

CT303 - Digital Communications

Lecture 24 : 7 December 2020

* Lecture 23 recap

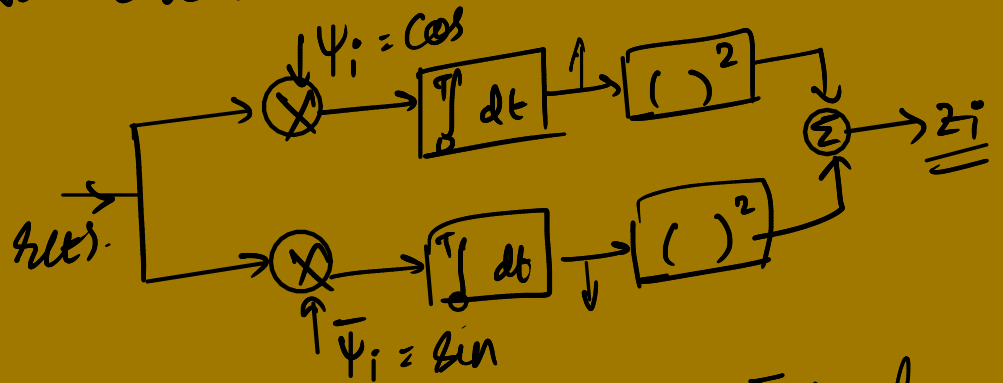
- Difference between Coherent and Non-Coherent detection

① Differential DPSK (Differential detection of differentially encoded PSK).

② Non-Coherent Orthogonal FSK

$$\underline{f_{i+1} - f_i = \frac{1}{T} //}$$

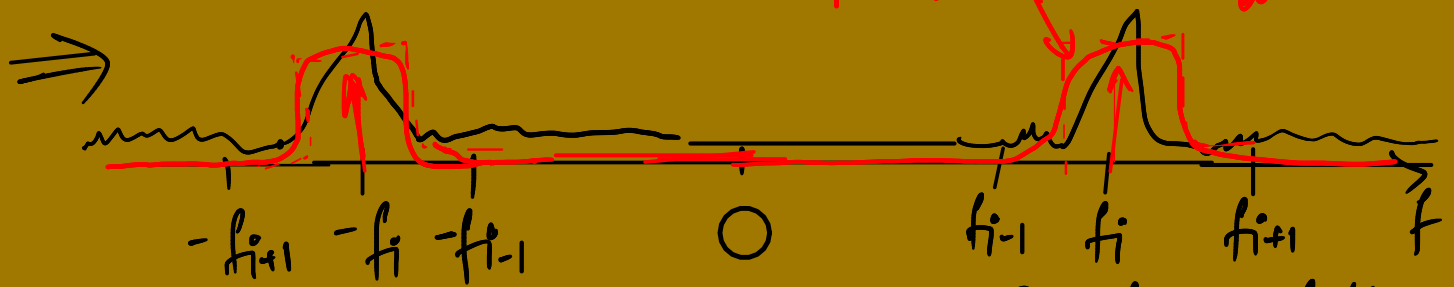
- Non-Coherent FSK demodulator.



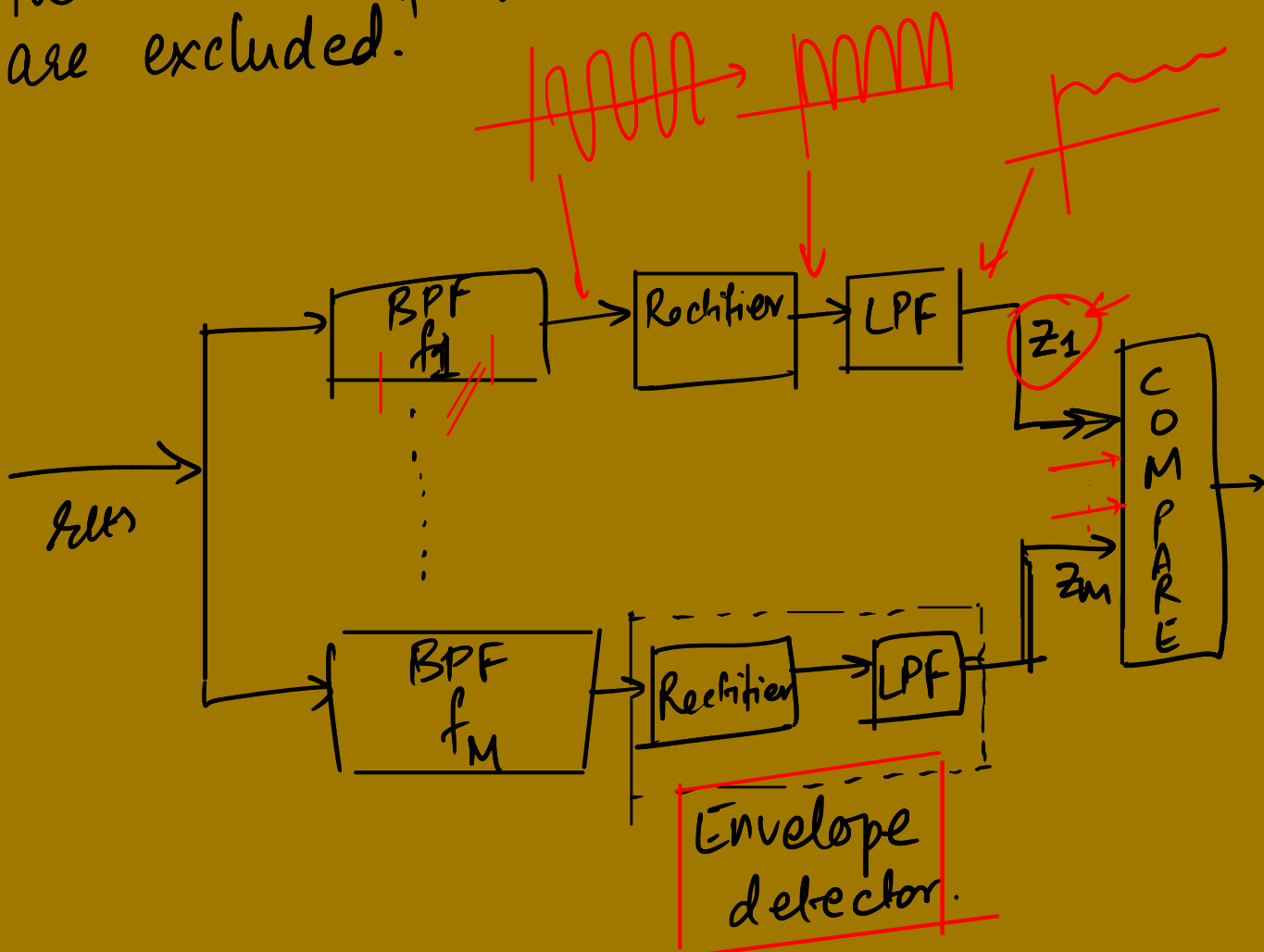
1 - Akm of the NC FSK demod

* Non-Coherent FSK demodulator 2.

- * We expect the amplitude spectrum of the received signal $r(t) = \sqrt{\frac{2E_b}{T}} \cos(\omega_i t + \phi) + \eta(t)$ (AWGN) when s_i was transmitted, to have higher values on and around ω_i (or f_i):



- * This can be detected using a Band pass filter centered at f_i , with a cut-off frequency that ensures frequencies close to f_{i-1} & f_{i+1} are excluded.



* Modulators

* Irrespective of whether we are using frequency, phase or amplitude modulation, the transmitted waveform is of the form:

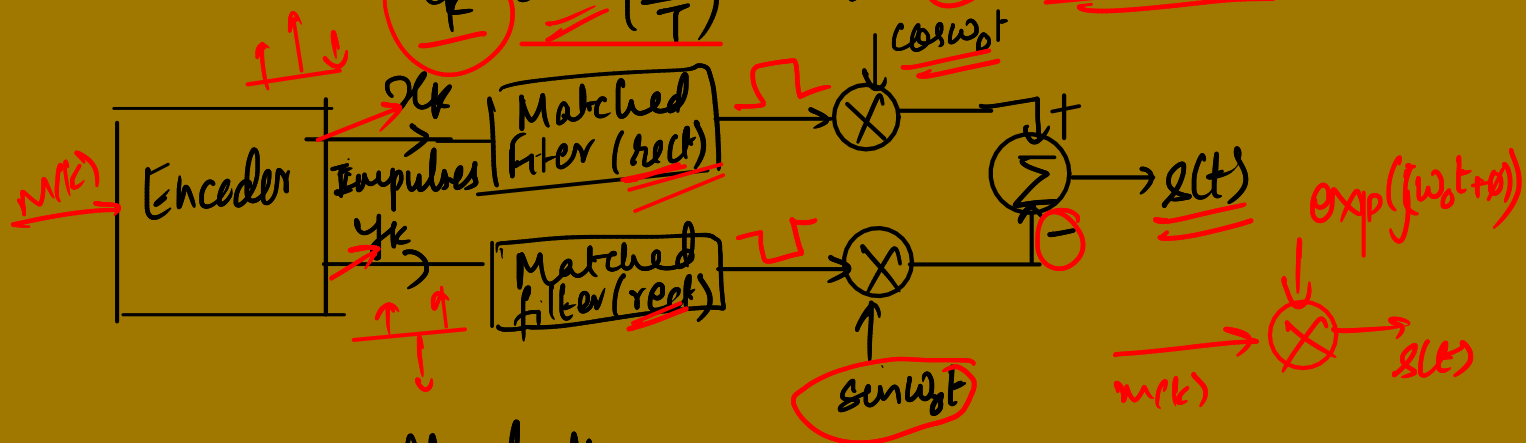
$$S(t) = A \cos(\omega t + \phi) = \text{Re}\{e^{j(\omega t + \phi)}\}$$

$$* S(t) = A(\cos \omega t \cos \phi - \sin \omega t \sin \phi)$$

$$= \underbrace{A \cos \phi}_{x_k} \underbrace{\cos \omega t}_{\text{Carrier (In phase component)}} - \underbrace{A \sin \phi}_{y_k} \underbrace{\sin \omega t}_{\text{Carrier (Quadrature component)}}$$

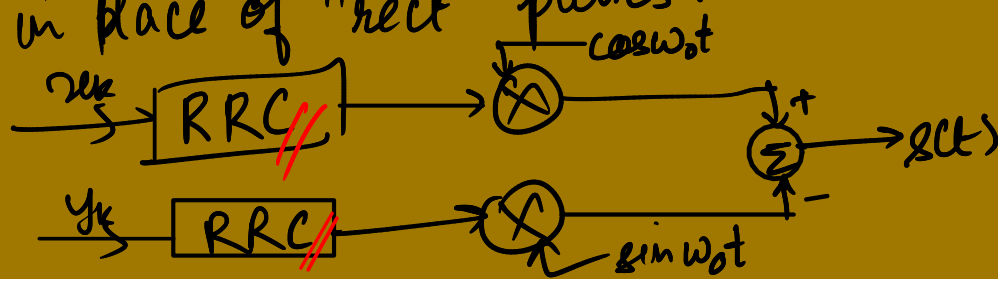
$$= x_k \cos \omega t - y_k \sin \omega t \quad 0 \leq t \leq T$$

$$= x_k \text{rect}\left(\frac{t}{T}\right) \cos \omega t - y_k \text{rect}\left(\frac{t}{T}\right) \sin \omega t$$



* This is called the "Quadrature Modulator."

* One can also use appropriate Pulse shaping filters in place of "rect" pulses.



* Quadrature Demodulator

Ideally, $x(t) = x_k \cos \omega_0 t - y_k \sin \omega_0 t$

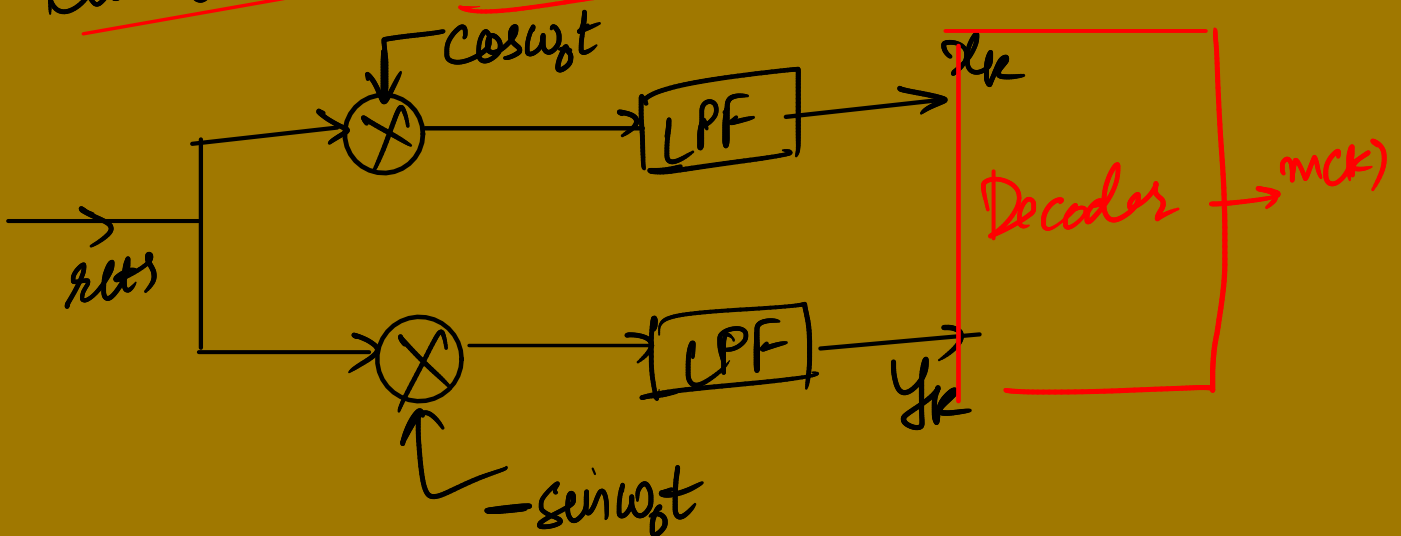
$$\begin{aligned} \underline{x(t) \cos \omega_0 t} &= x_k \cos^2 \omega_0 t - y_k \sin \omega_0 t \cos \omega_0 t \\ &= \underline{x_k \left(\frac{1 + \cos(2\omega_0 t)}{2} \right) - y_k \frac{\sin(2\omega_0 t)}{2}} \end{aligned}$$

* Passing $x(t) \cos \omega_0 t$ through a LPF (cut-off $< 2\omega_0$) we get

$$\frac{x_k}{2} //$$

* Similarly passing $x(t) \sin \omega_0 t$ through a LPF, gives $-y_k/2$.

* Quadrature Demodulator:



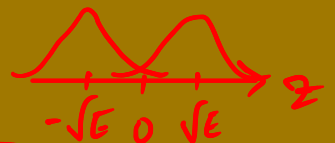
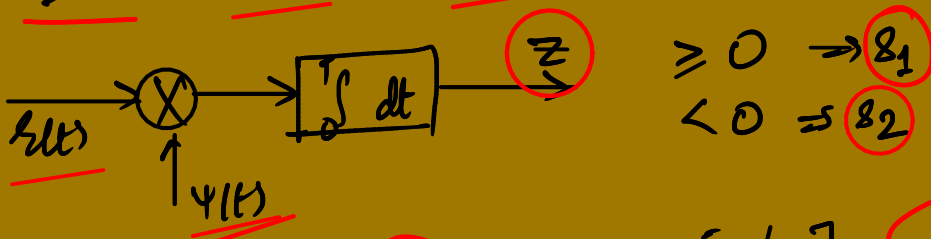
* ERROR PERFORMANCE

1. Binary Bandpass Modulation Systems

(i) Coherently detected BPSK

Let $\psi(t) = \sqrt{\frac{2}{T}} \cos \omega_c t$.

$s_1(t) = \sqrt{E} \psi(t)$, $s_2(t) = -\sqrt{E} \psi(t)$



$a_1 = E[Z/s_1] = \sqrt{E}$, $a_2 = E[Z/s_2] = -\sqrt{E}$

* $P_B = Q\left(\frac{a_1 - a_2}{2\sigma_0}\right)$, $\sigma_0^2 = \text{Noise Variance}$.

$P_B = Q\left(\sqrt{\frac{E_d}{2N_0}}\right)$ // \rightarrow energy of the difference signal $(s_1 - s_2)$

$E_d = (2\sqrt{E})^2 = 4E = 4E_b$

$\therefore P_B = Q\left(\sqrt{\frac{4E_b}{2N_0}}\right) = Q\left(\sqrt{\frac{2E_b}{N_0}}\right)$ (Case of Antipodal Signals) $\rightarrow \approx NRZ-L$

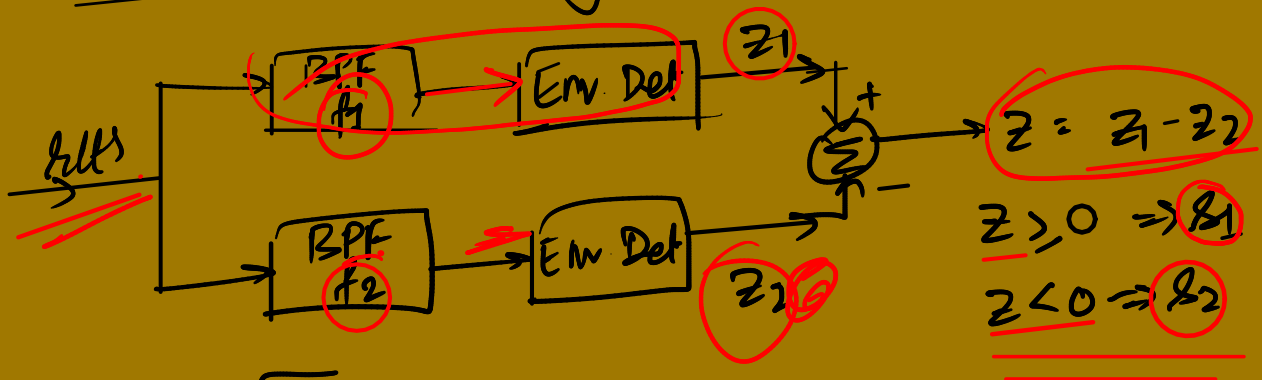
(ii) Coherently detected BFSK (Orthogonal)

$P_B = Q\left(\sqrt{\frac{E(1-P)}{N_0}}\right)$ // $(P(s_1) = P(s_2) = 1/2)$ $\rightarrow \angle s_1, s_2$

- For orthogonal signals, $P = 0$

$\therefore P_B = Q\left(\sqrt{\frac{E}{N_0}}\right)$

(iii) Non-Coherent Binary FSK ←



$$s_1(t) = \sqrt{\frac{2E}{T}} \cos(\omega_1 t) \leftarrow$$

$$s_2(t) = \sqrt{\frac{2E}{T}} \cos(\omega_2 t) \leftarrow$$

$$P_B = P(s_1) \cdot P(e|s_1) + P(s_2) P(e|s_2) \leftarrow$$

$$\text{Assuming } P(s_1) = P(s_2) = 1/2$$

$$P_B = 1/2 P(e|s_1) + 1/2 P(e|s_2) \checkmark$$

$$P(e|s_1) = P(z_2 > z_1 | s_1)$$

$$P(e|s_2) = P(z_1 > z_2 | s_2)$$

$$\text{Also, } E[z_1 | s_1] = \sqrt{\frac{2E}{T}}, \quad E[z_2 | s_2] = \sqrt{\frac{2E}{T}}$$

$$E[z_1 | s_2] = 0, \quad E[z_2 | s_1] = 0 //$$

$$P(z = z_1 - z_2 | s_1) = P(-z = z_2 - z_1 | s_2) \rightarrow \textcircled{1}$$

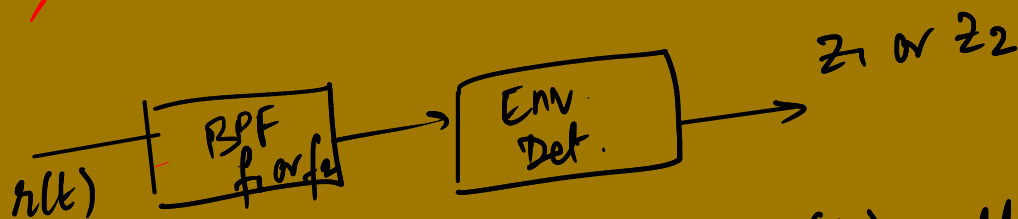
$$\therefore P_B = 1/2 P(e|s_1) + 1/2 P(e|s_2)$$

From $\textcircled{1}$,

$$P(e|s_1) = P(z < 0 | s_1) = P(z > 0 | s_2) = P(e|s_2)$$

$$P_B = P(e|s_2) = P(z > 0 | s_2) = P(\underline{z_1} > \underline{z_2} | s_2)$$

$$P_B = \int_{-\infty}^{\infty} P(z_2 | s_2) \left(\int_{z_2}^{\infty} P(z_1 | s_2) dz_1 \right) dz_2 \leftarrow$$



* When s_2 is transmitted, B.P.F (f_2) will allow the signal component of s_2 to pass through along with the noise in the B.W of the filter. $\rightarrow \underline{z_2} = s_2 + n$

* But the output of B.P.F (f_1) will eliminate s_2 , and allow only the noise in the B.W of the filter f_1 . $\rightarrow \underline{z_1} = n$.

* Since the Envelope detector is a nonlinear device, if the i/p to it is a Gaussian R.P., the o/p is not Gaussian.

* When s_2 is transmitted, the o/p of the Envelope detector connected to B.P.F f_2 is known to have a Rician distribution, i.e.,

$$P(\underline{z_2} | s_2) = \frac{\underline{z_2}}{\sigma_0^2} e^{-\frac{(\underline{z_2}^2 + A^2)}{2\sigma_0^2}} I_0\left(\frac{\underline{z_2} A}{\sigma_0^2}\right), \underline{z_2} \geq 0$$

$$= 0, \underline{z_2} < 0,$$

Where $A = \sqrt{\frac{2E}{T}}$, σ_0^2 is Noise power at B.P.F o/p, ...

... and $I_0(x)$ is the modified zero-order Bessel function of the first kind, defined as

$$I_0(x) = \frac{1}{2\pi} \int_0^{2\pi} \exp(x \cos \theta) d\theta //$$

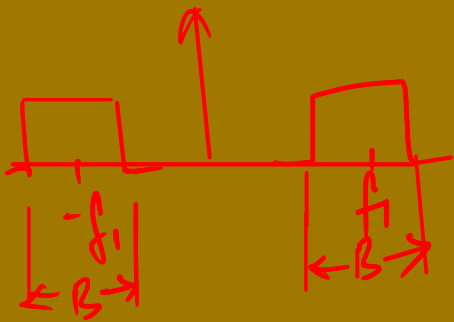
* Similarly, When the o/p of B.P.F f_1 is connected to the Envelope detector, the o/p has a Rayleigh distribution,

$$P(z_1|s_2) = \frac{z_1}{\sigma_0^2} e^{-\frac{z_1^2}{2\sigma_0^2}}, \quad z_1 \geq 0$$

$$= 0, \quad z_1 < 0.$$

$$\therefore P_B = \int_{-\infty}^{\infty} P(z_2|s_2) \left(\int_{z_2}^{\infty} P(z_1|s_2) dz_1 \right) dz_2$$

$$= \frac{1}{2} e^{-\frac{A^2}{4\sigma_0^2}} \text{ with } A = \sqrt{\frac{2E}{T}}$$



and $\sigma_0^2 = 2 \left(\frac{N_0}{2} \right) \cdot B$, where

B is the B.P.F B.W.

$$\Rightarrow P_B = \frac{1}{2} e^{-\frac{2E}{T \cdot 4N_0 B}} = \frac{1}{2} e^{-\frac{E}{2N_0 B T}} \quad T \rightarrow \text{symbol duration}$$

* Let the B.P.F B.W B match the BW of the transmitted symbols; i.e.,

$$B = R_s(1+h).$$

$$B_{\min} = R_s = \frac{1}{T} \Rightarrow \underline{B \cdot T = 1}$$

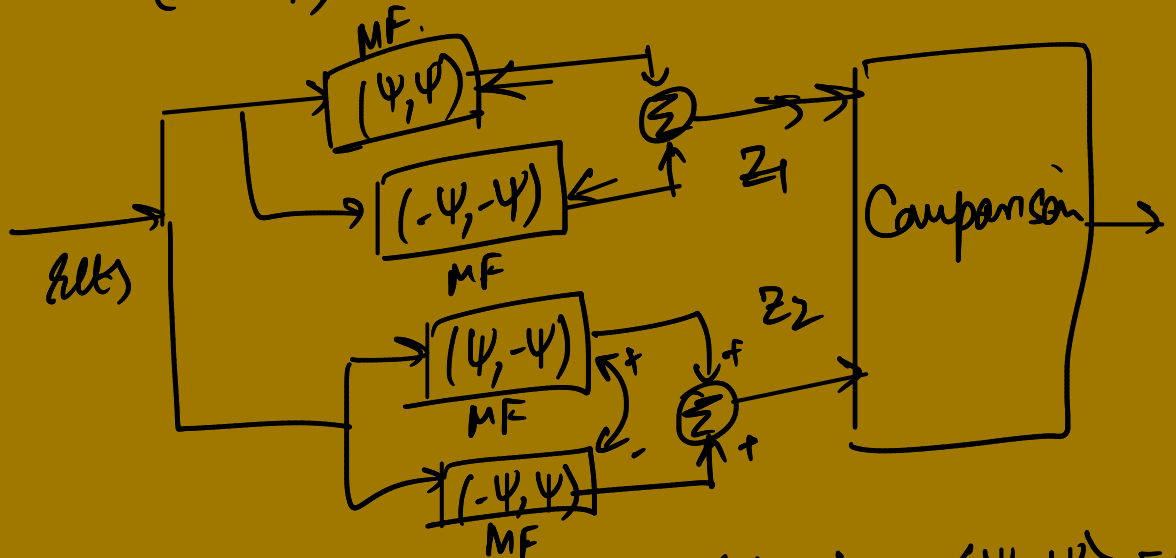
$$\Rightarrow P_B = \frac{1}{2} e^{-E/2N_0} = \frac{1}{2} e^{-E_b/2N_0}$$

(iv) Binary DPSK (Differential detection of Diff. encoded PSK).

$$\Psi(t) = \sqrt{\frac{2}{T}} \cos \omega_0 t, \quad \bar{\Psi}(t) = \sqrt{\frac{2}{T}} \sin \omega_0 t$$

Bit 0: $s_1(t) = (\Psi, \Psi) \text{ or } (-\Psi, -\Psi) \quad t \in [0, 2T]$

Bit 1: $s_2(t) = (\Psi, -\Psi) \text{ or } (-\Psi, \Psi) \quad t \in [0, 2T]$



$$\langle s_1, s_2 \rangle_{2T} = \langle (\Psi, \Psi), (\Psi, -\Psi) \rangle_{2T} = \langle \Psi, \Psi \rangle_T + \langle \Psi, -\Psi \rangle_T = 0$$

$$= 0$$

$$\Rightarrow s_1 \perp s_2$$

$$P_B = \frac{1}{2} e^{-\frac{E}{2N_0}}$$

$$P_B = \frac{1}{2} e^{-\frac{2E_b}{2N_0}} = \frac{1}{2} e^{-\frac{E_b}{N_0}}$$

