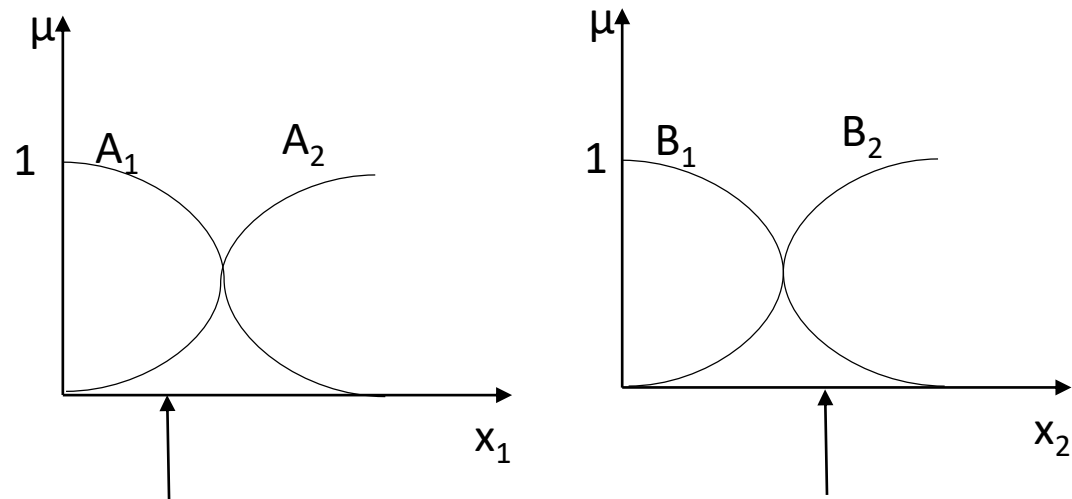


Neuro-Fuzzy Systems

- ✓ Neural Network can learn from input-output dataset, but appears as a black box to the human user i.e. lacks human like reasoning/interpretability
- ✓ Adaptivity and generalization of NN
- ✓ Fuzzy Systems follow human reasoning process, but they cannot learn
- ✓ However, both Fuzzy Systems and the Multilayer NN are universal approximators
- ✓ Combine learnability and adaptivity of NN with interpretability of FLS
- ✓ Suitable for on-line applications

Adaptive Neuro-Fuzzy Inference System (ANFIS):

- ✓ Sugeno Inference
- ✓ Algebraic Product T-norm
- ✓ Multilayer feedforward architecture
- ✓ Backpropagation learning
- ✓ Proposed in 1990's



$$A_1(x_1) = \frac{1}{1 + e^{b_1[x_1 - a_1]}}$$

$$A_2(x_1) = \frac{1}{1 + e^{-b_1[x_1 - a_1]}}$$

$$B_1(x_2) = \frac{1}{1 + e^{b_2[x_2 - a_2]}}$$

$$B_2(x_2) = \frac{1}{1 + e^{-b_2[x_2 - a_2]}}$$

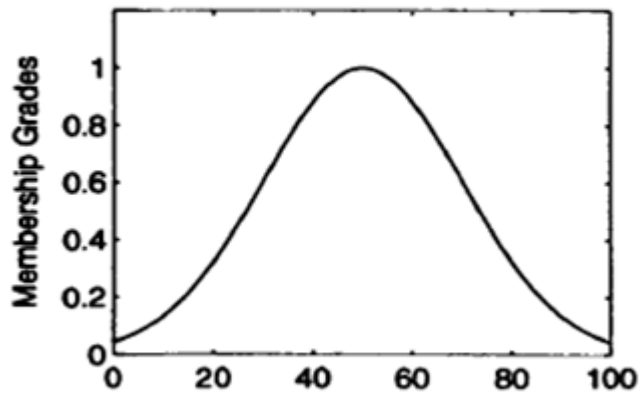
$x_1 \backslash x_2$	B_1	B_2
A_1	$f_1(\cdot, \cdot)$	$f_2(\cdot, \cdot)$
A_2	$f_3(\cdot, \cdot)$	$f_4(\cdot, \cdot)$

$$y_1 = f_1 = c_{11}x_1 + c_{12}x_2 + c_{13}$$

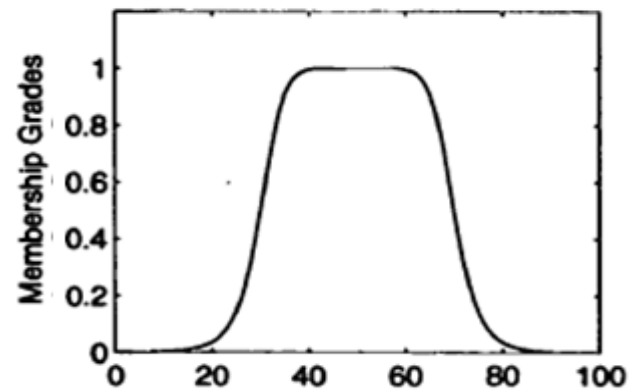
$$y_2 = f_2 = c_{21}x_1 + c_{22}x_2 + c_{23}$$

$$y_3 = f_3 = c_{31}x_1 + c_{32}x_2 + c_{33}$$

$$y_4 = f_4 = c_{41}x_1 + c_{42}x_2 + c_{43}$$



$$\text{gaussian}(x; c, \sigma) = e^{-\frac{1}{2} \left(\frac{x-c}{\sigma} \right)^2}$$



$$\text{bell}(x; a, b, c) = \frac{1}{1 + \left| \frac{x-c}{a} \right|^{2b}}$$

weights of rules:

$$w_1 = A_1(x_1) B_1(x_2)$$

$$w_2 = A_1(x_1) B_2(x_2)$$

$$w_3 = A_2(x_1) B_1(x_2)$$

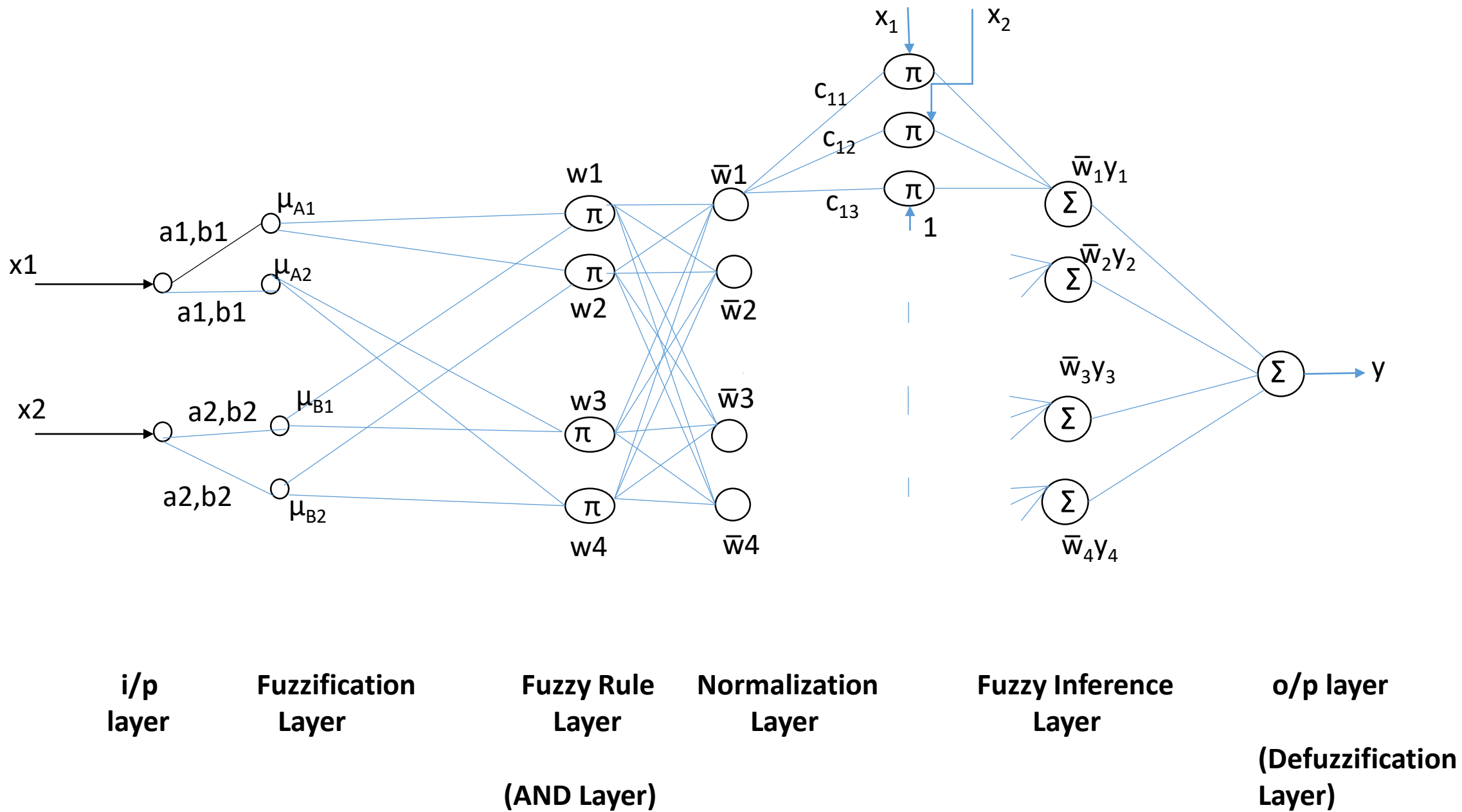
$$w_4 = A_2(x_1) B_2(x_2)$$

S.No.	x1	x2	T
1.	5.0	2.5	10.1
2.	3.5	-4.5	-8.2
⋮	⋮	⋮	⋮

$$y = \frac{w_1 y_1 + w_2 y_2 + w_3 y_3 + w_4 y_4}{w_1 + w_2 + w_3 + w_4} = \bar{w}_1 y_1 + \bar{w}_2 y_2 + \bar{w}_3 y_3 + \bar{w}_4 y_4$$

$$= w_1 y_1 + w_2 y_2 + w_3 y_3 + w_4 y_4$$

$$(\because w_1 + w_2 + w_3 + w_4 = A_1 B_1 + A_1 B_2 + A_2 B_1 + A_2 B_2 = 1)$$



$$E = \frac{1}{2}(T - y)^2$$

$$\Delta C_{11} = -\eta \frac{\partial E}{\partial C_{11}} = -\eta \frac{\partial E}{\partial y_1} \cdot \frac{\partial y_1}{\partial C_{11}} = -\eta \frac{\partial E}{\partial y} \cdot \frac{\partial y}{\partial y_1} \cdot \frac{\partial y_1}{\partial C_{11}} = \eta(T - y) \cdot w_1 x_1 = \eta(T - y) \cdot A_1 B_1 x_1$$

$$\Delta C_{12} = -\eta \frac{\partial E}{\partial C_{12}} = -\eta \frac{\partial E}{\partial y_1} \cdot \frac{\partial y_1}{\partial C_{12}} = -\eta \frac{\partial E}{\partial y} \cdot \frac{\partial y}{\partial y_1} \cdot \frac{\partial y_1}{\partial C_{12}} = \eta(T - y) \cdot w_1 x_2 = \eta(T - y) \cdot A_1 B_1 x_2$$

$$\Delta C_{13} = -\eta \frac{\partial E}{\partial C_{13}} = -\eta \frac{\partial E}{\partial y_1} \cdot \frac{\partial y_1}{\partial C_{13}} = -\eta \frac{\partial E}{\partial y} \cdot \frac{\partial y}{\partial y_1} \cdot \frac{\partial y_1}{\partial C_{13}} = \eta(T - y) \cdot A_1 B_1$$

$$\Delta C_{21} = -\eta \frac{\partial E}{\partial C_{21}} = -\eta \frac{\partial E}{\partial y_1} \cdot \frac{\partial y_1}{\partial C_{21}} = -\eta \frac{\partial E}{\partial y} \cdot \frac{\partial y}{\partial y_1} \cdot \frac{\partial y_1}{\partial C_{21}} = \eta(T - y) \cdot w_2 \cdot x_1 = \eta(T - y) \cdot A_1 B_2 \cdot x_1$$

...

Next tunable parameters are : a_1, b_1, a_2, b_2

$$A_1 + A_2 = 1$$

$$B_1 + B_2 = 1$$

$$\Delta a_1 = -\eta \frac{\partial E}{\partial a_1} = -\eta \cdot \frac{\partial E}{\partial y} \cdot \frac{\partial y}{\partial A_1} \cdot \frac{\partial A_1}{\partial a_1}$$

$$\text{Now, } \frac{\partial A_1}{\partial a_1} = \frac{\partial}{\partial a_1} \left(\frac{1}{1 + e^{b_1(x_1 - a_1)}} \right) = b_1 A_1 \cdot (1 - A_1) = b_1 A_1 \cdot A_2$$

$$y = w_1 y_1 + w_2 y_2 + w_3 y_3 + w_4 y_4$$

$$\therefore \frac{\partial y}{\partial A_1} = \frac{\partial}{\partial A_1} (A_1 B_1 y_1 + A_1 B_2 y_2 + A_2 B_1 y_3 + A_2 B_2 y_4)$$

$$= B_1 y_1 + B_2 y_2$$

$$\therefore \Delta a_1 = \eta(T - y) \cdot b_1 \cdot A_1 \cdot A_2 \cdot (B_1 y_1 + B_2 y_2)$$

Similarly,

$$\Delta a_2 = -\eta \frac{\partial E}{\partial a_2} = -\eta \cdot \frac{\partial E}{\partial y} \cdot \frac{\partial y}{\partial B_1} \cdot \frac{\partial B_1}{\partial a_2}$$

Now,

$$y = w_1 y_1 + w_2 y_2 + w_3 y_3 + w_4 y_4$$

$$\begin{aligned} \therefore \frac{\partial y}{\partial B_1} &= \frac{\partial}{\partial B_1} (A_1 B_1 y_1 + A_1 B_2 y_2 + A_2 B_1 y_3 + A_2 B_2 y_4) \\ &= A_1 y_1 + A_2 y_3 \end{aligned}$$

$$\text{Now} \quad \frac{\partial B_1}{\partial a_2} = \frac{\partial}{\partial a_2} \left(\frac{1}{1 + e^{b_2(x_2 - a_2)}} \right) = b_2 \cdot B_1 \cdot (1 - B_1) = b_2 \cdot B_1 \cdot B_2$$

$$\therefore \Delta a_2 = \eta(T - y) \cdot b_2 \cdot B_1 \cdot B_2 \cdot (A_1 y_1 + A_2 y_3)$$

$$\Delta a_1 = \eta(T - y) \cdot b_1 \cdot A_1 \cdot A_2 \cdot (B_1 y_1 + B_2 y_2)$$

Similarly b_1 and b_2 are updated as

$$\Delta b_1 = -\eta(T - y) \cdot (x_1 - a_1) \cdot A_1 \cdot A_2 \cdot (B_1 y_1 + B_2 y_2)$$

$$\Delta b_2 = -\eta(T - y) \cdot (x_2 - a_2) \cdot B_1 \cdot B_2 \cdot (A_1 y_1 + A_2 y_3)$$

Pseudoinverse Method:

- Consequent parameters can be updated at one go in a batch mode

$$y = \overline{\omega}_1 y_1 + \overline{\omega}_2 y_2 + \overline{\omega}_3 y_3 + \overline{\omega}_4 y_4$$

$$= \overline{\omega}_1(c_{11}x_1 + c_{12}x_2 + c_{13}) + \overline{\omega}_2(c_{21}x_1 + c_{22}x_2 + c_{23}) + \overline{\omega}_3(c_{31}x_1 + c_{32}x_2 + c_{33}) + \overline{\omega}_4(c_{41}x_1 + c_{42}x_2 + c_{43})$$

$$= \overline{\omega}_1 c_{11}x_1 + \overline{\omega}_1 c_{12}x_2 + \overline{\omega}_1 c_{13} + \overline{\omega}_2 c_{21}x_1 + \overline{\omega}_2 c_{22}x_2 + \overline{\omega}_2 c_{23} \\ + \overline{\omega}_3 c_{31}x_1 + \overline{\omega}_3 c_{32}x_2 + \overline{\omega}_3 c_{33} + \overline{\omega}_4 c_{41}x_1 + \overline{\omega}_4 c_{42}x_2 + \overline{\omega}_4 c_{43})$$

$$= [\overline{\omega}_1 x_1 \quad \overline{\omega}_1 x_2 \quad \overline{\omega}_1 \quad \overline{\omega}_2 x_1 \quad \overline{\omega}_2 x_2 \quad \overline{\omega}_2 \quad \overline{\omega}_3 x_1 \quad \overline{\omega}_3 x_2 \quad \overline{\omega}_3 \quad \overline{\omega}_4 x_1 \quad \overline{\omega}_4 x_2 \quad \overline{\omega}_4]$$

$$\begin{bmatrix} c_{11} \\ c_{12} \\ c_{13} \\ c_{21} \\ c_{22} \\ c_{23} \\ c_{31} \\ c_{32} \\ c_{33} \\ c_{41} \\ c_{42} \\ c_{43} \end{bmatrix}$$

$$T_1 = p_1 \underline{c}$$

$$\begin{bmatrix} T_1 \\ \vdots \\ T_N \end{bmatrix} = \begin{bmatrix} p_1 \\ \vdots \\ p_N \end{bmatrix} \underline{c}$$

$$\underline{c} = pinv \left(\begin{bmatrix} p_1 \\ \vdots \\ p_N \end{bmatrix} \right) \begin{bmatrix} T_1 \\ \vdots \\ T_N \end{bmatrix}$$

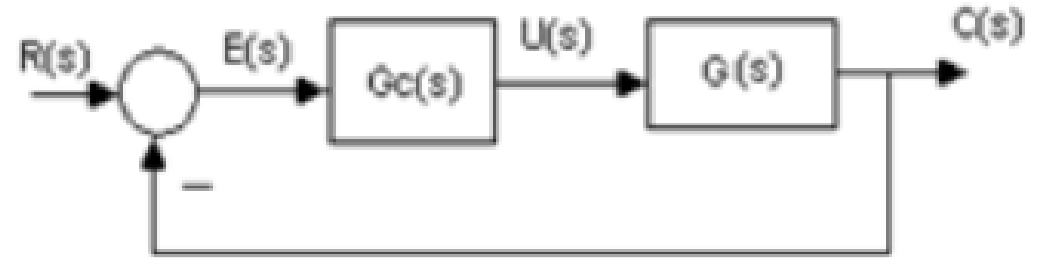
: least square error solution

(over-determined system)

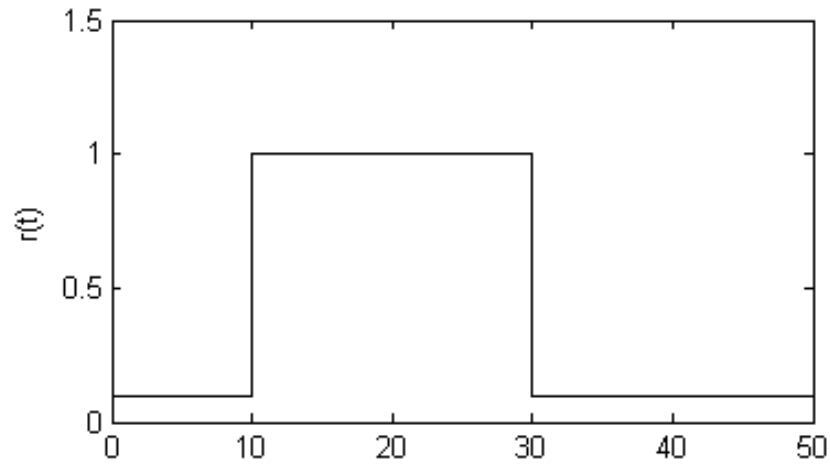
Fuzzy PID Control

A Primer on PID Control:

- ✓ Nicholas Minorsky in 1922
- ✓ Became well known from late 1930's
- ✓ Intuitive
- ✓ No guarantee of stability
- ✓ Linear Controller
- ✓ Three design parameters
- ✓ They can be set analytically or experimentally or through trial and error

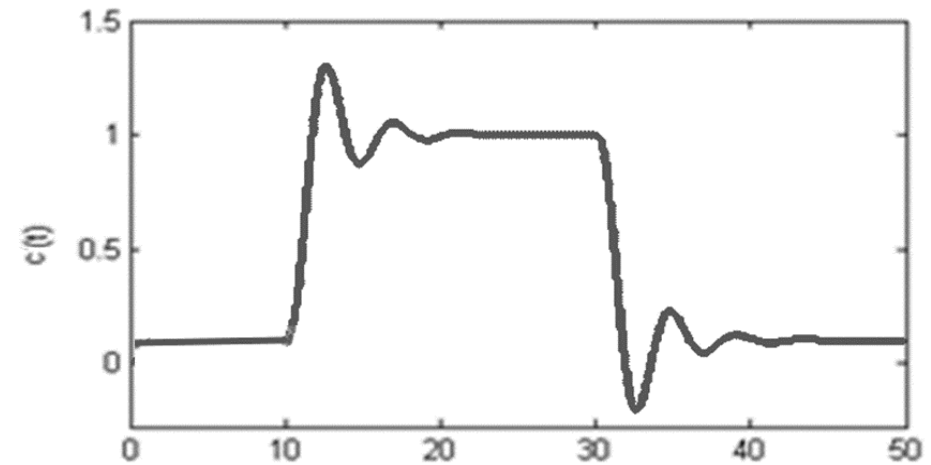


$$u(t) = K_P e(t) + K_I \int_0^t e(t) dt + K_D \frac{de(t)}{dt}$$



✓ Some Requirements:

- Fast response
- Low overshoot/undershoot
- Oscillations dying out fast
- Zero or low steady state error



✓ Other Requirements:

- Robustness to disturbances
- Robustness to plant uncertainties
- Handling nonlinearities, time delays

✓ P-term: $u(t) = K_P e(t)$

- Control effort is proportional to instantaneous error
- Makes the response faster
- Usually leaves some steady state error
- Higher K_P may reduce steady state error but at the cost of higher overshoot
- Very high K_P may even lead to instability

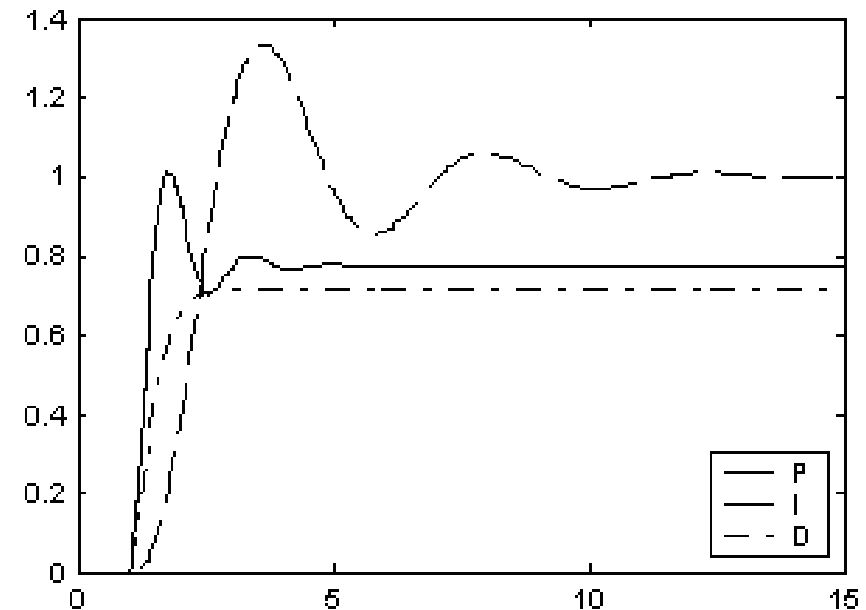
✓ I-term: $u(t) = K_I \int_0^t e(t) dt$

- Control effort is proportional to accumulation of error over time
- Reduces steady state error to a great extent
- Response becomes more oscillatory
- Closed loop system becomes more prone to instability

✓ D-term: $u(t) = K_D \frac{de(t)}{dt}$

- Control action is proportional to inertia
- Reduces overshoot
- Takes no action if there is steady state error (always used along with a P-controller)

✓ PI, PD, PID Controllers



Discretization of a PID Controller

$$\begin{aligned}\dot{u}(t) &= K_P \dot{e}(t) + K_I e(t) + K_D \ddot{e}(t) \\ &= K_P v(t) + K_I d(t) + K_D a(t)\end{aligned}$$

$$\frac{u(k) - u(k-1)}{T_s} = K_P v(k) + K_I d(k) + K_D a(k)$$

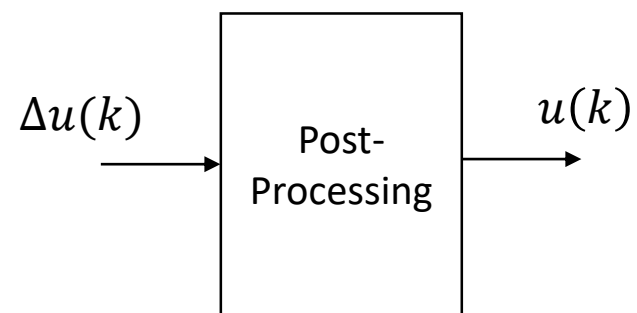
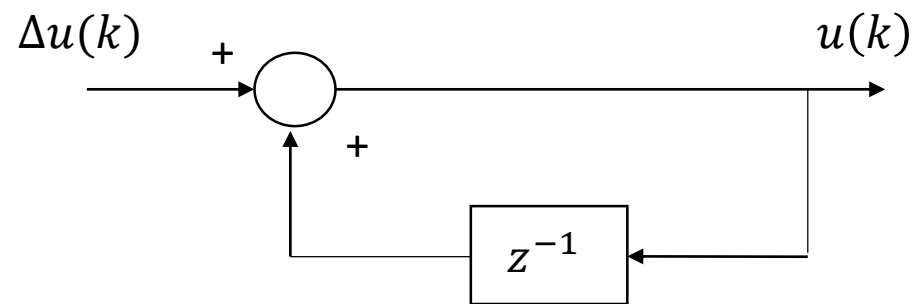
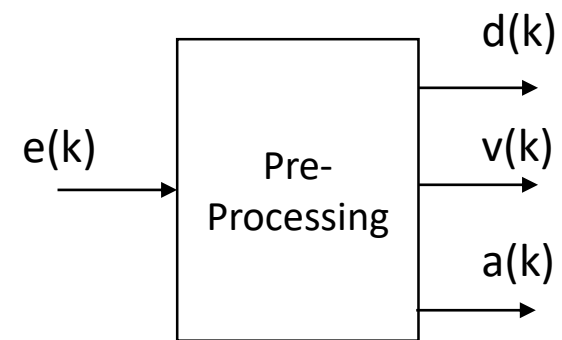
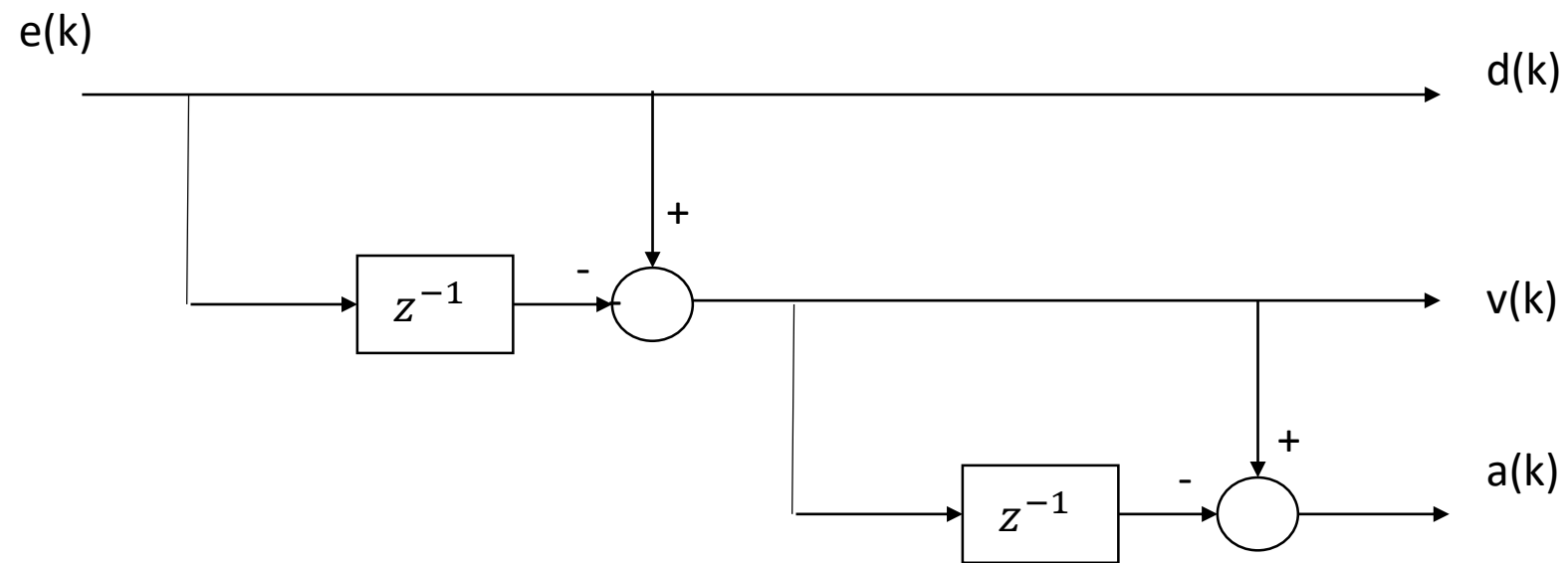
$$\Delta u(k) = K_I d(k) + K_P v(k) + K_D a(k)$$

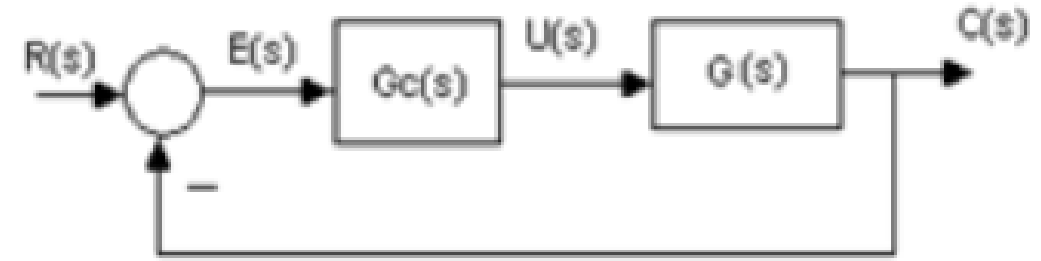
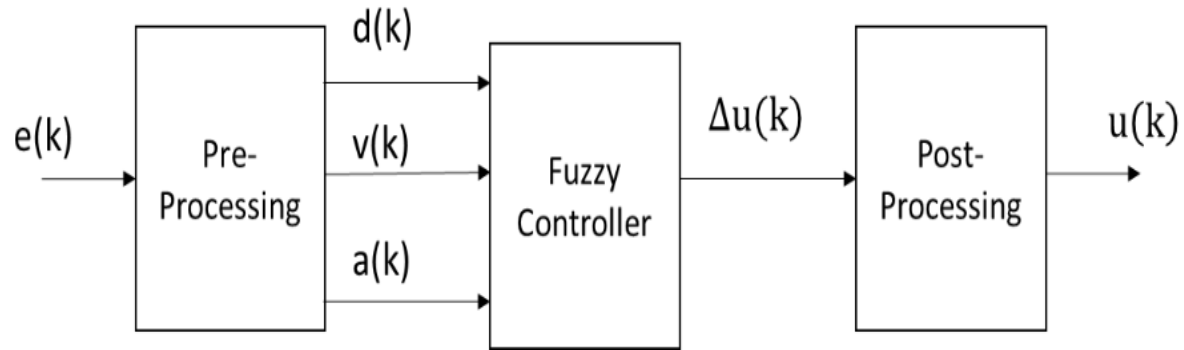
where $d(k) = \text{error}$

$v(k) = \text{change in error}$

$a(k) = \text{change in change in error}$

$$u(k) = u(k - 1) + \Delta u(k)$$





Advantages of Fuzzy PID

- ✓ A relatively easy way of designing nonlinear PID Control
- ✓ Bypassing the rigor of nonlinear control theory
- ✓ Without much dependence on the mathematical model of the plant

Fuzzy PI Controller

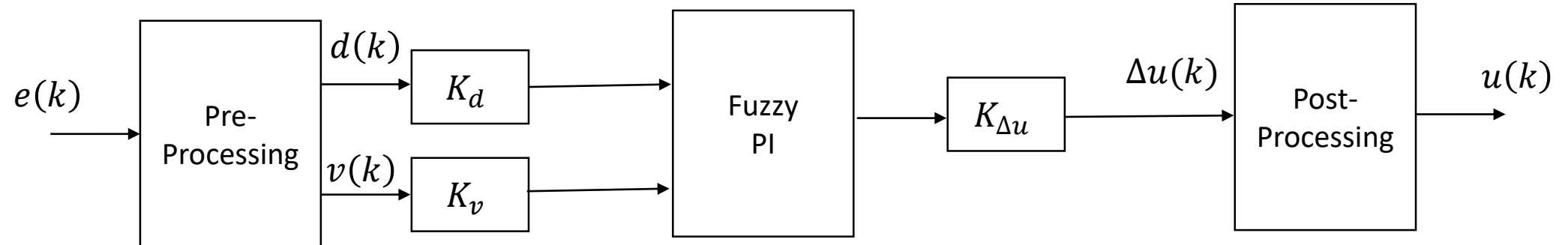
$$u(t) = K_P e(t) + K_I \int e(t) dt$$

$$\dot{u}(t) = K_P \dot{e}(t) + K_I e(t)$$

$$\frac{u(k) - u(k-1)}{T_s} = K_P \frac{e(k) - e(k-1)}{T_s} + K_I e(k)$$

$$\Delta u(k) = K_I e(k) + K_P \Delta e(k)$$

$$\Delta u(k) = f\{d(k), v(k)\}$$



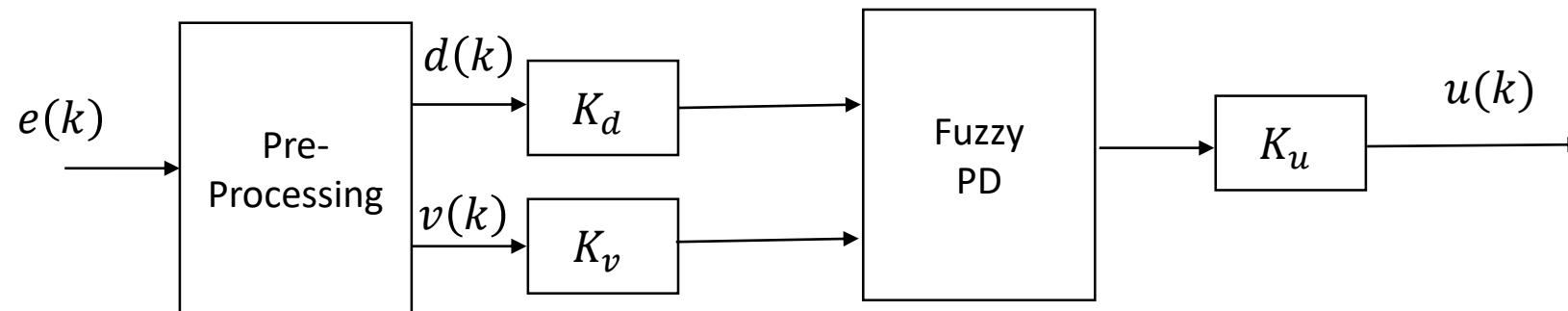
Fuzzy PD Controller

$$u(t) = K_P e(t) + K_D \dot{e}(t)$$

$$u(k) = K_P e(k) + K_D \frac{e(k) - e(k-1)}{T_s}$$

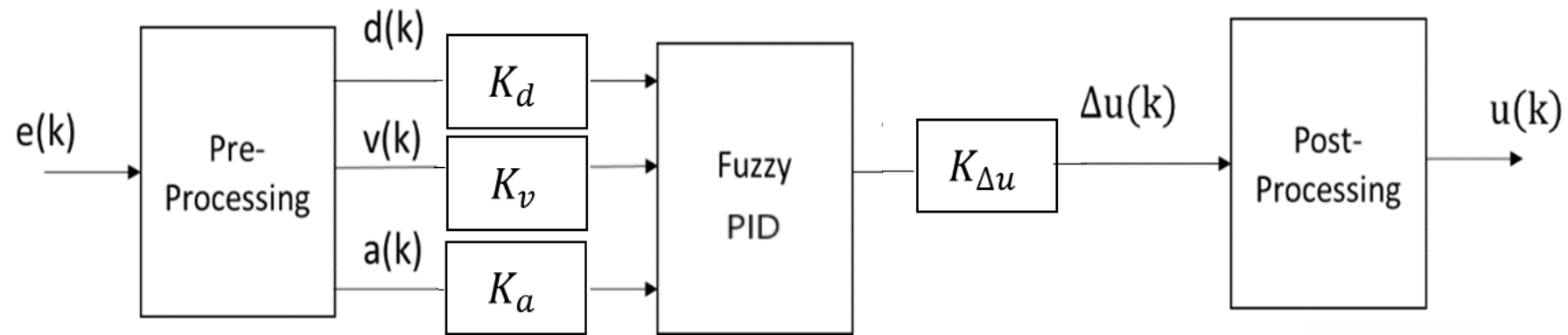
$$u(k) = K_P e(k) + K_D \Delta e(k)$$

$$u(k) = f\{d(k), v(k)\}$$



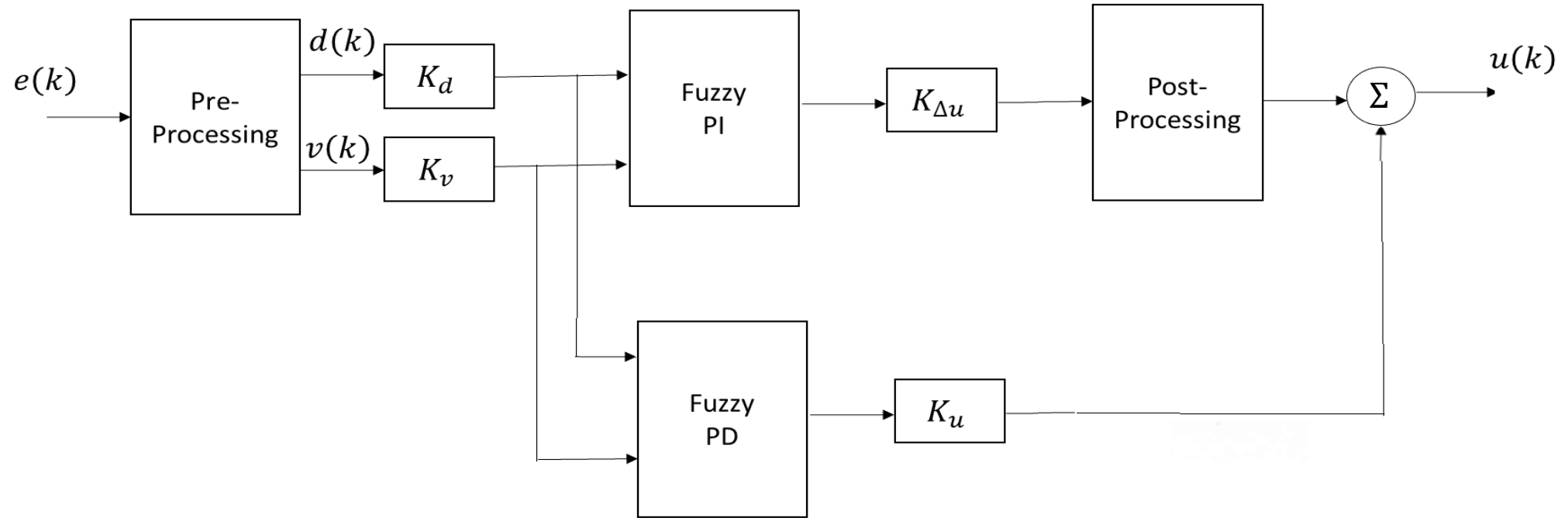
Three Term Fuzzy PID Controller

$$\Delta u(k) = f\{d(k), v(k), a(k)\}$$

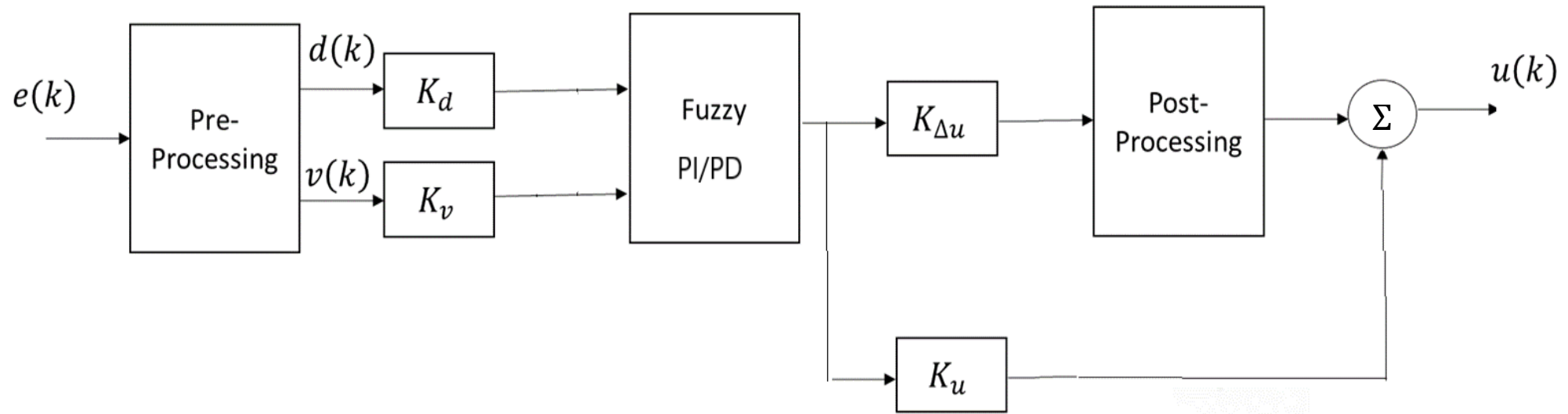


- ✓ Higher number of rules ($3^3 = 27$, $5^3 = 125$ etc.)

Two Term Fuzzy PID Controller

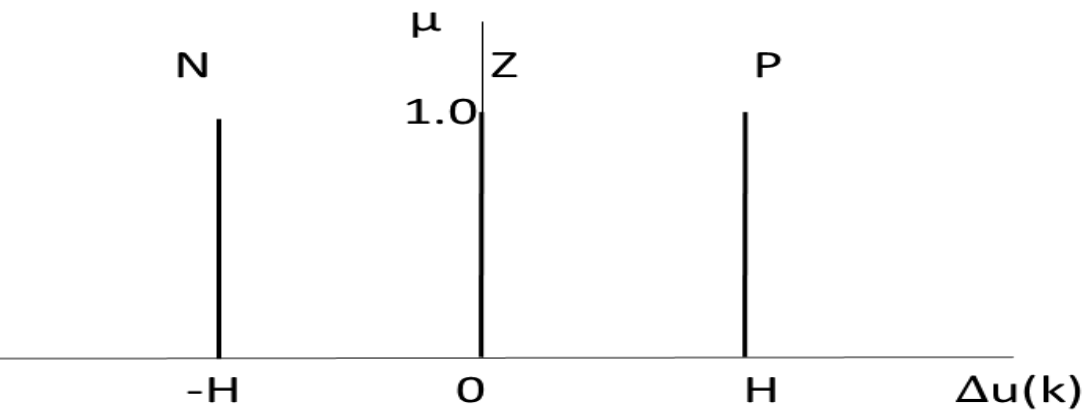
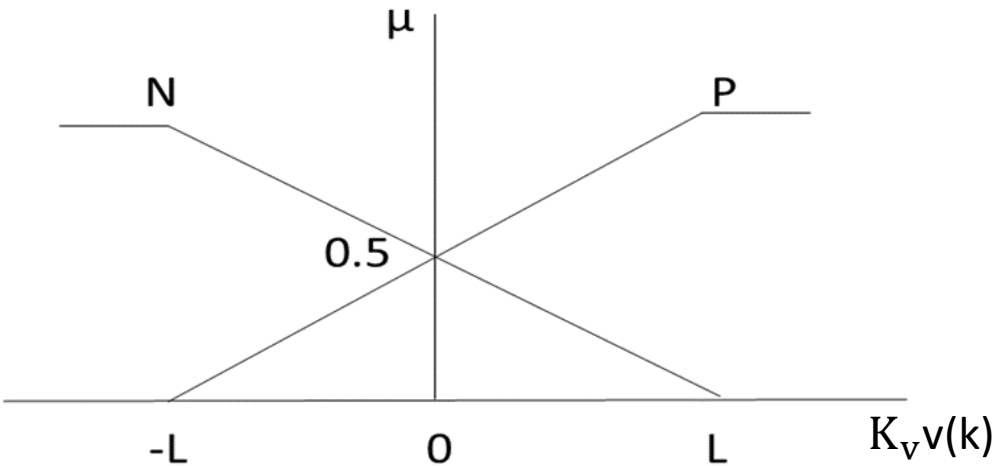
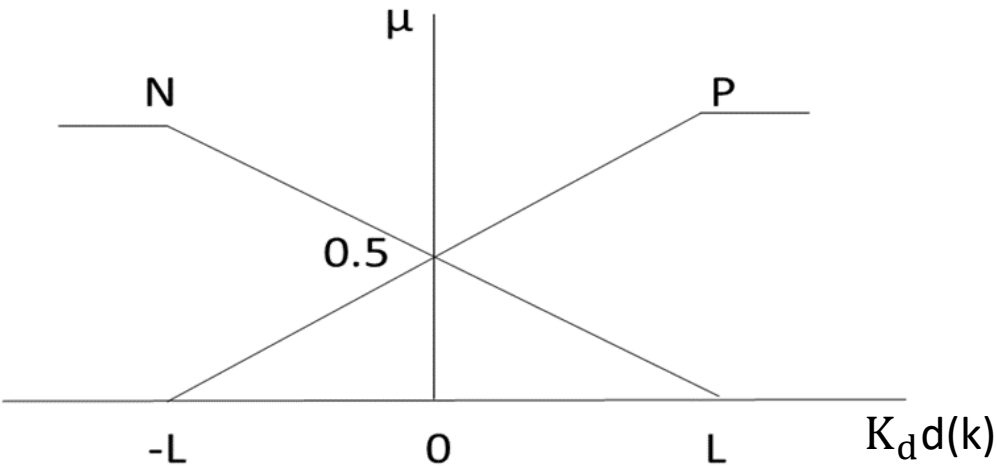


- ✓ Less number of rules ($2 \times 3^2 = 18$, $2 \times 5^2 = 50$ etc.)
- ✓ Scaling factors need to be properly tuned

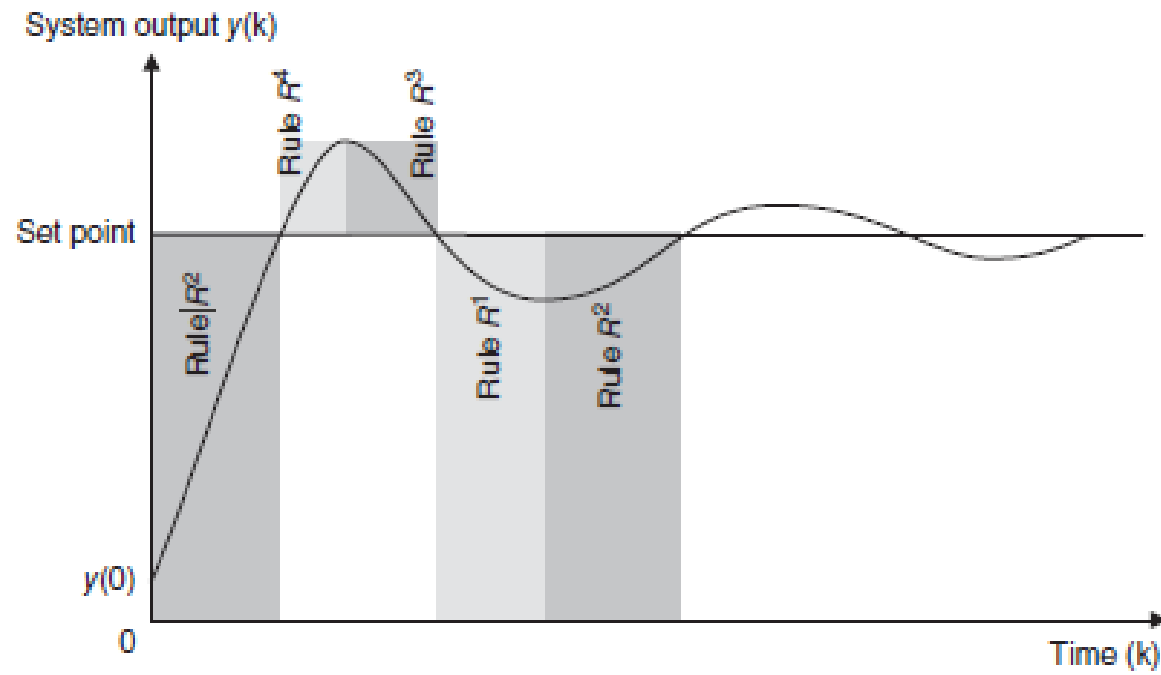


- ✓ Sometimes Fuzzy PI and Fuzzy PD may have identical rule base!
- ✓ No. of rules: 9, 25, ...
- ✓ Many other structures are possible and proposed in the literature
(E.g. FuzzyPD+I ; FuzzyPI+D etc.)

1) A Fuzzy PI Controller as a Conventional Linear PI Controller



		$v(k)$	
$d(k)$		P	N
		P	N
P		P	Z
N		Z	N



		$v(k)$	
		P	N
$d(k)$	P	P	Z
	N	Z	N

✓ A two-term controller with four rules is generic enough!

$$\mu_P(d) = \begin{cases} 0 & , \quad K_d d(k) < -L \\ \frac{K_d d(k) + L}{2L} & , \quad -L \leq K_d d(k) \leq L \\ 1 & , \quad K_d d(k) > L \end{cases}$$

$$\mu_P(v) = \begin{cases} 0 & , \quad K_v v(k) < -L \\ \frac{K_v v(k) + L}{2L} & , \quad -L \leq K_v v(k) \leq L \\ 1 & , \quad K_v v(k) > L \end{cases}$$

$$\mu_N(d) = \begin{cases} 1 & , \quad K_d d(k) < -L \\ \frac{-K_d d(k) + L}{2L} & , \quad -L \leq K_d d(k) \leq L \\ 0 & , \quad K_d d(k) > L \end{cases}$$

$$\mu_N(v) = \begin{cases} 1 & , \quad K_v v(k) < -L \\ \frac{-K_v v(k) + L}{2L} & , \quad -L \leq K_v v(k) \leq L \\ 0 & , \quad K_v v(k) > L \end{cases}$$

- ✓ Mamdani model with singleton output sets (or zero order Sugeno model)
- ✓ Algebraic product T-norm

$$\text{Weight of Rule1} = w1 = \mu_P(d) * \mu_P(v)$$

$$\text{Weight of Rule2} = w2 = \mu_P(d) * \mu_N(v)$$

$$\text{Weight of Rule3} = w3 = \mu_N(d) * \mu_P(v)$$

$$\text{Weight of Rule4} = w4 = \mu_N(d) * \mu_N(v)$$

<div> <div>$v(k)$</div> <div>$d(k)$</div> </div>		P	N
		P	Z
	N	Z	N

$$w1+w2+w3+w4 = \mu_P(d) * \mu_P(v) + \mu_P(d) * \mu_N(v) + \mu_N(d) * \mu_P(v) + \mu_N(d) * \mu_N(v)$$

$$= \mu_P(d) \{ \mu_P(v) + \mu_N(v) \} + \mu_N(d) \{ \mu_P(v) + \mu_N(v) \}$$

$$= \mu_P(d) + \mu_N(d) = 1$$

$$\Delta u(k) = K_{\Delta u} \frac{w1 * H + w4 * (-H)}{w1 + w2 + w3 + w4}$$

$$= K_{\Delta u} \{ \mu_P(d) * \mu_P(v) * H + \mu_N(d) * \mu_N(v) * (-H) \}$$

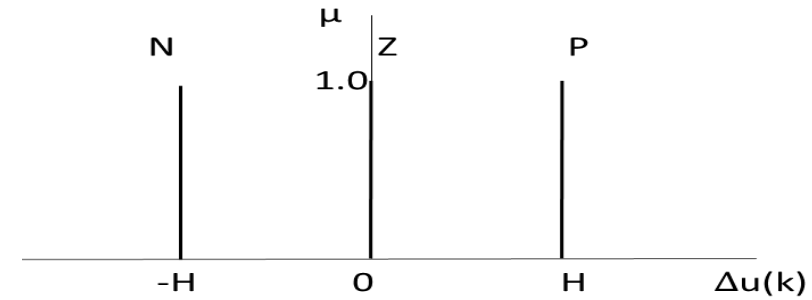
$$= K_{\Delta u} \left\{ \frac{K_d d + L}{2L} * \frac{K_v v + L}{2L} * H - \frac{-K_d d + L}{2L} * \frac{-K_v v + L}{2L} * H \right\}$$

$$= K_{\Delta u} \{ (K_d d + L) * (K_v v + L) - (-K_d d + L) * (-K_v v + L) \} \frac{H}{4L^2}$$

$$= K_{\Delta u} \{ 2 * K_d d * L + 2 * K_v v * L \} \frac{H}{4L^2}$$

$$= \frac{K_{\Delta u} K_d H}{2L} d(k) + \frac{K_{\Delta u} K_v H}{2L} v(k)$$

$$[\Delta u(k) = K_I e(k) + K_P \Delta e(k)]$$



d(k) \ v(k)		
	P	N
P	P	Z
N	Z	N

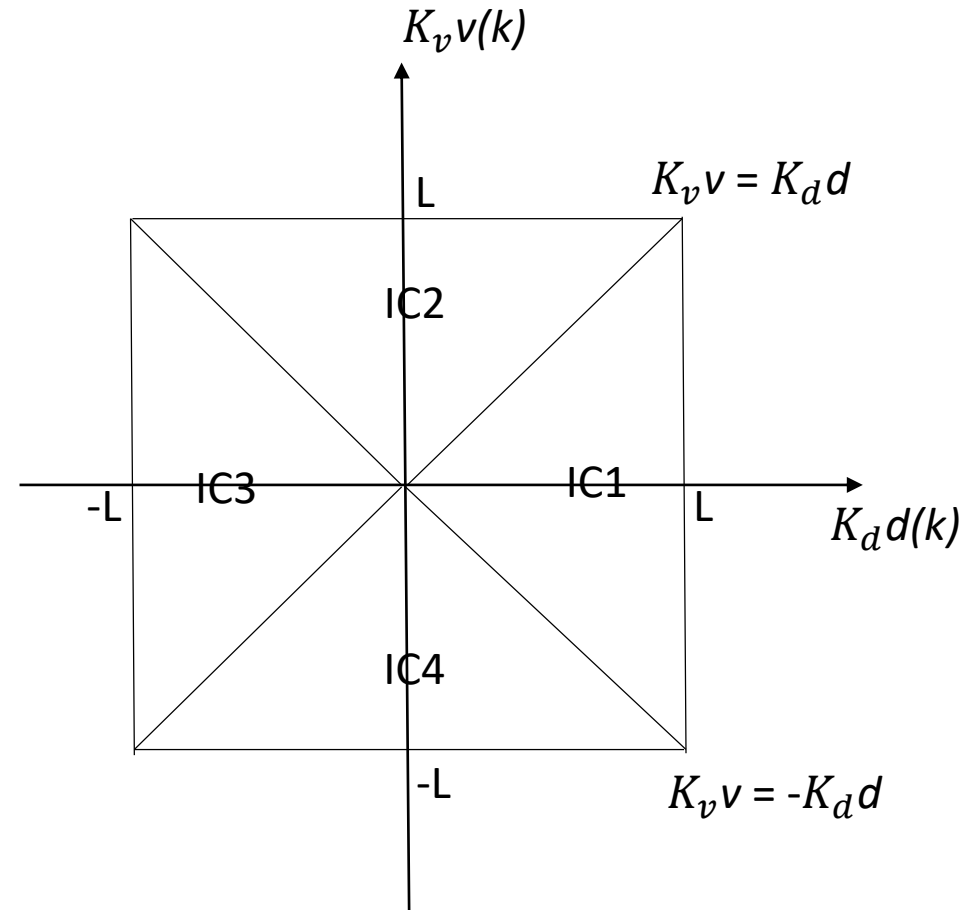
✓ Holds for Fuzzy PD Controller also (and therefore PID too)

2) A Fuzzy PI Controller as a Nonlinear PI Controller

- ✓ Minimum T-norm
- ✓ Linear and symmetric membership functions for both $d(k)$ and $v(k)$
- ✓ Zero order Sugeno Model
(Mamdani with singleton o/p)

$v(k)$	P	N
$d(k)$	P	Z
	Z	N

IC: Input Combination

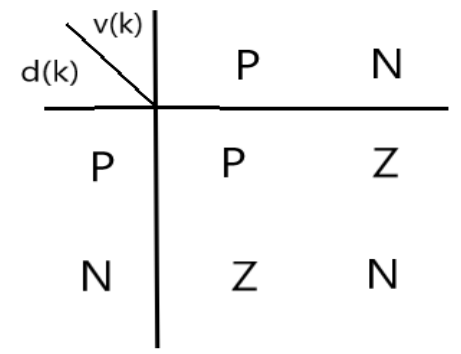
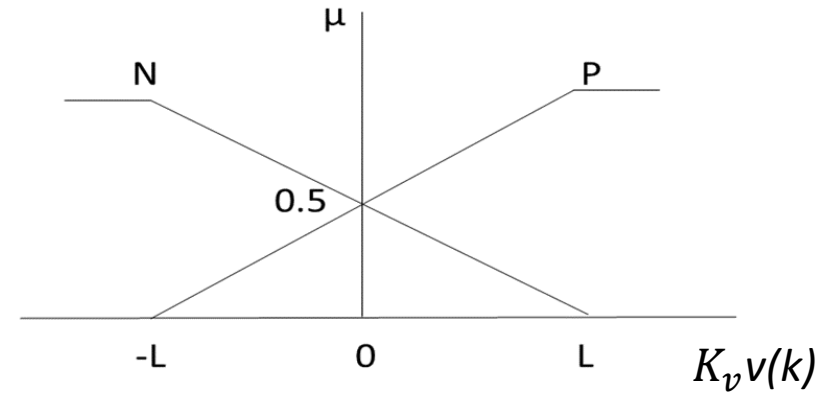
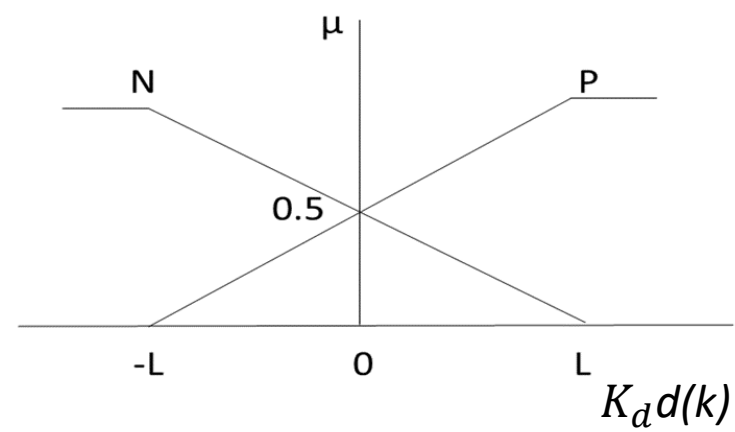


IC1: $0 \leq K_d d(k) \leq L$ and $-L \leq K_v v(k) \leq L$

IC2: $-L \leq K_d d(k) \leq L$ and $0 \leq K_v v(k) \leq L$

IC3: $-L \leq K_d d(k) \leq 0$ and $-L \leq K_v v(k) \leq L$

IC4: $-L \leq K_d d(k) \leq L$ and $-L \leq K_v v(k) \leq 0$



IC	Rule1	Rule2	Rule3	Rule4
IC1:	$\mu_P(v)$	$\mu_N(v)$	$\mu_N(d)$	$\mu_N(d)$
IC2:	$\mu_P(d)$	$\mu_N(v)$	$\mu_N(d)$	$\mu_N(v)$
IC3:	$\mu_P(d)$	$\mu_P(d)$	$\mu_P(v)$	$\mu_N(v)$
IC4:	$\mu_P(v)$	$\mu_P(d)$	$\mu_P(v)$	$\mu_N(d)$

IC1: $0 \leq K_d d(k) \leq L$ and $-L \leq K_v v(k) \leq L$

$|K_v v| \leq |K_d d|$

Output for IC1 (and IC3):

$$\Delta u(k) = K_{\Delta u} \frac{\mu_P(v)*H + \mu_N(d)*(-H)}{\mu_P(v) + \mu_N(v) + \mu_N(d) + \mu_N(d)}$$

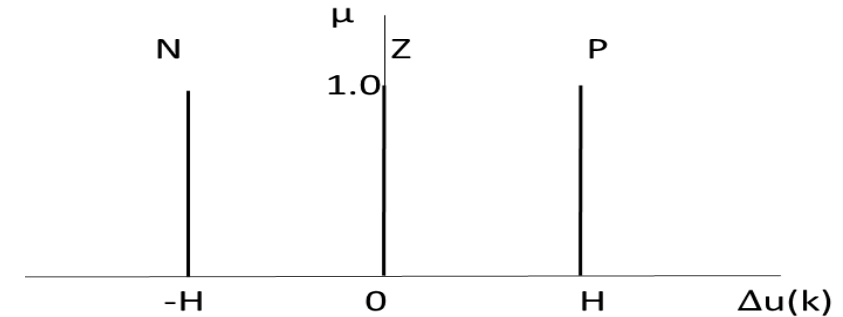
$$= K_{\Delta u} \frac{\mu_P(v) - \mu_N(d)}{1 + 2 \mu_N(d)} H$$

$$= K_{\Delta u} \frac{\frac{K_v v + L}{2L} - \frac{-K_d d + L}{2L}}{1 + 2 \frac{-K_d d + L}{2L}} H$$

$$= K_{\Delta u} \frac{K_d d + K_v v}{2L + 2(-K_d d + L)} H$$

$$= \frac{K_{\Delta u} H}{4L - 2 K_d d} (K_d d + K_v v)$$

$$= \frac{0.5 K_{\Delta u} H}{2L - K_d d} (K_d d + K_v v)$$



		v(k)	
		P	N
d(k)	P	P	Z
	N	Z	N

Output for IC2 and IC4:

$$\Delta u(k) = \frac{0.5 K_{\Delta u} H}{2L - K_v |v|} (K_d d + K_v v)$$

- ✓ Controller Gains are error or error rate dependent
- ✓ Higher gains for higher error or rate
- ✓ Faster convergence with less overshoot even for linear systems
- ✓ Gains vary smoothly across various regions (i.e. ICs)
- ✓ Larger no. of controller parameters
- ✓ Similar for Fuzzy PD Controller (and therefore PID controller)