

Applied Finite Element Method (ME7230)**Assignment-3**

Due Date: 2 May 2023

Maximum Marks: 50

Problem 1: 2D Poisson's problem - structured vs. trapezoidal mesh

The governing equations is

$$-\nabla^2 u = f \quad \text{on } \Omega \in [0, 1]^2 \quad \text{where } f = -6x - 10 + 60y - 12y^2$$

The exact solution is

$$u(x, y) = x^3 + 5y^2 - 10y^3 + y^4$$

The boundary conditions are

$$\text{on } \Gamma, \bar{u} = u \quad (\text{only dirichlet B.C.})$$

The weak form

$$\int_{\Omega} \nabla N^T \nabla N \, d\Omega \{u\} = \int_{\Omega} N^T f \, d\Omega$$

The domain is discretised with the 8-noded quadrilateral serendipity element as shown in Figure 1. The L_2 -norm and H_1 semi-norms are calculated for mesh sizes $h = \{1/2, 1/4, 1/8, 1/16, 1/32, 1/64\}$. Figure 2 shows the logarithmic plot of L_2 -norm and H_1 semi-norms vs. h . The calculated convergence rates are tabulated in Table 1. From

	Structured	Trapezoid
L2	2.9994	2.4936
H1	1.9994	1.3941

Table 1: convergence rates: structured vs. trapezoidal meshes

the Table 1, the calculated convergence rates for structured mesh are 2.9994 and 1.9994, which are close to expected values 3 and 2, respectively. Whereas for the trapezoidal mesh, the calculated convergence rates are 2.4936 and 1.3941, which are significantly lower than the expected values 3 and 2, respectively. From this, it can be concluded that distorted elements have a lower convergence rate than rectangular elements. And also, the error in the case of trapezoidal mesh is always higher than the structured mesh.

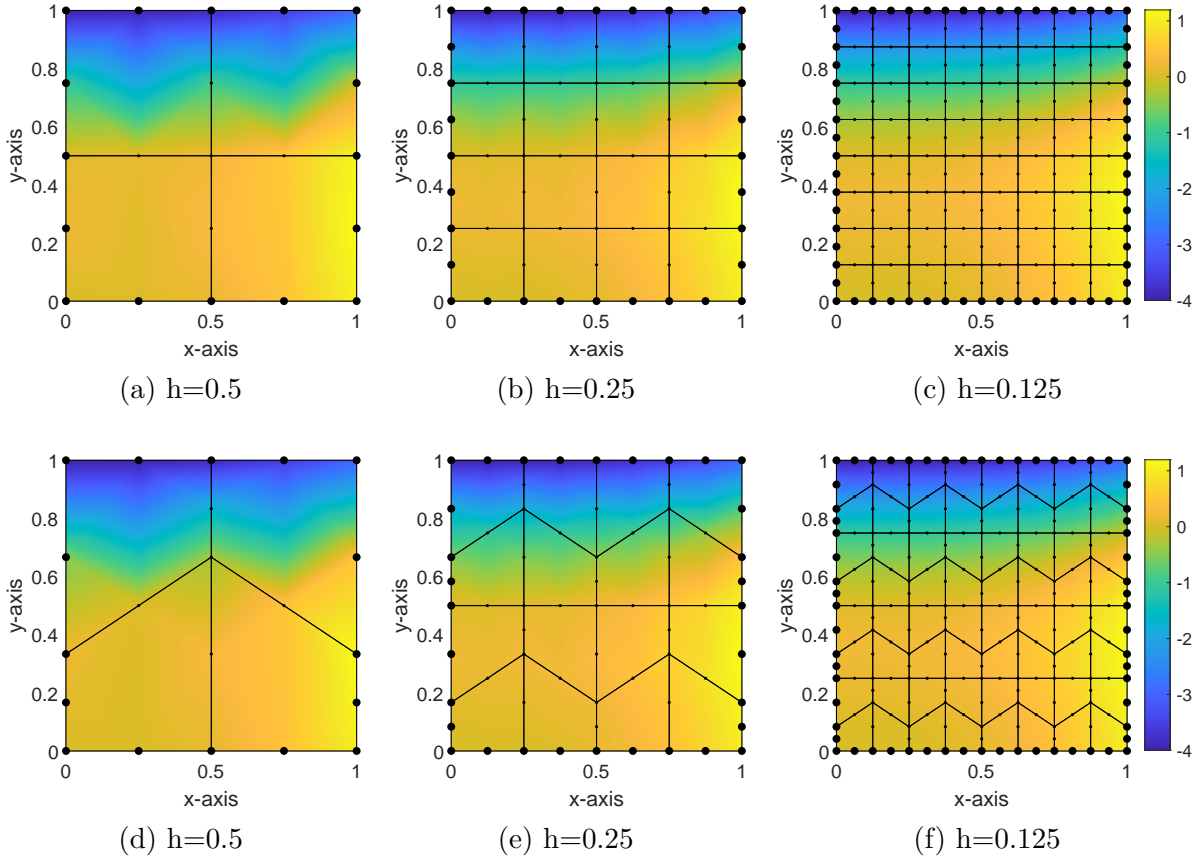


Figure 1: Structured(a,b,c) and trapezoidal(d,e,f) sample meshes

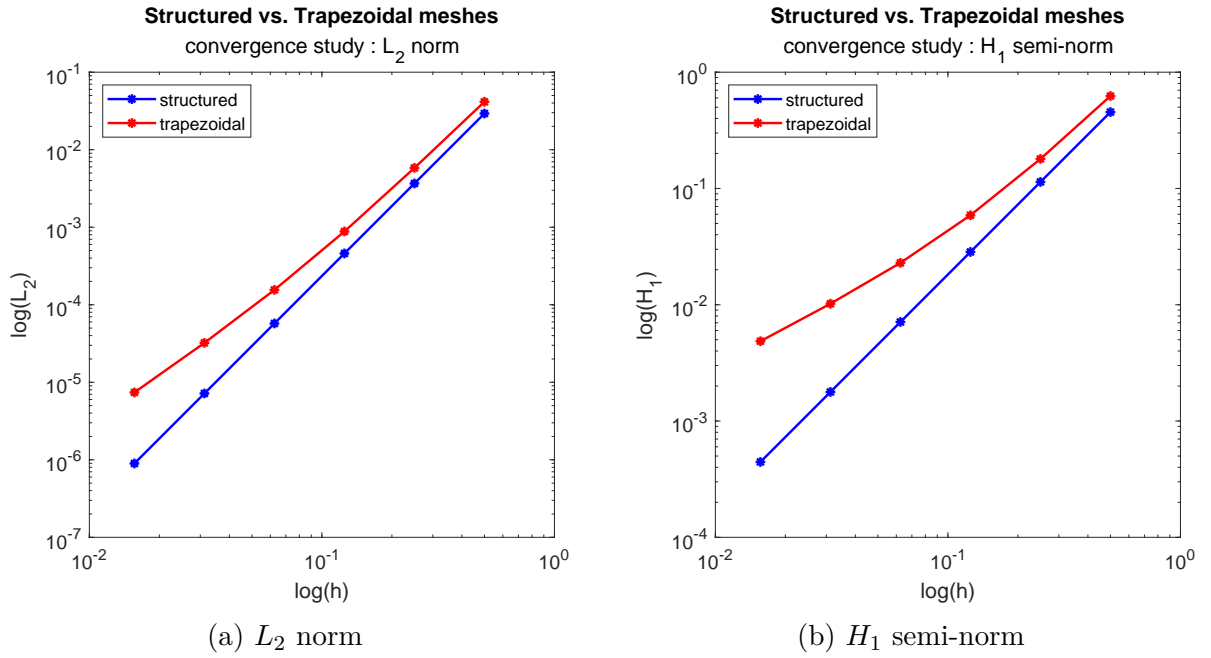


Figure 2: logarithmic plot of (a) L_2 norm and (b) H_1 semi-norm for different mesh discretisations (structured vs. trapezoidal elements)

Problem 2: 2D Acoustic Problem

The acoustic wave equation is

$$\Delta p' - \frac{1}{c^2} \frac{\partial^2 p'}{\partial t^2} = 0 \quad (1)$$

by assuming a harmonic solution,

$$p' = p e^{i\omega t} \implies \frac{\partial^2 p'}{\partial t^2} = -p \omega^2 e^{i\omega t}$$

from Equation 1

$$\begin{aligned} \implies e^{i\omega t} \nabla^2 p - \frac{1}{c^2} (-p \omega^2 e^{i\omega t}) &= 0 \\ \implies \nabla^2 p + k^2 p &= 0 \quad \text{where } k^2 = \frac{\omega^2}{c^2} \quad (\text{the Helmholtz equation}) \end{aligned}$$

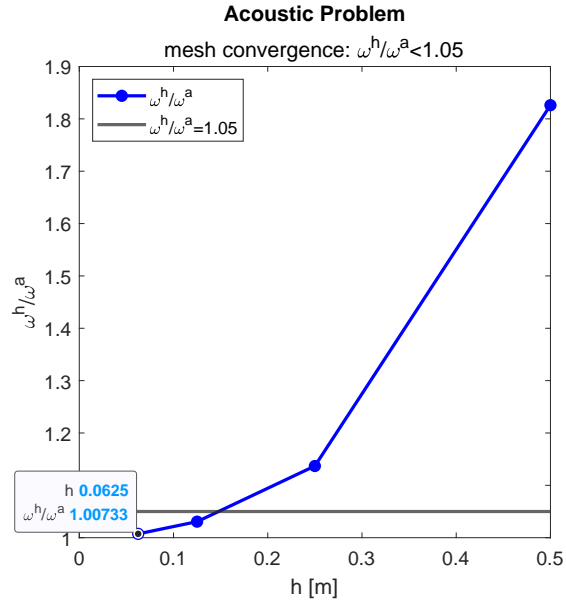
The weak form

$$\begin{aligned} \implies \left[\int_{\Omega} \nabla N^T \cdot \nabla N d\Omega - \int_{\Omega} N^T k^2 N d\Omega \right] \{p\} &= \underbrace{\int_{\partial\Omega} N^T \nabla p \cdot \hat{n} d\Omega}_{\text{natural B.C.}} \\ \implies \int_{\Omega} \nabla N^T \cdot \nabla N d\Omega - \int_{\Omega} N^T k^2 N d\Omega &= 0 \quad \because \text{zero Neumann B.C.} \\ \implies K - \omega^2 M &= 0 \quad \text{where } K = \int_{\Omega} \nabla N^T \cdot \nabla N d\Omega, \quad M = \int_{\Omega} N^T \frac{1}{c^2} N d\Omega \end{aligned}$$

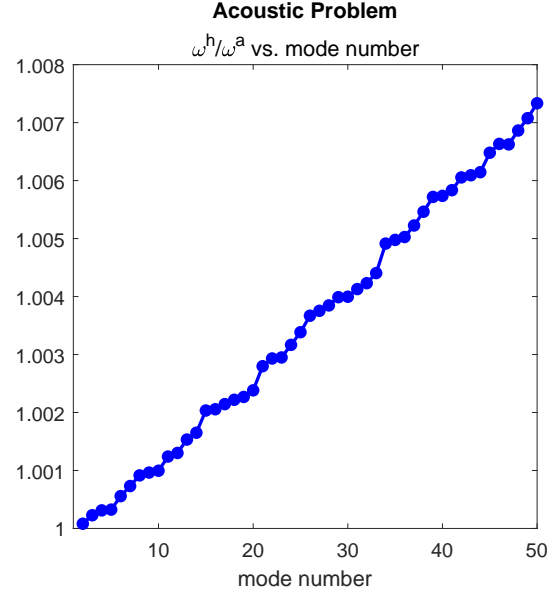
for a rectangular domain of length L and width D , the exact eigenmodes and eigenvalues are

$$\begin{aligned} \phi_{mn} &= \cos \frac{m\pi x}{L} \cos \frac{n\pi y}{D} \\ f_{mn} &= \frac{c}{2} \sqrt{\left(\frac{m}{L}\right)^2 + \left(\frac{n}{D}\right)^2} \quad m, n = \{0, 1, 2, 3, \dots\} \quad \text{where } f = \frac{\omega}{2\pi} \end{aligned}$$

for $L = 5$ m, $D = 3$ m and $c = 340$ m/s, the ratio of numerically computed frequency to the analytical frequency (ω^h/ω_{ana}) as a function of mode number is plotted in Figure 3



(a) mesh convergence



(b) first 50 frequencies

Figure 3: 2D acoustic problem

Problem 3: Cylindrical pipe subjected to internal pressure