

# EE Lecture 5: Diode Circuits

MS101 Makerspace

2024-25/II (Spring)

# 1. Rectifier Circuits

- Half-Wave Rectifier
- Full-wave Rectifier
  - Bridge rectifier circuit

# Step-Down Transformer (230 V - 12 V RMS)

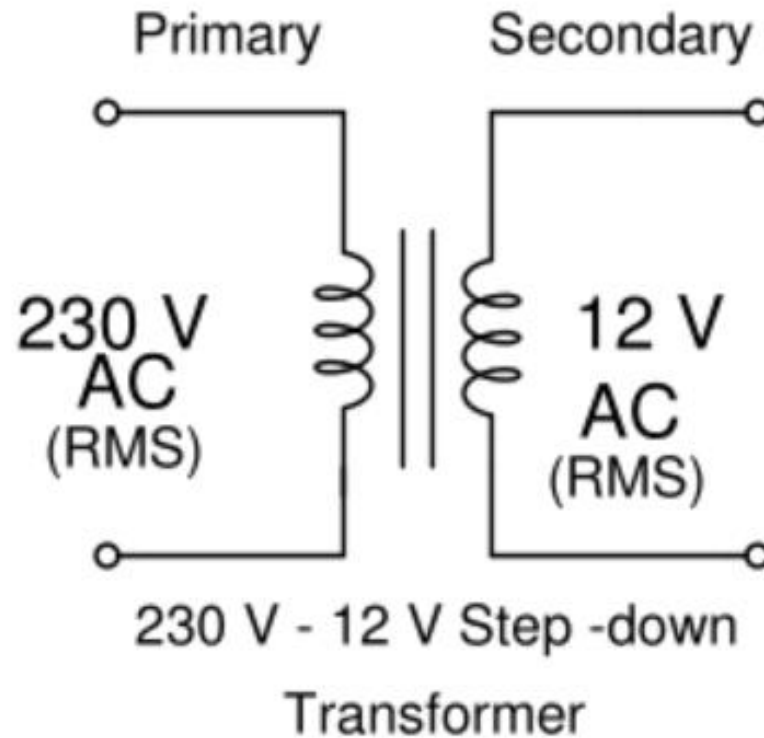


Fig. 1 Step-down Transformer

# A) Half-wave Rectifier

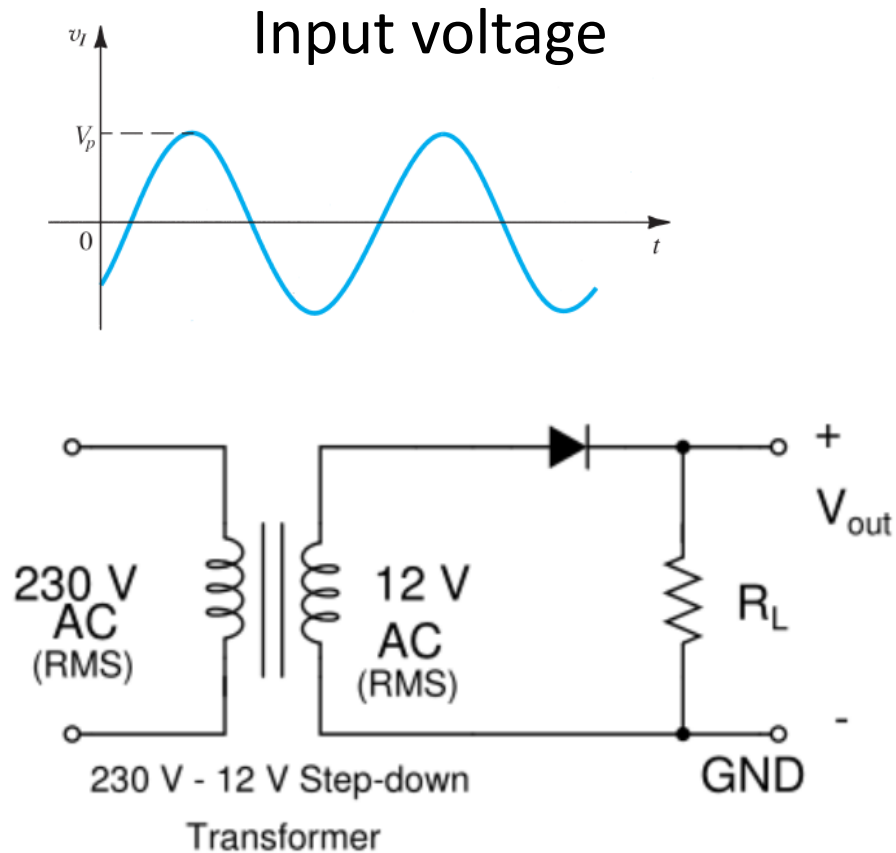
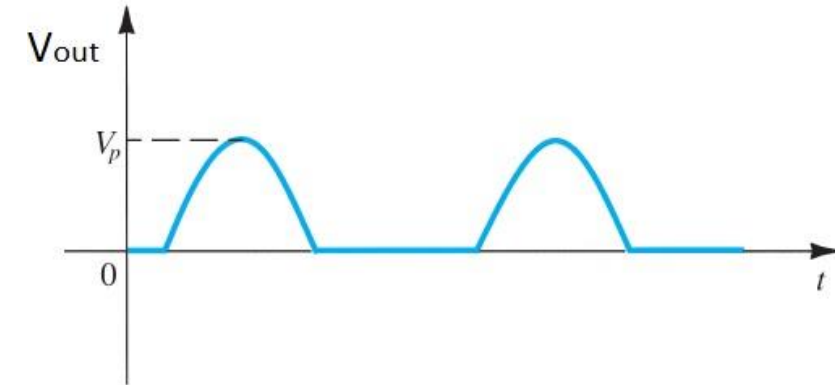


Fig. 2

Output voltage (assuming an ideal diode, i.e. zero voltage drop)



Output voltage (assuming a practical diode with voltage drop)

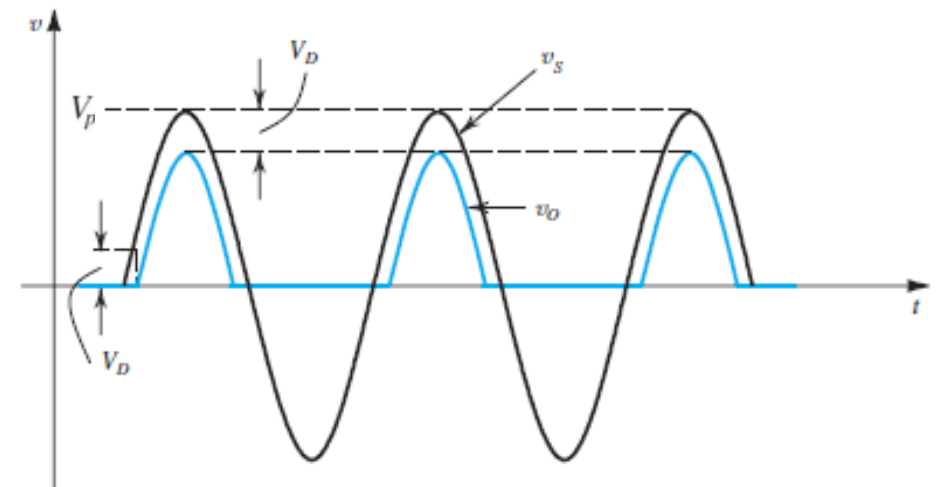


Fig. 3

## B) Full-wave (Bridge) Rectifier

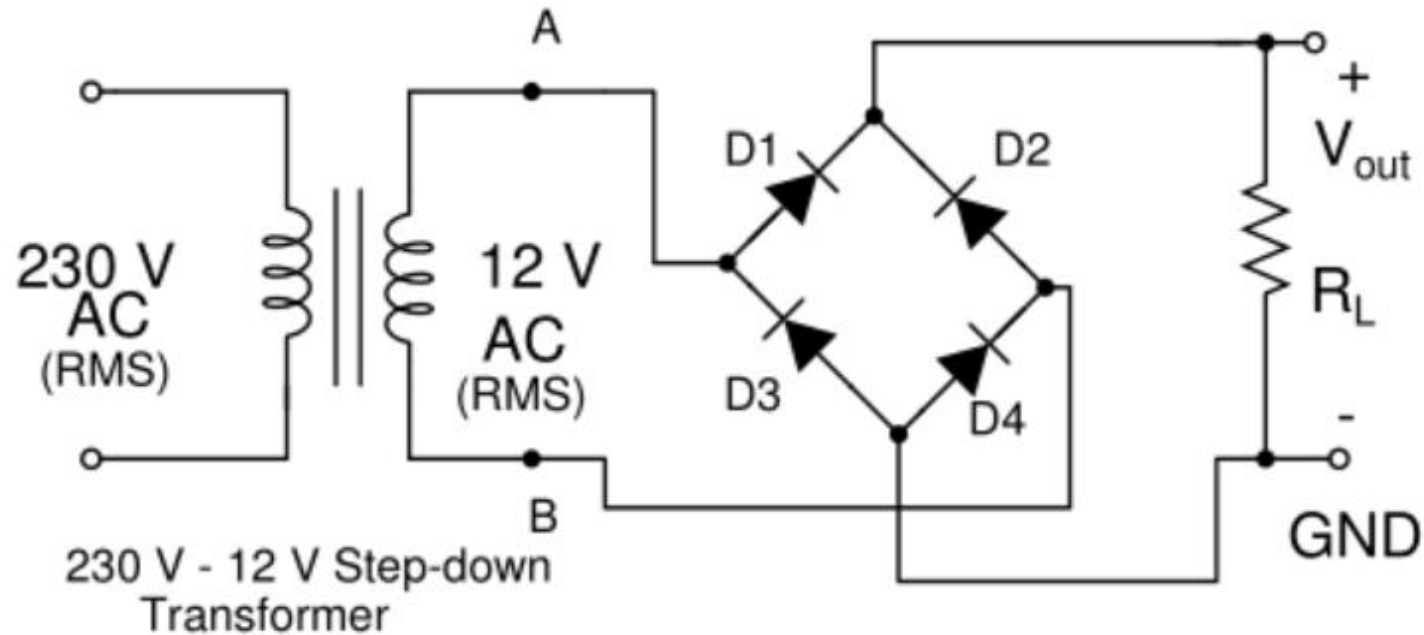
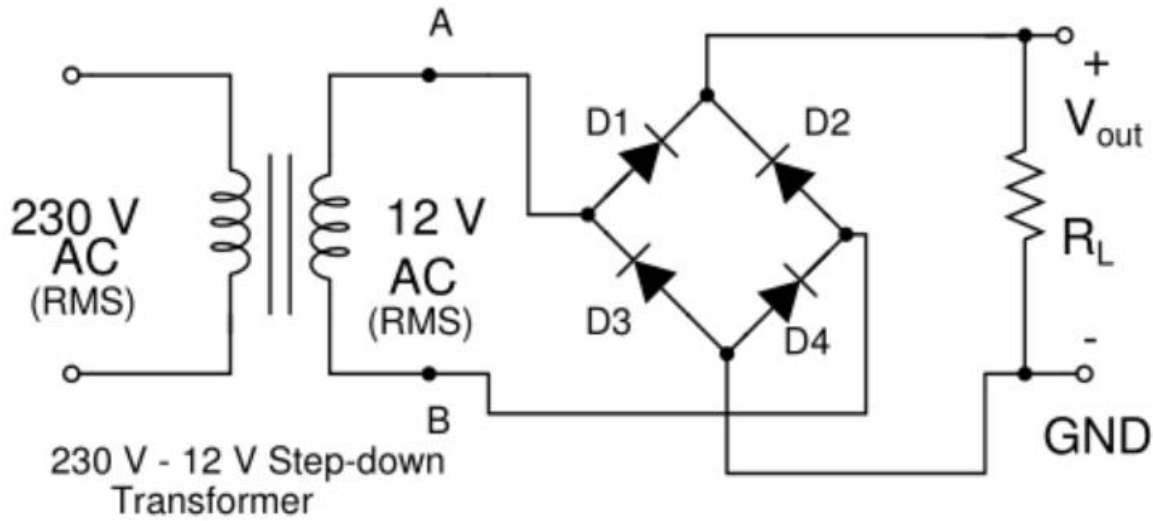


Fig. 4

- Bridge Rectifier: in every half cycle, two diodes will be in the current path



- 1<sup>st</sup> half cycle (output A is +ve w.r.t. Output B): current path – from output A  $\rightarrow$  D1  $\rightarrow$   $R_L$   $\rightarrow$  D4  $\rightarrow$  B; D2 and D3 will not conduct.
- 2<sup>nd</sup> half cycle (Output B is +ve w.r.t. output A): current path – from B  $\rightarrow$  D2  $\rightarrow$   $R_L$   $\rightarrow$  D3  $\rightarrow$  A; D1 and D4 will not conduct.

$V_D$ : voltage drop across two diodes (D1&D4, D3& D2)

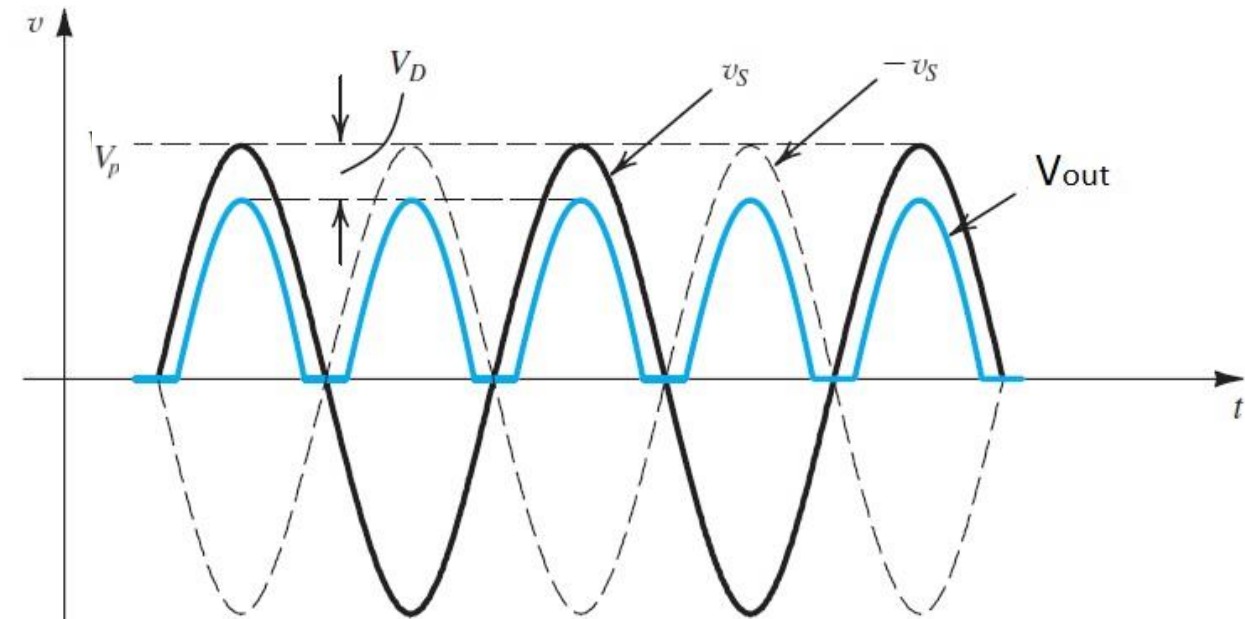


Fig. 5

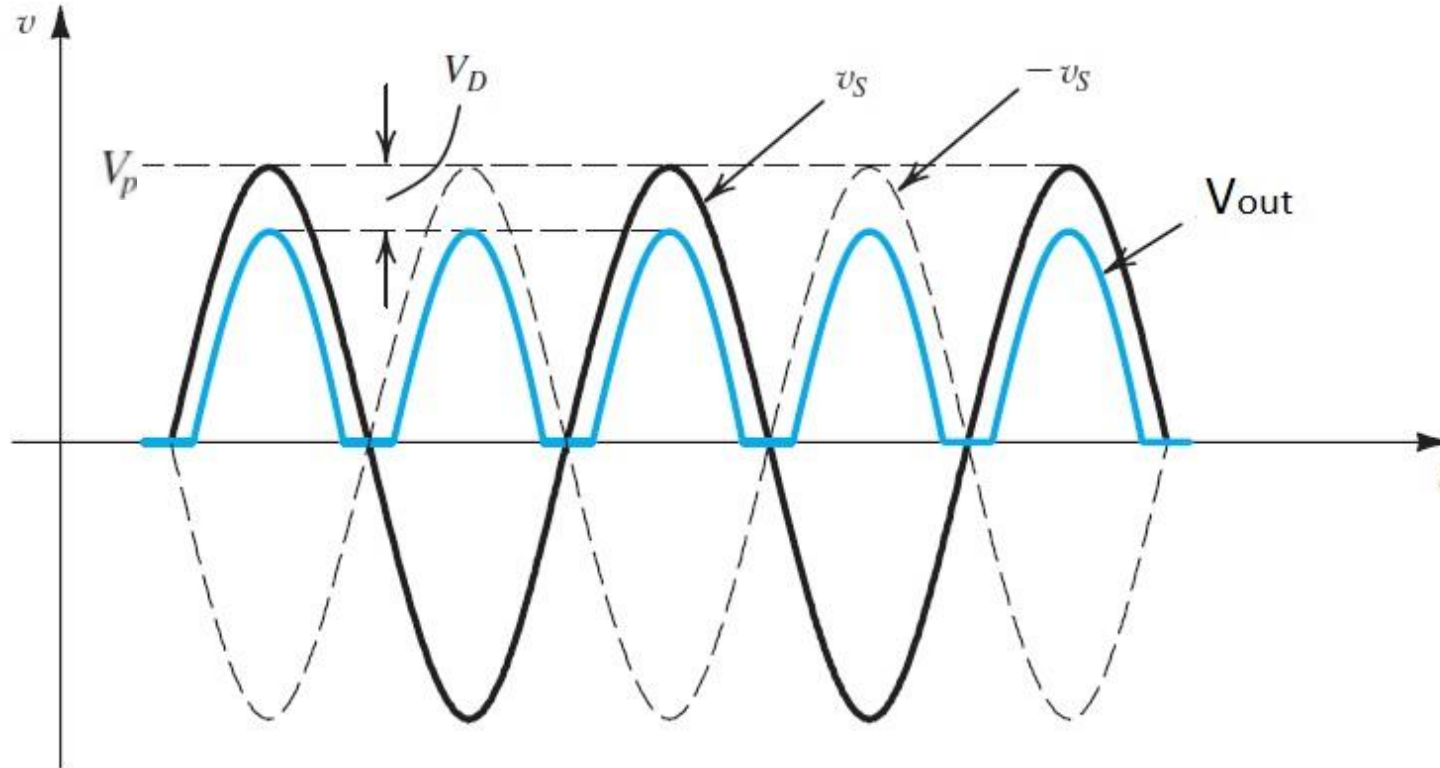


Fig. 6

- Full-wave Rectifier: Input and Output waveforms (considering diode drops)
- Peak output voltage will have the *two diode drops* lower than the input voltage. Typ. diode drop =  $2 \times 0.5 \text{ V} = 1 \text{ V}$

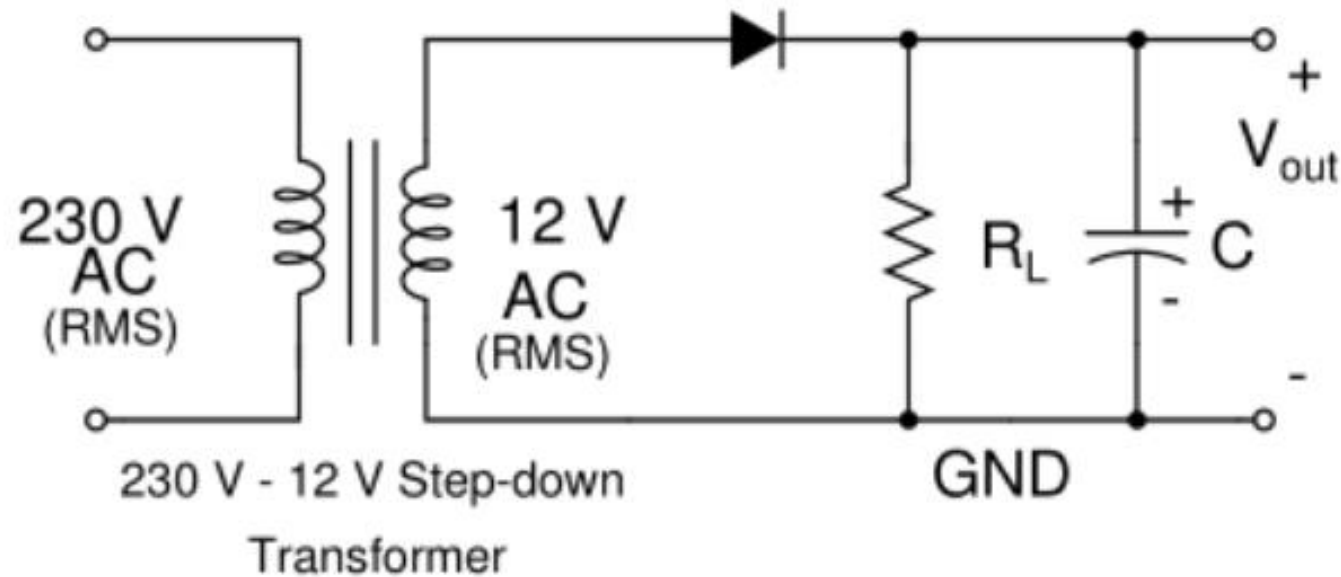
## 2. Unregulated Power Supply (Capacitive filter)

- Case A): Half-wave rectifier with a large value capacitor - ( $\gg 10 \mu\text{F}$ )
- Case B): Full-wave bridge rectifier with a large value capacitor ( $\gg 10 \mu\text{F}$ )



# Unregulated Power Supply

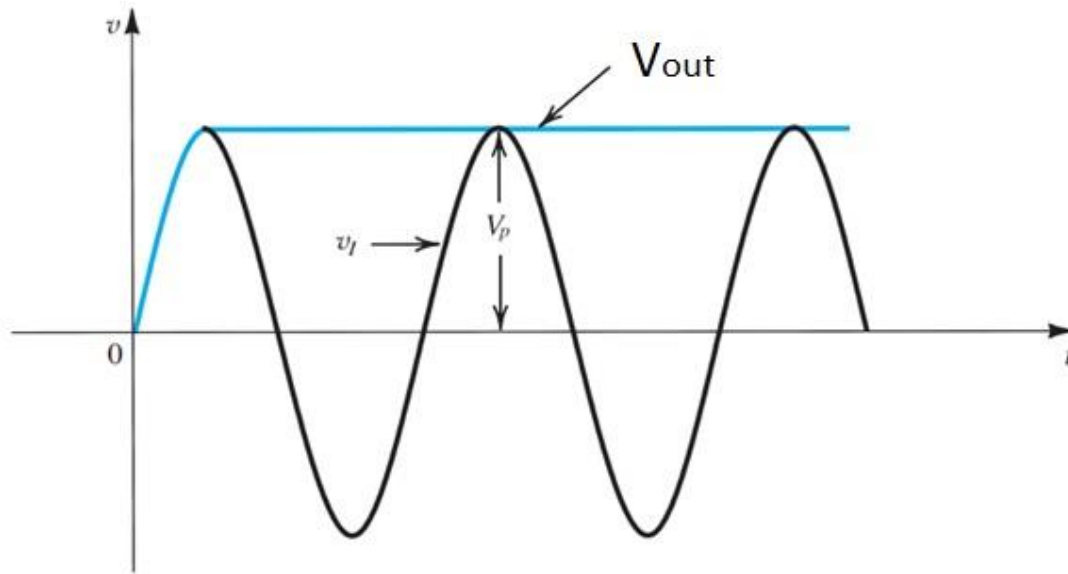
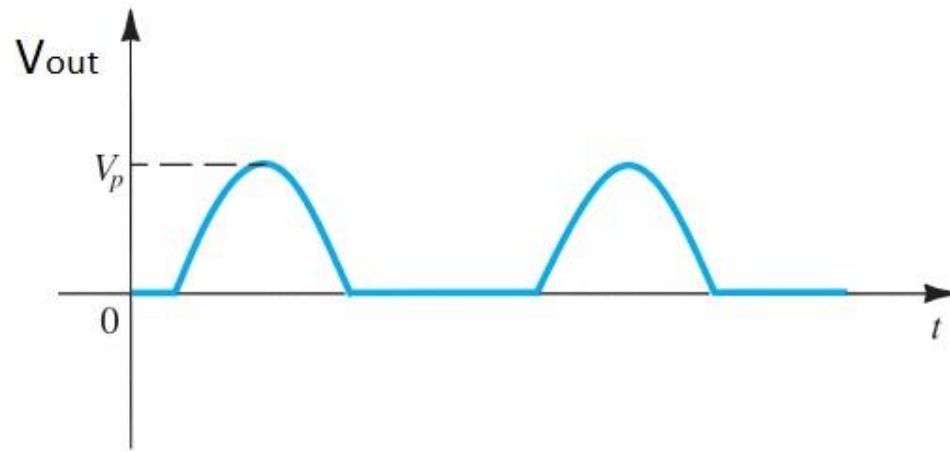
(Using Half-wave Rectifier and a Capacitive filter)



Note:

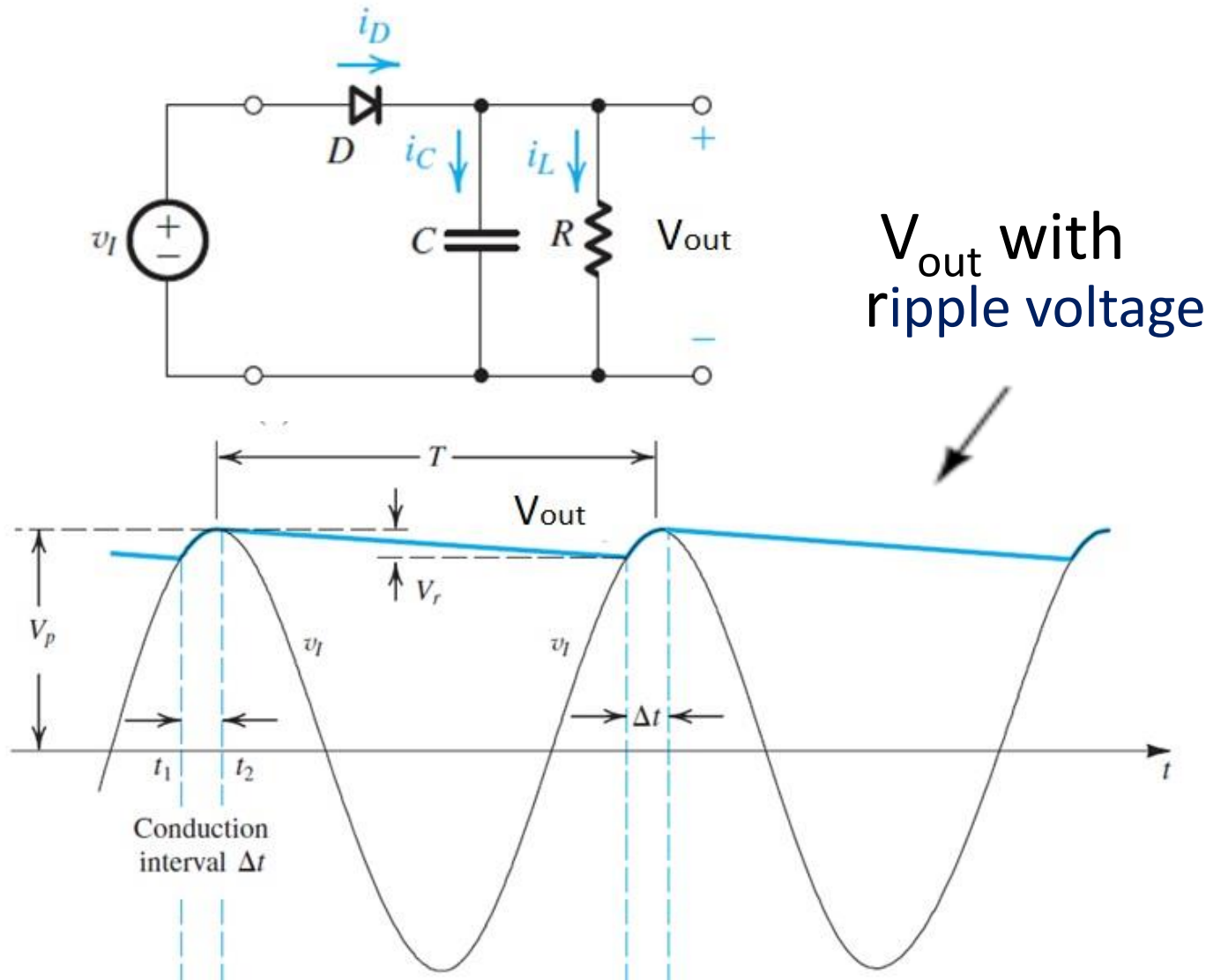
- Large value capacitors are usually "electrolytic" type capacitors, with the terminals having + and - polarities and should be connected across a dc voltage with matching terminal polarities.

Fig. 7



When there is no load (or open circuit),  $V_{out}$  has no ripple (i.e.  $V_{out}$  is a constant dc voltage)

Fig. 8

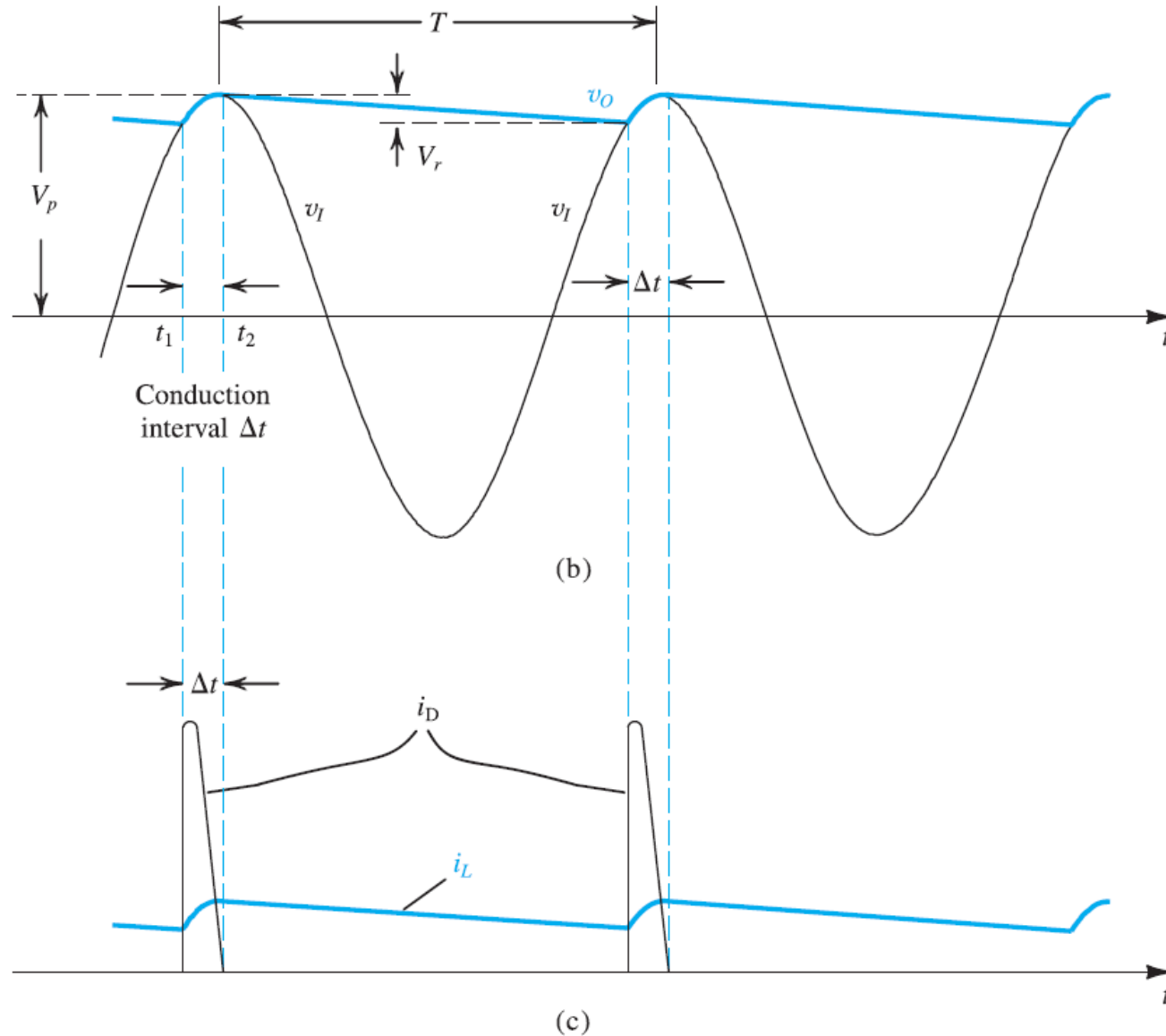


- The half-wave rectifier with C is very seldom used due to its higher ripple voltage

Fig. 9

## Operation with C across $R_L$

- C charges during  $\Delta_t$ , and discharges during  $(T - \Delta_t)$ .
- Ripple voltage,  $V_r$  increases with  $i_L$  (load current).
- Ripple voltage can be decreased by increasing C (not a good solution).
- For a given  $i_L$ , as  $C \uparrow$ ,  $\Delta_t \downarrow$  (which will make  $i_D \uparrow \uparrow$ )



- ### Operation with C across $R_L$
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  - For a given  $i_L$ , as  $C \uparrow$ ,  $\Delta_t \downarrow$  (which will make  $i_D \uparrow \uparrow$ )

# Unregulated Power Supply

(Using Full-wave Bridge Rectifier and a Capacitive filter)

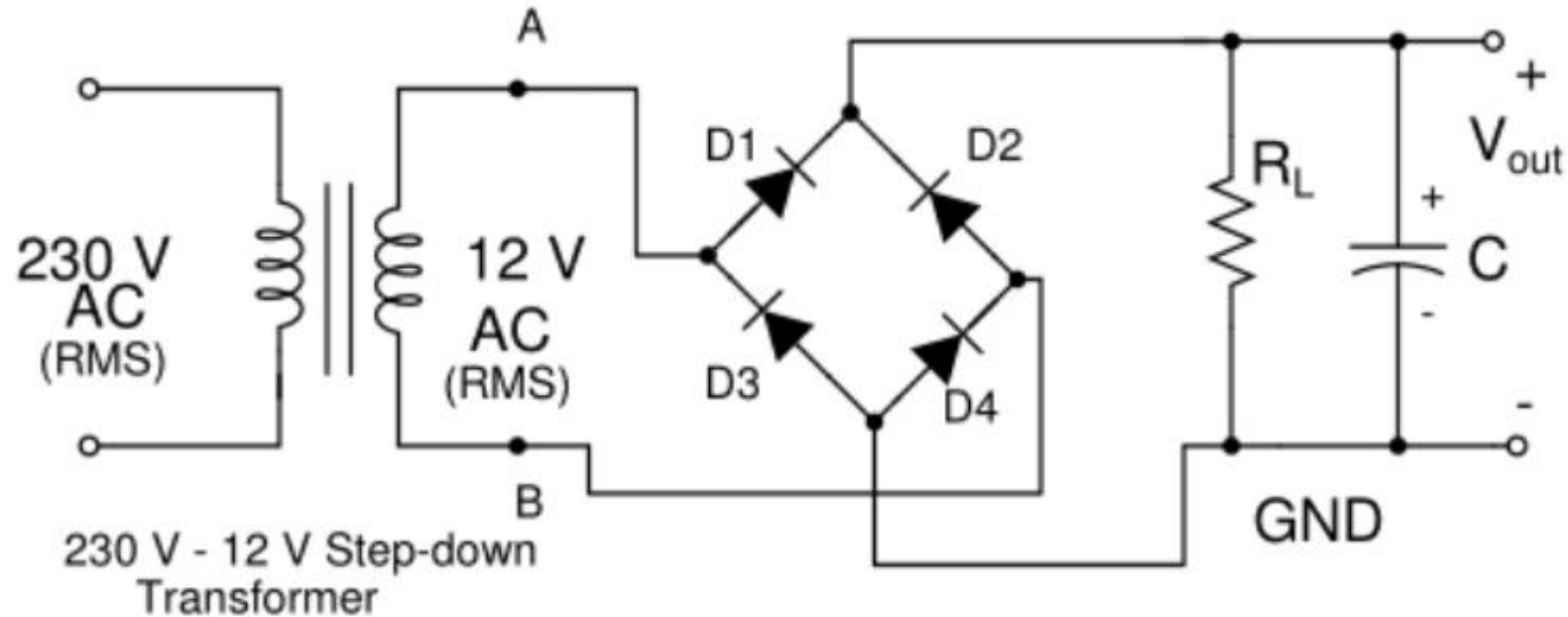


Fig. 10

- Much better than the half-wave (HW) rectifier
  - For the same  $C$  and  $R_L$ , peak-to-peak ripple voltage gets reduced to half that of HW

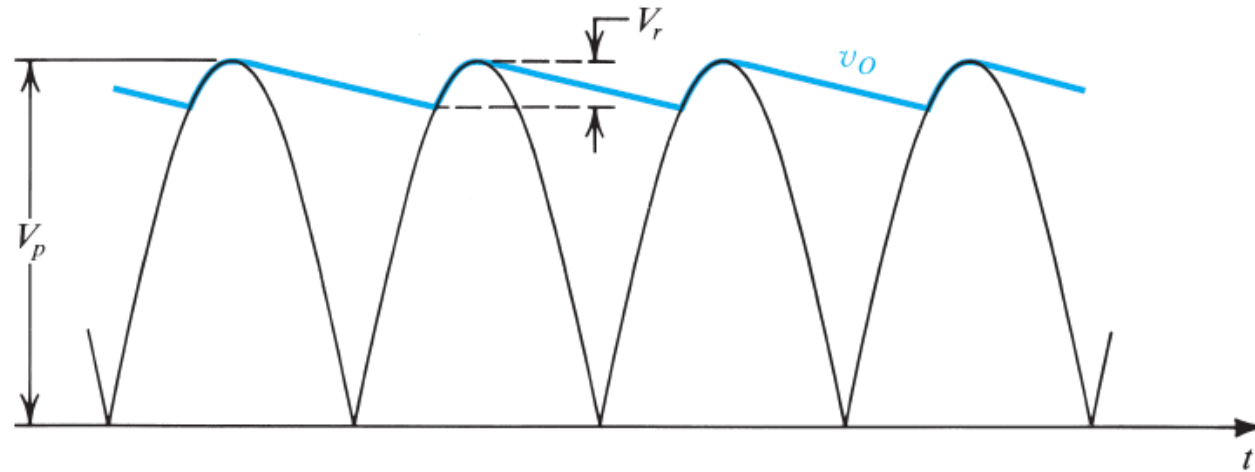
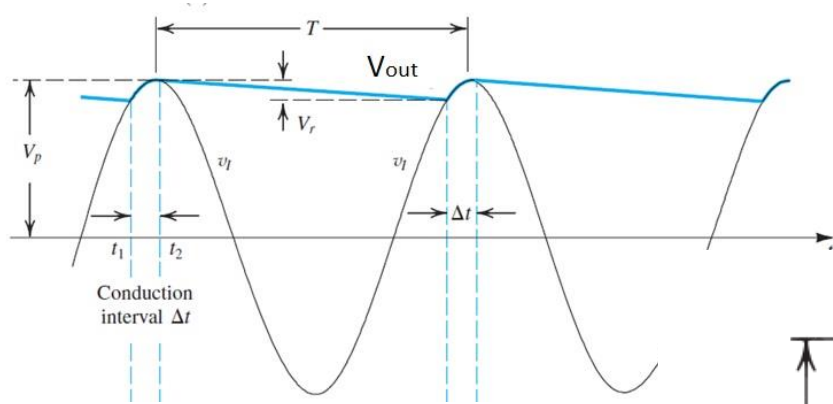
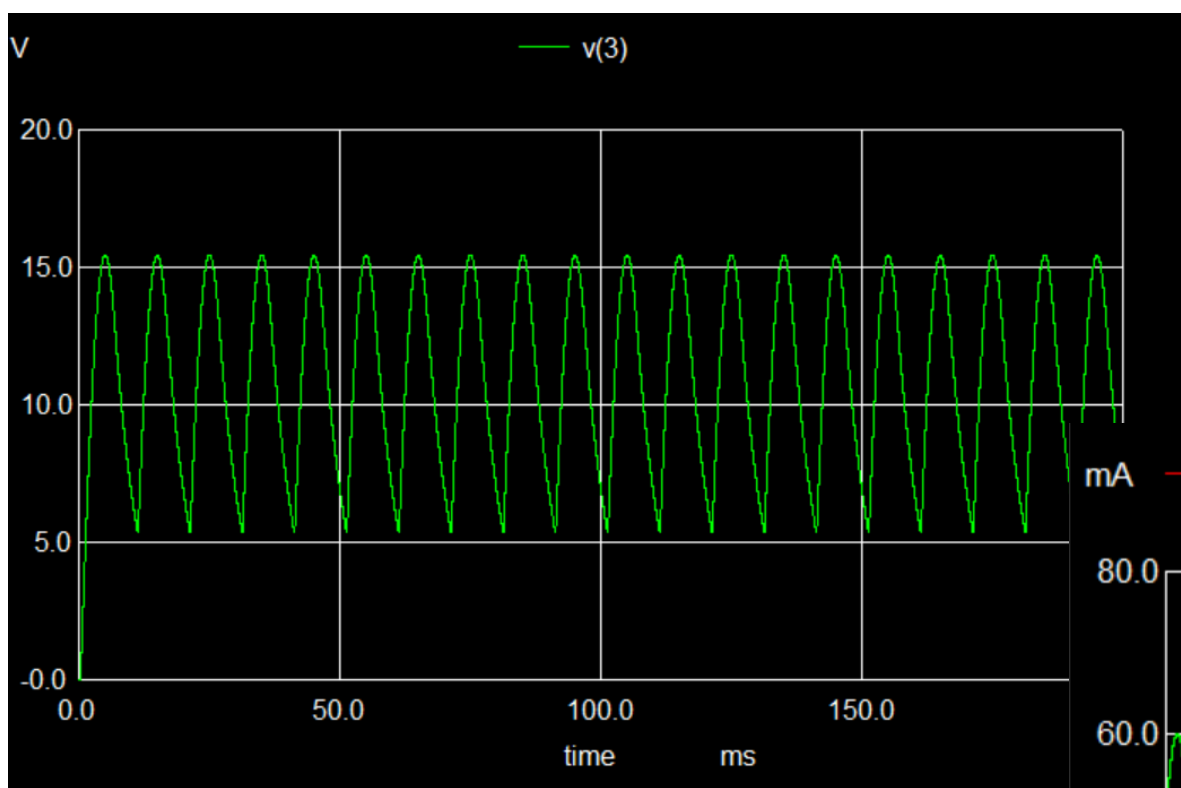


Fig. 11

- Full-wave rectifier output waveform (blue)
- Less Ripple voltage, compared to the Half-wave rectifier circuit
  - Discharge interval for C almost half that of HW case)

# NGSPICE Simulation Results (Bridge Rectifier)

- To show the effect of changing  $C$ 
  - on  $V_{\text{out}}$
  - on the diode currents
- Four values of  $C$  considered ( $R_L = 500 \, \Omega$ ,  $V_{\text{in(peak)}} = 17 \, \text{V}$ )
  - $C = 10 \, \mu\text{F}$
  - $C = 50 \, \mu\text{F}$
  - $C = 100 \, \mu\text{F}$
  - $C = 1000 \, \mu\text{F}$

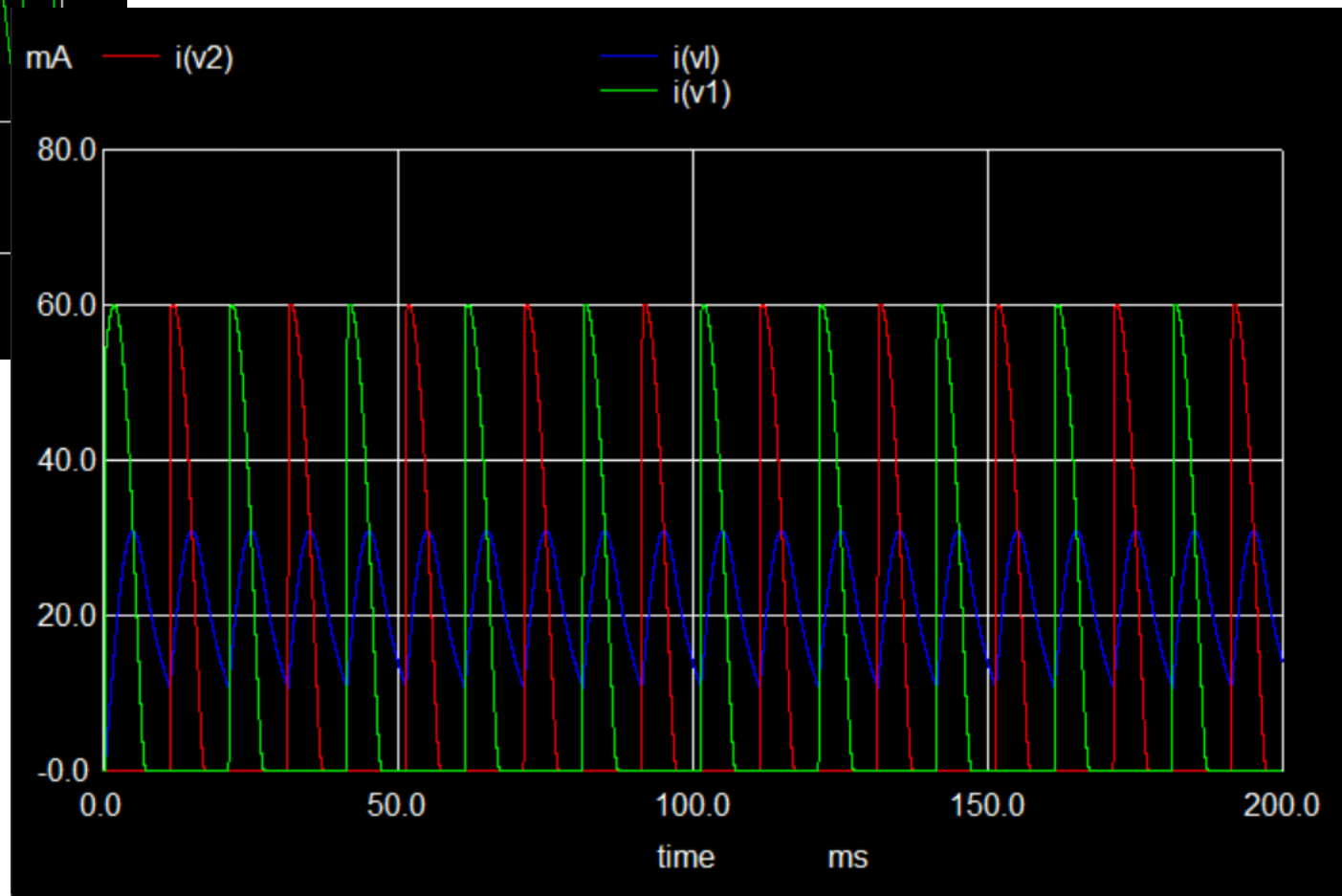


↑  
 $V_{out}$

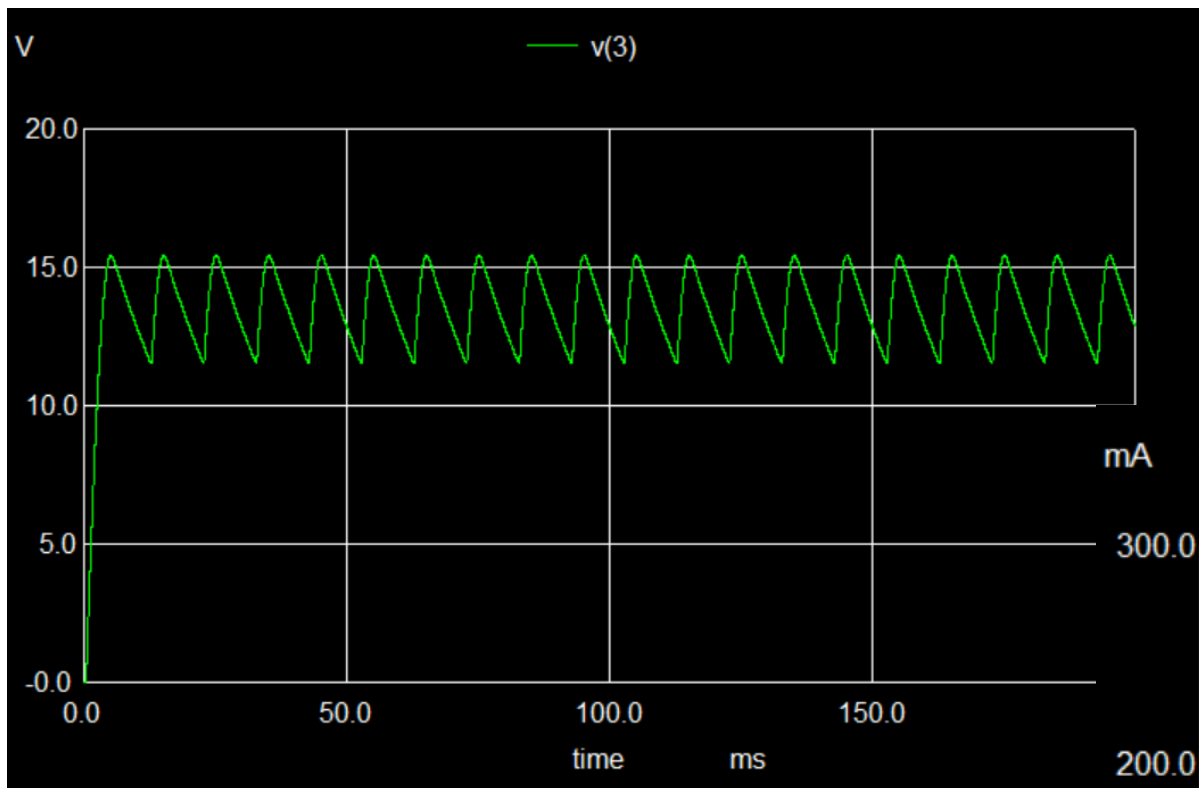
→  
Load current  $I_L$   
and the Diode  
currents

- NGSPICE Simulation - the effect of  $C$  on
  - Output ripple voltage
  - Diode currents

- $V_{in(peak)} = 17\text{ V}$
- $C = 10\text{ }\mu\text{F}; R_L = 500\text{ ohms}$
- $I_L = V_{out(avg)} / R_L \approx 20\text{ mA}$
- Peak-to-peak ripple  $\approx 10\text{ V}$





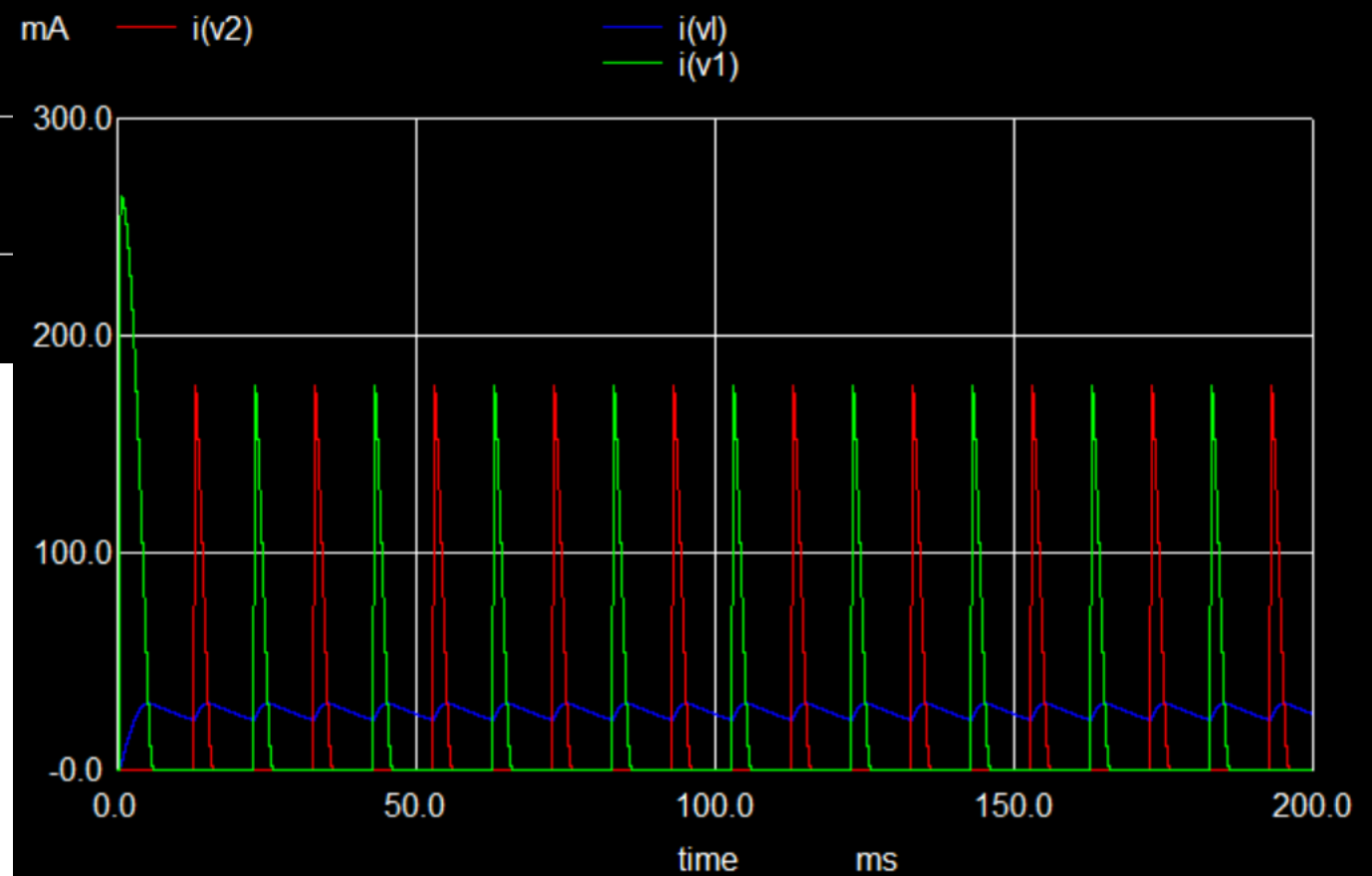


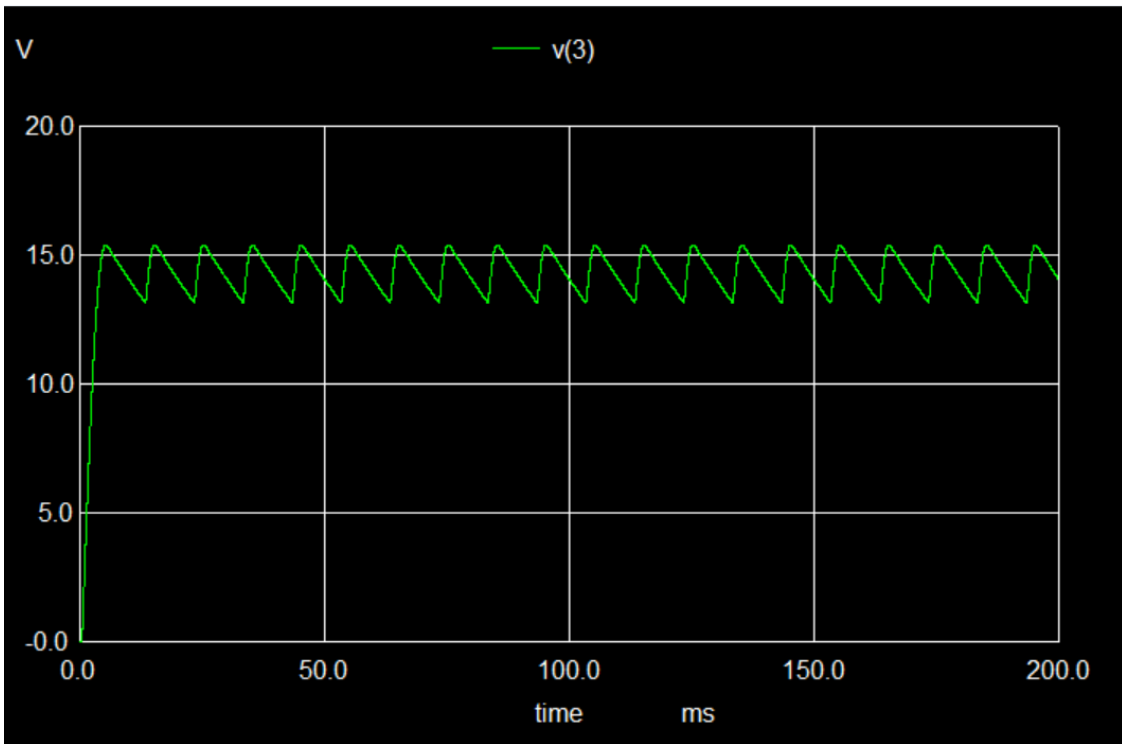
↑  
 $V_{out}$

→  
Load current  $I_L$   
and the Diode  
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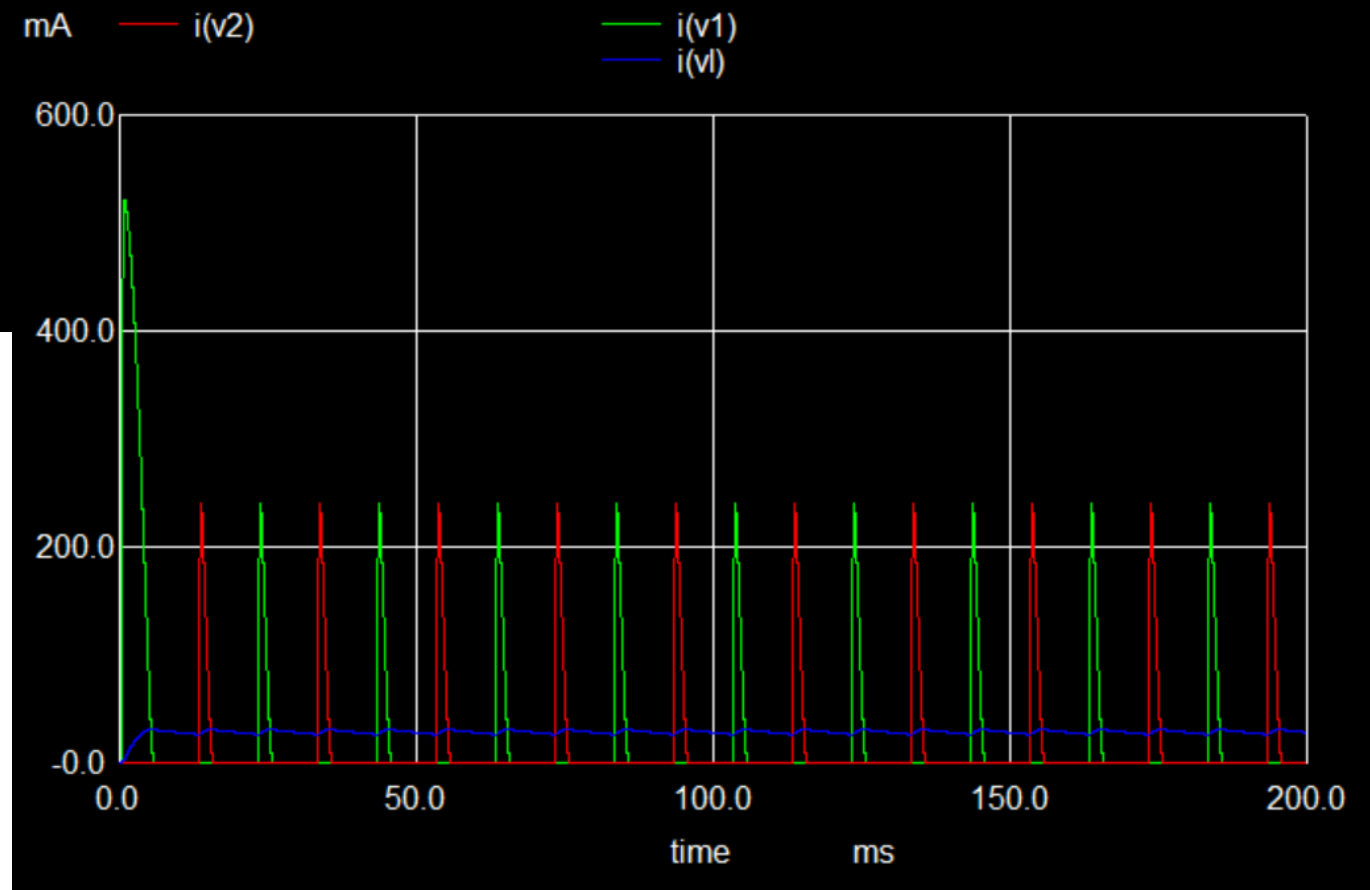
- NGSPICE Simulation - the effect of  $C$  on
  - Output ripple voltage
  - Diode currents

- $V_{in(peak)} = 17\text{ V}$
- $C = 50\text{ }\mu\text{F}$ ;  $R_L = 500\text{ ohms}$
- $I_L = V_{out(avg)}/R_L \approx 26\text{ mA}$
- Peak-to-peak ripple  $\approx 3\text{ V}$





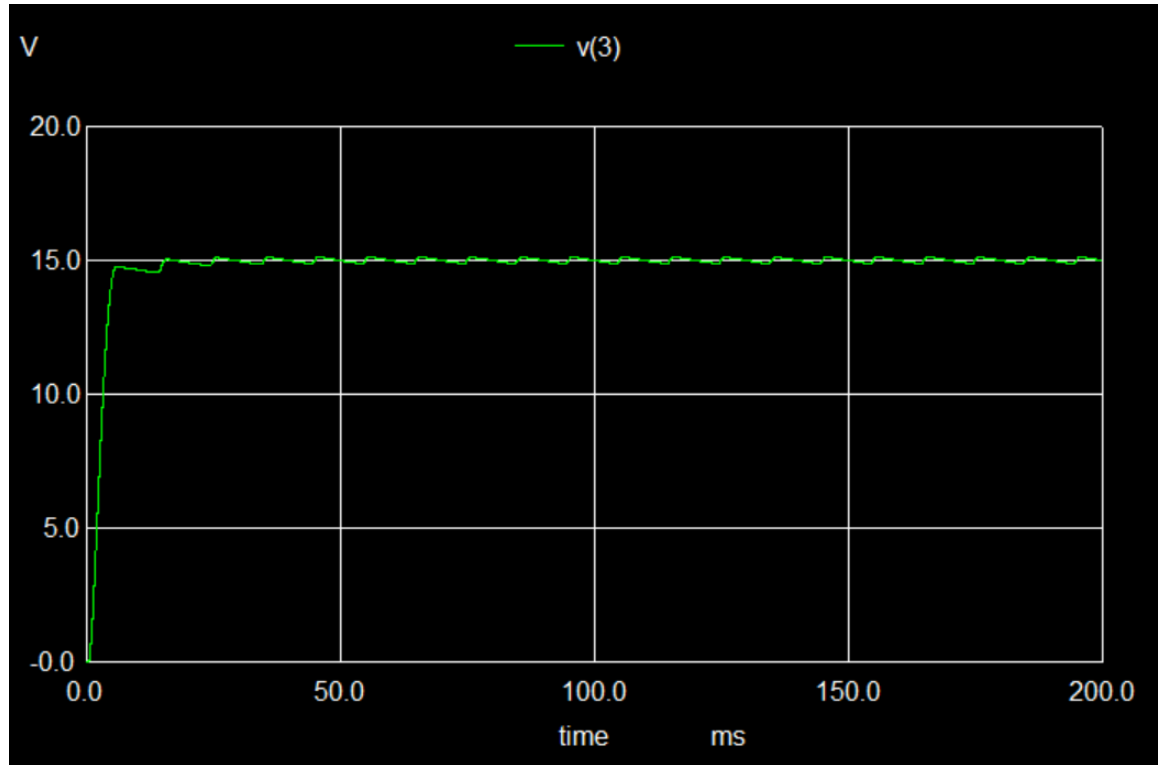
- $V_{in}(\text{peak}) = 17 \text{ V}$
- $C = 100 \mu\text{F}$  ;  $R_L = 500 \text{ ohms}$
- $I_L = V_{\text{out}(\text{avg})}/R_L \approx 28 \text{ mA}$
- Peak-to-peak ripple  $\approx 2 \text{ V}$



$V_{\text{out}}$  ↑

Load current  $I_L$   
and the Diode  
currents →

- NGSPICE Simulation - the effect of  $C$  on
  - Output ripple voltage
  - Diode currents

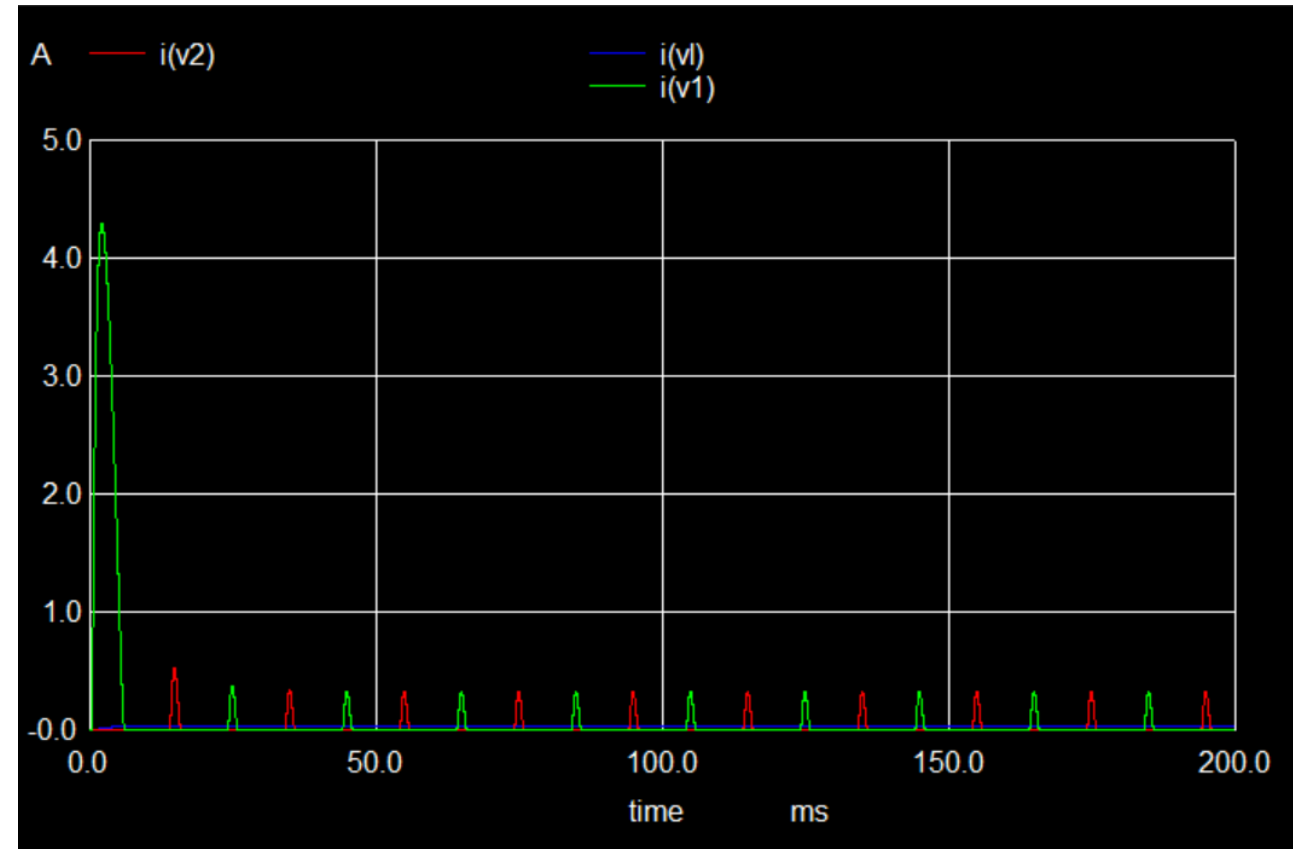


↑  
 $V_{out}$

Load current  $I_L$   
and the Diode currents →

- NGSPICE Simulation - the effect of  $C$  on
  - Output ripple voltage
  - Diode currents

- $V_{in(peak)} = 17\text{ V}$
- $C = 1,000\text{ }\mu\text{F}$  ;  $R_L = 500\text{ ohms}$
- $I_L = V_{out(avg)}/R_L \approx 30\text{ mA}$
- Peak-to-peak ripple  $\approx 0.3\text{ V}$



# Problems of Unregulated Power Supply

- Output voltage fluctuates
  - When ac input voltage fluctuates
  - When load current fluctuates
- Ripple voltage increases with load current
  - Ripple voltage for a given load current ( $i_L$ ) can be reduced only by increasing  $C$
  - Increasing  $C$  beyond a certain value can cause diode damages (as the peak diode current will always be many times the average load current)

# 3. Regulated Power Supply

- **Problems of the unregulated power supply**
  - Output voltage fluctuates with the input voltage (for a given load current) - Line regulation
  - Output voltage fluctuates for load current (for a given input voltage) - Load regulation
- **Regulated Power Supply**
  - Output voltage stays constant (reasonably well):
    - For varying input voltages
    - For varying load currents

# Two solutions

- Solution 1
  - Zener diode regulator circuit (usable for small variations in input voltage & load current)
- Solution 2
  - Voltage Regulator IC
- We will consider only Solution 2

## 3B: 7812 Three-terminal Voltage Regulator

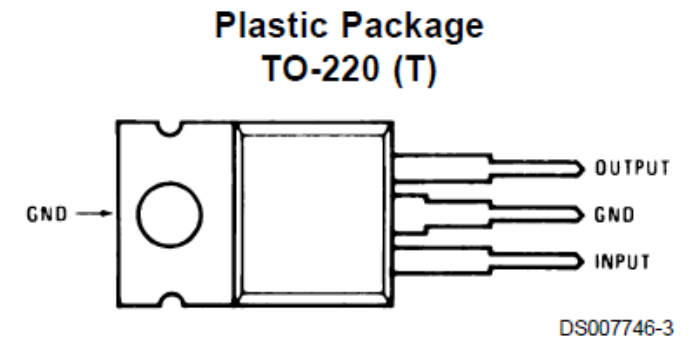
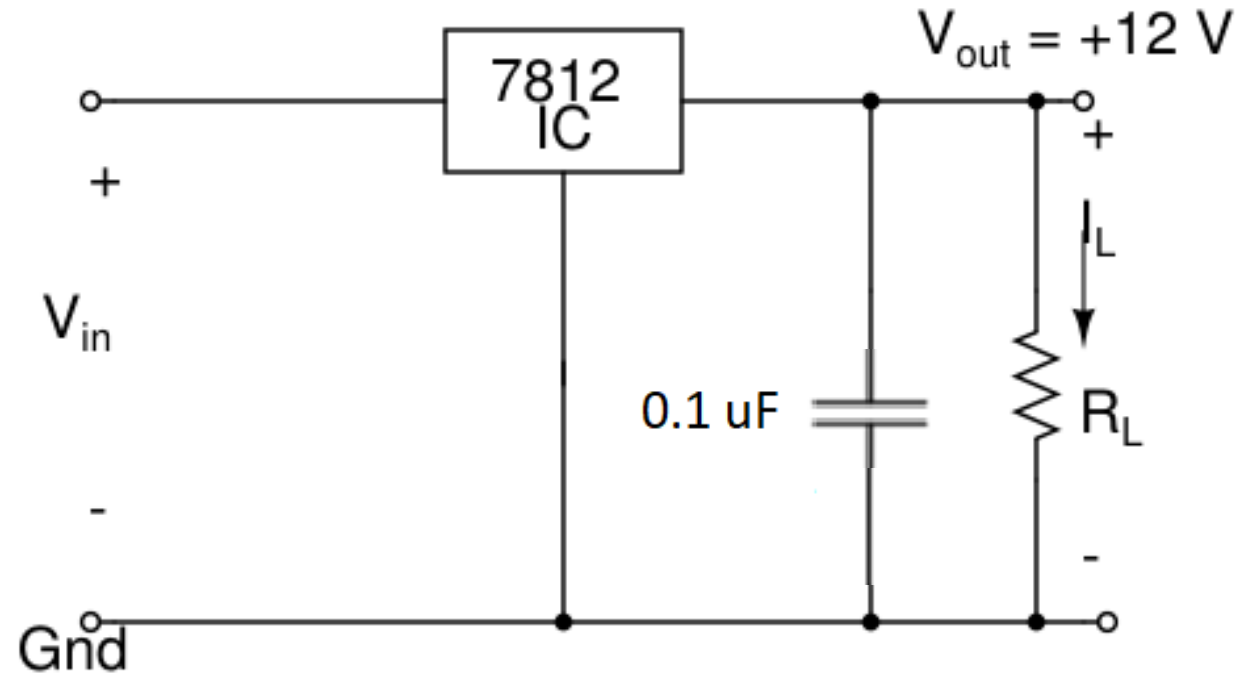


Fig. 12

$V_{in} : +14.5\text{ to }30\text{ V}$ ,  $V_{out} : 11.5\text{ to }12.5\text{ V}$

$I_L = \text{up to } 1\text{ A}$

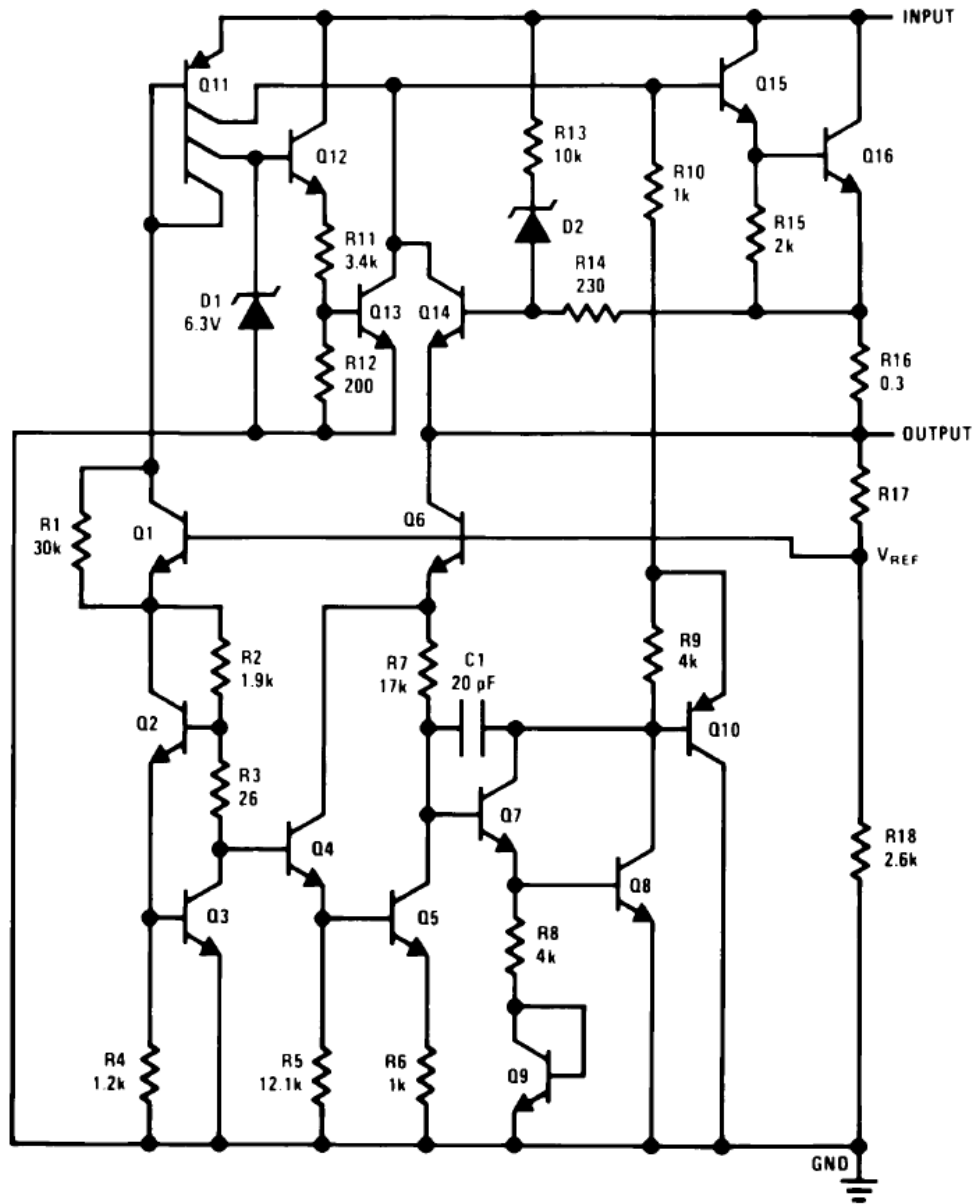


Fig. 13

DS007746-1

## Major blocks of the 7812 Voltage Regulator IC:

- Series-pass transistor (Q16)
- Stable Zener reference voltage
- Error amplifier
- Short-circuit protection

Source: 7812 Data sheet, National Semiconductor Corp., 2000



# Features of an IC Regulator

- $V_{out}$  will be steady for a large range of  $V_{in}$  and  $I_L$  values
- Minimum  $V_{in}$  to the IC regulator:  $V_{out} + 2$  or  $3$  V (typical)
- A small value of capacitor, typically  $1\ \mu\text{F}$  is put at the output for stability (i.e. to prevent oscillations)
  - The regulator IC uses a negative feedback error amplifier circuit, which could result in instability.

# Other Popular Three-terminal Voltage Regulator ICs

- Positive Voltage Regulator ICs
  1. 7805 :  $V_{\text{out}} = 5 \text{ V}$
  2. 7806 :  $V_{\text{out}} = 6 \text{ V}$
  3. 7809 :  $V_{\text{out}} = 9 \text{ V}$
- Negative Voltage Regulator ICs
  1. 7905 :  $V_{\text{out}} = -5 \text{ V}$
  2. 7906 :  $V_{\text{out}} = -6 \text{ V}$
  3. 7909 :  $V_{\text{out}} = -9 \text{ V}$
  4. 7912 :  $V_{\text{out}} = -12 \text{ V}$