circuit at Port 2 is measured to be 1 A (see (a) in the figure). Now, if an excitation of 5 V is applied across Port 2, and Port 1 is shorted (see (b) in the figure), what is the current through the short circuit at Port 1?



- (a) 0.5 A  
 (c) 1 A

- (b) 2.5 A  
 (d) 2 A

Ans. (c)

According to reciprocity theorem,

In a linear bilateral single source network the ratio of response to excitation remains the same even after their positions get interchanged.

$$\therefore \frac{I}{5} = \frac{1}{5} \Rightarrow I = 1 \text{ A}$$

● ● ● End of Solution

**Q.13** Consider the signal  $f(t) = 1 + 2\cos(\pi t) + 3\sin\left(\frac{2\pi}{3}t\right) + 4\cos\left(\frac{\pi}{2}t + \frac{\pi}{4}\right)$ , where  $t$  is in seconds. Its fundamental time period, in seconds, is \_\_\_\_\_.

Ans. (12)

$$f(t) = 1 + 2\cos(\pi t) + 3\sin\left(\frac{2\pi}{3}t\right) + 4\cos\left(\frac{\pi}{2}t + \frac{\pi}{4}\right)$$

$$\omega_1 = \pi$$

$$\omega_2 = \frac{2\pi}{3}$$

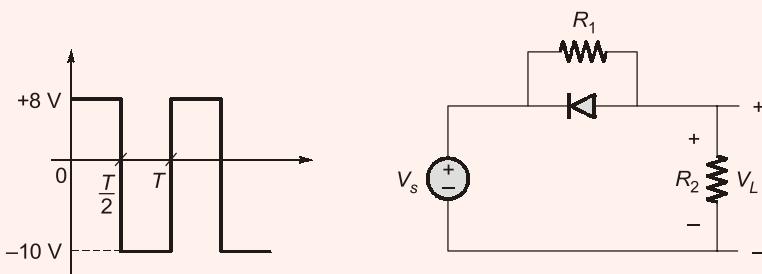
$$\omega_3 = \frac{\pi}{2}$$

$$\omega_0 = \text{GCD}\left(\pi, \frac{2\pi}{3}, \frac{\pi}{2}\right) = \frac{\pi}{6}$$

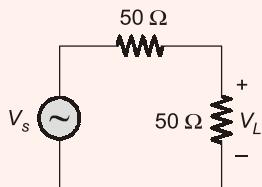
$$\text{Fundamental period, } N = \frac{2\pi}{\omega_0} = \frac{2\pi}{(\pi/6)} = 12$$

● ● ● End of Solution

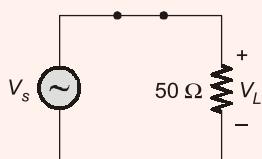
**Q.14** In the circuit shown,  $V_s$  is a square wave of period  $T$  with maximum and minimum values of 8 V and -10 V, respectively. Assume that the diode is ideal and  $R_1 = R_2 = 50 \Omega$ . The average value of  $V_L$  is \_\_\_\_\_ volts (rounded off to 1 decimal place).



Ans. (-3)

 When  $V_s = 8 \text{ V} \Rightarrow$  diode is in reverse bias


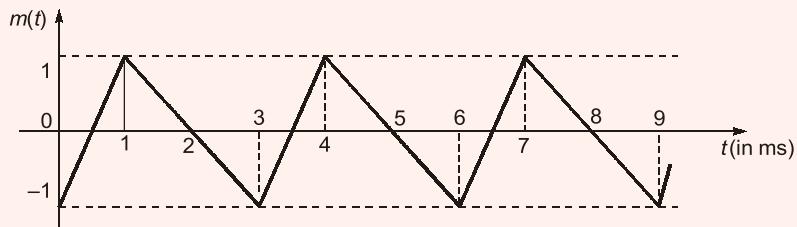
$$V_L = \frac{8 \times 50}{50 + 50} = 4 \text{ V}$$

 If  $V_s = -10 \text{ V}$ , diode is in forward bias


$$\text{Average value of } V_L = \frac{\text{Area}}{\text{Time period}} = \frac{4 \times 0.5T + (-10) \times 0.5T}{T} = -3 \text{ V}$$

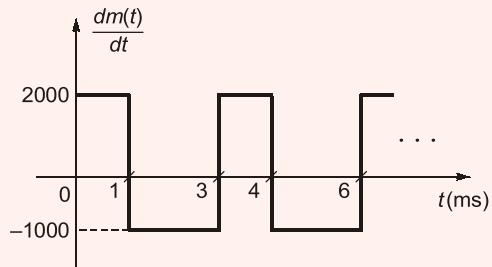
● ● ● End of Solution

- Q.15** The baseband signal  $m(t)$  shown in the figure is phase-modulated to generate the PM signal  $\phi(t) = \cos(2\pi f_c t + km(t))$ . The time  $t$  on the  $x$ -axis in the figure is in milliseconds. If the carrier frequency is  $f_c = 50 \text{ kHz}$  and  $k = 10\pi$ , then the ratio of the minimum instantaneous frequency (in kHz) to the maximum instantaneous frequency (in kHz) is \_\_\_\_\_ (rounded off to 2 decimal places).



Ans. (0.75)

$$f_i = \frac{1}{2\pi} \frac{d\theta(t)}{dt} = f_c + \frac{k}{2\pi} \frac{dm(t)}{dt} = f_c + 5 \frac{dm(t)}{dt}$$



So,

$$f_i(\text{min}) = 50 \text{ kHz} - (5 \times 1000 \text{ Hz}) = 45 \text{ kHz}$$

$$f_i(\text{max}) = 50 \text{ kHz} + (5 \times 2000 \text{ Hz}) = 60 \text{ kHz}$$

$$\frac{f_i(\text{min})}{f_i(\text{max})} = \frac{45}{60} = 0.75$$

 • • • **End of Solution**

**Q.16** The number of distinct eigen values of the matrix

$$A = \begin{bmatrix} 2 & 2 & 3 & 3 \\ 0 & 1 & 1 & 1 \\ 0 & 0 & 3 & 3 \\ 0 & 0 & 0 & 2 \end{bmatrix}$$

is equal to \_\_\_\_\_.

**Ans. (3)**

$$A = \begin{bmatrix} 2 & 2 & 3 & 3 \\ 0 & 1 & 1 & 1 \\ 0 & 0 & 3 & 3 \\ 0 & 0 & 0 & 2 \end{bmatrix}$$

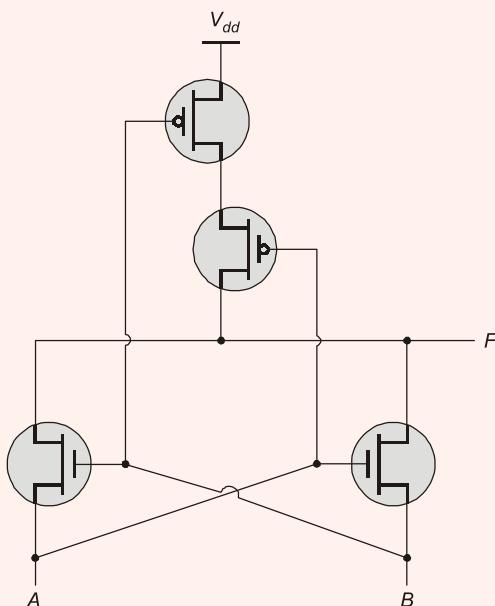
Eigen values are 2, 1, 3, 2

Distinct eigen values are 2, 1, 3

∴ Number of distinct eigen values = 3

 • • • **End of Solution**

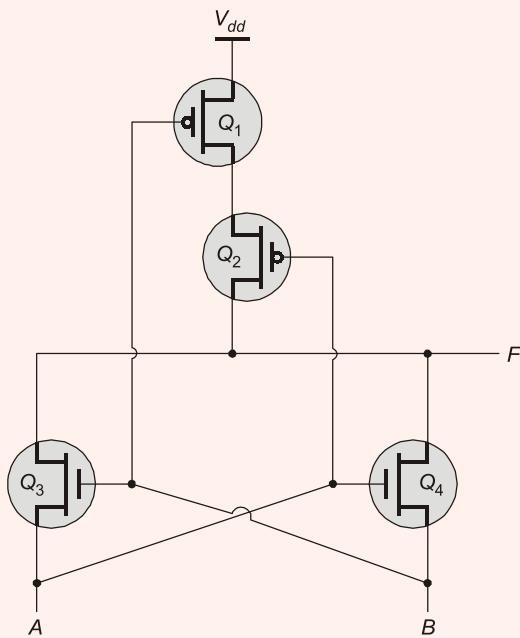
**Q.17** In the circuit shown, A and B are the inputs and F is the output. What is the functionality of the circuit?



- (a) XNOR  
 (c) XOR

- (b) SRAM Cell  
 (d) Latch

Ans. (a)



A	B	Q <sub>1</sub>	Q <sub>2</sub>	Q <sub>3</sub>	Q <sub>4</sub>	F
0	0	ON	ON	OFF	OFF	1
0	1	OFF	ON	ON	OFF	0
1	0	ON	OFF	OFF	ON	0
1	1	OFF	OFF	ON	ON	1

So, the given logic circuit acts as an XNOR gate.

● ● ● End of Solution

**Q.18** Let  $Y(s)$  be the unit-step response of a causal system, having a transfer function

$$G(s) = \frac{3-s}{(s+1)(s+3)}$$

that is,  $Y(s) = \frac{G(s)}{s}$ . The forced response of the system is

- |  |   |
|--|---|
| (a) $u(t)$                             | (b) $2u(t)$                             |
| (c) $u(t) - 2e^{-t}u(t) + e^{-3t}u(t)$ | (d) $2u(t) - 2e^{-t}u(t) + e^{-3t}u(t)$ |

Ans. (c)

Given,

$$G(s) = \frac{3-s}{(s+1)(s+3)}$$

∴

$$Y(s) = \frac{G(s)}{s} = \frac{3-s}{s(s+1)(s+3)}$$

Using partial fractions, we get,

$$Y(s) = \frac{A}{s} + \frac{B}{(s+1)} + \frac{C}{(s+3)}$$

$$A(s^2 + 4s + 3) + B(s^2 + 3s) + C(s^2 + s) = 3 - s$$

$$A + B + C = 0$$

$$4A + 3B + C = -1$$

and

$$3A = 3$$

Therefore, we get,

$$A = 1, B = -2 \text{ and } C = 1$$

So,

$$Y(s) = \frac{1}{s} - \frac{2}{(s+1)} + \frac{1}{(s+3)}$$

and

$$y(t) = u(t) - 2e^{-t}u(t) + e^{-3t}u(t)$$

• • • End of Solution

**Q.19** Which one of the following functions is analytic over the entire complex plane?

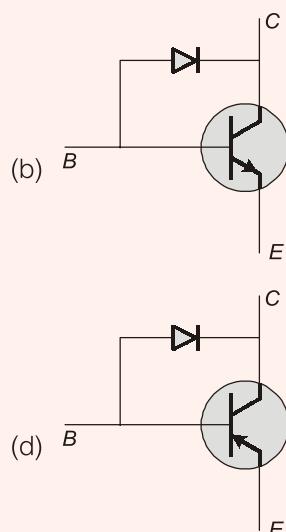
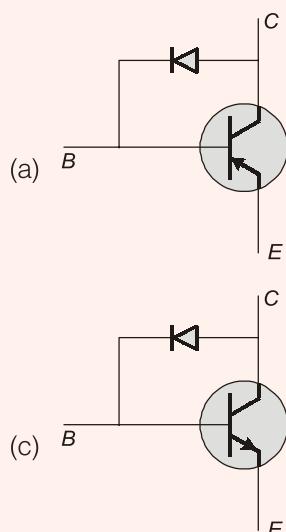
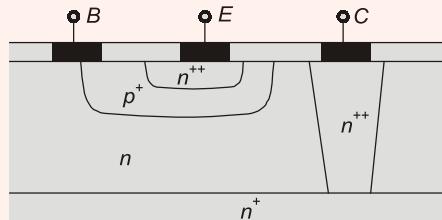
- (a)  $\cos(z)$
- (b)  $e^{1/z}$
- (c)  $\ln(z)$
- (d)  $\frac{1}{1-z}$

**Ans. (a)**

$f(z) = \cos z$  is analytic every where.

• • • End of Solution

**Q.20** The correct circuit representation of the structure shown in the figure is





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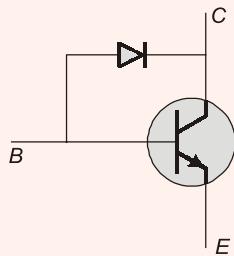
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Ans. (b)



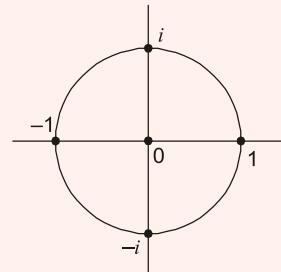
• • • End of Solution

- Q.21 The value of the contour integral  $\frac{1}{2\pi j} \oint \left(z + \frac{1}{z}\right)^2 dz$  evaluated over the unit circle  $|z| = 1$  is \_\_\_\_\_.

Ans. (0)

$$\frac{1}{2\pi j} \oint \left(z + \frac{1}{z}\right)^2 dz \text{ where } C \text{ is } |z| = 1$$

$$I = \frac{1}{2\pi j} \int_C \frac{(z^2 + 1)^2}{z^2} dz$$

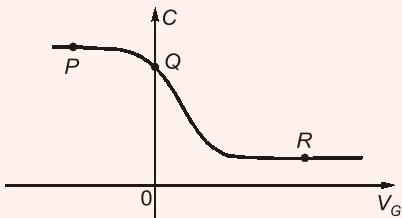


$z = 0$  lies inside the circle,

$$\begin{aligned} I &= \frac{1}{2\pi j} \left[ \frac{2\pi j}{1!} \frac{d}{dz} (z^2 + 1)^2 \right]_{z=0} = \left[ \frac{d}{dz} (z^2 + 1)^2 \right]_{z=0} \\ &= \left[ 2(z^2 + 1) \times 2z \right]_{z=0} = 0 \end{aligned}$$

• • • End of Solution

- Q.22 The figure shows the high-frequency  $C-V$  curve of a MOS capacitor (at  $T = 300$  K) with  $\phi_{ms} = 0$  V and no oxide charges. The flat-band, inversion, and accumulation conditions are represented, respectively, by the points



- (a) Q, R, P  
(c) Q, P, R

- (b) P, Q, R  
(d) R, P, Q

Ans. (a)

Since  $\phi_{ms} = 0$ , the MOS-capacitor is ideal.

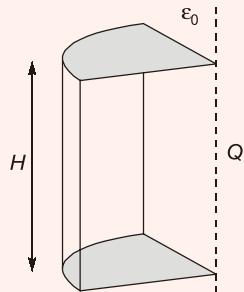
Point P Represents accumulation

Point Q Represents flat band

Point R Represents Inversion

● ● ● End of Solution

**Q.23** What is the electric flux  $(\int \vec{E} \cdot d\hat{a})$  through a quarter-cylinder of height  $H$  (as shown in the figure) due to an infinitely long line charge along the axis of the cylinder with a charge density of  $Q$ ?



(a)  $\frac{4H}{Q\epsilon_0}$

(b)  $\frac{H\epsilon_0}{4Q}$

(c)  $\frac{HQ}{\epsilon_0}$

(d)  $\frac{HQ}{4\epsilon_0}$

Ans. (d)

Electric field intensity ( $\vec{E}$ ) at ' $\rho$ ' distance due to infinite long line having line charge density  $Q$  is

$$\vec{E} = \frac{Q}{2\pi\epsilon_0\rho} \hat{a}_\rho$$

$$\int \vec{E} \cdot d\hat{a} = \iint \frac{Q}{2\pi\epsilon_0\rho} \hat{a}_\rho \cdot \rho d\phi dz \hat{a}_\rho$$

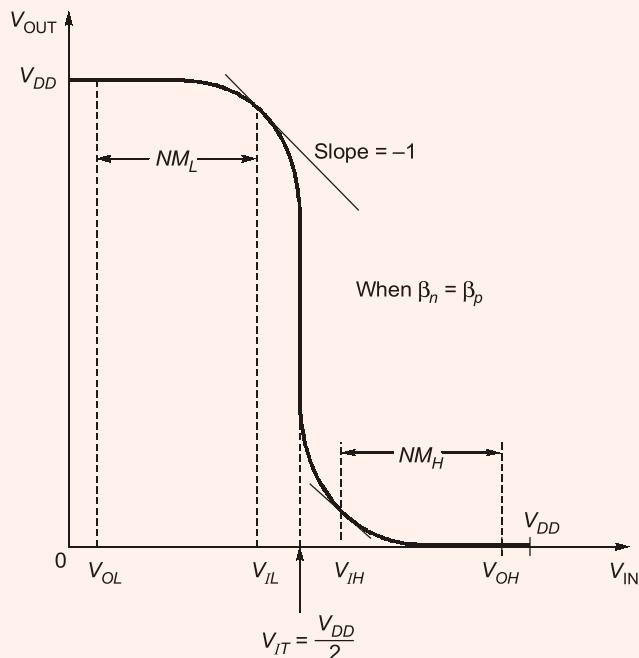
$$= \frac{Q}{2\pi\epsilon_0} \int_{\pi/2}^{\pi} d\phi \int_{z=0}^H dz = \frac{Q}{2\pi\epsilon_0} \left(\frac{\pi}{2}\right) H = \frac{HQ}{4\epsilon_0}$$

● ● ● End of Solution

**Q.24** A standard CMOS inverter is designed with equal rise and fall times ( $\beta_n = \beta_p$ ). If the width of the pMOS transistor in the inverter is increased, what would be the effect on the LOW noise margin ( $NM_L$ ) and the HIGH noise margin  $NM_H$ ?

- (a)  $NM_L$  decreases and  $NM_H$  increases.
- (b) No change in the noise margins.
- (c) Both  $NM_L$  and  $NM_H$  increase.
- (d)  $NM_L$  increases and  $NM_H$  decreases.

Ans. (d)



Making PMOS wider, shifts input transition point ( $V_{IT}$ ) towards  $V_{DD}$ .

Making NMOS wider, shifts input transition point ( $V_{IT}$ ) towards zero.

So, as PMOS made wider,  $NM_L$  increases and  $NM_H$  decreases.

• • • End of Solution

- Q.25** Let  $Z$  be an exponential random variable with mean 1. That is, the cumulative distribution function of  $Z$  is given by

$$F_Z(x) = \begin{cases} 1 - e^{-x} & \text{if } x \geq 0 \\ 0 & \text{if } x < 0 \end{cases}$$

Then  $\Pr(Z > 2 | Z > 1)$ , rounded off to two decimal places, is equal to \_\_\_\_\_.

Ans. (0.37)

**Sol.** Required probability =  $\frac{P[(z>2) \cap (z>1)]}{P[z>1]} = \frac{P[z>2]}{P[z>1]}$

$$P(z \leq 2) = 1 - e^{-2} \Rightarrow P(z > 2) = e^{-2}$$

$$P(z \leq 1) = 1 - e^{-1} \Rightarrow P(z > 1) = e^{-1}$$

$$\text{So, Required probability} = \frac{e^{-2}}{e^{-1}} = e^{-1} \approx 0.37$$

• • • End of Solution

**Q.26** Consider a differentiable function  $f(x)$  on the set of real numbers such that  $f(-1) = 0$  and  $|f'(x)| \leq 2$ . Given these conditions, which one of the following inequalities is necessarily true for all  $x \in [-2, 2]$ ?

(a)  $f(x) \leq 2|x + 1|$

(b)  $f(x) \leq \frac{1}{2}|x|$

(c)  $f(x) \leq 2|x|$

(d)  $f(x) \leq \frac{1}{2}|x + 1|$

**Ans. (a)**

$$\text{Given that, } |f'(x)| \leq 2; \quad f(-1) = 0$$

$$-2 \leq f'(x) \leq 2$$

$$x \in [-2, 2] \rightarrow -2 \leq x \leq 2$$

$$\therefore \text{By applying mean value theorem in } [-1, 2]$$

$$-2 \leq f'(x) \leq 2$$

$$-2 \leq \frac{f(2) - f(-1)}{2 - (-1)} \leq 2$$

$$-2 \leq \frac{f(2) - f(-1)}{3} \leq 2$$

$$-6 \leq f(2) - 0 \leq 6$$

$$-6 \leq f(2) \leq 6$$

It is satisfied by only option (a).

● ● ● End of Solution

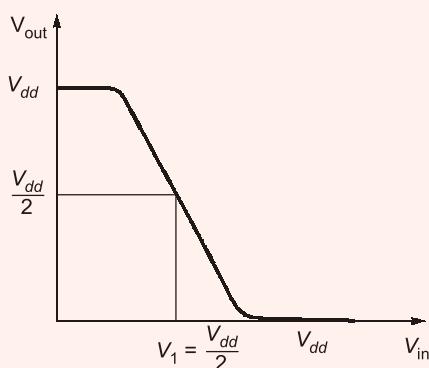
**Q.27** A CMOS inverter, designed to have a mid-point voltage  $V_1$  equal to half of  $V_{dd}$ , as shown in the figure, has the following parameters:

$$V_{dd} = 3 \text{ V}$$

$$\mu_n C_{ox} = 100 \text{ } \mu\text{A/V}^2; V_{tn} = 0.7 \text{ V for nMOS}$$

$$\mu_p C_{ox} = 40 \text{ } \mu\text{A/V}^2; |V_{tp}| = 0.9 \text{ V for pMOS}$$

The ratio of  $\left(\frac{W}{L}\right)_n$  to  $\left(\frac{W}{L}\right)_p$  is equal to \_\_\_\_\_ (rounded off to 3 decimal places).



Ans. (0.225)

$I_{Dn} = I_{Dp}$  and both will be in saturation.

$$\text{If } V_{IN} = \frac{V_{DD}}{2} = 1.5 \text{ V} = V_{GSN} = V_{SGP}$$

$$\Rightarrow \frac{1}{2}(\mu_n C_{ox}) \left( \frac{W}{L} \right)_n [V_{GSN} - V_{TN}]^2 = \frac{1}{2}(\mu_p C_{ox}) \left( \frac{W}{L} \right)_p [V_{GSP} + V_{TP}]^2$$

$$100 \times 10^{-6} \left( \frac{W}{L} \right)_n [1.5 - 0.7]^2 = 40 \times 10^{-6} \left( \frac{W}{L} \right)_p [1.5 - 0.9]^2$$

$$\Rightarrow \frac{\left( \frac{W}{L} \right)_n}{\left( \frac{W}{L} \right)_p} = \frac{40}{100} \times \frac{(0.6)^2}{(0.8)^2} = 0.225$$

• • • End of Solution

**Q.28** In an ideal  $pn$  junction with an ideality factor of 1 at  $T = 300$  K, the magnitude of the reverse-bias voltage required to reach 75% of its reverse saturation current, rounded off to 2 decimal places, is \_\_\_\_\_ mV.

[ $k = 1.38 \times 10^{-23}$  JK $^{-1}$ ,  $h = 6.625 \times 10^{-34}$  J-s,  $q = 1.602 \times 10^{-19}$ C]

Ans. (35.83)

$$V_T = \frac{kT}{q} = \frac{1.38 \times 10^{-23} \times 300}{1.602 \times 10^{-19}} \text{ V} = 25.843 \text{ mV}$$

$$I = I_0 (e^{V/V_T} - 1) = -\frac{3}{4} I_0$$

$$\Rightarrow V = V_T \ln 0.25 = -35.83 \text{ mV}$$

$$V_R = |V| = 35.83 \text{ mV}$$

• • • End of Solution

**Q.29** It is desired to find a three-tap causal filter which gives zero signal as an output to an input of the form

$$x[n] = c_1 \exp\left(-\frac{j\pi n}{2}\right) + c_2 \exp\left(\frac{j\pi n}{2}\right),$$

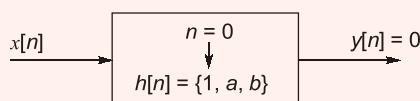
where  $c_1$  and  $c_2$  are arbitrary real numbers. The desired three-tap filter is given by

$$h[0] = 1, \quad h[1] = a, \quad h[2] = b$$

and

$$h[n] = 0 \text{ for } n < 0 \text{ or } n > 2$$

What are the values of the filter taps  $a$  and  $b$  if the output  $y[n] = 0$  for all  $n$ , where  $x[n]$  is as given above?



- (a)  $a = 0, b = -1$   
 (c)  $a = -1, b = 1$
- (b)  $a = 1, b = 1$   
 (d)  $a = 0, b = 1$

Ans. (d)

$$x(n) = c_1 e^{-j\frac{\pi}{2}n} + c_2 e^{j\frac{\pi}{2}n}$$

$$\omega_o = \frac{\pi}{2} \text{ rad/s}$$

$$H(e^{j\omega}) = 1 + ae^{-j\omega} + be^{-j2\omega}$$

To get  $y(n) = 0$ ,

$$H(e^{j\omega_o}) = H(e^{j\omega}) \Big|_{\omega=\frac{\pi}{2}} = 0$$

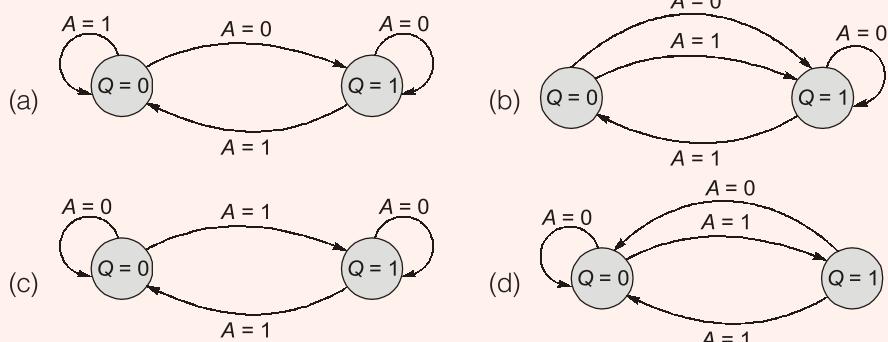
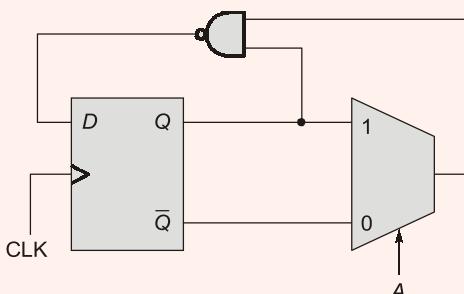
$$1 + ae^{-j\frac{\pi}{2}} + be^{-j2\frac{\pi}{2}} = 0$$

$$1 - ja - b = 0$$

From the given options,  $a = 0$  and  $b = 1$ .

● ● ● End of Solution

**Q.30** The state transition diagram for the circuit shown is

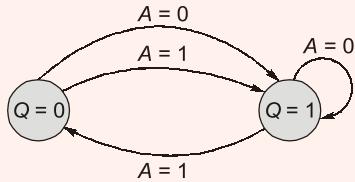


Ans. (b)

When  $A = 0$ ,  $Q_{n+1} = 1$

When  $A = 1$ ,  $Q_{n+1} = \bar{Q}_n$

So, the correct state transition diagram is,



● ● ● End of Solution

- Q.31** Let the state-space representation of an LTI system be  $\dot{X}(t) = AX(t) + Bu(t)$ ,  $y(t) = CX(t) + du(t)$  where  $A, B, C$  are matrices,  $d$  is a scalar,  $u(t)$  is the input to the system, and  $y(t)$  is its output. Let  $B = [0 \ 0 \ 1]^T$  and  $d = 0$ . Which one of the following options for  $A$  and  $C$  will ensure that the transfer function of this LTI system is

$$H(s) = \frac{1}{s^3 + 3s^2 + 2s + 1}$$

- (a)  $A = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -3 & -2 & -1 \end{bmatrix}$  and  $C = [0 \ 0 \ 1]$  (b)  $A = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -1 & -2 & -3 \end{bmatrix}$  and  $C = [0 \ 0 \ 1]$   
 (c)  $A = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -1 & -2 & -3 \end{bmatrix}$  and  $C = [1 \ 0 \ 0]$  (d)  $A = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -3 & -2 & -1 \end{bmatrix}$  and  $C = [1 \ 0 \ 0]$

**Ans. (c)**

$$X(t) = Ax(t) + Bu(t)$$

$$y(t) = Cx(t)$$

$$B = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$

$$\frac{Y(s)}{U(s)} = \frac{Y(s)}{X_1(s)} \times \frac{X_1(s)}{U(s)} = 1 \times \frac{1}{s^3 + 3s^2 + 2s + 1}$$

$$X_1(s)[s^3 + 3s^2 + 2s + 1] = U(s)$$

$$x_2 = \dot{x}_1(t) \Rightarrow X_2(s) = sX_1(s)$$

$$x_3 = \dot{x}_2(t) \Rightarrow X_3(s) = sX_2(s) = s^2X_1(s)$$

$$\text{So, } sX_3(s) = -X_1(s) - 2X_2(s) - 3X_3(s) + U(s)$$

$$\dot{x}_3(t) = -x_1(t) - 2x_2(t) - 3x_3(t) + u(t)$$

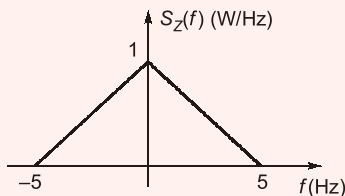
$$y(t) = x_1(t)$$

$$\dot{x}(t) = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -1 & -2 & -3 \end{bmatrix} x(t) + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} u(t)$$

$$y(t) = [1 \ 0 \ 0] x(t)$$

● ● ● End of Solution

- Q.32** Let a random process  $Y(t)$  be described as  $Y(t) = h(t) * X(t) + Z(t)$ , where  $X(t)$  is a white noise process with power spectral density  $S_X(f) = 5 \text{ W/Hz}$ . The filter  $h(t)$  has a magnitude response given by  $|H(f)| = 0.5$  for  $-5 \leq f \leq 5$ , and zero elsewhere.  $Z(t)$  is a stationary random process, uncorrelated with  $X(t)$ , with power spectral density as shown in the figure. The power in  $Y(t)$ , in watts, is equal to  $W$  \_\_\_\_\_ (rounded off to two decimal places).

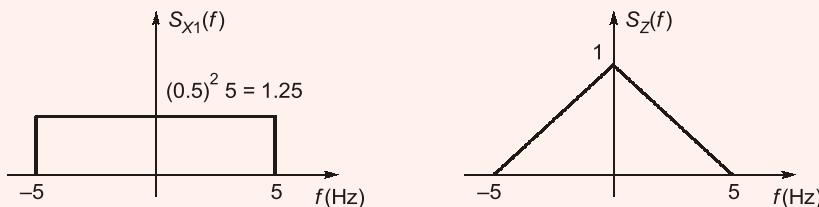


**Ans.** (17.5)

Let,

$$X_1(t) = h(t) * X(t)$$

$$S_{X1}(f) = |H(f)|^2 S_X(f)$$



Given that,  $Z(t)$  and  $X(t)$  are uncorrelated.

So,

$$S_Y(f) = S_{X1}(f) + S_Z(f)$$

Power in  $y(t)$ ,

$$P_Y = [\text{Area under } S_{X1}(f)] + [\text{Area under } S_Z(f)] \\ = (10 \times 1.25) + (5 \times 1) = 17.5 \text{ W}$$

● ● ● End of Solution

- Q.33** Consider the homogeneous ordinary differential equation

$$x^2 \frac{d^2y}{dx^2} - 3x \frac{dy}{dx} + 3y = 0, \quad x > 0$$

with  $y(x)$  as a general solution. Given that

$$y(1) = 1 \text{ and } y(2) = 14$$

the value of  $y(1.5)$ , rounded off to two decimal places, is \_\_\_\_\_.

**Ans.** (5.25)

$$(x^2 D^2 - 3x D + 3) y = 0$$

$$(\theta(\theta - 1) - 3\theta + 3)y = 0$$

$$(\theta^2 - 4\theta + 3)y = 0$$

AE is  $m^2 - 4m + 3 = 0$

$$m = 1, 3$$

$$\text{CF} = C_1 e^z + C_2 e^{3z}$$

Solution is

$$y = C_1 x + C_2 x^3$$

... (i)



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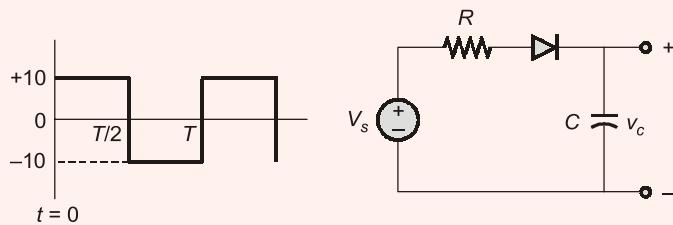
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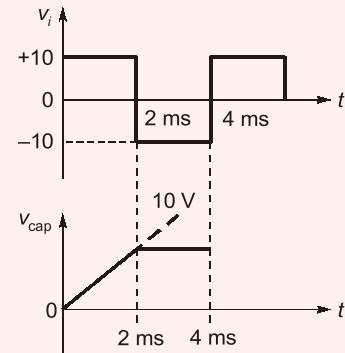
$$\begin{aligned}
 y(1) &= 1 & 1 &= C_1 + C_2 & \dots(ii) \\
 y(2) &= 14 & 14 &= 2C_1 + 8C_2 & \dots(iii) \\
 \text{From (ii) and (iii),} & & C_1 = -1, & C_2 = 2 \\
 \therefore & & y &= -x + 2x^3 \\
 & & y(1.5) &= -1.5 + 2(1.5)^3 = 5.25
 \end{aligned}$$

● ● ● End of Solution

- Q.34** In the circuit shown.  $V_s$  is a 10 V square wave of period,  $T = 4$  ms with  $R = 500 \Omega$  and  $C = 10 \mu\text{F}$ . The capacitor is initially uncharged at  $t = 0$ , and the diode is assumed to be ideal. The voltage across the capacitor ( $V_c$ ) at 3 ms is equal to \_\_\_\_ volts (rounded off to one decimal place).



Ans. (3.3)



$$\tau = RC = 500 \times 10 \times 10^{-6} = 5 \text{ ms}$$

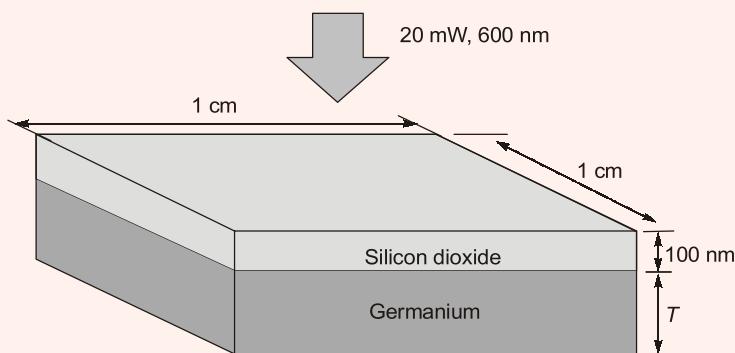
$$\begin{aligned}
 0 < t < \frac{T}{2} : \quad V_{\text{cap}} &= V_f + (V_i - V_f)e^{-t/\tau} \\
 &= 10 + (0 - 10)e^{-t/RC}
 \end{aligned}$$

$$\text{At } t = 2 \text{ msec, } V_{\text{cap}} = 10 - 10e^{\frac{-2 \times 10^{-3}}{5 \times 10^{-3}}} = 3.296 \text{ V} \approx 3.3 \text{ V}$$

For  $2 \text{ ms} < t < 4 \text{ ms}$ , diode is OFF and capacitor has no path to discharge. Hence, at  $t = 3 \text{ ms}$ ,  $V_{\text{cap}} = 3.3 \text{ V}$ .

● ● ● End of Solution

- Q.35** A Germanium sample of dimensions  $1 \text{ cm} \times 1 \text{ cm}$  is illuminated with a  $20 \text{ mW}$ ,  $600 \text{ nm}$  laser light source as shown in the figure. The illuminated sample surface has a  $100 \text{ nm}$  of loss-less Silicon dioxide layer that reflects one-fourth of the incident light. From the remaining light, one-third of the power is reflected from the Silicon dioxide- Germanium interface, one-third is absorbed in the Germanium layer, and one-third is transmitted through the other side of the sample. If the absorption coefficient of Germanium at  $600 \text{ nm}$  is  $3 \times 10^4 \text{ cm}^{-1}$  and the bandgap is  $0.66 \text{ eV}$ , the thickness of the Germanium layer, rounded off to 3 decimal places, is \_\_\_\_\_  $\mu\text{m}$ .



**Ans. (0.231)**

$$P_{\text{absorbed}} = P_{\text{incident}} (1 - e^{-\alpha T})$$

$$\frac{1}{3} = \frac{2}{3} (1 - e^{-\alpha T})$$

$$\frac{2}{3} e^{-\alpha T} = \frac{1}{3}$$

where  $\alpha = 3 \times 10^4 \text{ cm}^{-1}$ , absorption coefficient of Ge sample.

$$\therefore T = \frac{1}{\alpha} \ln(2) = \frac{1}{3 \times 10^4} \ln(2) \text{ cm} = 0.231 \mu\text{m}$$

● ● ● **End of Solution**

- Q.36** A rectangular waveguide of width  $w$  and height  $h$  has cut-off frequencies for  $\text{TE}_{10}$  and  $\text{TE}_{11}$  modes in the ratio  $1 : 2$ . The aspect ratio  $w/h$ , rounded off to two decimal places, is \_\_\_\_\_.

**Ans. (1.732)**

$$f_{cmn} = \frac{c}{2} \sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2}$$

$$\text{For } \text{TE}_{10} \text{ mode, } f_{c10} = \frac{c}{2w} \quad \dots(i)$$

$$\text{and For } \text{TE}_{11} \text{ mode, } f_{c11} = \frac{c}{2} \sqrt{\left(\frac{1}{w}\right)^2 + \left(\frac{1}{h}\right)^2} = \frac{c}{2w} \sqrt{1 + \left(\frac{w}{h}\right)^2} \quad \dots(ii)$$

$$\text{given, } \frac{f_{c10}}{f_{c11}} = \frac{1}{2} \quad \dots(iii)$$

put (i), (ii) in (iii)

$$\Rightarrow \frac{\frac{c}{2w}}{\frac{c}{2w}\sqrt{1+\left(\frac{w}{h}\right)^2}} = \frac{1}{2} \Rightarrow \sqrt{1+\left(\frac{w}{h}\right)^2} = 2$$

On solving above equation, we get,

$$\frac{w}{h} = \sqrt{3} = 1.732$$

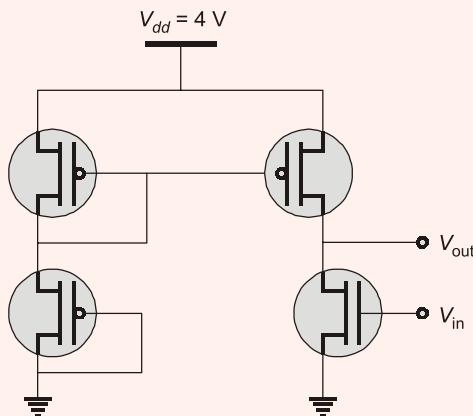
• • • **End of Solution**

- Q.37** In the circuit shown, the threshold voltages of the pMOS ( $|V_{tp}|$ ) and nMOS ( $V_{tn}$ ) transistors are both equal to 1 V. All the transistors have the same output resistance  $r_{ds}$  of  $6 \text{ M}\Omega$ . The other parameters are listed below:

$$\mu_n C_{ox} = 60 \mu\text{A/V}^2 ; \left(\frac{W}{L}\right)_{n\text{MOS}} = 5$$

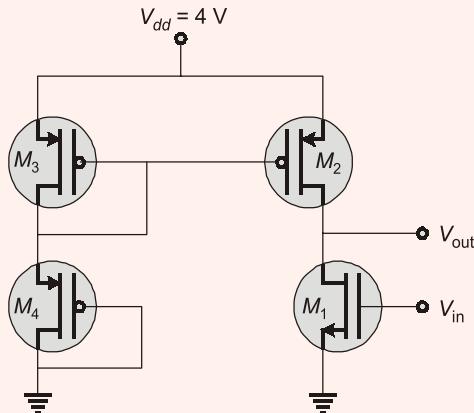
$$\mu_p C_{ox} = 30 \mu\text{A/V}^2 ; \left(\frac{W}{L}\right)_{p\text{MOS}} = 10$$

$\mu_n$  and  $\mu_p$  are the carrier mobilities, and  $C_{ox}$  is the oxide capacitance per unit area. Ignoring the effect of channel length modulation and body bias, the gain of the circuit is \_\_\_\_\_ (rounded off to 1 decimal place).



**Ans. (-900)**

$M_3$  and  $M_4$  are identical PMOS transistors and they have equal current.  
Hence their  $V_{SG}$  should be equal.



$$V_{SG3} = V_{SG4} = \frac{V_{DD}}{2} = 2 \text{ V}$$

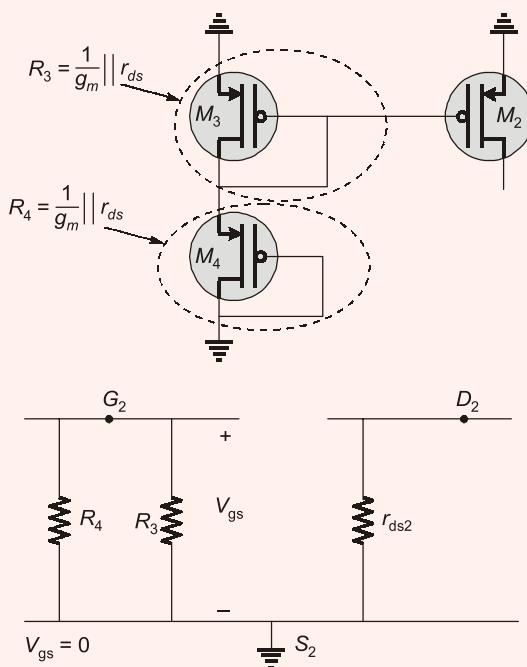
$$\begin{aligned} I_{SD} &= \frac{\mu_p C_{ox}}{2} \left( \frac{W}{L} \right)_p (V_{SG} - |V_T|)^2 \\ &= \frac{30}{2} \times 10 (2 - 1)^2 = 150 \mu\text{A} \end{aligned}$$

now, by using current mirror property all transistor should have equal current.

$$I_{DSN} = I_{SDP} = 150 \mu\text{A}$$

$$\begin{aligned} \text{For } M_1 \quad g_{m1} &= \sqrt{2\mu_n C_{ox} \frac{W}{L} \times I_{DS}} \\ &= \sqrt{2\mu_n C_{ox} \frac{W}{L} \times 150} = \sqrt{2 \times 60 \times 5 \times 150} = 300 \mu\text{V} \end{aligned}$$

$M_2$ ,  $M_3$  and  $M_4$  from active load for  $M_1$ . This active load in equivalent to resistance  $r_{ds2}$  i.e.  $6 \text{ M}\Omega$ .

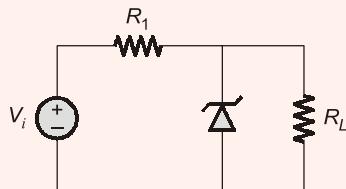


$M_1$  is common source amplifier.

$$\therefore \frac{V_{\text{out}}}{V_{\text{in}}} = A_v = -g_m \times (r_{ds2} \parallel r_{ds1}) \\ = -300 \text{ M}\Omega \times 3 \text{ M}\Omega = -900$$

● ● ● End of Solution

- Q.38** In the circuit shown, the breakdown voltage and the maximum current of the Zener diode are 20 V and 60 mA. respectively. The values of  $R_1$  and  $R_L$  are 200  $\Omega$  and 1 k $\Omega$ , respectively. What is the range of  $V_i$  that will maintain the Zener diode in the 'on' state?



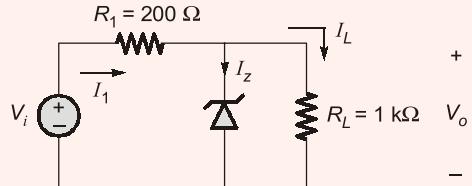
- (a) 20 V to 28 V      (b) 24 V to 36 V  
 (c) 18 V to 24 V      (d) 22 V to 34 V

**Ans. (b)**

$$V_z = 20 \text{ V} \\ I_{z \max} = 60 \text{ mA}$$

Set zener diode be OFF

$$V_o = \frac{V_i \times 1}{0.2 + 1} = \frac{V_i}{1.2}$$



Zener diode can become ON i.e. it goes into breakdown, when

$$\frac{V_i}{1.2} > 20 \text{ V}$$

$$V_i > 24 \text{ V}$$

When Zener diode is in breakdown region,

$$I_1 = \frac{V_i - 20}{0.2 \text{ k}\Omega} = \frac{V_i - 20}{0.2} \text{ mA}$$

$$I_L = \frac{V_o}{R_L} = \frac{20}{1 \text{ k}\Omega} = 20 \text{ mA}$$

$$I_z = I_1 - I_L = \frac{V_i - 20}{0.2} - 20$$

For safe operation,  $I_z \leq I_{z \max}$

$$\frac{V_i - 20}{0.2} - 20 \leq 60$$

$\Rightarrow$

$$V_i \leq 36 \text{ V}$$

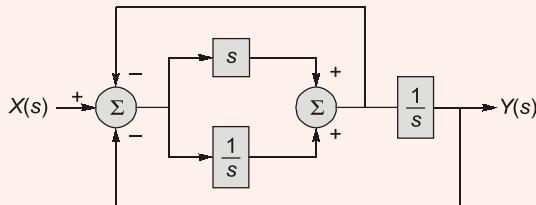
Hence,

$$24 < V_i < 36 \text{ V}$$

● ● ● End of Solution

**Q.39** The block diagram of a system is illustrated in the figure shown, where  $X(s)$  is the input

and  $Y(s)$  is the output. The transfer function  $H(s) = \frac{Y(s)}{X(s)}$  is



$$(a) H(s) = \frac{s^2 + 1}{2s^2 + 1}$$

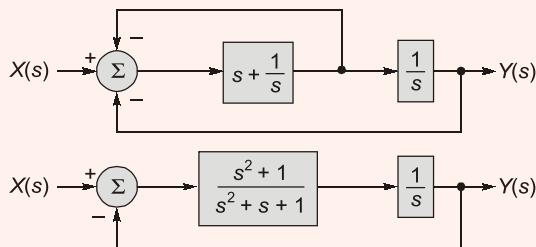
$$(b) H(s) = \frac{s^2 + 1}{s^3 + 2s^2 + s + 1}$$

$$(c) H(s) = \frac{s + 1}{s^2 + s + 1}$$

$$(d) H(s) = \frac{s^2 + 1}{s^3 + s^2 + s + 1}$$

**Ans. (b)**

Using block diagram reduction, we get,



$$\frac{Y(s)}{X(s)} = H(s) = \frac{s^2 + 1}{s^3 + 2s^2 + s + 1}$$

● ● ● End of Solution

**Q.40** A single bit, equally likely to be 0 and 1, is to be sent across an additive white Gaussian noise (AWGN) channel with power spectral density  $N_0/2$ . Binary signaling, with  $0 \rightarrow p(t)$  and  $1 \rightarrow q(t)$ , is used for the transmission, along with an optimal receiver that minimizes the bit-error probability.

Let  $\varphi_1(t), \varphi_2(t)$  form an orthonormal signal set.

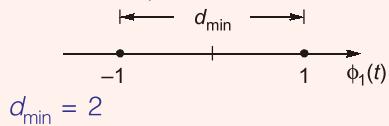
If we choose  $p(t) = \varphi_1(t)$  and  $q(t) = -\varphi_1(t)$ , we would obtain a certain bit-error probability  $P_b$ .

If we keep  $p(t) = \varphi_1(t)$ , but take  $q(t) = \sqrt{E} \varphi_2(t)$ , for what value of  $E$  would we obtain the same bit-error probability  $P_b$ ?

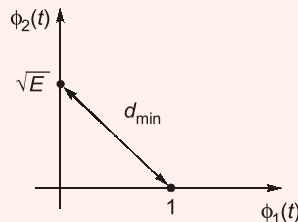
- |       |       |
|-------|-------|
| (a) 0 | (b) 3 |
| (c) 1 | (d) 2 |

Ans. (b)

When  $p(t) = \phi_1(t)$  and  $q(t) = -\phi_1(t)$ :



When  $p(t) = \phi_1(t)$  and  $q(t) = \sqrt{E} \phi_2(t)$ :



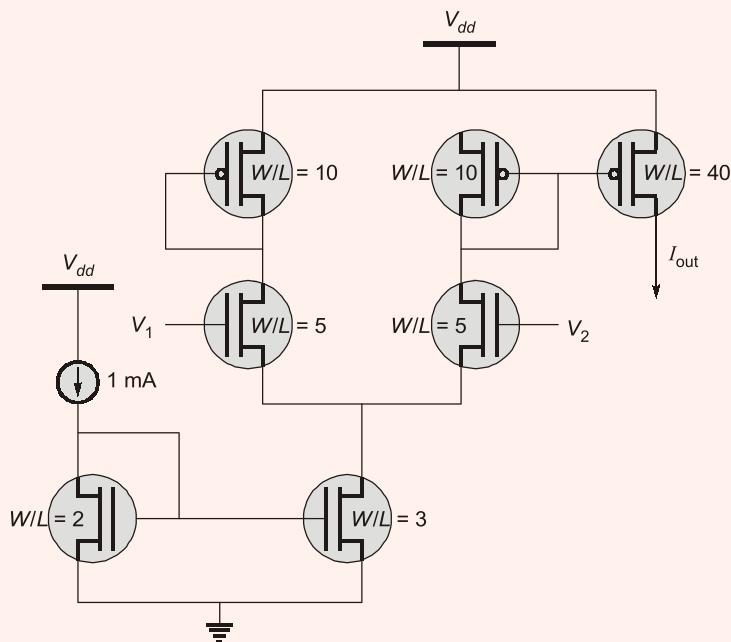
$$d_{\min} = \sqrt{(\sqrt{E})^2 + 1} = \sqrt{E+1}$$

To obtain same bit-error probability,  $d_{\min}$  should be same.

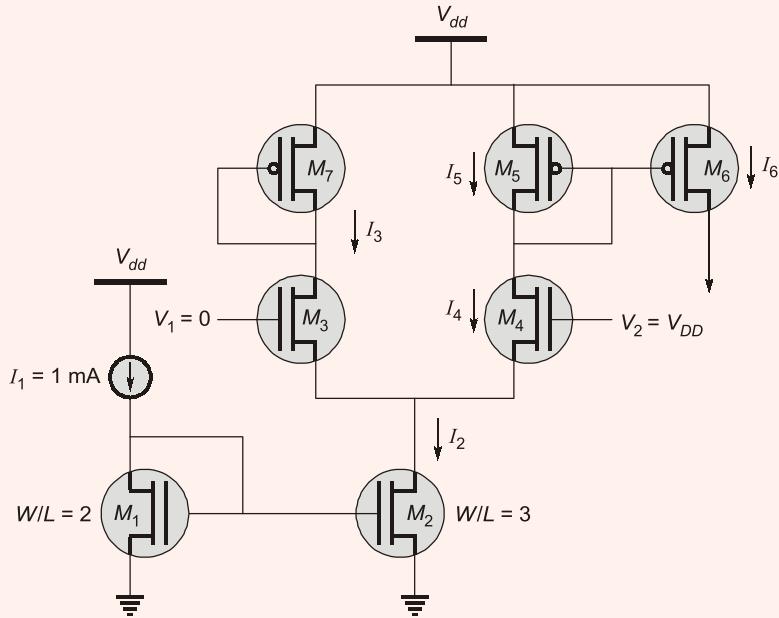
So,  $\sqrt{E+1} = 2$   
 $E = 3$

● ● ● End of Solution

**Q.41** In the circuit shown,  $V_1 = 0$  and  $V_2 = V_{dd}$ . The other relevant parameters are mentioned in the figure. Ignoring the effect of channel length modulation and the body effect, the value of  $I_{out}$  is \_\_\_\_\_ mA (rounded off to 1 decimal place).



Ans. (6)



$$\frac{I_2}{I_1} = \frac{(W/L)_2}{(W/L)_1} = \frac{3}{2}$$

$$I_2 = \frac{3}{2} \times I_1 = 1.5 \text{ mA}$$

$M_3$  is OFF because  $V_1 = 0 \Rightarrow I_3 = 0$

$M_4$  is ON because  $V_2 = V_{DD}$

$$I_5 = I_4 = I_2 = 1.5 \text{ mA}$$

$$\frac{I_6}{I_5} = \frac{(W/L)_6}{(W/L)_5} = \frac{40}{10} = 4$$

$$I_6 = 4I_5 = 4 \times 1.5 = 6 \text{ mA}$$

$$\therefore I_{\text{out}} = I_6 = 6 \text{ mA}$$

● ● ● End of Solution

**Q.42** Consider a causal second-order system with the transfer function

$$G(s) = \frac{1}{1 + 2s + s^2}$$

with a unit-step  $R(s) = \frac{1}{s}$  as an input. Let  $C(s)$  be the corresponding output. The time

taken by the system output  $c(t)$  to reach 94% of its steady-state value  $\lim_{t \rightarrow \infty} c(t)$ , rounded

off to two decimal places, is

- |          |          |
|----------|----------|
| (a) 5.25 | (b) 4.50 |
| (c) 2.81 | (d) 3.89 |

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Ans. (b)

$$G(s) = \frac{1}{s^2 + 2s + 1} = \frac{1}{(s+1)^2}$$

$$R(s) = \frac{1}{s}$$

$$C(s) = G(s)R(s) = \frac{1}{s(s+1)^2}$$

Using partial fraction expansion, we get,

$$C(s) = \frac{A}{s} + \frac{B}{(s+1)} + \frac{C}{(s+1)^2}$$

$$A(s^2 + 2s + 1) + B(s^2 + s) + Cs = 1$$

$$A = 1$$

$$A + B = 0 \Rightarrow B = -1$$

$$2A + B + C = 0 \Rightarrow C = -1$$

$$\therefore C(s) = \frac{1}{s} - \frac{1}{(s+1)} - \frac{1}{(s+1)^2} \quad \text{and} \quad c(t) = (1 - e^{-t} - te^{-t}) u(t)$$

$$\lim_{t \rightarrow \infty} c(t) = 1$$

In order to reach 94% of its steady-state value,

$$(1 - e^{-t} - te^{-t}) = 0.94$$

By trial and error, we get,

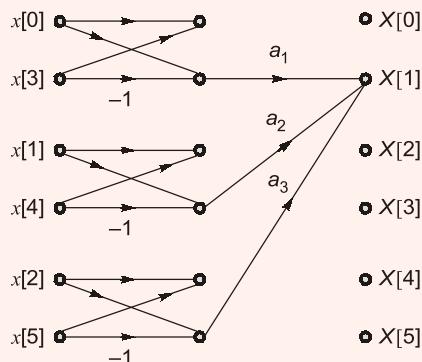
$$t \approx 4.50 \text{ sec}$$

● ● ● End of Solution

**Q.43** Consider a six-point decimation-in-time Fast Fourier Transform (FFT) algorithm, for which

the signal-flow graph corresponding to  $X[1]$  is shown in the figure. Let  $W_6 = \exp\left(-\frac{j2\pi}{6}\right)$ .

In the figure, what should be the values of the coefficients  $a_1, a_2, a_3$  in terms of  $W_6$  so that  $X[1]$  is obtained correctly?



- |  |  |
|--|--|
| (a) $a_1 = 1, a_2 = W_6^2, a_3 = W_6$  | (b) $a_1 = -1, a_2 = W_6^2, a_3 = W_6$ |
| (c) $a_1 = -1, a_2 = W_6, a_3 = W_6^2$ | (d) $a_1 = 1, a_2 = W_6, a_3 = W_6^2$  |

Ans. (d)

$$X(k) = \sum_{n=0}^{N-1} x(n) e^{-j \frac{2\pi}{N} kn} ; \quad X(1) = \sum_{n=0}^5 x(n) W_6^n$$

$$= x(0) + x(1) W_6 + x(2) W_6^2 + x(3) W_6^3 + x(4) W_6^4 + x(5) W_6^5 \quad \dots(i)$$

From the given flow graph,

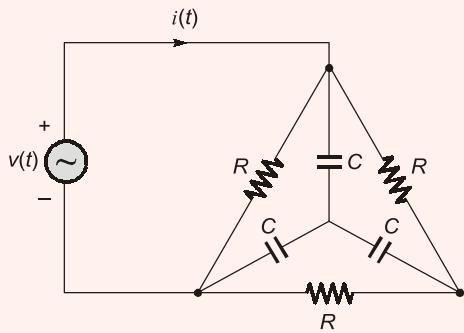
$$X(k) = [x(0) - x(3)]a_1 + [x(1) - x(4)]a_2 + [x(2) - x(5)]a_3 \quad \dots(ii)$$

By comparing equations (i) and (ii), we get,

$$a_1 = 1, a_2 = W_6, a_3 = W_6^2$$

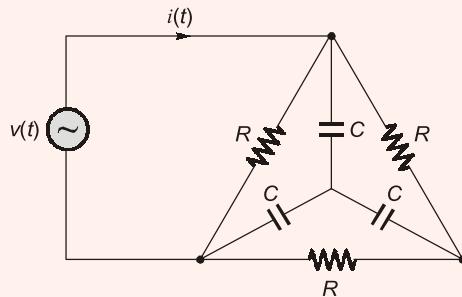
• • • End of Solution

- Q.44** In the circuit shown, if  $v(t) = 2 \sin(1000t)$  volts.  $R = 1 \text{ k}\Omega$  and  $C = 1 \mu\text{F}$ . then the steady-state current  $i(t)$ , in milliamperes (mA), is



- (a)  $3\sin(1000t) + \cos(1000t)$   
 (b)  $\sin(1000t) + \cos(1000t)$   
 (c)  $\sin(1000t) + 3\cos(1000t)$   
 (d)  $2\sin(1000t) + 2\cos(1000t)$

Ans. (a)



Here,

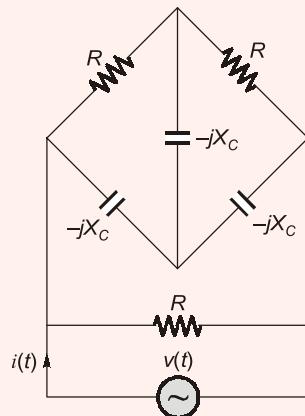
$$X_C = \frac{1}{\omega C} = \frac{1}{10^3 \times 10^{-6}} = \frac{1}{10^{-3}}$$

$$X_C = 10^3 \Omega$$

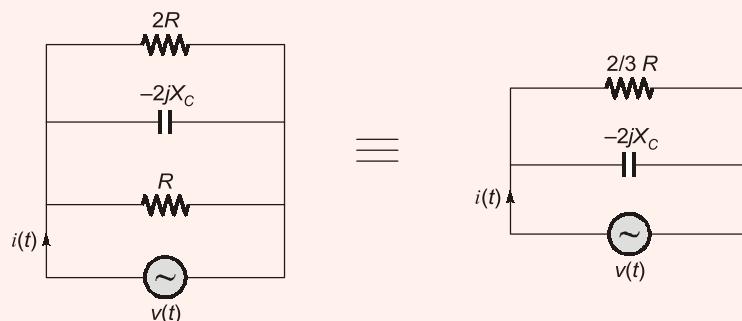
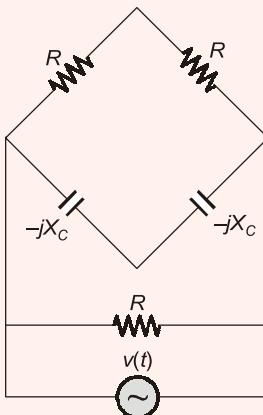
$$R = 10^3 \Omega \quad (\text{Given})$$

$$v(t) = 2\sin 1000t \text{ V} = 2\angle 0^\circ \text{ V}$$

Redrawing the given network, we get,



As the bridge is balanced, it can be redrawn as

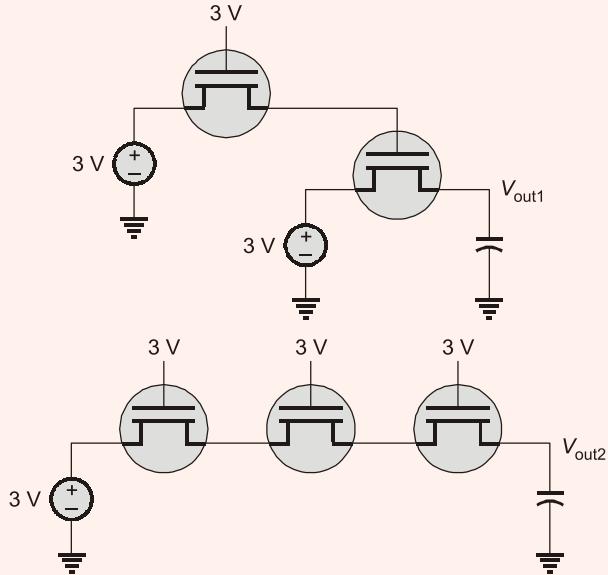


$$\therefore Y_{eq} = Y_1 + Y_2 = \frac{3}{2}R + \frac{1}{-2jX_C} = \frac{3}{2} \times 10^{-3} + j\frac{1}{2} \times 10^{-3}$$

$$\begin{aligned} \therefore i(t) &= v(t) \times Y_{eq} = 2\angle 0^\circ \left[ \frac{3}{2} + j\frac{1}{2} \right] \text{mA} \\ &= (3 + j1) \text{ mA} = 3\sin(1000t) + \cos(1000t) \text{ mA} \end{aligned}$$

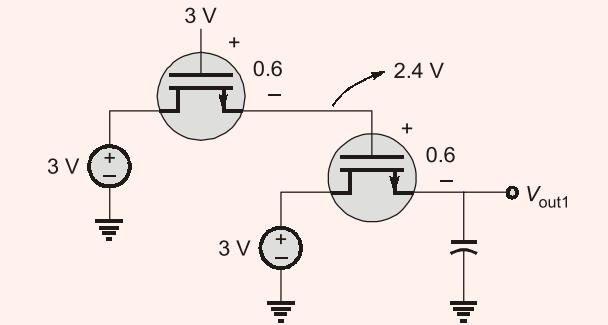
● ● ● End of Solution

**Q.45** In the circuits shown, the threshold voltage of each nMOS transistor is 0.6 V. Ignoring the effect of channel length modulation and body bias, the values of  $V_{out1}$  and  $V_{out2}$ , respectively, in volts, are

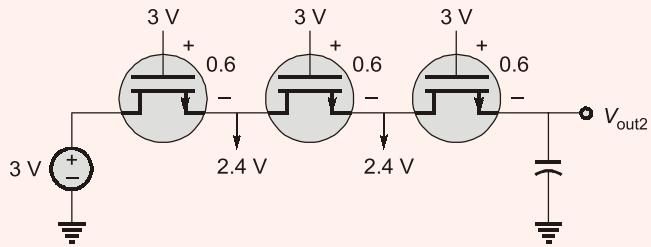





Ans. (a)



$$V_{\text{out } 1} = 3 - 0.6 - 0.6 = 1.8 \text{ V}$$



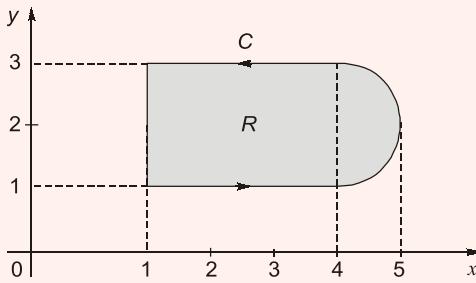
$$V_{\text{out } 2} = 2.4 \text{ V}$$

End of Solution

**Q.46** Consider the line integral

$$\int_C (xdy - ydx)$$

the integral being taken in a counterclockwise direction over the closed curve  $C$  that forms the boundary of the region  $R$  shown in the figure below. The region  $R$  is the area enclosed by the union of a  $2 \times 3$  rectangle and a semi-circle of radius 1. The line integral evaluates to



(a)  $12 + \pi$   
 (c)  $6 + \pi/2$

(b)  $16 + \pi$   
 (d)  $8 + \pi$

**Ans.** (a)

Given,  $\int -ydx + xdy$

here,  $F_1 = -y$  and  $\frac{\partial F_1}{\partial y} = -1$

$$F_2 = x \text{ and } \frac{\partial F_2}{\partial x} = 1$$

$\therefore \int F_1 dx + F_2 dy = \iint \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) dx dy$

$$\int -ydx + xdy = \iint 1 - (-1) dx dy = 2(\text{Area of region } R) = 2 \left( 6 + \frac{\pi}{2} \right) = 12 + \pi$$

● ● ● End of Solution

**Q.47** Two identical copper wires  $W_1$  and  $W_2$  placed in parallel as shown in the figure, carry currents  $I$  and  $2I$ , respectively, in opposite directions. If the two wires are separated by a distance of  $4r$ , then the magnitude of the magnetic field  $\vec{B}$  between the wires at a distance  $r$  from  $W_1$  is

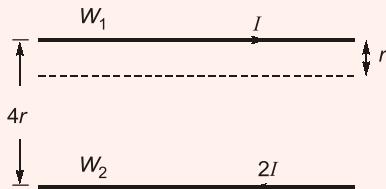


$W_1$                            $W_2$

(a)  $\frac{\mu_0 I^2}{2\pi r^2}$   
 (c)  $\frac{\mu_0 I}{6\pi r}$

(b)  $\frac{6\mu_0 I}{5\pi r}$   
 (d)  $\frac{5\mu_0 I}{6\pi r}$

Ans. (d)



Magnetic flux density ( $\vec{B}$ ) at  $r$  distance due to infinite line carrying current  $I$  is  $|\vec{B}| = \frac{\mu_0 I}{2\pi r}$ .

- $|\vec{B}|$  at  $r$  distance due to  $W_1$  wire  $= \frac{\mu_0 I}{2\pi r}$  ... (i)

- $|\vec{B}|$  at  $3r$  distance due to  $W_2$  wire  $= \frac{\mu_0 (2I)}{2\pi (3r)}$  ... (ii)

From right hand thumb rule,  $\vec{B}$  due to both lines add in between conductors.

So,

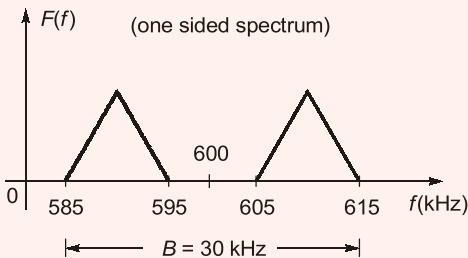
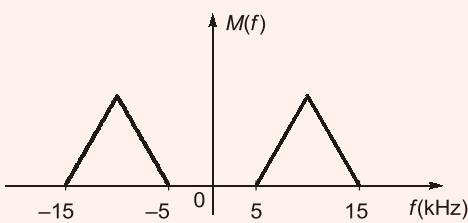
$$|\vec{B}| = |\vec{B}_1| + |\vec{B}_2|$$

$$\therefore |\vec{B}| = \frac{\mu_0 I}{2\pi r} + \frac{2\mu_0 I}{6\pi r} = \frac{5\mu_0 I}{6\pi r}$$

• • • End of Solution

**Q.48** A voice signal  $m(t)$  is in the frequency range 5 kHz to 15 kHz. The signal is amplitude-modulated to generate an AM signal  $f(t) = A(1 + m(t)) \cos 2\pi f_c t$ , where  $f_c = 600$  kHz. The AM signal  $f(t)$  is to be digitized and archived. This is done by first sampling  $f(t)$  at 1.2 times the Nyquist frequency, and then quantizing each sample using a 256-level quantizer. Finally, each quantized sample is binary coded using  $K$  bits, where  $K$  is the minimum number of bits required for the encoding. The rate, in Megabits per second (rounded off to 2 decimal places), of the resulting stream of coded bits is \_\_\_\_ Mbps.

Ans. (0.59)



$$\text{Nyquist rate} = \frac{2f_H}{[f_H/B]} = \frac{2 \times 615}{[615/30]} \text{ kHz}$$

$$= \frac{2 \times 615}{[20.5]} = \frac{2 \times 615}{20} = 61.5 \text{ kHz}$$

$$f_s = 1.2 \times 61.5 = 73.8 \text{ kHz}$$

Bits/sample,

$$n = \log_2(256) = 8$$

So,

$$R_b = n f_s = 8 \times 73.8 \text{ kbps}$$

$$= 590.4 \text{ kbps} = 0.5904 \text{ Mbps} \simeq 0.59 \text{ Mbps}$$

**Note:** If band-pass sampling is not considered by the examiner, then

$$f_s = 1.2 \times 2 \times 615 = 1476 \text{ kHz}$$

$$R_b = 8 \times 1.476 = 11.808 \simeq 11.81 \text{ Mbps}$$

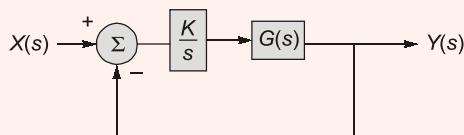
 • • • **End of Solution**

**Q.49** Consider a unity feedback system, as in the figure shown, with an integral compensator

$$\frac{K}{s}$$
 and open-loop transfer function

$$G(s) = \frac{1}{s^2 + 3s + 2}$$

where  $K > 0$ . The positive value of  $K$  for which there are exactly two poles of the unity feedback system on the  $j\omega$  axis is equal to \_\_\_\_\_ (rounded off to two decimal places).



**Ans. (6)**

$$\frac{Y(s)}{X(s)} = \frac{K}{s^3 + 3s^2 + 2s + K}$$

Two poles of this system lie on the  $j\omega$  axis when the system is marginally stable.

$$k_{\text{mar}} = 3 \times 2 = 6$$

 • • • **End of Solution**

**Q.50** Let  $h[n]$  be a length-7 discrete-time finite impulse response filter, given by

$$\begin{aligned} h[0] &= 4, & h[1] &= 3, & h[2] &= 2, & h[3] &= 1 \\ h[-1] &= -3, & h[-2] &= -2, & h[-3] &= -1, \end{aligned}$$

and  $h[n]$  is zero for  $|n| \geq 4$ . A length-3 finite impulse response approximation  $g[n]$  of  $h[n]$  has to be obtained such that

$$E(h, g) = \int_{-\pi}^{\pi} |H(e^{j\omega}) - G(e^{j\omega})|^2 d\omega$$

is minimized, where  $H(e^{j\omega})$  and  $G(e^{j\omega})$  are the discrete-time Fourier transforms of  $h[n]$  and  $g[n]$ , respectively. For the filter that minimizes  $E(h, g)$ , the value of  $10g[-1] + g[1]$ , rounded off to 2 decimal places, is \_\_\_\_\_.

**Ans. (-27)**

From Parseval's theorem,

$$\sum_{n=-\infty}^{\infty} |x[n]|^2 = \frac{1}{2\pi} \int_{-\pi}^{\pi} |X(e^{j\omega})|^2 d\omega$$

$$\text{So, } \int_{-\pi}^{\pi} |H(e^{j\omega}) - G(e^{j\omega})|^2 d\omega = 2\pi \sum_{n=-3}^3 |h(n) - g(n)|^2$$

The solution of  $g(n)$  that minimizes  $E(h, g)$  also minimizes  $\sum_{n=-3}^3 |h(n) - g(n)|^2$ .

$$\sum_{n=-3}^3 |h(n) - g(n)|^2 = |4 - g(0)|^2 + |3 - g(1)|^2 + |-3 - g(-1)|^2 + 10$$

The solution of  $g(n)$  that minimizes the above equation is

$$g(n) = \{ \begin{matrix} 4, \\ \uparrow \\ 3 \end{matrix} \}$$

$$\text{So, } 10g(-1) + g(1) = 10(-3) + 3 = -27$$

● ● ● **End of Solution**

- Q.51** Consider a long-channel MOSFET with a channel length  $1 \mu\text{m}$  and width  $10 \mu\text{m}$ . The device parameters are acceptor concentration  $N_A = 5 \times 10^{16} \text{ cm}^{-3}$ , electron mobility  $\mu_n = 800 \text{ cm}^2/\text{V}\cdot\text{s}$ , oxide capacitance/area  $C_{ox} = 3.45 \times 10^{-7} \text{ F/cm}^2$ , threshold voltage  $V_T = 0.7 \text{ V}$ . The drain saturation current ( $I_{D\text{sat}}$ ) for a gate voltage of  $5 \text{ V}$  is \_\_\_\_ mA (rounded off to two decimal places). [ $\epsilon_0 = 8.854 \times 10^{-14} \text{ F/cm}$ ,  $\epsilon_{Si} = 11.9$ ]

**Ans. (25.52)**

$$\begin{aligned} I_{D(\text{sat})} &= \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_T)^2 \\ &= \frac{1}{2} \times 800 \times 3.45 \times 10^{-7} \times \frac{10}{1} (5 - 0.7)^2 \text{ A} \\ &= 25.5162 \text{ mA} \simeq 25.52 \text{ mA} \end{aligned}$$

● ● ● **End of Solution**

- Q.52** A random variable  $X$  takes values  $-1$  and  $+1$  with probabilities  $0.2$  and  $0.8$ , respectively. It is transmitted across a channel which adds noise  $N$ , so that the random variable at the channel output is  $Y = X + N$ . The noise  $N$  is independent of  $X$ , and is uniformly distributed over the interval  $[-2, 2]$ . The receiver makes a decision

$$\hat{X} = \begin{cases} -1, & \text{if } Y \leq \theta \\ +1, & \text{if } Y < \theta \end{cases}$$

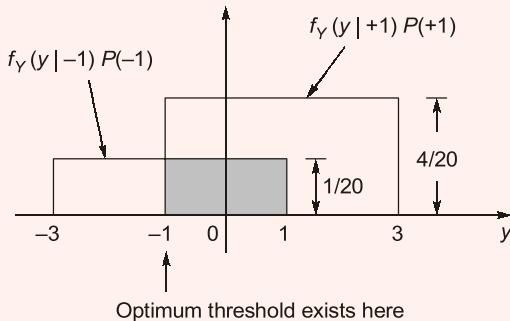
where the threshold  $\theta \in [-1, 1]$  is chosen so as to minimize the probability of error  $\Pr[\hat{X} \neq X]$ . The minimum probability of error, rounded off to 1 decimal place, is \_\_\_\_.

Ans. (0.10)

MAP criteria should be used to minimise the probability of error.

$$f_Y(y|+1)P(+1) \geq f_Y(y|-1)P(-1)$$

$$P(+1) = 0.80 \text{ and } P(-1) = 0.20$$



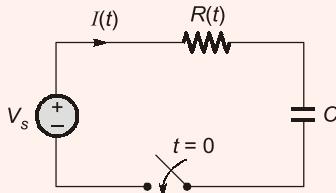
$$P_{e(\min)} = \text{Shaded area} = 2 \times \frac{1}{20} = 0.10$$

• • • End of Solution

**Q.53** The RC circuit shown below has a variable resistance  $R(t)$  given by the following expression:

$$R(t) = R_0 \left(1 - \frac{t}{T}\right) \text{ for } 0 \leq t < T$$

where  $R_0 = 1 \Omega$ , and  $C = 1 F$ . We are also given that  $T = 3R_0C$  and the source voltage is  $V_s = 1 V$ . If the current at time  $t = 0$  is 1 A, then the current  $I(t)$ , in amperes, at time  $t = T/2$  is \_\_\_\_\_ (rounded off to 2 decimal places).



Ans. (0.25)

$$T = 3R_0C = 3 \text{ sec}$$

$$R(t) = \left(1 - \frac{t}{3}\right); 0 \leq t \leq 3 \text{ sec}$$

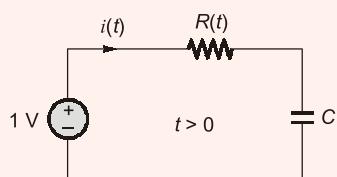
$$R(t)i(t) + \frac{1}{C} \int i(t)dt = 1$$

$$\left(1 - \frac{t}{3}\right)i(t) + \int i(t)dt = 1$$

Differentiating both sides, we get,

$$\left(1 - \frac{t}{3}\right) \frac{di}{dt} - \frac{i}{3} + i = 0$$

$$(3-t)\frac{di}{dt} + 2i = 0$$





$$\frac{di}{i} = -\frac{2}{(3-t)} dt$$

Integrating on both sides, we get,

$$\begin{aligned}\ln(i) &= 2\ln(3-t) + \ln(c) \\ i(t) &= c(3-t)^2 ; t \geq 0\end{aligned}$$

Given that,  $i(0) = 1$  A.

So,

$$c(3-0)^2 = 1 \text{ A}$$

$$c = \frac{1}{9} \text{ A}$$

$$i(t) = \frac{1}{9}(3-t)^2 \text{ A}$$

$$\text{At } t = \frac{T}{2} = 1.5 \text{ sec, } i(1.5) = \frac{1}{9}(1.5)^2 = 0.25 \text{ A}$$

● ● ● **End of Solution**

- Q.54** The dispersion equation of a waveguide, which relates the wave-number  $k$  to the frequency  $\omega$ , is

$$k(\omega) = \left(\frac{1}{c}\right)\sqrt{\omega^2 - \omega_0^2}$$

where the speed of light  $c = 3 \times 10^8$  m/s, and  $\omega_0$  is a constant. If the group velocity is  $2 \times 10^8$  m/s, then the phase velocity is

- |                           |                           |
|---------------------------|---------------------------|
| (a) $2 \times 10^8$ m/s   | (b) $3 \times 10^8$ m/s   |
| (c) $1.5 \times 10^8$ m/s | (d) $4.5 \times 10^8$ m/s |

**Ans. (d)**

$$\text{By definition } v_p = \frac{\omega}{\beta} = \frac{\omega}{k}$$

$$\text{where, } k(\omega) = \left(\frac{1}{c}\right)\sqrt{\omega^2 - \omega_0^2} \quad (\text{given})$$

$$\therefore v_p = \frac{c}{\sqrt{1 - \left(\frac{\omega_0}{\omega}\right)^2}}$$

$$\text{by definition, } v_g = \frac{d\omega}{d\beta} = \frac{d\omega}{dk} \Rightarrow \frac{dk}{d\omega} = \frac{1}{c} \frac{1}{2\sqrt{\omega^2 - \omega_0^2}} \times 2\omega$$

$$\text{or } v_g = c \sqrt{1 - \left(\frac{\omega_0}{\omega}\right)^2}$$

$$\therefore v_p \cdot v_g = c^2$$

$$\therefore v_p = \frac{c^2}{v_g} = \frac{(3 \times 10^8)^2}{2 \times 10^8} = 4.5 \times 10^8 \text{ m/sec}$$

● ● ● **End of Solution**

**Q.55** The quantum efficiency ( $\eta$ ) and responsivity ( $R$ ) at a wavelength  $\lambda$  (in  $\mu\text{m}$ ) in a p-i-n photodetector are related by

(a)  $R = \frac{1.24 \times \lambda}{\eta}$

(b)  $R = \frac{\eta \times \lambda}{1.24}$

(c)  $R = \frac{\lambda}{\eta \times 1.24}$

(d)  $R = \frac{1.24}{\eta \times \lambda}$

**Ans.** (b)

$$\eta = \frac{I_{\text{out}}}{q} \times \frac{hf}{P_{\text{in}}}$$

$$R = \frac{I_{\text{out}}}{P_{\text{in}}}$$

So,

$$R = \eta \times \frac{q}{hf} = \eta \times \frac{q\lambda}{hc}$$

If  $\lambda$  is given in  $\mu\text{m}$ , then

$$R = \eta \lambda \times \frac{q \times 10^{-6}}{hc}$$

$$\frac{hc}{q \times 10^{-6}} \simeq 1.24$$

So,

$$R = \frac{\eta \lambda}{1.24}$$



● ● ● End of Solution

