Numerical Simulation of Two-phase Heat Flow and

Transient Partial Melting in the Lower Crust with

Adaptive Mesh Refinement

Soon Hoe Lim

Thesis Advisor: Eric Hetland

Department of Physics

University of Michigan, Ann Arbor

April 5, 2013

Abstract

We have developed a 2D finite element program based on the finite element software library deal.II

in order to investigate transient partial melting of the lower crust following intrusion of a single sill.

Transient melting of the crust is crucial to the onset of migration and segregation of melt out of the lower

crust to the Earth surface, and thus affects the thermal evolution of crust. We numerically solve for

temperature and melt fraction in the governing time dependent heat balance equation using an adaptive

h-mesh refinement scheme in a structured finite element mesh. The numerical techniques employed for

the modeling includes space-time discretization using continuous Galerkin method for space and finite

difference method for time, an iterative approach to the nonlinear problem, and parameter experiments

to determine optimal adaptive remeshing strategy. Our study has identified two primary parameters that

control the degree of transient melting of the crust: the initial crustal temperature and the dimensions

of the intruded sills. Both parameters are related to the productivity of partial crustal melt through a

power law.

Keywords: finite element method, space-time discretization, adaptive mesh refinement, intrusion of

sill, transient partial melting, migration and segregation of melt

1

An honors thesis submitted in partial fulfillment of the requirements for an Honors degree of B.S. in Physics at the University of Michigan, Ann Arbor

CONTENTS 3

Contents

Li	st of Figures	5
Li	st of Tables	6
1	Introduction	8
2	The Mathematical Model	9
3	The Finite Element Method	11
	3.1 Time Discretization	12
	3.2 Space Discretization	13
4	Implementation and Mesh Refinement	14
5	Validations	17
6	Numerical Models of Partial Transient Melting	25
7	Conclusions	29
8	References	30
$\mathbf{A}_{]}$	ppendices	39
A	Derivation of Analytical Solution to Validation Problems	39
В	Source Codes	42
	B.1 Verification codes for validation models	42
	B.2 Program codes	44

CONTENTS 4

Acknowledgements

I would like to thank many people who have helped and guided me in writing my honors thesis. Firstly, I would like to express special gratitude to my thesis advisor, Prof. Eric Hetland, for giving me the opportunity to work with him for the past 12 months in his geophysics lab. I would like to thank him for his patient and selfless guidance of my research and thesis writing, as well as his encouragement and support.

I would also like to thank Prof. Wolfgang Bangerth, Prof. Timo Heister, and other deal.II developers for making deal.II library available for writing the finite element program. The materials in this thesis are far from original. I acknowledge that a large parts of the codes in the program and the numerical methods are inherited from the tutorial programs published in the documentation for deal.II and my primary contribution has been to borrow, assimilate, and modify the data structures and algorithms provided by the library in order to solve a problem in an application. I have relied heavily on the tutorial programs and the online compact course organized by Prof. B. Janssen and Prof. T. Wick from the Institute of Applied Mathematics at University of Heidelberg in learning the finite element method and writing the program.

I would also like to thank other deal.II users in deal.II users forum and other members in the geophysics lab for providing me constructive hints and feedbacks in the process of the program development. Lastly, I would like to thank the Department of Physics at the University of Michigan for allowing me to complete and publish my honors thesis. LIST OF FIGURES 5

List of Figures

1	Conceptual illustration of the problem setting: A sill is emplaced at the lower crust, causing	
	partial crustal melting and advection of melt (from [6])	8
2	(a) Density mixing relationship; (b) Melt equilibrium assumed in (4)	10
3	(a) Numbering of nodes for a linear element, which consists of one cell; (b) Numbering of	
	nodes for a quadratic element, which consists of four cells [1]	15
4	Flow chart summarizing the implementation of the finite element program	17
5	Illustration of hanging nodes, resulting from mesh refinement for Q1 finite elements (from [1]).	18
6	Computation of area of a cell with associated crustal melt fraction above 0.2, $A_{X>0.2}$. Let	
	$x = \frac{x_1 + x_2}{2}, y = \frac{y_1 + y_2}{2}$. For the crustal area of $(x_2 - x_1)(y_2 - y_1)$ to contribute to $A_{X>0.2}$,	
	the criterion that needs to be satisfied is: interpolated melt solution at (x,y) , X_{interp}	
	$(1-x)(1-y)X(x_1,y_1) + x(1-y)X(x_2,y_1) + y(1-x)X(x_1,y_2) + xyX(x_2,y_2) \ge 0.2$, where	
	$X(x_i, y_i)$ is the melt fraction solution obtained at (x_i, y_i)	18
7	Validation model 1: Convergence of series solution with increasing number of terms, $N.\dots$	21
8	Validation model 2: Convergence of series solution with increasing number of terms, $N.\dots$	22
9	Validation model 1: Projected initial conditions on the mesh after K times of pre-adaptive	
	refinement with Kelly Error Estimator as error indicator. Left: Adaptive mesh with $K=\ $	
	4, $K=5$, $K=6$ and $K=7$; Right: Projected initial conditions on the mesh with $K=$	
	4, $K=5$, $K=6$ and $K=7$. Observe that the projection on the mesh tends to the idealized	
	projection as K increases	23
10	Validation model 1: Adaptive meshes using KellyErrorEstimator as error indicator every 50	
	time steps. From top left to top right to bottom: Adaptive mesh obtained at $t=0,10,20,$	
	30 and 40 years	24
11	Validation model 1: Numerical solutions at specified locations using KellyErrorEstimator over	
	time	24
12	Validation model 2: Numerical solutions at specified locations using KellyErrorEstimator over	
	time	25
13	Validation model 1: Comparison of DoFs over time using different refinement strategies. Here	
	the DoFs is on order of 10^4	25
14	Validation model 1: Comparison of relative error obtained using different refinement strategies.	26
15	Validation model 2: Relative error of numerical solutions over time at specified locations	26

LIST OF TABLES 6

16	Left: Relative difference between analytical solutions to validation model 1 and 2 over time	
	at specified locations; Right: Relative difference between numerical solutions (with Kelly-	
	ErrorEstimator as error indicator for refinement) to validation model 1 and 2 over time at	
	specified locations. Relative difference is computed as the absolute value of the difference in	
	solutions over the solution to validation model 2 multiplied by 100%	27
17	Computational cost for Model 4	29
18	Adaptive meshes for Model 4 at $t=30,60,90,$ and 120 year	30
19	The melt fraction solutions for Model 4 at $t=5$ year and $t=10$ year. Note that the melt	
	fraction decreases significantly during the period of 5 years	30
20	Max. $A_{X>0.2}$ vs. time	31
21	Top left: τ_s and τ_c vs. L_{sill} with $T_0 = 873$ K; Top right: τ_s and τ_c vs. L_{sill} with $T_0 = 973$ K;	
	Bottom left: τ_s and τ_c vs. H_{sill} with $T_0 = 873$ K; Bottom right: τ_s and τ_c vs. T_0	32
22	Crustal area (m^2) vs. time (years) plots for Models 1-16	33
23	Melt fraction, X, following emplacement of a sill with $H_{sill} = 50$ m and L_{sill} varied, where	
	$L_{sill} = 50$ m (a-b), 100 m (c-d), 500 m (e-f), and 1000 m (g-h), at times, $t = 10$ and $t = 20$	
	years in a crust with temperature, $T_0 = 873 \text{ K.} \dots \dots \dots \dots \dots \dots \dots$	34
24	Melt fraction, X , following emplacement at a 1 km by 50 m sill in a crust with temperatures	
	$T_0=873~\mathrm{K}$ (a-f) and $T_0=973~\mathrm{K}$ (g-l) at times, $t=20,~40,~60,~80,~100,$ and 200 years	35
25	Power laws deduced from simulations for the variables τ_c (a-b), τ_s (c-d), and max. $A_{X>0.2}$	
	(e-f) vs. L_{sill} . The power laws seem to fit the solution well in (e-f), reasonably well in (a-b),	
	and poorly in (c-d). Here $a = \text{slope}$ of the graph and $b = \text{y-intercept}$	36
26	Power laws deduced from simulations for the variables τ_c (a) , τ_s (b), and max. $A_{X>0.2}$ (c)	
	vs. H_{sill} . Here $a =$ slope of the graph and $b =$ y-intercept	37
27	Power laws deduced from simulations for the variables τ_c (a), τ_s (b), and max. $A_{X>0.2}$ (c) vs.	
	T_0 . Here $a = \text{slope}$ of the graph and $b = \text{y-intercept}$	38
List	of Tables	
1	Description of variables used and their units	11
2	Numerical values of variables used in the models	11
3	Models with sill height $H_{sill} = 0.05$ km at $T_0 = 873$ K	27
4	Models with sill height $H_{sill}=0.05$ km at $T_0=973$ K	28
5	Models with sill length $L_{cill} = 1.0$ km at $T_0 = 873$ K	28

LIST OF TABLES 7

6 Models with sill length $L_{sill}=1.0~{\rm km}$ and sill height $H_{sill}=0.05~{\rm km},\,873~{\rm K} < T_0 < 973~{\rm K}.$. 28

1 INTRODUCTION 8

1 Introduction

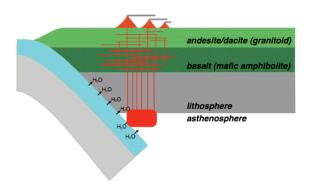


Figure 1: Conceptual illustration of the problem setting: A sill is emplaced at the lower crust, causing partial crustal melting and advection of melt (from [6]).

The temperature distribution in arc crust is driven by emplacement of sills into the lower crust, along with subsequent advection of melt up the crustal column or erupted to the surface [4]. The advected melt could be residual melt from the solidifying sills or partial melt of the crust surrounding the sills. Depending on the size of the sills and the background temperature in which the sills are intruding, a significant portion of the lower crust may be partially molten and sustain melt fractions higher than 20%. One of the consequences of such high melt fraction is migration and segregation of melt over large distances [9], resulting in crustal partial melt possibly either advected up the crustal column or erupted to the surface.

In this paper, we develop numerical models of temperature and melt fraction in order to investigate transient partial melting of the crust surrounding an intruded sill during the solidification of the sill. For simplicity, we only consider the case of a single sill emplacement in the lower crust at a specified background temperature. Specifically, the numerical models in this study investigate the effects of varying size of emplaced sills into crust with different background temperatures on the domain solidification time and evolution of crustal melt fraction.

The models are developed using deal.II 7.1.0 library, or Differential Equations Analysis Library, a C++ program library aimed at the computational solution of partial differential equations using adaptive finite elements [2]. We utilize space-time continuous Galerkin method and local h-adaptive refinement techniques in a structured mesh. The source codes of the developed program, which contain the files source.cc, parameter.prm, and Makefile are included in Appendix B for reference. From this investigation, we hope that a quantitative assessment of the simplified problem can shed light on the more general problem

of transient crustal partial melting and the evolution of the crustal geotherm in response to repeated sill emplacement in arc crust.

2 The Mathematical Model

Following [3], [4], and others, we model the thermal evolution of arc crust by the heat equation

$$\rho C_p \partial_t T + \rho L \partial_t X = \nabla k \nabla T, \tag{1}$$

where T is temperature, t is time, ρ is density, C_p is specific heat capacity, L is specific latent heat, $X \in [0,1]$ is melt fraction, and k is thermal conductivity (Tables 1 and 2). To model melt fraction X as a function of temperature T, we assume a piecewise linear melting equilibrium relationship (Figure 2b), given by

$$X = \phi_i T + b_i, \tag{2}$$

where ϕ_i and b_i are experimentally determined equilibrium coefficients [3]. The time derivative of (2) is

$$\partial_t X = \phi_i \partial_t T + T \partial_t \phi_i, \tag{3}$$

which we approximate as

$$\partial_t X = \phi_i \partial_t T \tag{4}$$

by assuming $\partial_t \phi_i = 0$, which is true except at discrete temperatures where there are slope breaks (Figure 2b). We come back to this point in Section 3.1. With the approximation in (4), (1) can be expressed as

$$\partial_t T = \nabla k^* \nabla T,\tag{5}$$

where

$$k^* = \frac{k}{\rho(C_p + \phi_i L)}. (6)$$

We solve (5) numerically to find T(x, y, t), $x, y \in \Omega$, $t \in [0, \tau]$, where τ is total simulation time, x and y are spatial variables, and Ω is the solution domain. Since X, and thus ∇X , are functions of T, k^* is also a function of T, which introduces nonlinearity to the problem. We assume the following initial and boundary

conditions

$$T(x, y, 0) = \begin{cases} T_{sill} & \text{on } \Omega_{sill} = [L_1, L_2] \times [H_1, H_2], \\ T_0 & \text{elsewhere,} \end{cases}$$

$$(7)$$

$$\nabla T(x, y, 0) = 0 \text{ in } \Omega \times [0, \tau], \tag{8}$$

and

$$T(x, y, t)|_{\partial\Omega} = T_0 \text{ on } \partial\Omega \times [0, \tau],$$
 (9)

where T_{sill} is temperature of intruded sill and T_0 is crustal background temperature. We denote $L_{sill} = L_2 - L_1$ to be sill length and $H_{sill} = H_2 - H_1$ to be sill height.

In all the models we consider, we neglect any melt advection, and we represent the intruded sill in the domain by (7). We assume that the intruded sill is basaltic in composition while the surrounding crust is and exist in composition (Table 2). We assume that the thermal conductivity k is constant within the sill and crust during the melting and solidification time (i.e, independent of X). We further neglect any pressure dependence on thermal properties. We take the density, ρ to be linearly dependent on melt fraction X (Figure 2a).

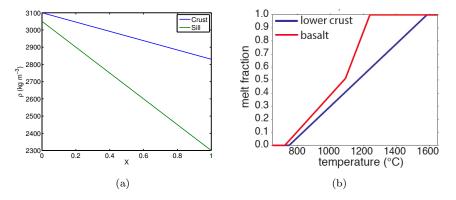


Figure 2: (a) Density mixing relationship; (b) Melt equilibrium assumed in (4).

Variable	Description	Unit
\overline{T}	Temperature	K
X	Melt fraction	-
$ au_s$	Solidification time	years
$ au_c$	Time duration with crustal $X > 0.2$	years
T_{sill}	Sill temperature	K
T_0	Background temperature	K
ho	Density	$ m kg~m^{-3}$ J $ m kg^{-1}$
C_p	Specific heat capacity	$\rm J~kg^{-1}$
L	Specific latent heat	$\rm J~kg^{-1}~m^{-1}~K^{-1}$
k	Thermal conductivity	${ m W} { m m}^{-1} { m K}^{-1}$
$A_{X>0.2}$	Area with crustal $X > 0.2$	m^2

Table 1: Description of variables used and their units.

Table 2: Numerical values of variables used in the models

Parameters					
Symbol [unit]	Domain	Value			
	$\Omega_{sill} \ (X=0)$	3100			
$\rho [\mathrm{kg} \mathrm{m}^{-3}]$	$\Omega_{sill} (X=1)$	2830			
	$\Omega (X=0)$	3050			
	$\Omega (X=1)$	2300			
$C_p \; [\mathrm{J} \; \mathrm{kg}^{-1}]$	Ω_{sill}	1480			
	Ω	1390			
I [I l _r α-1 K-1]	Ω_{sill}	4.0×10^{5}			
$L [J kg^{-1} K^{-1}]$	Ω	3.5×10^{5}			
$k [\rm J \ s^{-1} \ m^{-1} \ K^{-1}]$	Ω_{sill}	2.6			
	Ω	2.6			
T_{sill} [K]	Ω_{sill}	1558			
T_0 [K]	Ω	varies			

3 The Finite Element Method

The finite element method is one of the most widely used methods to solve a boundary value partial differential equations on a given domain [13]. We review the essentials of the method here. Generally, the domain is first subdivided into a finite number of subdomains known as finite elements. The solution of the differential equation is then approximated by a set of polynomial functions on each of the elements, where the approximate solution is spanned by a set of orthogonal basis functions in a finite dimensional space V. The finite element solution is an approximate solution $T_{approx} \approx T$ in a subspace $V_h \subset V$ with chosen basis functions $\{\psi_i\}_{i=1}^d = \{\psi_1, \psi_2, ..., \psi_d\}$ such that $T_{approx}(x, y) = \sum_{i=1}^d \xi_i \psi_i(x, y)$, where $d = dim(V_h)$ and ξ_i 's are unknown nodal coefficients. Hence, the problem reduces to determine $V_h \subset V$ such that $||T_{approx} - T|| < TOL$, where TOL is the tolerance of error in a specified norm. All of our numerical models in this study employ the standard finite element method.

Since our problem is both time and space dependent, we use Rothe's method to discretize space and time. We first discretize time resulting in a stationary PDE at each time step, which is then solved by standard finite element techniques [1]. The major advantage of using the Rothe's method is the flexibility to use a different finite element mesh at each time step, allowing for adaptive mesh refinement where needed [1]. As such, we solve a time-independent PDE at each time step that can be discretized independently of the mesh used for the previous time steps [1]. Adaptivity of the finite element mesh is used to increase the accuracy of the solution while reducing the computational cost.

3.1 Time Discretization

We discretize time using a finite difference approximation of $\partial_t T$. Let T^n be an approximation at time $t = t_n = n\Delta t$, where $\Delta t = t_n - t_{n-1}$ denotes the length of the present time step. The finite difference approximation of (1) is

$$\frac{T^n - T^{n-1}}{\Delta t} - \nabla k^{*n} \nabla [\theta T^n + (1 - \theta) T^{n-1}] = 0, \tag{10}$$

on Ω , where $\theta \in [0,1]$ is a constant,

$$k^{*n} = \frac{k}{\rho(C_p + \phi_i^{n-1}L)},\tag{11}$$

and ϕ_i^{n-1} is the equilibrium coefficient in the previous time step. The boundary condition is $T^n = T_0$ on $\partial\Omega$.

When $\theta = 0$, (10) reduces to the forward, or explicit, Euler Method. When $\theta = 1$, it reduces to the backward, or implicit, Euler method. Both explicit and implicit Euler methods yield first order accurate solutions. If $\theta = 0.5$, then the semi-discretized equation (10) results in the Crank-Nicholson method which yields a second order accurate solution. We include θ as one of the user defined parameters in our developed program; however, since the PDE in (1) is parabolic, we use $\theta = 1$. For parabolic PDEs, the implicit method guarantees unconditional stability [14].

One of the major challenges in solving the problem described in Section 2 is the presence of the nonlinear variable k^* , which is dependent on T through (4). In order to compute the solution at the present time step, we use the solution at the previous time step which allows us to solve the time dependent problem trivially. Since we assume piecewise linear melting equilibrium equations, ϕ_i is constant except at discrete times

(Figure 2b). However, this technique is inaccurate unless the time step is very small and the equilibrium equation is chosen such that the phase change occurs over sufficiently large temperature interval [7]. In view of this restriction, we minimize the time step size to be between 0.01 and 0.1 year for each of the simulations in this study, which results in small change in temperatures between successive time steps.

3.2 Space Discretization

We discretize space using the standard finite element method [8]. We find the weak form of (1) by first multiplying with a test function from the left, and integrating over the entire domain, integrating by parts wherever necessary. We use the discrete approximation of the solution at the n^{th} time step, $T_h^n \in V_h$, where V_h is the finite dimensional subspace of the Sobolev space V, and solve

$$(T_h^0, \varphi_h) = \begin{cases} (T_{sill}, \varphi_h) & \text{on } \Omega_{sill} = [L_1, L_2] \times [H_1, H_2], \\ (T_0, \varphi_h) & \text{elsewhere,} \end{cases}$$
(12)

 $\forall \varphi_h \in V_h \text{ for } n = 0$, where φ_h is the basis of V_h , $(u, v) = \int_{\Omega} uv \, d\Omega$ is the L^2 inner product, T_h^0 is the approximate solution at t = 0, and

$$(T_h^n, \varphi_h) + \frac{k}{\rho(C_p + \varphi_i^{n-1}L)} \Delta t \ \theta(\nabla T_h^n, \nabla \varphi_h) = (T_h^{n-1}, \varphi_h) - \frac{k}{\rho(C_p + \varphi_i^{n-1}L)} \Delta t \ (1 - \theta)(\nabla T_h^{n-1}, \nabla \varphi_h)$$
 (13)

 $\forall \varphi_h \in V_h \text{ for } n \geq 1$. Using the standard Galerkin approximation [1], we approximate $T^n(x,y)$ at the n^{th} time step as

$$T^{n}(x,y) \approx T_{h}^{n}(x,y) = \sum_{i} \xi_{i}^{n}(x,y) \ \psi_{i}^{n}(x,y)$$

$$\tag{14}$$

where T_h^n are trial functions, $\psi_i^n(x,y)$ are shape functions used at the nth time step and ξ_i^n are unknown temperature solutions at the nodes.

Substituting approximation (14) into (13), we reach the following equation

$$\left(M^{n} + \frac{k}{\rho(C_{p} + \phi_{i}^{n-1}L)}\Delta t \,\theta A^{n}\right)\xi^{n} = M^{n,n-1}\xi^{n-1} - \frac{k}{\rho(C_{p} + \phi_{i}^{n-1}L)}\Delta t \,(1-\theta)A^{n,n-1}\xi^{n-1},\tag{15}$$

where

$$\begin{split} M_{i,j}^n &= (\psi_i^n, \psi_j^n), \ M_{i,j}^{n,n-1} = (\psi_i^n, \psi_j^{n-1}), \\ \\ A_{i,j}^n &= (\nabla \psi_i^n, \nabla \psi_j^n), \ A_{i,j}^{n,n-1} = (\nabla \psi_i^n, \nabla \psi_j^{n-1}). \end{split}$$

Lastly (15) is recast into a more convenient form by dividing both sides by $\Delta t > 0$, to yield

$$\left(\frac{1}{\Delta t}M^n + \frac{k}{\rho(C_p + \phi_i^{n-1}L)}\theta A^n\right)\xi^n = \left[\frac{1}{\Delta t}M^{n,n-1} - \frac{k}{\rho(C_p + \phi_i^{n-1}L)}(1-\theta)A^{n,n-1}\right]\xi^{n-1},$$
(16)

where M^n and A^n in (16) are commonly referred as the mass matrix and stiffness matrix respectively. Solving (16) at the current time step allows us to advance to the next time step using the finite difference approximation in (10) to achieve time dependent solutions of T and X. Note that since the solution of the previous step may have been computed on a different mesh, we use the shape functions $\psi_i^{n-1}(x,y)$ from the previous time step to map T_h^{n-1} onto the current mesh [1].

4 Implementation and Mesh Refinement

Our finite element program employs object-oriented programming to organize data and functions via the use of classes. One of the advantages of this practice is that we can compose finite element implementations into smaller blocks. All user defined inputs are read at the beginning of the program from the input file called parameter.prm.

In Section 3.2, we approximate the solution to the problem described in Section 2 at the n^{th} time step by

$$T_h^n(x,y) = \sum_{i} \xi_i^n(x,y) \ \psi_i^n(x,y), \tag{17}$$

where $T_h^n(x,y) \in V_h$, ψ_i^n 's are shape functions at the n^{th} time step, and $\xi_i^n(x,y)$'s are unknown temperature nodal solutions. The total number of nodal temperatures is referred to as the degree of freedom, DoF, of the problem. In order to solve for the temperatures, the finite dimensional function $T_h^n(x,y) \in V_h$ in (17) needs to satisfy the weak formulation given in (15) for all test functions in V_h . To do so, we numerically integrate all the integral terms that appear in (15) by using Gauss-Legendre quadrature formula on a mesh [1].

We choose our subspace V_h to be the scalar Lagrangian space to obtain a finite element space of contin-

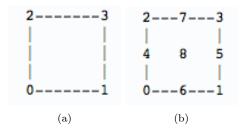


Figure 3: (a) Numbering of nodes for a linear element, which consists of one cell; (b) Numbering of nodes for a quadratic element, which consists of four cells [1].

uous, piecewise polynomials of degree 2 in each coordinate direction [1]. In other words, we use quadratic or Q2 finite elements, with each element composed of 9 nodes.

In deal.II, the finite element mesh is considered to be composed of cells. A cell is a geometrical image in \mathbb{R}^d connecting two or more nodes. In 1D, a cell is simply a line and in 2D it is a quad. In contrast, a finite element is a subdomain of the solution domain, and a cell is equivalent to an element only for linear (Q1) elements (Figure 3a). In 2D, each quadratic (Q2) element is composed of four cells (Figure 3b). Each of the cells represents crust material. Figure 3 illustrates the distinction between a cell and an element as well as the node numbering for Q1 and Q2 elements in 2D.

In the numerical computation of the problem, we aim to increase the spatial resolution where the solution is less regular. We do this by implementing a scheme to locally refine (i.e. increasing the grid points) at the interface between the emplaced sill and the surrounding crustal area. We achieve this goal via local adaptive mesh refinement based on error estimator¹ proposed by Kelly et al. (1983). The error estimator is implemented as the function KellyErrorEstimator within the deal.II library. This estimator approximates the error of the finite element solution in each element by integration of the jump of the gradient of the solution along the faces of each cell [10]. In other words, the error estimator assigns to each cell K the indicator

$$\eta_K = \left(\frac{h_K}{24} \int_{\partial K} \left[\frac{\partial T_h}{\partial n}\right]^2 d\sigma\right)^{1/2},\tag{18}$$

where h_K is greatest length of the diagonals of cell K and $[\cdot]$ denotes the jump of the normal derivatives across a face $\gamma \subset \partial K$ of the cell K [1], [10]. It is used to refine the regions of the mesh with the largest R% error and coarsen the regions of the mesh with the smallest C% error, where R and C are user specified refinement parameters.

¹Note that it is not an a posteriori error estimator. It merely acts as an indicator for mesh refinement [1].

We implement h-refinement in our finite element program. With h-refinement, the mesh connectivity changes as the mesh is refined. All of the meshes used in this study are structured, square grids. For each level of adaptive refinement, a marked cell is isotropically subdivided into four equivalent square child cells, resulting in a change in the overall number of nodal points, but that preserves the topology of the overall mesh [2]. The finer mesh overlies the coarser one, and the DoF increases after each level of refinement. This results in a new, more localized mesh after the marked cells are refined. The adaptivity strategy in deal.II uses grids in which neighboring cells are refined independently, which can result in additional nodes on the interfaces of cells which belong to one side but not the other side (Figure 5). These so-called hanging nodes are constrained in order to guarantee the continuity of solution [1]. The constraint on hanging nodes is such that the temperature on the element face containing a hanging node is linear [1].

One particular challenge to obtain an accurate solution is the interpolation and projection of the problem geometry and initial conditions on the initial mesh at t = 0. Specifically, the temperature jump between the sill and surrounding crust is difficult to resolve since the initial temperature field is not differentiable at the sill-crust interface. We compute the L^2 projection² of the initial temperature field onto our discretized finite element mesh, which results in a smooth projection of the initial temperatures onto the initial mesh. The smoothness of the projected initial temperatures technically violates our initial condition of a finite jump in temperature at the sill-crust interface. However, we minimize the difference between the idealized and applied initial conditions by adaptively refining the initial mesh a few times so that an increased density of cells around the sill-crust interface more closely approximates the idealized initial conditions (Figure 9). This initial refinement increases our computational cost and we choose the optimal number of pre-refinement steps on the initial mesh via trial and error.

In deal.II, the linear finite element system is assembled at each time step by computing the contribution of each cell in a small matrix, and then transferring these to the global matrix [1]. The k^* at the present time step is computed based on the solution in the last time step (see Section 3.2). The linear system, which is almost symmetric and positive definite, is solved using a conjugate gradient solver with SSOR preconditioner [1], obtaining the numerical solution at the current time step. The solution is updated through time using the finite difference approximation as described in Section 3.1. The mesh is adaptively refined between time steps based on user specifications, and the solution is mapped onto the new mesh when refined. We do this

The L^2 projection $P_h u \in V_h$ of a function $u \in L_2(\Omega)$ into the space V_h on a triangulation of a domain Ω is defined as $(u - P_h u, v) = 0 \ \forall \ v \in V_h$ [13].

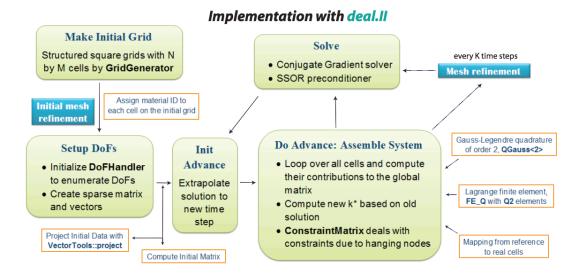


Figure 4: Flow chart summarizing the implementation of the finite element program.

via the function SolutionTransfer in deal.II, and regenerate the system matrix after each refinement [1]. However, it is worthwhile to note that this approach introduces unavoidable interpolation error each time we adaptively refine the mesh [1]. We stop the simulation when the entire domain is completely solidified, i.e. when melt fraction X = 0 for all $(x, y) \in \Omega$ and we denote the final time as the solidification time, τ_s . Figure 4 shows a flow chart of the organization and steps of our program. We recommend interested readers to refer to [1] for complete discussion of related implementation details.

Our program postprocesses the computed temperature solutions using Gnuplot for visualization. We use the obtained temperature solutions to calculate the corresponding melt fraction in the sill and crustal domain. Another quantity of interest that we compute is the area with crustal melt fraction above 0.2, denoted as A or $A_{>0.2}$ (see Section 6) and we do so by using bilinear interpolation of the melt fraction solutions to determine if the associated area of the cells on the mesh contributes to $A_{X>0.2}$ (Figure 6).

5 Validations

We first validate our finite element program using two cases in which an analytical solution is known. These cases are heat conduction following an intrusion of a 500 m \times 50 m rectangular sill of temperature $T_{sill} = 1558$ K into the 2.5 km \times 1.0 km crustal domain at time, t = 0. The intruded sill occupies the subdomain $[L_1, L_2] \times [H_1, H_2]$ and we choose this subdomain such that the sill is intruded at the center of

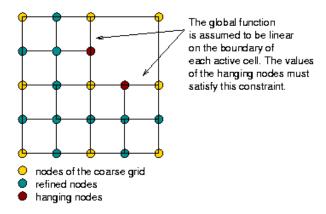


Figure 5: Illustration of hanging nodes, resulting from mesh refinement for Q1 finite elements (from [1]).

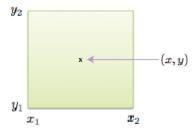


Figure 6: Computation of area of a cell with associated crustal melt fraction above 0.2, $A_{X>0.2}$. Let $x=\frac{x_1+x_2}{2},\ y=\frac{y_1+y_2}{2}$. For the crustal area of $(x_2-x_1)(y_2-y_1)$ to contribute to $A_{X>0.2}$, the criterion that needs to be satisfied is: interpolated melt solution at $(x,y),\ X_{interp}=(1-x)(1-y)X(x_1,y_1)+x(1-y)X(x_2,y_1)+y(1-x)X(x_1,y_2)+xyX(x_2,y_2))\geq 0.2$, where $X(x_i,y_i)$ is the melt fraction solution obtained at (x_i,y_i) .

the domain. We assume that both the crustal domain and the intruded sill share the same coefficient of thermal conductivity $k^* = k/C_p\rho$ with $\phi_i = 0$. This assumption eliminates any nonlinearity introduced in the governing PDE as there is no temperature dependence in k^* . In other words, we assume $\nabla X = 0$ so that $k^* = \frac{k}{C_p\rho}$ is a constant over the entire domain. We choose $\Omega = [0, L] \times [0, H] = [0, 2.5] \times [0, 1.0]$, dt = 0.1 years, and the following boundary and initial conditions

$$\frac{\partial T(x,y,t)}{\partial y}|_{\partial\Omega} = g_0, \tag{19}$$

$$\frac{\partial T(x,y,t)}{\partial x}|_{\partial\Omega} = 0, \tag{20}$$

$$T(x, y, 0) = \begin{cases} T_{sill} = 1558 \text{ K} & \text{on } [1.0, 1.5] \text{ x } [0.475, 0.525], \\ T_0 - \frac{g_0 H}{2} + g_0 y & \text{elsewhere,} \end{cases}$$
 (21)

such that $T(x, H/2, 0) = T_0$, where g_0 represents a linear geotherm. We take $g_0 = 0$ K/m and $g_0 = 30$ K/m for the first and the second case respectively, and refer to these two cases as validation model 1 and validation model 2, respectively. Our goal in these validation models is to demonstrate that over the domain assumed, the geotherm g_0 has negligible effect on the temperature solution, which justifies our assumption that the background temperature in the crustal region is a constant (see Section 6). The boundary conditions in (19) and (20) imply that $T(x, 0, t) = T_0 - g_0 H/2$, $T(x, H, t) = T_0 + g_0 H/2$, and $T_y(0, y, t) = T_y(L, y, t) = g_0$. See Appendix A for the derivation of the analytical solution.

To solve both validation problems, we choose the initial mesh to consist of 10×10 cells and refine the initial mesh adaptively 7 times. At t > 0, we allow adaptive refinement every 50 time steps and stop the program after 50 years (500 time steps). Adaptive mesh refinement in both problems are performed by using the error estimator KellyErrorEstimator. We specify the program to refine the regions with the highest 30% error and coarsen the regions with the lowest 10% error for the initial adaptive refinement and to refine the regions with the highest 0.5% error and coarsen the regions with the lowest 0.25% error for adaptive refinement at later times (Figure 10). We evaluate the accuracy of the numerical solutions to both validation models by comparing them to the analytical solutions. The analytical solution is expressed as an infinite series which decays in time, and we compute only the first 500 terms of the series (Figure 7 and 8). There is a negligible error associated with the truncated series solution.

Figure 11 shows the numerical solution at four specified locations near the sill-crust interface for validation problem 1. Figure 12 and Figure 15 show the numerical solution at four specified locations near the sill-crust interface and the relative error, respectively for validation problem 2. With validation problem 1, we further compare the performance yielded by different mesh refinement strategies, namely adaptive refinement with KellyErrorEstimator as error indicator vs. adaptive refinement with DerivativeApproximation as error indicator vs. a global refinement of the initial mesh (15 \times 15 cells) three times without adaptive remeshing at later times, where DerivativeApproximation is an error estimator function available within deal.II and is based on the finite difference approximation to the second derivative of the cells [1]. The error estimator function DerivativeApproximation assigns to each cell K the indicator

$$\eta_K = h_K^3 \|\nabla_h T_h(K)\|_{\infty},\tag{22}$$

where h_K is greatest length of the diagonals of cell K and $T_h(K)$ denotes T evaluated at the center of the cells [1]. Comparing the performance of these three refinement strategies allows us to determine the optimal strategy for numerical modeling in Section 6.

Figure 13 compares the nodal temperatures using the three refinement strategies, while Figure 14 illustrates the relative error yielded by using those strategies. The relative error is computed as

$$e = \frac{T_c - T_a}{T_a} \times 100\%, (23)$$

where T_a are the temperatures from the analytical solution and T_c are from the numerical solution. We observe that the three refinement strategies yield somewhat equally accurate solutions over time, but the first and second refinement strategies perform better than the global refinement strategy in projecting the initial conditions onto the mesh. In terms of DoFs required by these three strategies, we note that although the initial global refinement strategy yields equally accurate solution as the first and second strategy, the DoFs (and hence computational cost) required when using this strategy is much higher. On the other hand, the first and second strategies require roughly equal DoFs, with DoFs of the first strategy slightly lower than the second strategy. In view of this analysis, we employ the first strategy for mesh refinement in the numerical models presented in Section 6.

For both validation problems, we observe that the temperatures in the crustal region near the sill-crust interface increase rapidly in the first decade and decay exponentially thereafter. The relative error of the numerical solutions for both cases decreases rapidly from roughly 10% (due to projection of initial conditions onto the mesh) at initial time to less than 0.1% in about three years time. Note that the reason we only choose four specified points near the sill-crust interface to perform error analysis but not evaluate the error norms³ is that local pointwise error analysis yields more meaningful analysis for our problems since we are mainly interested in melt fraction near the sill-crust interface. In Figure 16, we confirm that the difference in solutions to the two validation problems is bounded above by 0.1%, justifying our assumption that the geotherm in the domain can be neglected in the models presented in Section 6.

³In fact, evaluating the error norms is computationally costly due to the huge number of cells on the mesh after the initial adaptive refinements.

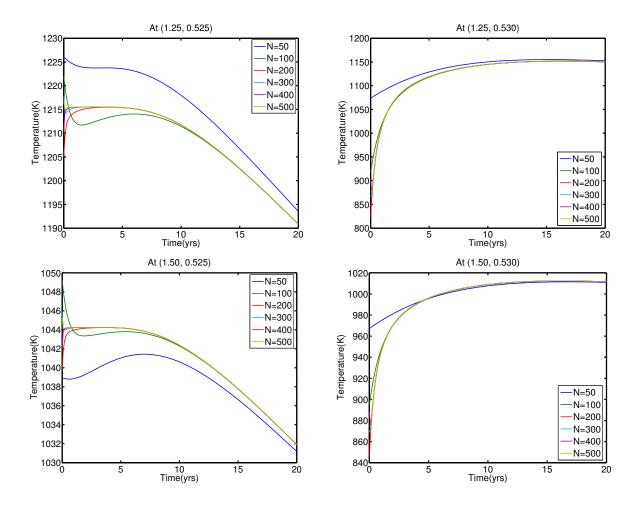


Figure 7: Validation model 1: Convergence of series solution with increasing number of terms, N.

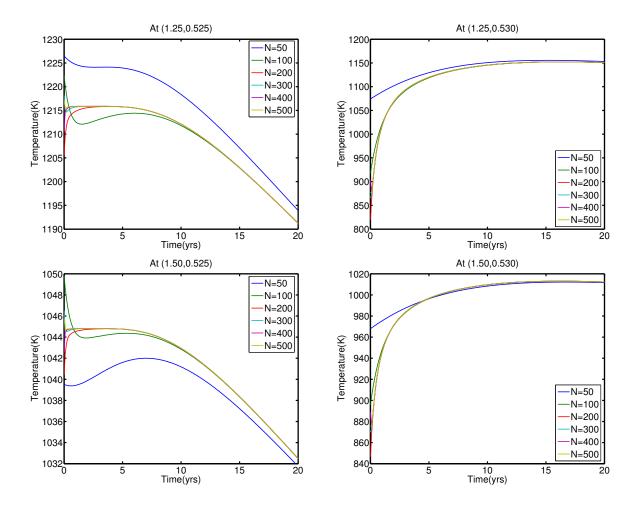


Figure 8: Validation model 2: Convergence of series solution with increasing number of terms, N.

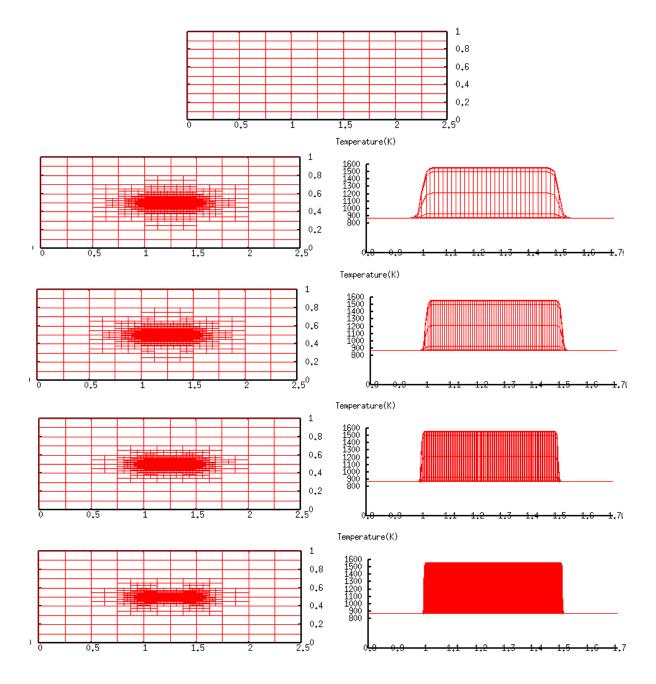


Figure 9: Validation model 1: Projected initial conditions on the mesh after K times of pre-adaptive refinement with KellyErrorEstimator as error indicator. Left: Adaptive mesh with K=4, K=5, K=6 and K=7; Right: Projected initial conditions on the mesh with K=4, K=5, K=6 and K=7. Observe that the projection on the mesh tends to the idealized projection as K increases.

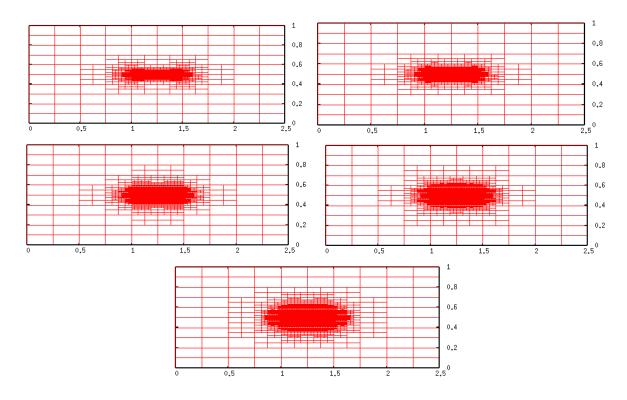


Figure 10: Validation model 1: Adaptive meshes using KellyErrorEstimator as error indicator every 50 time steps. From top left to top right to bottom: Adaptive mesh obtained at t = 0, 10, 20, 30 and 40 years.

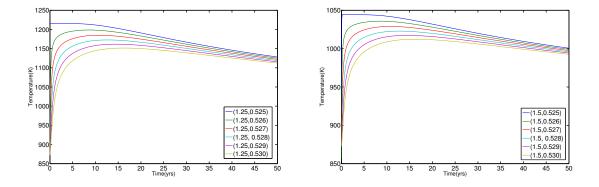


Figure 11: Validation model 1: Numerical solutions at specified locations using KellyErrorEstimator over time.

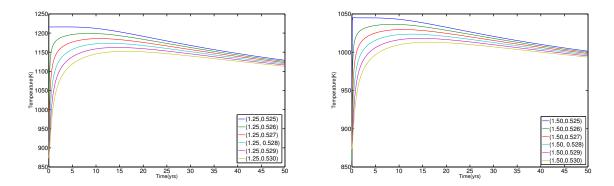


Figure 12: Validation model 2: Numerical solutions at specified locations using KellyErrorEstimator over time

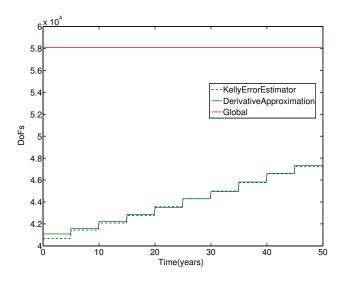


Figure 13: Validation model 1: Comparison of DoFs over time using different refinement strategies. Here the DoFs is on order of 10^4 .

6 Numerical Models of Partial Transient Melting

We consider 16 models with rectangular sills of initial $T_{sill} = 1558$ K, initially placed into the domain of length L and height H with lower crustal composition and initial background temperature of $T_0 = 873 - 973$ K. We consider H and L to be between 0.2 - 4.0 km and 2.5 - 20 km, respectively, where the exact size depends on the sill size and background temperature. That we assume a constant background temperature surrounding the intruded sill is justified in Section 5. We define τ_c and A (or $A_{X>0.2}$) as the time duration and area, respectively, with crustal melt fractions above 0.2. We consider X>0.2, since this level of melt fraction may result in melt migration and segregation in the lower crust [9]. It is worth noting that all the models considered here are local in nature and that we have neglected external forcings and interactions that

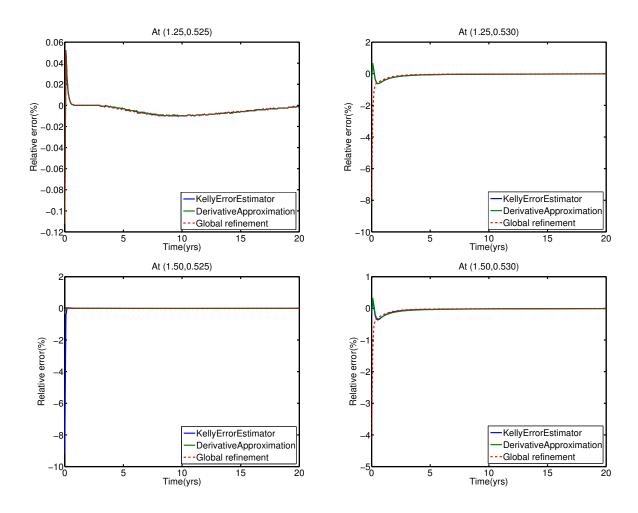


Figure 14: Validation model 1: Comparison of relative error obtained using different refinement strategies.

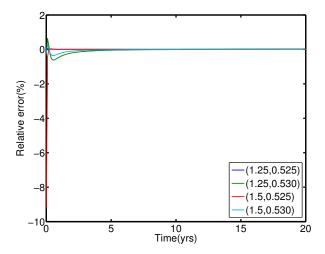


Figure 15: Validation model 2: Relative error of numerical solutions over time at specified locations.

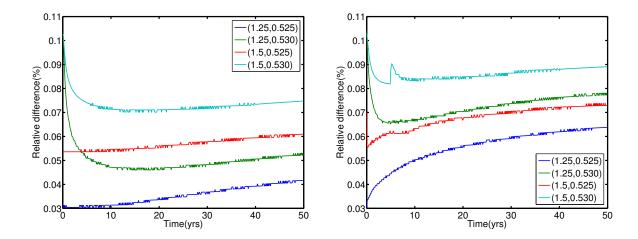


Figure 16: Left: Relative difference between analytical solutions to validation model 1 and 2 over time at specified locations; Right: Relative difference between numerical solutions (with KellyErrorEstimator as error indicator for refinement) to validation model 1 and 2 over time at specified locations. Relative difference is computed as the absolute value of the difference in solutions over the solution to validation model 2 multiplied by 100%.

Table 3: Models with sill height $H_{sill} = 0.05$ km at $T_0 = 873$ K.

Model	L_{sill} (km)	τ_s (yrs)	$\tau_c \; ({\rm yrs})$	Max. $A_{X>0.2} \; (\text{m}^2)$
1	0.05	57.48	0.49	8.09
2	0.1	111.04	1.54	35.2
3	0.5	310.2	10.3	370.5
4	1.0	318.1	19.2	843.2
5	5.0	317.9	47.2	19950

could contribute to the process. Tables 3 - 6 summarize the results of the models. Figure 17 shows the cost of performing the major operations in our finite element program for model 4.

We find that both initial crustal temperature and dimensions of the sills are important parameters for the transient partial melting process. Following the intrusion of a 1 km by 50 m sill, the surrounding lower crust partially melts, with melt fractions greater than 0.2 persisting over an area up to 843 m² and 11015 m² for a crust with background temperature of 873 K and 973 K, respectively. If the partial crustal melt at time of maximum melting migrated to a secondary sill of the same length, this area would correspond to secondary sill of at least ~ 1 m or 3 m if originating in 873 K or 973 K respectively.

Although the highest amount of the crustal melt is generated early after sill emplacement, the complete partial melting process can occur over a long time period, depending on the parameter values chosen (Figure 19). For instance, the crustal melt generated by the 5 km long intruded sill in Model 5 and Model

0.5

1.0

5.0

8

9

10

Model	L_{sill} (km)	τ_s (yrs)	$\tau_c \text{ (yrs)}$	Max. $A_{X>0.2} \text{ (m}^2\text{)}$
6	0.05	238.67	11.49	241.66
7	0.1	473.8	27.2	486.09

53.7

58.4

149

5107.1

11014.7

94742

2113.3

3436.7

5281

Table 4: Models with sill height $H_{sill} = 0.05$ km at $T_0 = 973$ K.

Table 5: Models with sill length $L_{sill}=1.0~\mathrm{km}$ at $T_0=873~\mathrm{K}.$

Model	H_{sill} (km)	τ_s (yrs)	$\tau_c \; ({\rm yrs})$	Max. $A_{X>0.2} \text{ (m}^2\text{)}$
11	0.01	12.79	1.45	122.8
12	0.02	50.94	4.46	278.5
13	0.1	1239	31.3	1412

10 decreases at a slower rate towards complete solidification compared to the models where the length of the intruded sill is shorter, demonstrating high persistence of crustal melting over time. However, it takes 318 years and 5281 years for the crust in Model 5 and Model 10 to completely solidify, respectively. The fact that τ_s approaches an asymptote with increasing L_{sill} in Figure 21 supports this observation. Figure 20 shows the effect of varying background temperature on max. $A_{X>0.2}$. Figure 23 show that sills of longer length melt the surrounding crust to a larger degree, while Figure 24 demonstrates the evolution of melts generated by an intruded sill in a crust of background temperature of 873 K vs. that of 973 K over time.

High crustal melt fractions persist for decades following emplacement of a sill, with the time scale at which the melt persisting depending on the sill dimension and initial crustal temperature (Figure 22). At initial crustal temperature of 873 K, a melt fraction as high as 0.2 can persists up to 0.49 years for a 0.05 km by 0.05 km sill and up to 47.2 years for a 1 km by 0.05 km sill. The crustal area with melt fraction of up to 0.2 also increases with the initial crustal temperature. The relationship of max. $A_{X>0.2}$ and initial crustal crustal temperature appears to follow a power law.

The relationship of both max. $A_{X>0.2}$ and τ_c to L_{sill} can be described by a power law (Figure 25). The power laws deduced are max. $A_{X>0.2} \sim L_{sill}^{1.6356}$ and max. $A_{X>0.2} \sim L_{sill}^{1.3144}$ for the case with background

Table 6: Models with sill length $L_{sill} = 1.0$ km and sill height $H_{sill} = 0.05$ km, 873 K < $T_0 < 973$ K.

Model	T_0 (K)	τ_s (yrs)	$\tau_c \; ({\rm yrs})$	Max. $A_{X>0.2}$ (m ²)
14	898	425.9	16.8	534.7
15	923	621.9	29.9	1455.5
16	948	1009	41.2	3023.7

7 CONCLUSIONS 29

Total wallclock time elapsed sinc	3.05e+05s	 	
Section		wall time	 % of total
Assembling system Rebuilding matrix	3107 3115	1.77e+04s	5.8%
Solve system Remeshing	3107 17	1.89e+05s 132s	70
Setup dof systems	1 +	0.252s	

Figure 17: Computational cost for Model 4.

temperature of 873 K and 973 K, respectively. Additionally, $\tau_c \sim L_{sill}^{0.9991}$ and $\tau_c \sim L_{sill}^{0.5070}$ for the case with background temperature of 873 K and 973 K, respectively. The relationships of τ_c , τ_s , and max. $A_{X>0.2}$ to H_{sill} for the case with background temperature of 873 K can also be described by a power law (Figure 26): max. $A_{X>0.2} \sim H_{sill}^{1.0809}$, $\tau_c \sim H_{sill}^{1.3696}$, and $\tau_s \sim H_{sill}^{1.9880}$. Similarly, the relationship of τ_s and L_{sill} , as well as that of τ_c , τ_s , and max. $A_{X>0.2}$ to T_0 , seem to obey a power law (Figure 27).

Our results that the amount of crustal melting generally increases with sill dimension and initial crustal temperature suggests that segregation and migration of melt is more important for larger sills and as the geotherm increases due to continued intrusion. While these results yield some insights about the effect of transient partial melting from a single sill, the actual scenario in the lower crust is much more complicated due to the repetitive intrusion of sills over time. However, the duration between emplacement of successive sills is on order of 10⁴ years [3], [4], which is much longer than the duration of these simulations. Intuitively, more emplaced sills into the crust raises background temperature, and thus later sills will generate more crustal melt. This may result in migration and segregation of the crustal partial melt and subsequent cooling of the lower crust and heating of the upper crust [5]. For completeness, we need to consider the geometry of the sills, the randomness of the intrusion events, and the orientations in which the sills are intruded in the lower crust [4].

7 Conclusions

We have developed a finite element program based on the deal.II library to solve for the time dependent transient partial melting problem following the intrusion of a single sill into the lower crust with a constant background temperature. We employ the continuous Galerkin method with h-adaptive refinement in a structured mesh and an iterative approach to obtain the numerical solutions of both temperature and melt fraction.

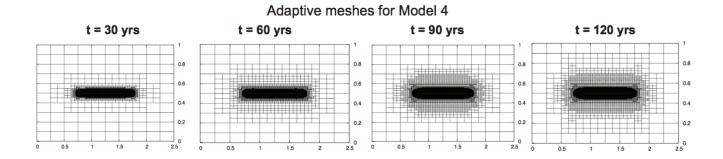


Figure 18: Adaptive meshes for Model 4 at t = 30, 60, 90, and 120 year.

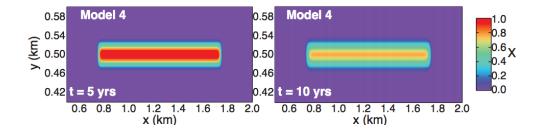


Figure 19: The melt fraction solutions for Model 4 at t = 5 year and t = 10 year. Note that the melt fraction decreases significantly during the period of 5 years.

We find that initial crustal temperature and the dimensions of the sills are the two primary parameters controlling the production of crustal melt. The amount of crustal melting increases with both sill dimension and initial crustal temperature. A higher portion of the lower crust is partially molten and sustain melt fraction higher than 0.2 when we increase the value of both parameters. As a result, migration and segregation of melt may occur due to the high crustal melt productivity generated by the intrusion event. We further deduce that the relationship of τ_c and L_{sill} as well as that of max. $A_{X>0.2}$ and L_{sill} appear to follow power law relationships. The future direction would be to extend the single sill intrusion problem to multiple and repetitive emplacement of sills.

8 References

- [1] Bangerth, W., Heister, T., & Kanschat, G. deal.II differential equations analysis library, technical reference. http://www.dealii.org.
- [2] Bangerth, W., Hartmann, R. & Kanschat, G. (2007). deal.II a general purpose object oriented finite element library, ACM Trans. Math. Softw., pp. 24/1-24/27.

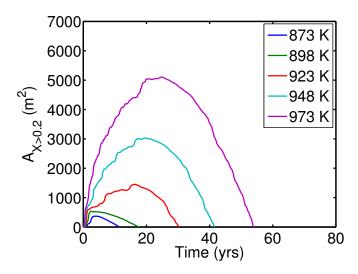


Figure 20: Max. $A_{X>0.2}$ vs. time.

- [3] Annen, C., Blundy, J.D. & Sparks, R.S.J. (2006). The genesis of intermediate and silicic magmas in deep crustal hot zones. *Journal of Petrology* **47(3)**, 505-539.
- [4] Dufek, J. & Bergantz, G. W. (2005). Lower crustal genesis and preservation: a stochastic framework fort the evaluation of basalt-crust interaction. Journal of Petrology 46(11), 2167-2195.
- [5] Lange, R.A. & Hetland, E. A. (2010). The Thermal Evolution of the Lower Arc Crust During Basalt Emplacement: Importance of Melt Advection out of the Lower Crust in Maintaining a Relatively Cool Steady State Geotherm. AGU Fall Meeting Abstracts. V13G-01.
- [6] Lim, S., Hetland, E. A. & Lange, R.A. (2012). Numerical models of transient partial melting of the lower crust during repeated emplacement of basalt sills and subsequent cooling due to advection of melt out of the lower crust. AGU Fall Meeting Abstracts. T13G-2708.
- [7] Hu, H. & Argyropoulos, S.A. (1996). Mathematical modeling of solidification and melting: a review. Modeling Simul. Mater. Sci. Eng. 4, 371-396.
- [8] Janssen, B. & Wick, T. (2010). deal.II compact course. University of Heidelberg, Institute of Applied Mathematics. Session 1-7.
- [9] Vigneresse, J. L., Tikoff, B. & Ameglio, L. (1999). Modification of the regional stress field by magma intrusion and formation of tabular granitic plutons. Elsevier. 302(3), pp. 203-224(22).
- [10] Kelly, D.W., Gago, J. P. & Zienkiewicz, O.C. (1983). A posteriori error analysis and adaptive processes in the finite element method: Part I Error analysis. Int. J. Num. Meth. Eng. 19, 1593-1619.

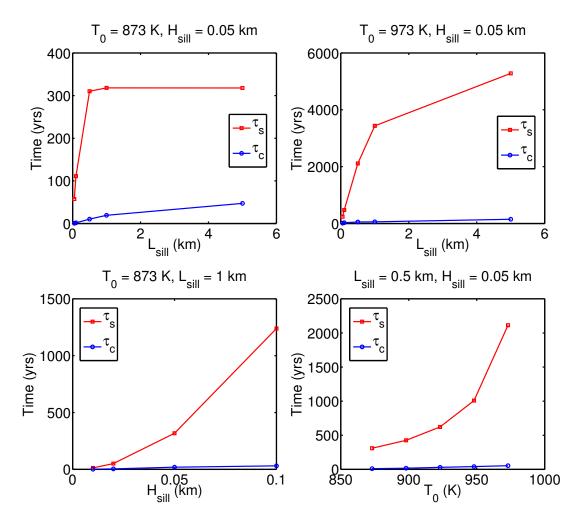


Figure 21: Top left: τ_s and τ_c vs. L_{sill} with $T_0=873$ K; Top right: τ_s and τ_c vs. L_{sill} with $T_0=973$ K; Bottom left: τ_s and τ_c vs. H_{sill} with $T_0=873$ K; Bottom right: τ_s and τ_c vs. T_0 .

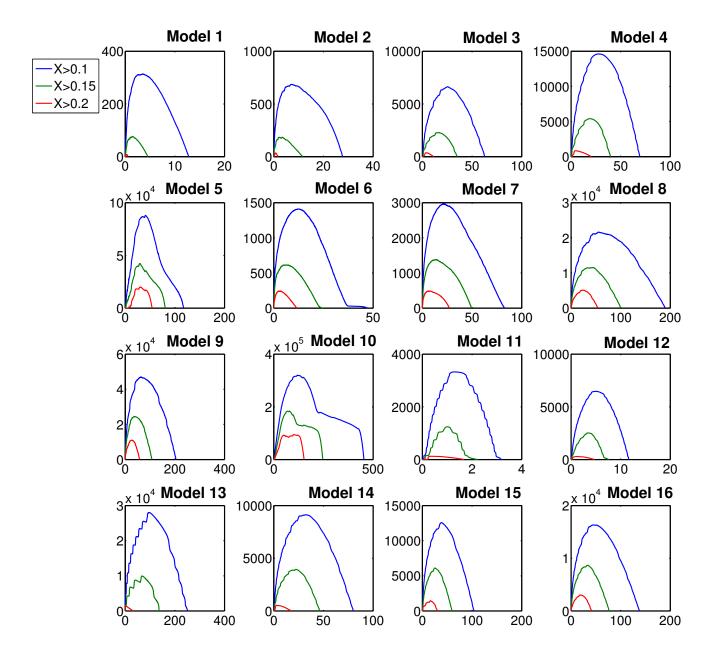


Figure 22: Crustal area (m^2) vs. time (years) plots for Models 1-16.

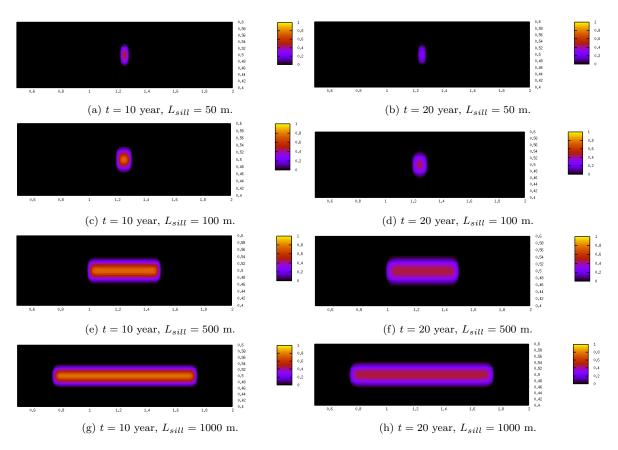


Figure 23: Melt fraction, X, following emplacement of a sill with $H_{sill}=50$ m and L_{sill} varied, where $L_{sill}=50$ m (a-b), 100 m (c-d), 500 m (e-f), and 1000 m (g-h), at times, t=10 and t=20 years in a crust with temperature, $T_0=873$ K.

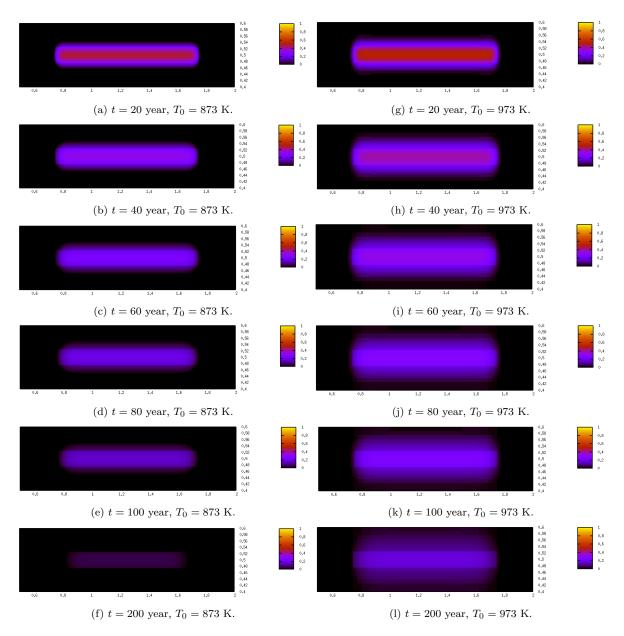


Figure 24: Melt fraction, X, following emplacement at a 1 km by 50 m sill in a crust with temperatures $T_0 = 873$ K (a-f) and $T_0 = 973$ K (g-l) at times, t = 20, 40, 60, 80, 100, and 200 years.

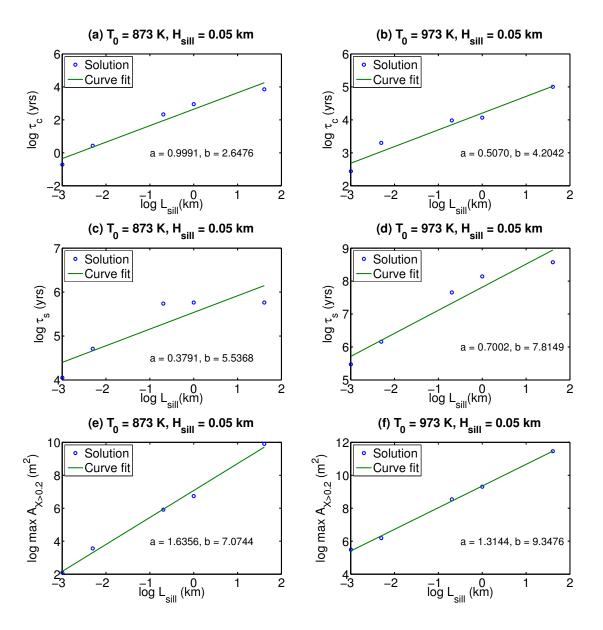


Figure 25: Power laws deduced from simulations for the variables τ_c (a-b), τ_s (c-d), and max. $A_{X>0.2}$ (e-f) vs. L_{sill} . The power laws seem to fit the solution well in (e-f), reasonably well in (a-b), and poorly in (c-d). Here a = slope of the graph and b = y-intercept.

8 REFERENCES 37

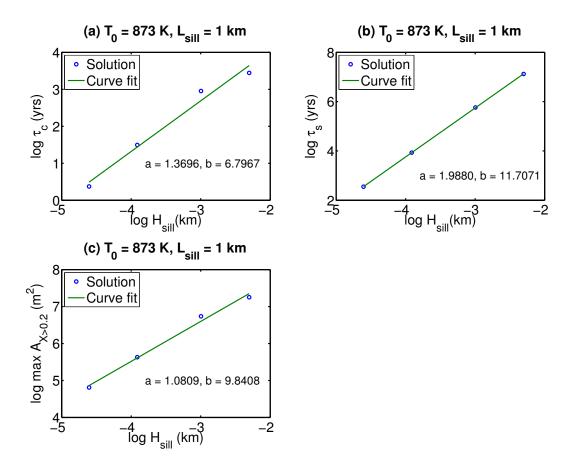


Figure 26: Power laws deduced from simulations for the variables τ_c (a) , τ_s (b), and max. $A_{X>0.2}$ (c) vs. H_{sill} . Here a= slope of the graph and b= y-intercept.

8 REFERENCES 38

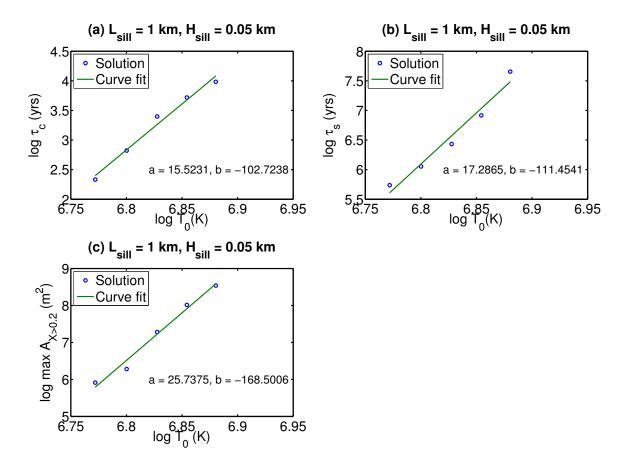


Figure 27: Power laws deduced from simulations for the variables τ_c (a), τ_s (b), and max. $A_{X>0.2}$ (c) vs. T_0 . Here a= slope of the graph and b= y-intercept.

- [11] Annen, C. & Sparks, R.S.J. (2002). Effects of repetitive emplacement of basaltic intrusions on thermal evolution and melt generation in the crust. *Earth and Planetary Science Letters* **203**, 937-955.
- [12] Huppert, H.E. & Sparks, S.J. (1988). The generation of granitic magmas by intrusion of basalt into continental crust. *Journal of Petrology* 29(3), 599-624.
- [13] Eriksson, K., Estep, D., Hansbo, P. & Johnson, C. (1996). Computational differential equations, Cambridge University Press.
- [14] Bradie, B., (2006) A friendly introduction to numerical analysis, Pearson Prentice Hall.
- [15] Gratsch, T. & Bathe, K.J. (2004). A posteriori error estimation techniques in practical finite element analysis, *Elsevier*, doi:10.1016/j.compstruc.2004.08.011
- [16] Verfurth, R. (2003). A posteriori error estimates for finite element discretizations of the heat equation, AMS 40(3), 195-212.
- [17] Flaherty, J.E. (2012). Finite element analysis course notes. RPI. CSCI, MATH 6860: Finite element analysis.
- [18] Farlow, S.J. (1993). Partial differential equations for scientists and engineers, Dover Publications.

Appendices

A Derivation of Analytical Solution to Validation Problems

We consider the problem introduced in Section 5: Find the time-dependent solution T(x, y, t) on $\Omega = [0, L] \times [0, H]$ to the 2D heat balance equation

$$\partial_t T = k^* \nabla^2 T, \tag{24}$$

where $k^* = k/C_p\rho$ is a constant. The solution is subjected to the initial and boundary conditions as stated in (19) - (21).

We find an analytical solution using separation of variables. Since the boundary conditions are not homogeneous, separation of variables cannot be applied directly to find the solution. Instead, we transform the original problem to the one with homogeneous boundary conditions by

$$T(x,y,t) = T_0 - \frac{g_0 H}{2} + g_0 y + w(x,y,t), \tag{25}$$

where

$$w_t = \kappa^* (w_{xx} + w_{yy}), \tag{26}$$

which is subjected to the boundary conditions

$$w(x,0,t) = w(x,H,t) = w_y(0,y,t) = w_y(L,y,t) = 0,$$
(27)

and the initial condition

$$w(x, y, 0) = \begin{cases} T_{sill} - T_0 + \frac{g_0 H}{2} - g_0 y & \text{in } [L_1, L_2] \times [H_1, H_2], \\ 0 & \text{elsewhere.} \end{cases}$$
(28)

We find a solution to the transformed problem of the form

$$w(x, y, t) = X(x)Y(y)T(t)$$
(29)

to

$$w_t = k^* (w_{xx} + w_{yy}). (30)$$

Substituting (29) into (30) and rearranging terms, we find

$$X(x)Y(y)T'(t) = k^* \{X'' Y(y) T(t) + X(x)Y''(y)T(t)\}.$$
(31)

Therefore,

$$\frac{T'(t)}{k^*T(t)} = \frac{X''(x)}{X(x)} + \frac{Y''(y)}{Y(y)} = -\lambda,$$
(32)

and

$$T'(t) = -\lambda \ k^* T(t) \implies T(t) = A e^{-\lambda k^* t}, \tag{33}$$

$$\frac{X''(x)}{X(x)} = -\lambda - \frac{Y''(y)}{Y(y)} = -\beta, \tag{34}$$

where

$$X''(x) = -\beta X(x) \implies X(x) = B\cos(\sqrt{\beta}x) + C\sin(\sqrt{\beta}x), \tag{35}$$

$$Y''(y) = (\beta - \lambda)Y(y) \implies Y(y) = D\cos(\sqrt{\lambda - \beta}y) + E\sin(\sqrt{\lambda - \beta}y), \tag{36}$$

and

$$Y(0) = 0 \implies D = 0 \implies Y(y) = E\sin(\sqrt{\lambda - \beta}y),$$
 (37)

$$Y(H) = 0 \implies E\sin(\sqrt{\lambda - \beta}H) = 0 \implies \sqrt{\lambda - \beta}H = m\pi \implies \lambda - \beta = \left(\frac{m\pi}{H}\right)^2, \ m = 1, 2, 3.$$
 (38)

Plugging in the X(x) and Y(y) obtained and applying the boundary conditions, we get

$$w(x, y, t) = Ae^{-\lambda k^* t} \{ B\cos(\sqrt{\beta}x) + C\sin(\sqrt{\beta}x) \} E\sin\left(\frac{m\pi y}{H}\right), \tag{39}$$

$$w_y(0, y, t) = ABE \ e^{-\lambda k^* t} \frac{m\pi}{H} \cos\left(\frac{m\pi y}{H}\right) = 0, \tag{40}$$

$$w_y(L, y, t) = Ae^{-\lambda k^* t} \frac{m\pi}{H} \left[B\cos(\sqrt{\beta}L) + C\sin(\sqrt{\beta}L) \right] \left[E\cos\left(\frac{m\pi y}{H}\right) \right] = 0, \tag{41}$$

$$B = 0 \implies C \sin(\sqrt{\beta}L) = 0 \implies \beta = \left(\frac{n\pi}{L}\right), \ n = 1, 2, 3, ...,$$
 (42)

$$\lambda - \left(\frac{n\pi}{L}\right)^2 = \left(\frac{m\pi}{H}\right)^2 \implies \lambda_{mn} = \left(\frac{n\pi}{L}\right)^2 + \left(\frac{m\pi}{H}\right)^2, \ n, m = 1, 2, 3, ..., \tag{43}$$

$$w_{nm}(x,y,t) = A_{nm}C_{nm}E_{nm} e^{-\left[\left(\frac{n\pi}{L}\right)^2 + \left(\frac{m\pi}{H}\right)^2\right]k^*t} \sin\left(\frac{n\pi x}{L}\right)\sin\left(\frac{m\pi y}{H}\right),\tag{44}$$

$$w(x,y,t) = \sum_{n=1}^{\infty} \sum_{m=1}^{\infty} \tilde{C}_{nm} e^{-\left[\left(\frac{n\pi}{L}\right)^2 + \left(\frac{m\pi}{H}\right)^2\right]k^*t} \sin\left(\frac{n\pi x}{L}\right) \sin\left(\frac{m\pi y}{H}\right). \tag{45}$$

Applying the initial condition, we find \tilde{C}_{nm} .

$$w(x,y,0) = \sum_{n=1}^{\infty} \sum_{m=1}^{\infty} \tilde{C}_{nm} \sin\left(\frac{n\pi x}{L}\right) \sin\left(\frac{m\pi y}{H}\right) = \begin{cases} T_{sill} - T_0 + \frac{g_0 H}{2} - g_0 y & \text{on } \Omega_{sill} = [L_1, L_2] \times [H_1, H_2], \\ 0 & \text{elsewhere,} \end{cases}$$

$$(46)$$

where

$$\tilde{C}_{nm} = \frac{4(T_{sill} - T_0 + \frac{g_0 H}{2} - g_0 y)}{nm\pi^2} \left[\cos\left(\frac{n\pi L_2}{L}\right) - \cos\left(\frac{n\pi L_1}{L}\right) \right] \left[\cos\left(\frac{m\pi H_2}{H}\right) - \cos\left(\frac{m\pi H_1}{H}\right) \right]. \tag{47}$$

Hence, the desired solution is

$$w(x,y,t) = \sum_{n=1}^{\infty} \sum_{m=1}^{\infty} \tilde{C}_{nm} \ e^{-\left[\left(\frac{n\pi}{L}\right)^2 + \left(\frac{m\pi}{H}\right)^2\right]k^*t} \sin\left(\frac{n\pi x}{L}\right) \sin\left(\frac{m\pi y}{H}\right), \tag{48}$$

where

$$\tilde{C}_{nm} = \frac{4(T_{sill} - T_0 + \frac{g_0 H}{2} - g_0 y)}{nm\pi^2} \left[\cos\left(\frac{n\pi L_2}{L}\right) - \cos\left(\frac{n\pi L_1}{L}\right) \right] \left[\cos\left(\frac{m\pi H_2}{H}\right) - \cos\left(\frac{m\pi H_1}{H}\right) \right]. \tag{49}$$

Finally, the complete solution to the validation problems in Section 5 is

$$T(x,y,t) = T_0 - \frac{g_0 H}{2} + g_0 y + w(x,y,t).$$
 (50)

B Source Codes

B.1 Verification codes for validation models

 $_{6}$ // REQUIRES: t > 0, x and y must be in the range of the domain.

^{2 #}include <fstream>

^{3 #}include <iostream>

^{4 #}include <cmath>

```
// MODIFIES: none.
   // EFFECTS: compute the analytical solution up to N terms for a specified geotherm g_0.
    double compute (double t, double x, double y){
      double pi = 3.14159265;
10
      double series_soln = 0;
11
      const double sec = (365.25*24*3600);
12
      const double k = 8.154421735e19;
13
      const double rho = 3.05e12;
14
      const double cp = 1390*sec*sec/1000000;
15
      const double k1 = k/(rho*cp);
16
17
      const double T_o = 1558.;
      const double L1 = 1.0;
18
      const double L2 = 1.5;
19
      const double W1 = 0.475;
20
      const double W2 = 0.525;
21
      const double L = 2.5;
22
23
      const double H = 1.0;
24
      const double back_temp = 873;
      const double grad = 0; /* specify which validation models to compute */
25
      const int N = 50; /* specify number of terms computed */
26
27
28
      for(int n=1; n<N; n++){
29
              for(int m=1; m<N; m++){
30
                   cos(W1*m*pi/H))*(cos(L2*n*pi/L)-cos(L1*n*pi/L));
31
32
                   series_soln += bnm*exp(-(((n*n/(L*L)+m*m/(H*H))*pi*pi)*k1*t))
                                   * sin(n*pi*x/L)*sin(m*pi*y/H);
33
34
35
     series_soln += back_temp - grad*H/2 + grad*y;
36
37
     return series_soln;
38
   }
39
40
   int main ()
41
   {
42
      int k = 0;
43
      const double dt = 0.1;
44
      std::ofstream file;
45
      file.open("series_solution.txt");
46
      while (k \le 500){ /* run for 500 time steps */
47
         std::cout << "Time: " << k*0.1 << std::endl;
48
49
50
         /* compute series solution at 4 different points in the domain */
         file << k
51
52
              << " " << compute(k*dt, 1.25, 0.525)
              << " " << compute(k*dt, 1.25, 0.530)
53
              << " " << compute(k*dt, 1.5, 0.525)
              << " " << compute(k*dt, 1.5, 0.530)
55
```

B.2 Program codes

Note: Makefile is available upon installation of deal.II.

```
# List of parameters for numerical experiments
65
     # Specify the test case we want to run:
     # TEST_ZERO - test case with analytical solution
     \mbox{\tt\#} TEST_ONE - test case with variable k and a melt profile
     set TestCase = TEST_ZERO
70
     subsection Physical data
       # Declare the initial time, final time, time step size, and domain length
71
72
73
       set final_time = 50.
       set time_step
74
75
       # Declare the onset temperature of solid and liquid in the crust (TC) and basalt (TM)
76
       # Irrelevant if Test0 is set
77
       set TC_solid = 1025.0
78
       set TC_liquid = 1858.0
79
       set TM_solid = 999.0
80
       set TM_interm = 1366.0
81
       set TM_liquid = 1513.0
82
     end
83
84
     subsection Space discretization
85
       \ensuremath{\mathtt{\#}} Declare the data that is relevant to the space discretization
86
       set deg = 2
87
       set freq = 50
88
       set ini_refinement_level = 10
89
       set n_pre_refinement_steps = 7
90
92
       # Specify the refinement criterion to use for adaptive remeshing:
       \# 1- global refinement, 2- KellyErrorEstimator, 3- 2ndDerivativeApproximation
93
       set mode = 2
       # If mode = 1, specify the levels of global refinement
       set level = 3
```

```
100
    ------ source.cc
101
    /* Disclaimer: This program is developed by modifying the existing tutorial programs
102
                   in deal.II documentation. A large parts of the codes in this program
103
                   are inherited from the tutorial programs for the purpose of solving
104
                   a problem in an application
105
106
    /* Copyright (C) 2009-2012 by deal.II authors
107
108
    /* Instruction: To perform numerical experiments, either change the variables in
109
       parameter.prm or in the namespace SillData @line 78
110
111
    #include <deal.II/base/parameter_handler.h>
112
    #include <deal.II/base/data out base.h>
113
    #include <base/quadrature_lib.h>
114
115
    #include <base/function.h>
116
    #include <base/logstream.h>
    #include <base/utilities.h>
117
118
    #include <base/smartpointer.h>
    #include <base/timer.h>
119
120
    #include <lac/vector.h>
    #include <lac/full_matrix.h>
121
    #include <lac/sparse_matrix.h>
122
123
    #include <lac/solver_cg.h>
    #include <lac/compressed_sparsity_pattern.h>
124
    #include <lac/precondition.h>
125
    #include <lac/filtered_matrix.h>
    #include <lac/constraint_matrix.h>
    #include <grid/tria.h>
128
    #include <grid/grid_generator.h>
129
    #include <grid/grid_tools.h>
130
    #include <grid/tria_accessor.h>
131
    #include <grid/tria_iterator.h>
132
    #include <grid/grid_refinement.h>
133
    #include <deal.II/grid/grid_out.h>
134
    #include <deal.II/dofs/dof_tools.h>
135
    #include <dofs/dof_handler.h>
136
    #include <dofs/dof_accessor.h>
137
    #include <dofs/dof_tools.h>
138
    #include <dofs/dof_constraints.h>
139
    #include <dofs/dof_renumbering.h>
140
    #include <fe/fe_q.h>
141
    #include <fe/fe_values.h>
142
    #include <fe/mapping_q.h>
143
    #include <numerics/vectors.h>
144
    #include <numerics/matrices.h>
145
    #include <numerics/data_out.h>
146
    #include <numerics/error_estimator.h>
```

147

```
#include <numerics/solution_transfer.h>
148
     #include <numerics/derivative_approximation.h>
149
150
    #include <cmath>
151
     #include <fstream>
152
     #include <iostream>
153
     #include <list>
154
     #include <iomanip>
155
     #include <algorithm>
156
157
158
     namespace Earth
     {
159
     using namespace dealii;
160
161
     {\tt namespace} \ {\tt EquationConstants}
162
                                                       /* UNITS
                                                                             */
163
      {
         const double sec = (365.25*24*3600);
                                                       /* s
164
                                                                             */
         const double k = 8.154421735e19;
                                                       /* kg*km/(K*yr^3)
165
         const double rho_cs = 3.05e12;
                                                       /* kg/km^3
166
         const double rho_cl = 2.3e12;
                                                       /* kg/km^3
168
         const double rho_bs = 3.1e12;
                                                       /* kg/km^3
         const double rho_bl = 2.83e12;
                                                       /* kg/km^3
169
         const double L_b = (4.0e5)*sec*sec/1000000; /* km^2/(K*yr^2)
         const double L_c = (3.5e5)*sec*sec/1000000; /* km^2/(K*yr^2)
171
         const double cp_b = 1480*sec*sec/1000000; /* km^2/yr^2
172
173
         const double cp_c = 1390*sec*sec/1000000;  /* km^2/yr^2
         double kstar = 0;
174
     }
175
176
     namespace SillData
177
178
        const double DomainLength = 2.5;
                                                       /* km
                                                                             */
179
        const double DomainHeight = 1.0;
                                                       /* km
180
        const double L1 = 1.0;
                                                       /* km
181
        const double L2 = 1.5;
                                                       /* km
                                                                             */
182
                                                       /* km
        const double W1 = 0.475;
183
                                                       /* km
        const double W2 = 0.525;
184
        const double ini_temp = 1558.;
                                                       /* K
                                                                             */
185
        const double geotherm = 0.;
                                                      /* K/km
                                                                            */
186
        const double back_temp = 873.;
                                                       /* K
187
     }
188
189
190
     namespace Parameters
191
     {
192
        enum TestCase
193
194
          TEST_ZERO,
195
           TEST_ONE
196
        };
```

```
class DataInput
198
199
          public:
200
             DataInput ();
201
             "DataInput ();
202
             void read_data (const char *filename);
203
             TestCase test;
204
             double time,
205
             final_time,
206
207
             time_step,
             TC_liquid,
208
             TC_solid,
209
             TM_liquid,
210
             TM_interm,
211
             TM_solid,
212
             dm_meltfrac;
213
             unsigned int deg;
             unsigned int freq,
215
             mode,
217
             ini_refinement_level,
             n_pre_refinement_steps,
218
219
             level;
220
          protected:
             ParameterHandler prm;
221
222
        };
223
        DataInput::DataInput()
224
225
             prm.declare_entry ("TestCase", "TEST_ONE",
226
                                 Patterns::Selection ("TEST_ZERO|TEST_ONE"),
227
                                  "Used to select the test case that we are going "
228
                                 "to use. ");
229
230
             prm.enter_subsection ("Physical data");
231
232
                prm.declare_entry ("time", "0.", Patterns::Double (0.),
233
                                     "Time of simulation. ");
234
                prm.declare_entry ("final_time", "0.", Patterns::Double (0.),
235
                                     "Final time of simulation. ");
236
                prm.declare_entry ("time_step", "0.", Patterns::Double (0.),
237
                                     "Time step of simulation. ");
238
                prm.declare_entry ("TC_solid", "0.", Patterns::Double (0.),
239
240
                                     "Solid temp for crust. ");
                prm.declare_entry ("TC_liquid", "0.", Patterns::Double (0.),
241
242
                                     "Liquid temp for crust. ");
                prm.declare_entry ("TM_solid", "0.", Patterns::Double (0.),
243
244
                                     "Solid temp for sill. ");
                prm.declare_entry ("TM_interm", "0.", Patterns::Double (0.),
245
```

197

```
"Intermediate temp for sill. ");
246
                 prm.declare_entry ("TM_liquid", "0.", Patterns::Double (0.),
247
                                     "Liquid temp for sill. ");
248
249
             }
250
             prm.leave_subsection();
251
252
             prm.enter_subsection ("Space discretization");
253
             {
254
                 prm.declare_entry ("deg", "1", Patterns::Integer (1,3),
255
256
                                     "Polynomial degree for the temperature space");
                 prm.declare_entry ("freq", "0", Patterns::Integer (0,10000),
257
                                     "Frequency of pre-time adaptive refinement");
258
                 prm.declare_entry ("ini_refinement_level", "2",
259
260
                                     Patterns::Integer (2,1000),
                                     "Initial number of cells = this*this");
261
262
                 {\tt prm.declare\_entry~("n\_pre\_refinement\_steps",~"0",}
                                     Patterns::Integer (0,10),
264
                                     "Number of pre adaptive refinement steps");
                 prm.declare_entry ("mode", "1", Patterns::Integer (1, 5),
                                     "Choice of refinement strategy. ");
266
                 prm.declare_entry ("level", "0", Patterns::Integer (0, 10),
267
                                     "Number of global refinements for mode 1. ");
             }
269
             prm.leave_subsection();
270
271
        }
272
273
        DataInput::~DataInput()
274
        {}
275
276
        void DataInput::read_data (const char *filename)
277
        {
278
             std::ifstream file (filename);
279
             AssertThrow (file, ExcFileNotOpen (filename));
280
281
             prm.read_input (file);
282
283
             if (prm.get ("TestCase") == std::string ("TEST_ZERO")){
284
                 test = TEST_ZERO;
285
             }
286
287
             else{
                 test = TEST_ONE;
288
289
             }
290
291
             prm.enter_subsection ("Physical data");
292
293
                 time = prm.get_double ("time");
294
                 final_time = prm.get_double ("final_time");
```

```
time_step = prm.get_double ("time_step");
295
                TC_solid = prm.get_double ("TC_solid");
296
                TC_liquid = prm.get_double ("TC_liquid");
297
                TM_solid = prm.get_double ("TM_solid");
298
                TM_interm = prm.get_double ("TM_interm");
299
                TM_liquid = prm.get_double ("TM_liquid");
300
             }
301
             prm.leave_subsection();
302
303
             prm.enter_subsection ("Space discretization");
304
305
                deg = prm.get_integer ("deg");
306
                freq = prm.get_integer ("freq");
307
                ini_refinement_level = prm.get_integer ("ini_refinement_level");
308
                n_pre_refinement_steps = prm.get_integer ("n_pre_refinement_steps");
309
                mode = prm.get_integer ("mode");
310
                level = prm.get_integer ("level");
311
             }
313
             prm.leave_subsection();
        }
315
      }
316
317
318
      /* class denoting the initial conditions for case with zero geotherm */
319
      class InitialValues_ZeroGeotherm : public Function<2>
320
      {
321
        public:
322
             InitialValues_ZeroGeotherm (const unsigned int n_components = 2,
323
                      const double time = 0.)
324
325
                      Function<2>(n_components, time)
326
             {}
327
             virtual double value (const Point<2> &p,
328
                      const unsigned int component = 0) const;
329
             virtual void vector_value (const Point<2> &p,
330
                      Vector<double> &value) const;
331
     };
332
333
      double InitialValues_ZeroGeotherm::value (const Point<2> &p,
334
             const unsigned int /*component*/) const
335
336
      {
             const double x = p[0];
337
             const double y = p[1];
338
339
340
             if(x>=SillData::L1 && x<=SillData::L2 && y>= SillData::W1
341
                      && y<=SillData::W2){
342
                      return SillData::ini_temp;
343
             }
```

```
else{
344
                      return SillData::back_temp;
345
             }
346
      }
347
348
      void InitialValues_ZeroGeotherm::vector_value (const Point<2> &p,
349
             Vector<double> &value) const
350
351
      {
             for (unsigned int c=0; c<this->n_components; ++c){
352
                      value(c) = InitialValues_ZeroGeotherm::value(p,c);
353
354
             }
      }
355
356
      /st class denoting the initial conditions for case with nonzero geotherm st/
357
      class InitialValues_Geotherm : public Function<2>
358
359
      {
360
        public:
361
             InitialValues_Geotherm (const unsigned int n_components = 2,
                      const double time = 0.)
362
                      Function<2>(n_components, time)
364
             {}
365
366
             virtual double value (const Point<2> &p,
                      const unsigned int component = 0) const;
367
             virtual void vector_value (const Point<2> &p,
368
                      Vector<double> &value) const;
369
      };
370
371
      double InitialValues_Geotherm::value (const Point<2> &p,
372
             const unsigned int /*component*/) const
373
      {
374
             const double x = p[0];
375
             const double y = p[1];
376
377
             if(x>=SillData::L1 && x<=SillData::L2 && y>= SillData::W1
378
                      && y<=SillData::W2){
379
                      return SillData::ini_temp;
380
             }
381
             else{
382
                      return (SillData::back_temp-SillData::geotherm*SillData::DomainHeight/2) +
383
                              SillData::geotherm*y;
384
385
             }
386
      }
387
      void InitialValues_Geotherm::vector_value (const Point<2> &p,
388
389
             Vector<double> &value) const
390
391
             for (unsigned int c=0; c<this->n_components; ++c){
                      value(c) = InitialValues_Geotherm::value(p,c);
392
```

```
}
393
     }
394
395
396
      /* class denoting the boundary conditions for case with zero geotherm */
397
      class BoundaryData_ZeroGeotherm : public Function<2>
398
399
      {
        public:
400
             BoundaryData_ZeroGeotherm (const double time = 0.) : Function<2>(1, time) {}
401
             virtual double value (const Point<2> &p,
402
403
                                    const unsigned int component = 0) const;
             virtual void value_list (const std::vector<Point<2> > &points,
404
405
                                       std::vector<double>
                                                                      &values.
                                       const unsigned int component = 0) const;
406
407
     };
408
409
      double BoundaryData_ZeroGeotherm::value (const Point<2> & /*p*/,
410
             const unsigned int /*component*/ ) const
411
             return SillData::back_temp;
     }
413
414
415
      void BoundaryData_ZeroGeotherm::value_list(const std::vector<Point<2> > &points,
416
                                      std::vector<double>
                                                                     &values,
                                      const unsigned int component) const
417
      {
418
              Assert (values.size() == points.size(),
419
                     ExcDimensionMismatch (values.size(), points.size()));
420
              Assert (component == 0,
421
                     ExcIndexRange (component, 0, 1));
422
423
             const unsigned int n_points = points.size();
424
425
             for (unsigned int i=0; i<n_points; ++i)</pre>
426
             {
427
                     values[i] = BoundaryData_ZeroGeotherm::value(points[i]);
428
             }
429
     }
430
431
      /* class denoting the boundary conditions for case with nonzero geotherm */
432
      class BoundaryData_Geotherm : public Function<2>
433
434
      {
435
         public:
436
             BoundaryData_Geotherm (const double time = 0.) : Function<2>(1, time) {}
             virtual double value (const Point<2> &p,
437
438
                                    const unsigned int component = 0) const;
439
             virtual void value_list (const std::vector<Point<2> > &points,
440
                                       std::vector<double>
                                                                      &values,
441
                                       const unsigned int component = 0) const;
```

```
};
442
443
      double BoundaryData_Geotherm::value (const Point<2>
                                                               &p,
444
             const unsigned int /*component*/ ) const
445
446
      {
             const double x = p[0];
447
             const double y = p[1];
448
449
             if(x>=SillData::L1 && x<=SillData::L2 && y>= SillData::W1
450
                      && y<=SillData::W2){
451
452
                      return SillData::ini_temp;
             7
453
             else{
454
                      return (SillData::back_temp-SillData::geotherm*SillData::DomainHeight/2) +
455
                              SillData::geotherm*y;
456
457
             }
458
      }
460
      void BoundaryData_Geotherm::value_list(const std::vector<Point<2> > &points,
                                       std::vector<double>
462
                                       const unsigned int component) const
      {
463
464
              Assert (values.size() == points.size(),
465
                      ExcDimensionMismatch (values.size(), points.size()));
              Assert (component == 0,
466
                      ExcIndexRange (component, 0, 1));
467
468
             const unsigned int n_points = points.size();
469
470
             for (unsigned int i=0; i<n_points; ++i)
471
472
                      values[i] = BoundaryData_Geotherm::value(points[i]);
473
             }
474
     }
475
476
      /* class denoting the right hand side */
477
      class RightHandSide : public Function<2>
478
      {
479
        public:
480
             RightHandSide (double time = 0.) : Function<2>(1, time) {}
481
             virtual double value (const Point<2> &p,
482
483
                                    const unsigned int component = 0) const;
             virtual void value_list (const std::vector<Point<2> > &points,
484
485
                                        std::vector<double>
                                                                      &values,
                                        const unsigned int component = 0) const;
486
487
      };
489
      double RightHandSide::value (const Point<2> &/*p*/,
490
                                    const unsigned int /*component*/ ) const
```

```
{
491
             return 0;
492
      }
493
494
      void RightHandSide::value_list(const std::vector<Point<2> > &points,
495
                                      std::vector<double>
                                                                    &values.
496
                                      const unsigned int component) const
497
      {
498
             Assert (values.size() == points.size(),
499
             ExcDimensionMismatch (values.size(), points.size()));
500
501
             Assert (component == 0,
             ExcIndexRange (component, 0, 1));
502
503
             const unsigned int n_points = points.size();
504
505
             for (unsigned int i=0; i<n_points; ++i){
506
                      values[i] = RightHandSide::value(points[i]);
507
             }
509
      }
511
      /* the main class */
      class Model
512
513
514
        public:
          Model (const Parameters::DataInput &data);
515
          void run ();
516
517
        protected:
518
          Parameters::TestCase test;
519
          unsigned int deg;
520
          unsigned int freq, ini_refinement_level;
521
          unsigned int n_pre_refinement_steps, mode, level;
522
          double time, time_step;
523
          const double final_time;
524
          const double TC_0, TC_1, TM_0, TM_1, TM_i;
525
526
527
        private:
          void make_initial_grid ();
528
          void setup_dof ();
529
          void refine_by_Kelly ();
530
          void refine_by_derivative ();
531
          void refine_grid (const unsigned int max_grid_level);
532
          void assemble_term ();
533
534
          void compute_oldterm ();
          void compute_newterm ();
535
536
          void compute_matrix ();
537
          void assemble_system ();
538
          void solve ();
          void output_results (const unsigned int timestep_number) const;
```

```
double evaluate_soln (double x, double y) const ;
540
          double compute_kstar (double temp, unsigned char id);
541
542
          Triangulation<2>
                                        triangulation;
543
          FE_Q<2>
                                        fe;
544
          DoFHandler<2>
                                        dof_handler;
545
546
          {\tt SparsityPattern}
                                        sparsity_pattern;
547
          SparseMatrix<double>
548
                                        system_matrix;
549
550
          ConstraintMatrix
                                        constraints;
551
          PreconditionSSOR<>
                                        preconditioner;
552
553
          const MappingQ<2>
554
                                        mapping;
555
556
          bool
                                        rebuild_matrix;
558
          Vector<double>
                                        solution, old_solution, melt_fraction;
          Vector<double>
                                        system_rhs;
560
          std::vector<double>
                                        error;
561
562
          double
                                        theta;
563
          RightHandSide
                                        rhs;
564
565
          BoundaryData_ZeroGeotherm
                                        boundarydata1;
          BoundaryData_Geotherm
                                        boundarydata2;
566
          InitialValues_ZeroGeotherm initialvalues1;
567
          InitialValues_Geotherm
                                        initialvalues2;
568
          TimerOutput
                                        computing_timer;
569
          std::ofstream
                                        summary;
570
      };
571
572
      Model::Model (const Parameters::DataInput &data)
573
574
         test (data.test),
575
         freq (data.freq),
576
         ini_refinement_level (data.ini_refinement_level),
577
         n_pre_refinement_steps (data.n_pre_refinement_steps),
578
         mode (data.mode),
579
         level (data.level),
580
         time (data.time),
581
         time_step (data.time_step),
582
583
         final_time (data.final_time),
         TC_0 (data.TC_solid),
584
585
         TC_1 (data.TC_liquid),
586
         TM_0 (data.TM_solid),
587
         TM_1 (data.TM_liquid),
         TM_i (data.TM_interm),
```

```
fe (data.deg),
589
         dof_handler (triangulation),
590
         mapping (4),
591
         rebuild_matrix (false),
592
         theta (1.0), /* 0 <= theta <= 1
593
                         theta = 0 corresp to explicit Euler scheme - 1st order acc
594
                         theta = 1 corresp to implicit Euler scheme - 1st order acc
595
                         theta = 0.5 corresp to Crank-Nicolson scheme - 2nd order acc
596
597
         rhs (time),
598
599
         boundarydata1 (time),
         boundarydata2 (time),
600
601
         computing_timer (summary, TimerOutput::summary, TimerOutput::wall_times)
      {}
602
603
604
      /* compute k* at a particular time step using previous solution */
      double Model::compute_kstar(double temp, unsigned char id)
605
607
           const double k = EquationConstants::k;
           const double cp_c = EquationConstants::cp_c;
           const double cp_b = EquationConstants::cp_b;
609
           const double L_c = EquationConstants::L_c;
610
611
           const double L_b = EquationConstants::L_b;
           const double rho_cs = EquationConstants::rho_cs;
612
           const double rho_cl = EquationConstants::rho_cl;
613
           const double rho_bs = EquationConstants::rho_bs;
614
           const double rho_bl = EquationConstants::rho_bl;
615
           double kstar = 10000000;
616
           double denom = 1.;
617
618
           if(test == Parameters::TEST_ZERO){
619
                      kstar = k/(rho_cs*cp_c);
620
621
           else if(id == 'c'){
622
              if(temp >= TC_0 && temp <= TC_1){
623
                      double dc_mf = 1/(TC_1 - TC_0);
624
                      double meltf = dc_mf*temp-1.230492197;
625
                      double rho = meltf*(rho_cl - rho_cs) + rho_cs;
626
                      kstar = (k/(rho*cp_c + rho*L_c*dc_mf))/denom;
627
              7
628
              else if(temp > TC_1){
629
                      kstar = (k/(rho_cl*cp_c + rho_cl*L_c*1))/denom;
630
              }
631
632
              else{
                      kstar = (k/(rho_cs*cp_c + rho_cs*L_c*0))/denom;
633
634
              }
635
           7
636
           else if(id == 'm'){
              if(temp >= TM_0 && temp <= TM_i)\{
```

```
double dm_mf = 1.4e-3;
638
                      double meltf = dm_mf*temp - 1.3986;
639
                      double rho = meltf*(rho_bl - rho_bs) + rho_bs;
640
                      kstar = (k/(rho*cp_b + rho*L_b*dm_mf))/denom;
641
642
              else if(temp >= TM_i && temp <= TM_1){
643
                      double dm_mf = 3.307482993e-3;
644
                      double meltf = dm_mf*temp - 4.004221768;
645
                      double rho = meltf*(rho_bl - rho_bs) + rho_bs;
646
                      kstar = (k/(rho*cp_b + rho*L_b*dm_mf))/denom;
647
648
              }
              else if(temp > TM_1){
649
                      kstar = (k/(rho_bl*cp_b + rho_bl*L_b*1))/denom;
650
              }
651
652
              else{
                      kstar = (k/(rho_bs*cp_b + rho_bs*L_b*0))/denom;
653
654
              }
           }
656
           else{
                      std::cout << " Error in allocating subdomains! " << std::endl;</pre>
           }
658
659
660
           return kstar;
661
       }
662
663
       /* adaptive refinement with KellyErrorEstimator */
       void Model::refine_by_Kelly ()
664
       {
665
           std::cout << "===== Refined adaptively using KellyErrorEstimator =======
666
                        << std::endl;
667
           Vector<float> estimated_error_per_cell (triangulation.n_active_cells());
668
669
           KellyErrorEstimator<2>::estimate (mapping, dof_handler,
670
                                                QGauss<1>(3),
671
                                                FunctionMap<2>::type(),
672
                                                solution,
673
                                                estimated_error_per_cell);
674
675
           if(time == 0){
676
               GridRefinement::refine_and_coarsen_fixed_number (triangulation,
677
                                                                    estimated_error_per_cell,
678
679
                                                                    0.3, 0.1);
           }
680
681
           else if (time < 1000*time_step){</pre>
               GridRefinement::refine_and_coarsen_fixed_number (triangulation,
682
683
                                                                    estimated_error_per_cell,
                                                                    0.005, 0.0025);
684
685
           }
           else{
```

```
GridRefinement::refine_and_coarsen_fixed_number (triangulation,
687
                                                                  estimated_error_per_cell,
688
                                                                  0.003, 0.0025);
689
           }
690
       }
691
692
693
       /* adaptive refinement with DerivativeApproximation */
694
       void Model::refine_by_derivative ()
695
696
697
           std::cout << "====== Refined adaptively using DerivativeApproximation ======="
                        << std::endl;
698
699
           Vector<float> gradient_indicator (triangulation.n_active_cells());
701
702
           DerivativeApproximation::approximate_second_derivative (mapping,
703
                                                                       dof_handler,
                                                                       solution,
705
                                                                       gradient_indicator);
           DoFHandler<2>::active_cell_iterator
707
           cell = dof_handler.begin_active(),
708
709
           endc = dof_handler.end();
           for (unsigned int cell_no=0; cell!=endc; ++cell, ++cell_no)
710
               gradient_indicator(cell_no)*=std::pow(cell->diameter(), 3.);
711
712
               if(time == 0){
713
                      GridRefinement::refine_and_coarsen_fixed_number (triangulation,
714
                                                                          gradient_indicator,
715
                                                                          0.3, 0.1);
716
717
               else if (time < 1000*time_step){</pre>
718
                      GridRefinement::refine_and_coarsen_fixed_number (triangulation,
719
                                                                          gradient_indicator,
720
                                                                          0.005, 0.0025);
721
               }
722
               else{
723
                      GridRefinement::refine_and_coarsen_fixed_number (triangulation,
724
                                                                          gradient_indicator,
725
                                                                          0.002, 0.0025);
726
              }
727
728
       }
729
730
       /* main function for adaptive mesh refinement*/
       void Model::refine_grid (const unsigned int max_grid_level)
731
732
       {
          computing_timer.enter_section ("Remeshing");
733
734
          if(mode == 1){
735
```

```
std::cout << "====== Refined globally " << level << " times ======"
736
                         << std::endl;
737
738
          else if(mode == 2){
739
             refine_by_Kelly();
740
          }
741
742
          else{
             refine_by_derivative();
743
          7
744
745
746
          if(triangulation.n_levels() > max_grid_level)
             for(Triangulation<2>::active_cell_iterator
747
                      cell = triangulation.begin_active(max_grid_level);
748
                      cell != triangulation.end(); ++cell){
749
750
                              cell->clear_refine_flag();
             }
751
752
             SolutionTransfer<2> soltrans (dof_handler);
754
             /* Transfer old soln to new mesh */
             triangulation.prepare_coarsening_and_refinement();
757
758
             soltrans.prepare_for_coarsening_and_refinement (solution);
759
             triangulation.execute_coarsening_and_refinement ();
760
761
             dof_handler.distribute_dofs(fe);
762
763
             constraints.clear();
764
             DoFTools::make_hanging_node_constraints (dof_handler, constraints);
765
             constraints.close();
766
767
             system_matrix.clear();
768
769
             CompressedSparsityPattern c_sparsity (dof_handler.n_dofs());
770
             DoFTools::make_sparsity_pattern (dof_handler, c_sparsity);
771
             constraints.condense (c_sparsity);
772
             sparsity_pattern.copy_from(c_sparsity);
773
774
775
             Vector<double> interpolated_soln(dof_handler.n_dofs());
776
777
             soltrans.interpolate(solution, interpolated_soln);
             solution = interpolated_soln;
778
779
             system_matrix.reinit(sparsity_pattern);
780
781
             old_solution.reinit(dof_handler.n_dofs());
782
             system_rhs.reinit(dof_handler.n_dofs());
783
784
             rebuild_matrix = true;
```

```
785
             computing_timer.exit_section();
786
       }
787
788
789
       /* set up all data structures needed for computation */
790
       void Model::setup_dof ()
791
       {
792
             computing_timer.enter_section("Setup dof systems");
793
794
             dof_handler.distribute_dofs (fe);
795
796
             constraints.clear ();
797
             DoFTools::make_hanging_node_constraints (dof_handler, constraints);
             constraints.close ();
799
             system_matrix.clear();
801
             CompressedSparsityPattern c_sparsity (dof_handler.n_dofs());
803
             DoFTools::make_sparsity_pattern (dof_handler, c_sparsity, constraints,
805
             sparsity_pattern.copy_from(c_sparsity);
806
807
             system_matrix.reinit(sparsity_pattern);
808
809
810
             solution.reinit (dof_handler.n_dofs());
             old_solution.reinit(dof_handler.n_dofs());
811
             system_rhs.reinit (dof_handler.n_dofs());
812
813
             /* Optional: display sparsity of global matrix */
814
             // std::ofstream out("sparsity_pattern.m2");
815
             // sparsity_pattern.print_gnuplot(out);
816
             computing_timer.exit_section();
817
       }
818
819
       /* compute the main matrix and right hand side */
820
       void Model::assemble_term ()
821
       {
822
             computing_timer.enter_section (" Assembling system");
823
             system_rhs = 0;
824
             compute_oldterm ();
825
             rhs.advance_time (time_step);
826
             compute_newterm ();
827
828
             computing_timer.exit_section();
       }
829
830
831
832
       void Model::compute_oldterm ()
833
       {
```

```
const QGauss<2> quadrature_formula (3);
834
             FEValues<2>
                              fe_values (mapping, fe, quadrature_formula,
835
                                          update_values | update_gradients |
836
                                          update_JxW_values | update_q_points);
837
838
             const unsigned int dofs_per_cell = dof_handler.get_fe().dofs_per_cell;
839
840
             const unsigned int n_q_points
                                              = quadrature_formula.size();
             double coeff = 0.;
841
             double cont = 1.;
842
843
844
             Vector<double> local_term (dofs_per_cell);
             std::vector<unsigned int> local_dof_indices (dofs_per_cell);
845
846
             std::vector<double> old_data_values (n_q_points);
             std::vector<Tensor<1,2> > old_data_grads (n_q_points);
847
848
849
             std::vector<double> rhs_values_old (n_q_points);
850
             DoFHandler<2>::active_cell_iterator
852
             cell = dof_handler.begin_active(),
             endc = dof_handler.end();
             for(; cell!=endc; ++cell){
855
856
                     local_term = 0;
                      fe_values.reinit (cell);
857
                      fe_values.get_function_values (old_solution, old_data_values);
858
                      fe_values.get_function_grads (old_solution, old_data_grads);
859
                     rhs.value_list(fe_values.get_quadrature_points(), rhs_values_old);
860
861
             for(unsigned int q_point=0; q_point<n_q_points; ++q_point){</pre>
862
                      coeff = compute_kstar(old_data_values[q_point], cell->material_id());
863
864
                for(unsigned int i=0; i<dofs_per_cell; ++i){</pre>
865
                     local_term(i) += (1/(time_step)*old_data_values[q_point]*
866
                                        fe_values.shape_value(i,q_point) + (1-theta)*
867
                                        rhs_values_old[q_point]*
868
                                        fe_values.shape_value(i, q_point) - coeff*cont*
869
                                        (1-theta)*old_data_grads[q_point]*
870
                                        fe_values.shape_grad(i,q_point))*
871
                                        fe_values.JxW (q_point);
872
873
                }
             }
874
875
876
             cell->get_dof_indices (local_dof_indices);
877
                for (unsigned int i=0; i<dofs_per_cell; ++i){</pre>
878
879
                      system_rhs(local_dof_indices[i]) += local_term(i);
880
                }
881
             }
             constraints.condense (system_rhs);
```

```
}
883
884
       void Model::compute_newterm ()
885
886
             const QGauss<2> quadrature_formula (3);
887
             FEValues<2>
                              fe_values (mapping, fe, quadrature_formula,
888
                                          update_values | update_gradients |
889
                                          update_JxW_values | update_q_points);
890
891
              const unsigned int dofs_per_cell = fe.dofs_per_cell;
892
893
             const unsigned int n_q_points
                                                = quadrature_formula.size();
894
             Vector<double> local_term (dofs_per_cell);
895
              std::vector<unsigned int> local_dof_indices (dofs_per_cell);
897
898
             std::vector<double> rhs_values_new (n_q_points);
899
             DoFHandler<2>::active_cell_iterator
             cell = dof_handler.begin_active(),
901
              endc = dof_handler.end();
903
              for(; cell!=endc; ++cell){
904
905
                      local_term = 0;
                      fe_values.reinit (cell);
906
                      rhs.value_list(fe_values.get_quadrature_points(), rhs_values_new);
907
908
                 for (unsigned int q_point=0; q_point<n_q_points; ++q_point){</pre>
909
                      for (unsigned int i=0; i<dofs_per_cell; ++i){</pre>
910
                              local_term(i) += theta*rhs_values_new[q_point]*
911
                                                fe_values.shape_value(i,q_point)*
912
                                                fe_values.JxW (q_point);
913
914
915
916
                 cell->get_dof_indices (local_dof_indices);
917
918
                 for (unsigned int i=0; i<dofs_per_cell; ++i){</pre>
919
                      system_rhs(local_dof_indices[i]) += local_term(i);
920
                 }
921
922
923
924
             constraints.condense(system_rhs);
925
       }
926
       /* compute initial matrix */
927
928
       void Model::compute_matrix ()
929
930
             computing_timer.enter_section (" Rebuilding matrix");
931
```

```
system_matrix = 0;
932
933
              QGauss<2>
                          quadrature_formula (3);
934
             FEValues<2> fe_values (mapping, fe, quadrature_formula,
935
                                      update_values | update_gradients | update_JxW_values |
936
                                      update_q_points);
937
938
              const unsigned int dofs_per_cell = fe.dofs_per_cell;
939
                                              = quadrature_formula.size();
940
             const unsigned int n_q_points
             double coeff = 0;
941
942
              double cont = 1.;
943
             FullMatrix<double> local_matrix (dofs_per_cell, dofs_per_cell);
944
              std::vector<unsigned int> local_dof_indices (dofs_per_cell);
945
946
              std::vector<double> old_data_values (n_q_points);
948
             DoFHandler<2>::active_cell_iterator
              cell = dof_handler.begin_active(),
950
              endc = dof_handler.end();
             for (; cell!=endc; ++cell){
952
                      local_matrix = 0;
953
954
                      fe_values.reinit (cell);
                      fe_values.get_function_values (old_solution, old_data_values);
955
956
                for (unsigned int q_point=0; q_point<n_q_points; ++q_point){</pre>
                      coeff = compute_kstar(old_data_values[q_point], cell->material_id());
958
                  for (unsigned int i=0; i<dofs_per_cell; ++i){</pre>
959
                      for (unsigned int j=0; j<dofs_per_cell; ++j){</pre>
960
                              local_matrix(i,j) += (1/(time_step)*
961
                                                     fe_values.shape_value(i,q_point)*
962
                                                     fe_values.shape_value(j,q_point) +
963
                                                     theta*coeff*cont*
964
                                                     fe_values.shape_grad(i, q_point)*
965
                                                     fe_values.shape_grad(j, q_point))*
966
                                                     fe_values.JxW (q_point);
967
                      }
968
                 }
969
              }
970
971
              cell->get_dof_indices (local_dof_indices);
972
973
974
              for (unsigned int i=0; i<dofs_per_cell; ++i){</pre>
                   for (unsigned int j=0; j<dofs_per_cell; ++j){
975
                       system_matrix.add(local_dof_indices[i], local_dof_indices[j],
976
977
                                          local_matrix(i,j));
978
                   }
979
              }
            }
```

```
981
             constraints.condense (system_matrix);
982
             computing_timer.exit_section();
983
       }
984
985
986
        /* rebuilding matrix if necessary */
987
        void Model::assemble_system ()
988
        {
989
              if(rebuild_matrix == true){
990
991
                       compute_matrix();
992
              assemble_term ();
993
       }
994
995
        /* solve the resulting system with a cg solver */
996
        void Model::solve ()
997
999
              computing_timer.enter_section (" Solve system");
1000
1001
              SolverControl solver_control (1000, 1e-12, false, false);
1002
              SolverCG<> cg (solver_control);
1003
              preconditioner.initialize(system_matrix, 1.2);
1004
              FilteredMatrix<Vector<double> > f_matrix(system_matrix);
1005
1006
              std::map<unsigned int,double> boundary_values;
1007
              if(SillData::geotherm == 0){
1008
              VectorTools::interpolate_boundary_values (dof_handler,
1009
1010
                                                           boundarydata1,
1011
                                                           boundary_values);
1012
              }
1013
              else{
1014
                       VectorTools::interpolate_boundary_values (dof_handler,
1015
                                                                    Ο,
1016
                                                                    boundarydata2,
1017
                                                                    boundary_values);
1018
              }
1019
1020
              {\tt f\_matrix.add\_constraints(boundary\_values);}
1021
1022
              f_matrix.apply_constraints(system_rhs, true);
              cg.solve (f_matrix, solution, system_rhs, preconditioner);
1023
1024
              constraints.distribute (solution);
              std::cout << solver_control.last_step()</pre>
1025
1026
                         << " CG iterations."
                         << std::endl;
1027
1028
              computing_timer.exit_section();
1029
       }
```

```
1030
1031
        /* output results with gnuplot */
1032
        void Model::output_results (const unsigned int timestep_number) const
1033
        {
1034
              DataOut<2> data out one:
1035
              data_out_one.attach_dof_handler (dof_handler);
1036
              data_out_one.add_data_vector (solution, "u");
1037
              data_out_one.build_patches ();
1038
              std::string name = "not_the_solution.";
1039
1040
              switch (test){
1041
                      case Parameters::TEST_ZERO:
1042
                      name = "fsolution.TESTO.";
1043
1044
                      break;
1045
                      case Parameters::TEST_ONE:
1046
                      name = "fsolution.TEST1.";
1048
                      break;
1049
1050
                      default:
                       Assert (false, ExcNotImplemented());
1051
1052
              };
1053
              std::string tname = "not";
1054
1055
              tname = "0.";
1056
1057
              const std::string filename1 = name + tname +
1058
                                              Utilities::int_to_string (timestep_number, 5) +
1059
                                              ".gnuplot";
1060
1061
              std::ofstream output_one (filename1.c_str());
1062
              data_out_one.write_gnuplot (output_one);
1063
       }
1064
1065
1066
        /* evaluate numerical solution at a particular point */
1067
        double Model::evaluate_soln (double x, double y) const
1068
        {
1069
              return VectorTools::point_value (mapping, dof_handler, solution,
1070
                                                 Point<2>(x, y));
1071
       }
1072
1073
        /* create initial uniform grid */
1074
1075
        void Model::make_initial_grid(){
1076
              const Point<2> botleft = (Point<2> (0., 0.));
1077
              const Point<2> upright = (Point<2> (SillData::DomainLength,
                                         SillData::DomainHeight));
1078
```

```
1079
1080
             std::vector<unsigned int> n_div;
             n_div.push_back(ini_refinement_level);
1081
             n_div.push_back(ini_refinement_level);
1082
1083
1084
             {\tt GridGenerator::subdivided\_hyper\_rectangle(triangulation, n\_div,}
                                                      botleft, upright);
1085
       }
1086
1087
1088
1089
      /* run the simulation in time */
      void Model::run ()
1090
      {
1091
         std::cout << "========== Running TEST_" << test
1092
1093
                   << std::endl;
         1094
1095
                   << std::endl;
         std::cout << "Time step #0" << std::endl;
1097
1098
         /* open file to read temperature solutions */
1099
         std::ofstream file_one;
1100
1101
         std::string name, tname, tmode;
1102
         if(test == Parameters::TEST_ZERO){
             name = "TO_";
1103
1104
         else{
1105
             name = "T1_";
1106
1107
1108
         tname = "0_";
1109
1110
         std::string filename1 = name + tname + "soln.txt";
1111
1112
         file_one.open(filename1.c_str());
1113
1114
         make_initial_grid();
1115
1116
         if(mode == 1){
1117
             triangulation.refine_global(level);
1118
         }
1119
1120
         setup_dof();
1121
1122
         unsigned int pre_refinement_step = 0;
1123
1124
1125
         start_time_iteration:
1126
1127
         time = 0.;
```

```
unsigned int timestep_number = 1;
1128
1129
          /* assign material id to each cell */
1130
          if(test != Parameters::TEST_ZERO){
1131
              for (Triangulation<2>::active_cell_iterator
1132
                    cell = triangulation.begin_active();
1133
                    cell!=triangulation.end();
1134
                   ++cell){
1135
                       if(cell->center()[0] <= SillData::L2 && cell->center()[0]
1136
                               >= SillData::L1 && cell->center()[1] <= SillData::W2 &&
1137
                               cell->center()[1] >= SillData::W1){
1138
                               cell->recursively_set_material_id('m');
1139
                        }
1140
                        else{
1141
                               cell->recursively_set_material_id('c');
1142
1143
                   }
1144
1145
          }
1146
1147
          compute_matrix();
1148
1149
          /* project initial conditions onto initial mesh */
1150
          if(SillData::geotherm == 0){
1151
              VectorTools::project (mapping, dof_handler,
                       constraints,
1152
1153
                       QGauss<2>(4),
                       InitialValues_ZeroGeotherm (1, time),
1154
                       solution);
1155
          }
1156
          else{
1157
               VectorTools::project (mapping, dof_handler,
1158
                       constraints,
1159
                       QGauss<2>(4),
1160
                       InitialValues_Geotherm (1, time),
1161
1162
                       solution);
         }
1163
1164
1165
1166
         if(mode != 1 && timestep_number == 1 &&
1167
              pre_refinement_step < n_pre_refinement_steps){</pre>
1168
                       refine_grid(n_pre_refinement_steps);
1169
                       ++pre_refinement_step;
1170
1171
                       goto start_time_iteration;
        }
1172
1173
1174
         output_results (0);
1175
         /\ast loop over time to compute temperature solutions \ast/
         for(time+=time_step; time<=final_time; time+=time_step, ++timestep_number){</pre>
1176
```

```
1177
1178
              std::cout << "Time step dt = " << time_step << std::endl;</pre>
1179
              std::cout << "Number of active cells: "
1180
              << triangulation.n_active_cells()</pre>
1181
              << std::endl
1182
              << "Total number of cells: "
1183
              << triangulation.n_cells()</pre>
1184
              << std::endl
1185
              << "Total dofs: " << dof_handler.n_dofs()
1186
1187
              << std::endl;
1188
              /* adaptive mesh refinement every "freq" time steps */
1189
              if(mode != 1 && (timestep_number \% freq == 0)){
1190
                       refine_grid(n_pre_refinement_steps);
1191
              }
1192
1193
              if(SillData::geotherm == 0){
1194
                       boundarydata1.advance_time(time_step);
1195
              }
1197
              else{
1198
                       boundarydata2.advance_time(time_step);
1199
              }
1200
              if(timestep_number == 1){
1201
1202
                       file_one << timestep_number-1 << " "
                                 << dof_handler.n_dofs()
1203
                                 << " " << evaluate_soln(1.25,0.525)
1204
                                 << " " << evaluate_soln(1.25,0.530)
1205
                                 << " " << evaluate_soln(1.5,0.525)
1206
                                 << " " << evaluate_soln(1.5,0.530)
1207
                                 << std::endl;
1208
              }
1209
1210
1211
              old_solution = solution;
1212
              std::cout << std::endl
1213
                         << "Time step #" << timestep_number << "; "
1214
                         << "advancing to t = " << time << "."
1215
                         << std::endl;
1216
1217
1218
              assemble_system ();
1219
1220
              solve ();
1221
1222
              output_results (timestep_number);
1223
1224
              if(timestep_number >= 1){
                       file_one << timestep_number
1225
```

```
<< " " << dof_handler.n_dofs()
1226
                               << " " << evaluate_soln(1.25,0.525)
1227
                               << " " << evaluate_soln(1.25,0.530)
1228
                               << " " << evaluate_soln(1.5,0.525)
1229
                               << " " << evaluate_soln(1.5,0.530)
1230
                               << std::endl;
1231
1232
             }
1233
1234
             /* stop the program when the entire crust domain solidifies */
1235
             if(evaluate_soln((SillData::L1 + SillData::L2)/2,
1236
                      (SillData::W1 + SillData::W2)/2 ) < TM_0){
1237
                              summary.open("Timer.txt");
1238
                              computing_timer.print_summary ();
1239
                              summary.close();
1240
                              file_one << "Solidification time : " << time << std::endl;</pre>
1241
                              file_one.close();
1242
                              return;
1243
1244
             }
1245
1246
1247
     /* end of Earth namespace */
1249
1250
1251
     int main ()
1252
1253
       using namespace dealii;
1254
       using namespace Earth;
1255
1256
       try
1257
       {
1258
         /* read inputs from parameter.prm */
1259
1260
         Parameters::DataInput data;
         data.read_data ("parameter.prm");
1261
1262
         deallog.depth_console (0);
1263
1264
         Model model(data);
1265
         model.run ();
1266
1267
       catch (std::exception &exc)
1268
        {
1269
         std::cerr << std::endl << std::endl
1270
           << "-----"
1271
1272
           << std::endl;
1273
         std::cerr << "Exception on processing: " << std::endl
           << exc.what() << std::endl
1274
```

```
<< "Aborting!" << std::endl
1275
           << "----"
1276
          << std::endl;
1277
1278
1279
        return 1:
      }
1280
       catch (...)
1281
1282
1283
        std::cerr << std::endl << std::endl
          << "-----"
1284
1285
          << std::endl;
        std::cerr << "Unknown exception!" << std::endl
1286
          << "Aborting!" << std::endl
1287
          << "-----"
1288
1289
          << std::endl;
        return 1;
1290
1291
      }
1292
1293
       return 0;
1294
    }
1295
     ------ Makefile ------
1296
1297
     # $Id: Makefile 24349 2011-09-21 08:38:41Z kronbichler $
1298
     # For the small projects Makefile, you basically need to fill in only
1299
1300
     # four fields.
1301
     # The first is the name of the application. It is assumed that the
1302
     # application name is the same as the base file name of the single C++
1303
     # file from which the application is generated.
1304
        target = source
1305
1306
     # The second field determines whether you want to run your program in
1307
     # debug or optimized mode. The latter is significantly faster, but no
1308
     # run-time checking of parameters and internal states is performed, so
1309
     # you should set this value to 'on' while you develop your program,
1310
     # and to 'off' when running production computations.
1311
     debug-mode = on
1312
1313
     # As third field, we need to give the path to the top-level deal.II
1314
     # directory. You need to adjust this to your needs. Since this path is
1315
     # probably the most often needed one in the Makefile internals, it is
1316
     # designated by a single-character variable, since that can be
1317
1318
     # reference using $D only, i.e. without the parentheses that are
     # required for most other parameters, as e.g. in $(target).
1319
1320
     D = .../.../
1321
1322
     # The last field specifies the names of data and other files that
     # shall be deleted when calling 'make clean'. Object and backup files,
```

70

```
# executables and the like are removed anyway. Here, we give a list of
1324
     # files in the various output formats that deal.II supports.
1325
     clean-up-files = *gmv *gnuplot *gpl *eps *pov *vtk *ucd *.d2
1326
1327
1328
1329
     # Usually, you will not need to change anything beyond this point.
1330
1331
1332
     # The next statement tells the 'make' program where to find the
1333
1334
     # deal.II top level directory and to include the file with the global
     # settings
1335
     include $D/common/Make.global_options
1336
1337
1338
     # Since the whole project consists of only one file, we need not
     # consider difficult dependencies. We only have to declare the
1339
     # libraries which we want to link to the object file. deal.II has two
1340
     # libraries: one for the debug mode version of the
     # application and one for optimized mode.
1342
     libs.g := $(lib-deal2.g)
     libs.o := $(lib-deal2.o)
1345
     # We now use the variable defined above to switch between debug and
     # optimized mode to select the set of libraries to link with. Included
     # in the list of libraries is the name of the object file which we
1348
1349
     # will produce from the single C++ file. Note that by default we use
     # the extension .g.o for object files compiled in debug mode and .o for
1350
     # object files in optimized mode (or whatever local default on your
1351
     # system is instead of .o)
1352
     ifeq ($(debug-mode),on)
1353
       libraries = $(target).g.$(OBJEXT) $(libs.g)
1354
     else
1355
       libraries = $(target).$(OBJEXT) $(libs.o)
1356
1357
1358
     # Now comes the first production rule: how to link the single object
1359
     # file produced from the single C++ file into the executable. Since
1360
     # this is the first rule in the Makefile, it is the one 'make' selects
1361
     # if you call it without arguments.
1362
     $(target)$(EXEEXT) : $(libraries)
1363
     @echo ====== Linking $@
1364
     @$(CXX) -o $@ $^ $(LIBS) $(LDFLAGS)
1365
1366
     # To make running the application somewhat independent of the actual
1367
     # program name, we usually declare a rule 'run' which simply runs the
1368
     # program. You can then run it by typing 'make run'. This is also
1369
1370
     # useful if you want to call the executable with arguments which do
     # not change frequently. You may then want to add them to the
1372
     # following rule:
```

```
run: $(target)$(EXEEXT)
1373
           @echo ====== Running $<
1374
           @./$(target)$(EXEEXT)
1375
1376
           # As a last rule to the 'make' program, we define what to do when
1377
           # cleaning up a directory. This usually involves deleting object files
1378
           # and other automatically created files such as the executable itself,
1379
           # backup files, and data files. Since the latter are not usually quite
1380
           # diverse, you needed to declare them at the top of this file.
1381
1382
1383
           -rm -f *.$(OBJEXT) *~ Makefile.dep $(target)$(EXEEXT) $(clean-up-files)
1384
           # Since we have not yet stated how to make an object file from a C++
1385
           # file, we should do so now. Since the many flags passed to the
1386
           # compiler are usually not of much interest, we suppress the actual
1387
           # command line using the 'at' sign in the first column of the rules
1388
           # and write the string indicating what we do instead.
1389
           ./%.g.$(OBJEXT) :
           @echo "=======debug====== $(<F) -> $@"
1391
           @$(CXX) $(CXXFLAGS.g) -c $< -o $@
1392
           ./%.$(OBJEXT) :
           @echo "=======optimized===== $(<F) -> $0"
1394
           @$(CXX) $(CXXFLAGS.o) -c $< -o $@
1396
           # The following statement tells make that the rules 'run' and 'clean'
1397
1398
           # are not expected to produce files of the same name as Makefile rules
           # usually do.
1399
           .PHONY: run clean
1400
1401
1402
           # Finally there is a rule which you normally need not care much about:
1403
           # since the executable depends on some include files from the library,
1404
           # besides the C++ application file of course, it is necessary to
1405
           # re-generate the executable when one of the files it depends on has
1406
           # changed. The following rule creates a dependency file
1407
           # 'Makefile.dep', which 'make' uses to determine when to regenerate
1408
           # the executable. This file is automagically remade whenever needed,
1409
           # i.e. whenever one of the cc-/h-files changed. Make detects whether
1410
           # to remake this file upon inclusion at the bottom of this file.
1411
1412
           # If the creation of Makefile.dep fails, blow it away and fail
1413
           Makefile.dep: $(target).cc Makefile \
1414
                                       $(shell echo $D/include/deal.II/*/*.h)
1415
           @echo ====== Remaking $@
1416
           \verb§@$D/common/scripts/make\_dependencies $(INCLUDE) -B. $(target).cc \setminus (INCLUDE) = (INCLUDE) = (INCLUDE) -B. $(target).cc \setminus (INCLUDE) = (INCLUDE) -B. $(target).
1417
1418
                                           > $@ \
1419
                               || (rm -f $0; false)
           @if test -s $@ ; then : else rm $@ ; fi
1420
1421
```

- $^{1422}\,$ $\,$ $\!$ $\!$ $\!$ $\!$ To make the dependencies known to 'make', we finally have to include
- 1423 # them:
- 1424 include Makefile.dep