

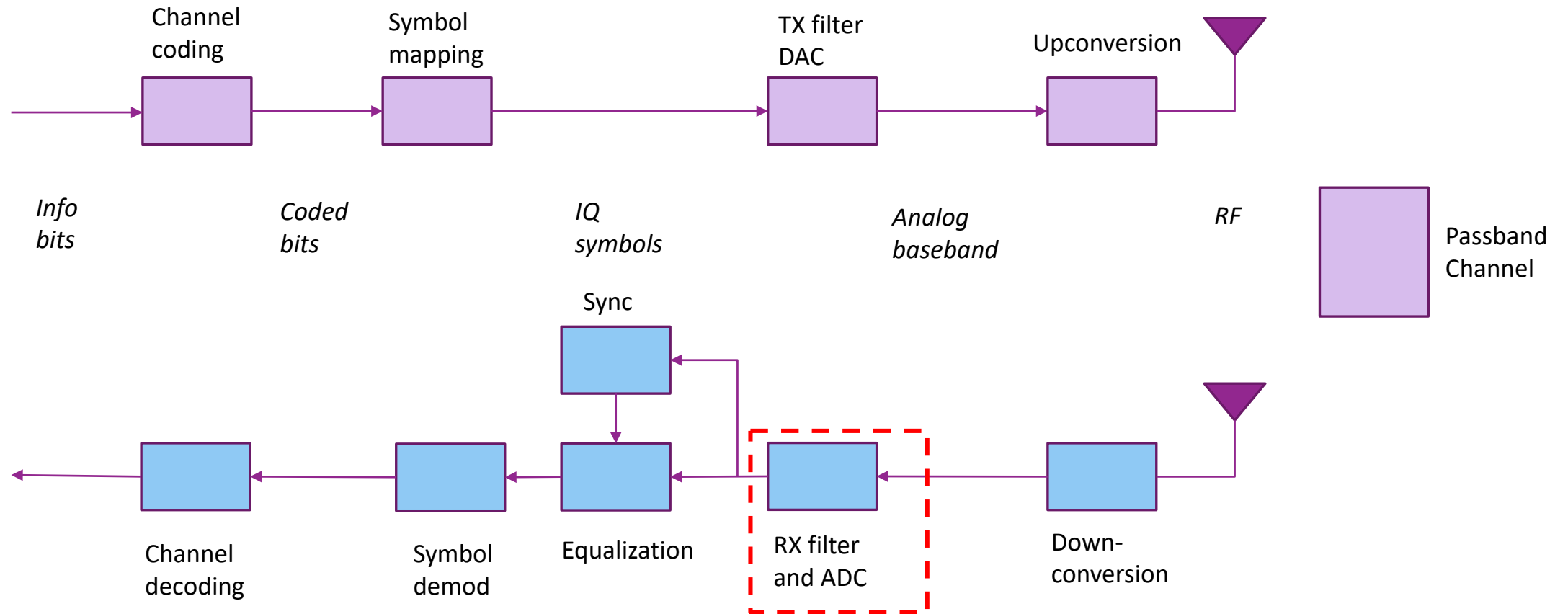
# Unit 3: Receive Filtering

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EL-GY 6013: DIGITAL COMMUNICATIONS

PROF. SUNDEEP RANGAN

# This Unit



# Learning Objectives

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- ❑ Describe the steps in recovering symbols for a linearly modulated signal
  - Determine the matched filter response
- ❑ Determine MF for known gain and delay in the channel
- ❑ Compute the effective discrete-time channel given
  - Channel response, TX and RX filter
  - Time-domain or frequency-domain method
- ❑ Determine if there is ISI
- ❑ Compute the frequency response using digital RX filtering and downsampling
- ❑ Determine specifications on the digital and analog filters

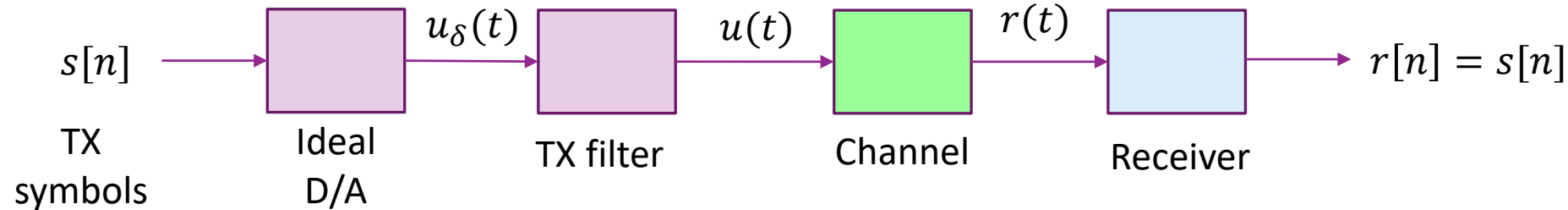
# Outline

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- Receiver filtering and sampling
  - Perfect reconstruction with orthonormal modulation
  - General channels: Time-domain analysis
  - General channels: Frequency-domain analysis
  - PSD Analysis
  - Practical RX filter design
  - Channel sounding

# Receiver Problem



## □ Transmit steps so far:

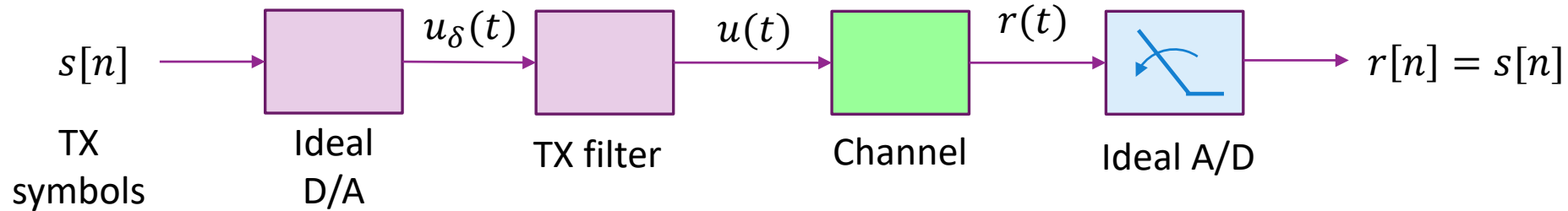
- Symbols  $s[n]$
- Linearly modulate:  $u(t) = \sum s[n]p_{tx}(t - nT)$
- Baseband equivalent channel  $r(t) = h_{chan}(t) * u(t)$

## □ Question at the receiver: Can we recover the transmitted symbols?

## □ Want a mapping that input $r(t)$ to samples $r[n]$

## □ Ideally $r[n] = s[n]$

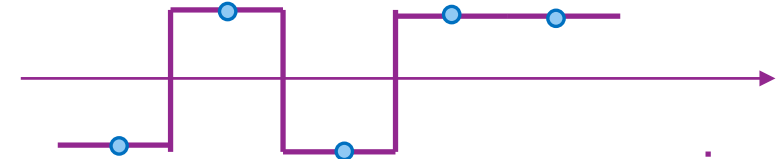
# Simple Idea: Sampling



□ Take samples with an ideal A/D:  $r[n] = r(nT)$

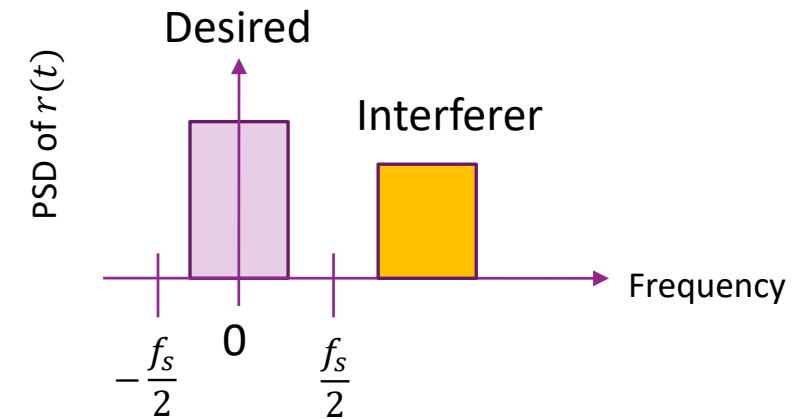
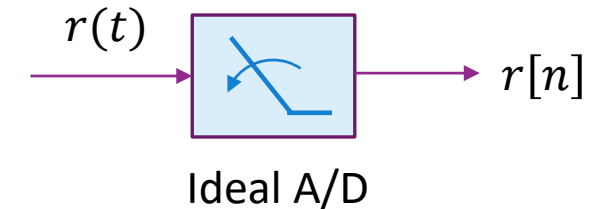
□ This could work: Example

- Suppose  $p_{tx}(t) = \text{Rect}\left(\frac{t}{T}\right)$  (Ideal zero-order-hold D/A)
- $h_{chan}(t) = \delta(t)$  (no channel effect)
- Then:  $r(t) = u(t) = \sum_n s[n] \text{Rect}\left(\frac{t-nT}{T}\right)$
- So,  $r(nT) = s[n]$
- Hence, if we sample at exactly the right time, we can recover  $s[n]$



# Problems with Ideal Sampling

- ❑ Three problems in implementing an ideal A/D
- ❑ **Problem 1:** No circuit exactly samples at one instant
  - Most circuits integrate over some period
  - Ex: Charge fills a capacitor at the input to the A/D
- ❑ **Problem 2:** Out-of-band emissions (“blockers”)
  - The received signal may contain signals at neighboring frequencies
  - Ex: Transmissions in other wireless channels
  - The system may not have control over these
  - Without filtering, these will be aliased into  $r[n]$
  -



# Problems with Ideal Sampling

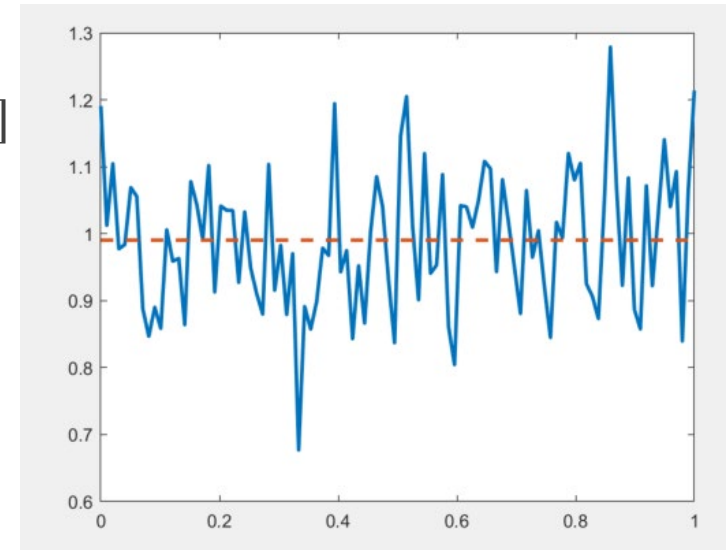
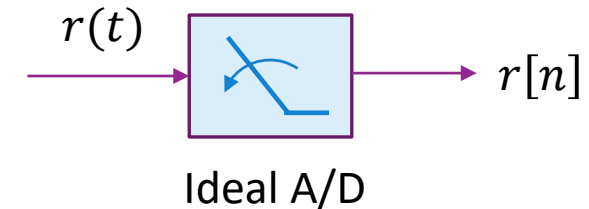
❑ Three problems in implementing an ideal A/D

❑ **Problem 3:** No noise filtering

- Suppose that in some symbol period:

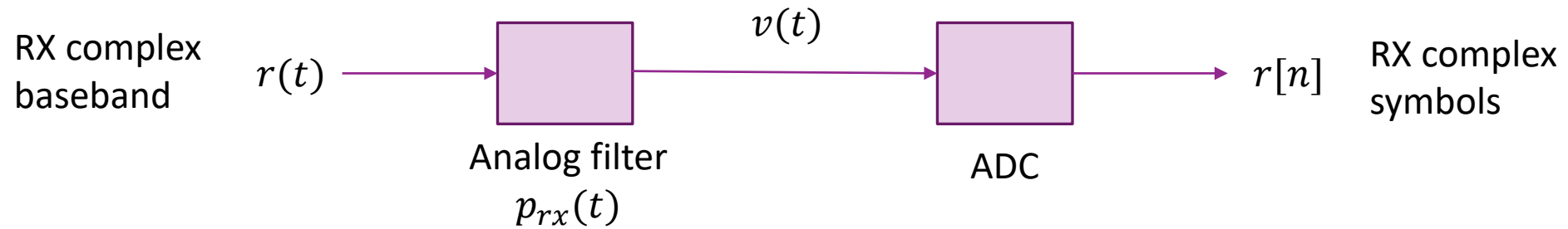
$$r(t) = s[n] + w(t), \quad t \in [nT, (n+1)T)$$

- $r(t)$  = “desired signal” + “noise”.
- Noise  $w(t)$  will appear in any sample.
- But, suppose we average:  $r_{avg}[n] = \frac{1}{T} \int_{nT}^{(n+1)T} r(t) dt = s[n] + v[n]$
- Effective noise is  $v[n] = \frac{1}{T} \int_{nT}^{(n+1)T} w(t) dt$
- This will, in general, have a lower variance
- We will describe this more next unit






# Two Step Receiver



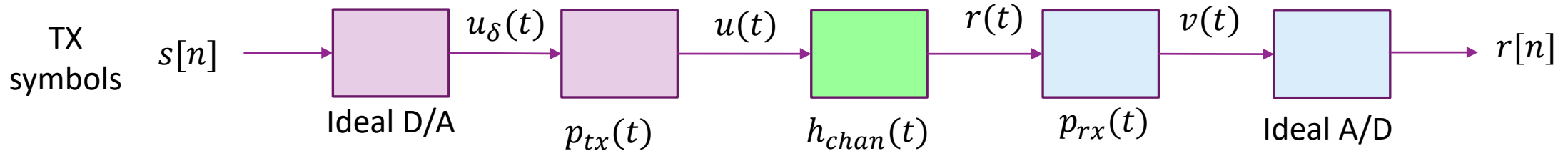
- ❑ Discussion motivates a two step process
- ❑ Step 1: Receive filter:  $v(t) = p_{rx}(t) * r(t)$ 
  - $p_{rx}(t)$  is the RX filter response
- ❑ Step 2: Sample  $r[n] = v(nT)$
- ❑ Filter is useful to:
  - Model imperfections in the sampling
  - Filter out blockers. Anti-aliasing
  - Average out noise (more on this later)

# Outline

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- ☐ Receiver filtering and sampling
-  ☐ Perfect reconstruction with orthonormal modulation
- ☐ General channels: Time-domain analysis
- ☐ General channels: Frequency-domain analysis
- ☐ PSD Analysis
- ☐ Practical RX filter design
- ☐ Channel sounding

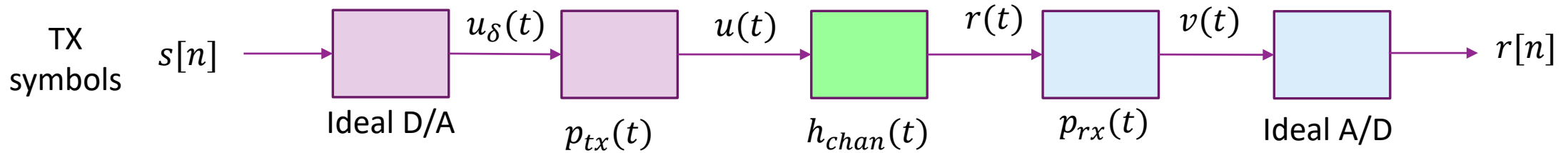
# End-to-end TX and RX Chain so Far



## □ Steps:

- Impulse D/A:  $u_\delta(t) = \sum s[n]\delta(t - nT)$
- TX pulse shape:  $u(t) = u_\delta(t) * p_{tx}(t) = \sum s[n]p_{tx}(t - nT)$
- Channel:  $r(t) = u(t) * h_{chan}(t)$
- RX filter:  $v(t) = r(t) * p_{rx}(t)$
- Sampling A/D:  $r[n] = v(nT)$

# Basic Questions



- ❑ Under what circumstances can we construct transmitted signals.
- ❑ That is, how do we select  $p_{rx}(t)$  such that  $r[n] = s[n]$ ?
- ❑ We first analyze this for a simple case:
  - Orthonormal pulse shapes
  - No channel impairments

# Inner Products and Orthonormal Signals

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□ Let  $f(t), g(t)$  be two complex-valued signals

□ **Definition 1:** The **inner product** of  $f, g$  is:

$$\langle f, g \rangle = \int_{-\infty}^{\infty} f^*(t)g(t)dt$$

◦ Here  $f^*(t)$  = complex-conjugate of  $f(t)$

□ **Definition 2:** We say  $f(t), g(t)$  are **orthogonal** if  $\langle f, g \rangle = 0$

◦ We will write this as  $f \perp g$

□ **Definition 3:** The **signal energy** is  $\|f\|^2 := \langle f, f \rangle = \int_{-\infty}^{\infty} |f(t)|^2 dt$

□ We will discuss this in much more detail in the next unit on signal spaces

# Example Problem

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□ Suppose  $f(t) = a \text{Rect}\left(\frac{t}{T}\right)$ ,  $g(t) = (b + ct) \text{Rect}\left(\frac{t}{T}\right)$

- Complex  $a, b, c$  with  $a \neq 0$

□ Compute  $\langle f, g \rangle$

□ When is  $f \perp g$ ?

□ Solution:

- $\langle f, g \rangle = \int_{-\infty}^{\infty} f^*(t)g(t)dt = \int_{-T/2}^{T/2} a^*(b + ct)dt = a^*bT$
- Therefore  $f \perp g = 0 \iff \langle f, g \rangle = a^*bT = 0$ .
- Since  $a, T \neq 0$ ,  $f \perp g = 0 \iff b = 0$

# Orthogonality in Frequency Domain

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□ Sometimes it is more convenient to evaluate inner products in frequency domain

□ Parseval's Theorem: Let  $f(t), g(t)$  be any two signals. Then:

$$\langle f, g \rangle = \int f^*(t)g(t)dt = \int F^*(f)G(f)df$$

□ This is useful whenever the Fourier transforms  $F(f), G(f)$  are simple to work out.

# Example

□ Suppose  $f(t) = A \operatorname{sinc}\left(\frac{t}{T}\right)$ ,  $g(t) = B \operatorname{sinc}\left(\frac{t-\tau}{T}\right)$

□ Compute  $\langle f, g \rangle$ . When are they orthogonal?

□ Solution:

- Do this in frequency domain
- $F(f) = AT \operatorname{Rect}(fT)$ ,  $G(f) = BT \operatorname{Rect}(fT) e^{-2\pi i f \tau}$
- From Parseval's Theorem: Let  $f_0 = 1/(2T)$

$$\begin{aligned} \langle f, g \rangle &= \langle F, G \rangle = \int F^*(f) G(f) df = AB T^2 \int_{-f_0}^{f_0} e^{-2\pi i f \tau} df \\ &= \frac{AB T^2}{2\pi i \tau} \left[ e^{2\pi i f_0 \tau} - e^{-2\pi i f_0 \tau} \right] = AB T \operatorname{sinc}(2f_0 \tau) = AB T \operatorname{sinc}\left(\frac{\tau}{T}\right) \end{aligned}$$

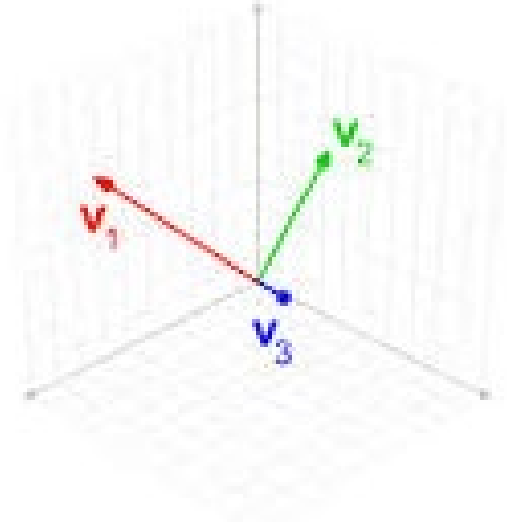
- $\langle f, g \rangle = 0$  when  $\tau = kT$  for some integer  $k$





# Orthonormal Signals

- Let  $\phi_n(t), n = 0, 1, \dots$  be a set of signals
  - This can be indexed from  $n = -\infty$  to  $\infty$  as well
- **Definition:** The set  $\phi_n(\cdot)$  is **orthonormal** if:
  - $\|\phi_n\| = 1$  for all  $n$  (all signals have unit energy)
  - $\langle \phi_n, \phi_m \rangle = 0$  for all  $n \neq m$  (different signals are orthogonal)
- This generalizes the concept of orthonormal vectors
- We will discuss orthonormal sets much more in signal space theory



# Orthonormal Pulses and Matched Filtering

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□ Consider the linear modulation:  $u(t) = \sum_n s[n]p_{tx}(t - nT)$

□ **Definition 1:** We will say that the modulation is orthogonal if

$$\phi_n(t) = p_{tx}(t - nT), \quad n = \dots, -2, -1, 0, 1, 2, \dots$$

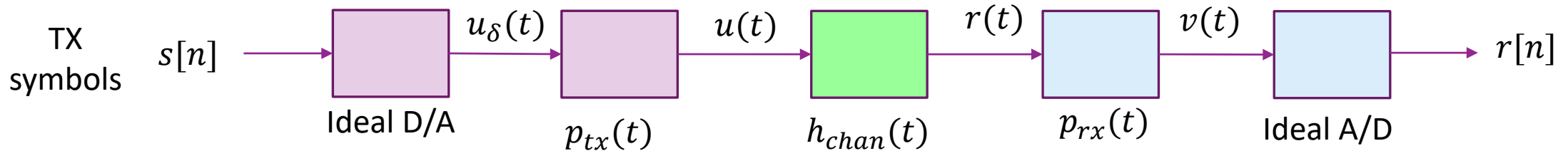
is an orthonormal set.

□ **Definition 2:** Given any transmit pulse,  $p_{tx}(t)$ , the matched filter RX pulse is:

$$p_{rx}(t) = p_{tx}^*(-t)$$

- The pulse that is complex conjugate and flipped in time
- Note that if TX filter is causal, RX filter is anti-causal

# Reconstruction With Orthonormal Pulses



□ **Theorem:** Suppose that:

- $p_{tx}(t)$  generates orthonormal pulse at sample rate  $\frac{1}{T}$
- $h_{chan}(t) = \delta(t)$  (i.e.  $r(t) = u(t)$  so there are no channel impairments)
- $p_{rx}(t) = p_{tx}^*(-t)$  (RX uses matched filter)

Then the receiver will exactly recover the TX samples in that  $r[n] = s[n]$

□ **Theorem** answers our question. We can reconstruct the RX samples

- Under several assumptions

# Proof of Reconstruction Theorem

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- TX signal is:  $u(t) = \sum_n s[n]p_{tx}(t - nT)$
- Since  $h_{chan}(t) = \delta(t) \Rightarrow r(t) = h_{chan}(t) * u(t) = u(t) = \sum_n s[n]p_{tx}(t - nT)$
- RX filtered signal is:  $v(t) = p_{rx}(t) * u(t) = \sum_n s[n](p_{rx} * p_{tx})(t - nT)$
- Sampling is:  $r[m] = v(mT) = \sum_n s[n](p_{rx} * p_{tx})((m - n)T)$
- Now look at convolution:  
$$(p_{rx} * p_{tx})(t) = \int p_{rx}(t - s)p_{tx}(s)ds = \int p_{tx}^*(s - t)p_{tx}(s)ds$$
- At  $t = kT$ :  $(p_{rx} * p_{tx})(kT) = \int p_{tx}^*(s - kT)p_{tx}(s)ds$
- But  $\phi_k(t) = p_{tx}(t - kT)$  is an orthonormal set
- So,  $(p_{rx} * p_{tx})(kT) = \langle \phi_k, \phi_0 \rangle = \delta_k$
- Hence:  $r[m] = v(mT) = \sum_n s[n]\delta_{m-n} = s[m]$

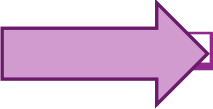
# “Practical” Orthogonal Pulses

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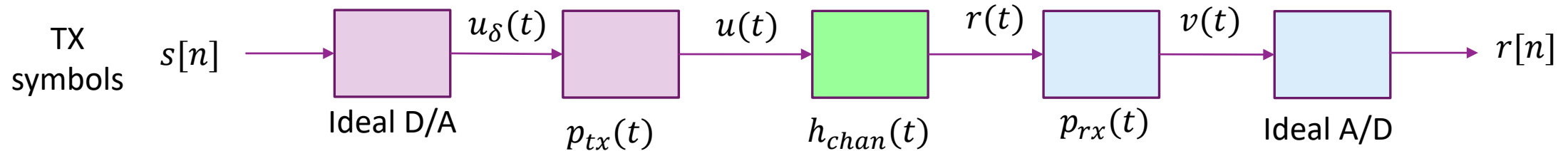
- ❑ There are two important “practical” orthonormal pulses
- ❑ Rectangles:  $p_{tx}(t) = \frac{1}{\sqrt{T}} \text{Rect}\left(\frac{t}{T}\right)$ 
  - Orthonormal since  $p_{tx}(t - nT)$  and  $p_{tx}(t - mT)$  do not overlap when  $n \neq m$
  - Scaling by  $\frac{1}{\sqrt{T}}$  ensures they are normalized
  - This can be achieved (with some scaling) by a zero-order hold ADC
- ❑ Sinc pulses:  $p_{tx}(t) = \frac{1}{\sqrt{T}} \text{Sinc}\left(\frac{t}{T}\right)$ 
  - Use similar frequency domain calculation as before to prove these are orthonormal
  - This would arise with ideal filtering at the TX and RX.
  - No filter is exactly ideal.
  - But, practical filters get quite close to this response.

# Outline

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- ☐ Receiver filtering and sampling
- ☐ Perfect reconstruction with orthonormal modulation
-  ☐ General channels: Time-domain analysis
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- ☐ PSD Analysis
- ☐ Practical RX filter design
- ☐ Channel sounding

# Modeling the End-to-End System



□ We have seen so far that when:

- Pulse shapes are matched
- Modulation is orthonormal
- No channel impairments

□ Then:  $r[n] = s[n]$

□ What happens when these conditions fail?

# Channel Gain

□ Consider simple deviation: Channel gain  $r(t) = Gu(t)$

- Gain can be due to attenuation in wire, for example.

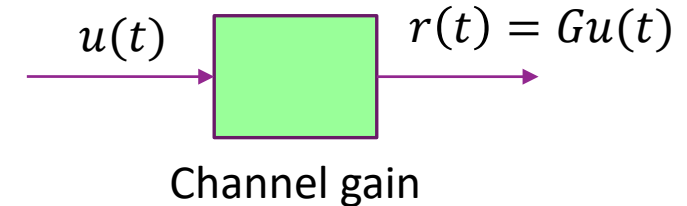
□ Suppose, as before, that:

- $p_{tx}(t - nT)$  are orthonormal for different  $n$
- $p_{rx}(t) = p_{tx}^*(-t)$ , i.e. matched filter

□ Then  $r[n] = Gs[n]$

- Proof on board
- Simply scales symbols.
- Can recover symbols from  $r[n]/G$

□ But, requires that gain is known. More on this later





# Channel Gain and With Known Delay

- Now consider gain and delay

- $r(t) = Gu(t - \tau)$

- Then,  $r(t) = \sum G s_n p_{tx}(t - \tau - nT)$

- Suppose gain and delay are known

- Use shifted and scaled receive filter

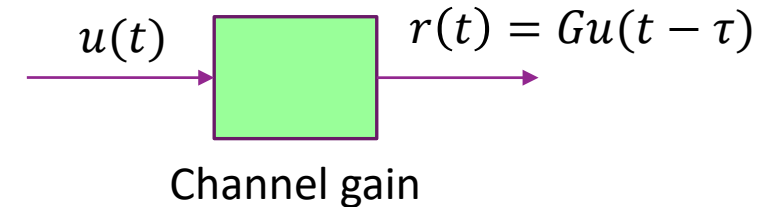
$$p_{rx}(t) = \frac{1}{G} p_{tx}^*(-t + \tau)$$

- Then:  $r[n] = s[n]$

- Proof on board

- RX filter is shifted to delay

- Must know the gain and delay
  - Requires **synchronization**



# Integer Delays

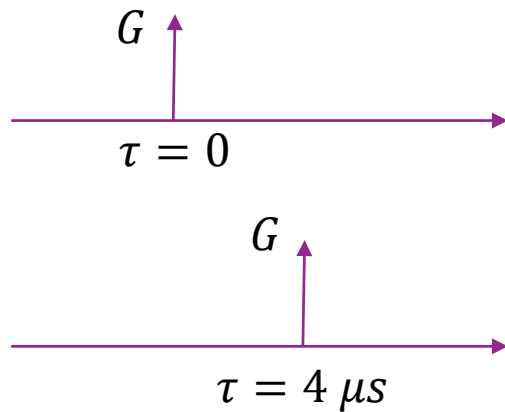
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- Suppose:  $r(t) = Gs(t - \tau)$ 
  - Delay is an integer multiple of the sample period:  $\tau = k_0 T$
- Suppose, as before:
  - TX uses orthonormal modulation
  - MF receiver  $p_{rx}(t) = p_{rx}^*(-t)$  (but, not shifted and scaled)
- Then:  $r[n] = Gs[n - k_0]$ 
  - Channel delay of  $\tau = k_0 T \Rightarrow$  Symbol delay of  $k_0$
  - Proof on board

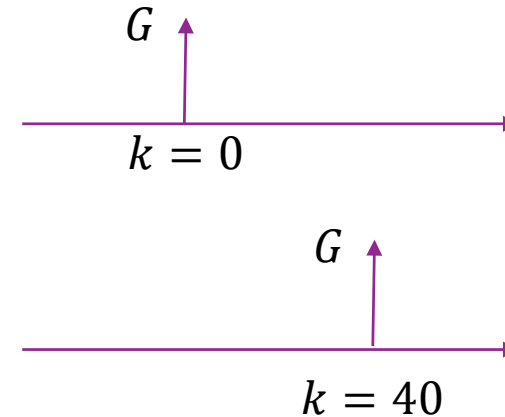
# Integer Delays visualized

- Suppose TX uses orthonormal modulation and RX uses matched filter
- Suppose sample rate is  $T = 0.1 \mu s$  ( $f = 10$  Msym/s)

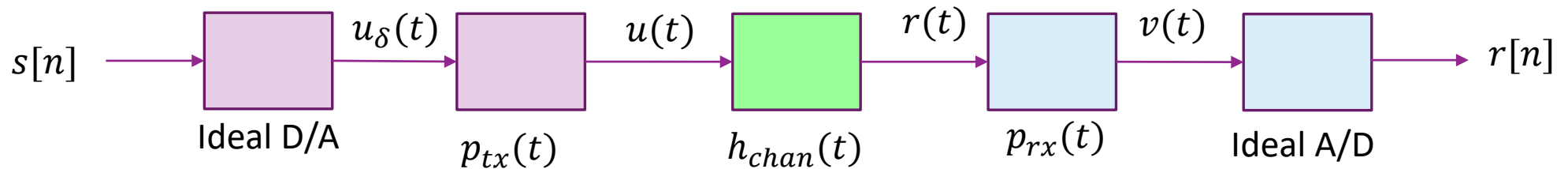
Baseband channel impulse response



Effective discrete-time channel



# General case



- Define **channel impulse response with filtering**  $g(t) = p_{tx}(t) * h_{chan}(t) * p_{rx}(t)$ 
  - Represents path from DAC output to ADC input
- **Theorem**: Mapping from  $r[n]$  to  $s[n]$  is LTI with impulse response is  $h[n] = g(nT)$ ,
- Receive symbols will be given by  $r[n] = \sum_{k=-\infty}^{\infty} h[k]s[n - k]$

# Example 1: Rectangular Pulse

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- Suppose that  $p_{tx}(t) = p_{rx}(t) = \text{Rect}(t/T)$
- If channel is  $r(t) = Gu(t - \tau)$ , what is effective DT channel  $h[n]$
- Solution:
  - Impulse response is  $h_{chan}(t) = \delta(t - \tau)$
  - Impulse response from  $u_{\delta}(t) \mapsto v(t)$  is  $g(t) = p_{tx}(t) * p_{rx}(t) * h_{chan}(t) = GT \text{Tri}(t - \tau)$
  - Then  $h[n] = g(nT)$

# Example 2 Illustrated

- Channel response with filtering

$$g(t) = GT \operatorname{Tri}(t - \tau)$$

- Effective discrete-time channel:

$$h[n] = g(nT)$$

- Plot to right:  $GT = 1, T = 1$

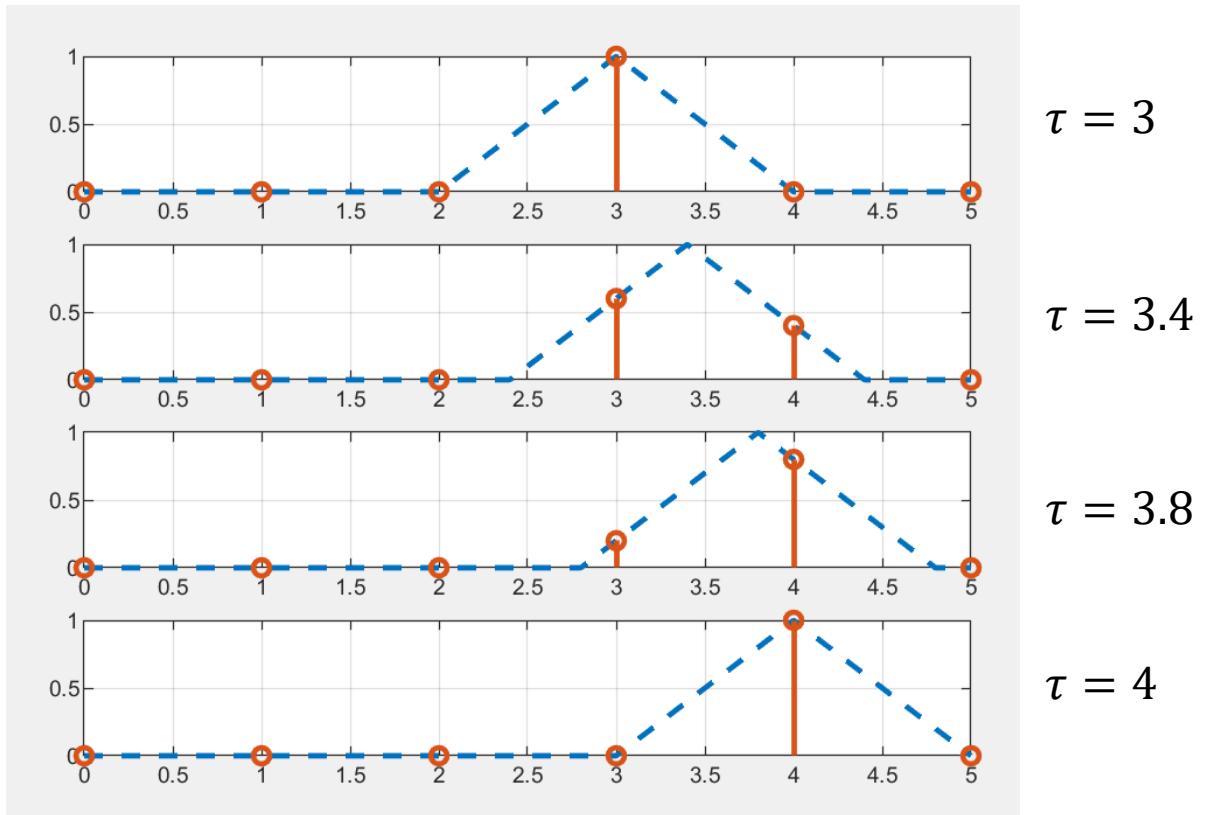
- $g(t)$ : Blue dashed
- $h[n]$ : Red stem

- When  $\tau = kT$  is an integer:

- $h[n] = \delta_{n-k}$
- Single tap

- When  $\tau \in (kT, (k+1)T)$

- $h[n]$  has two taps



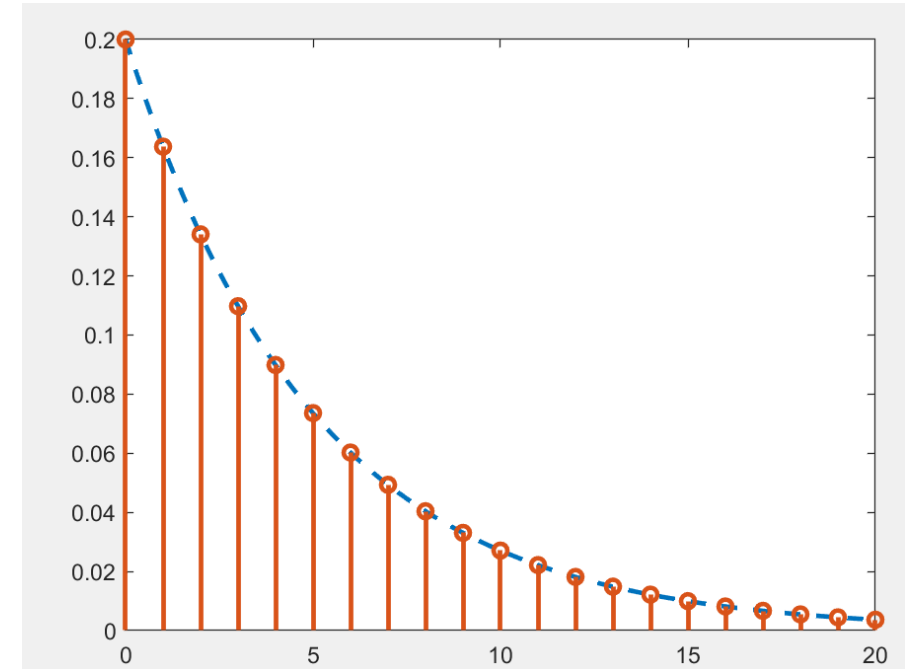
# Example 2: Exponential

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- Suppose that  $p_{tx}(t) = \delta(t), p_{rx}(t) = T\delta(t)$
- Baseband channel is:  $\frac{dr(t)}{dt} = \frac{\alpha}{T}(u(t) - r(t))$
- Find filtered channel response  $g(t)$  and effective discrete-time response  $h[n]$
- Solution:
  - Take Laplace transform of differential eqn:  $R(s) = \frac{c}{s+c}U(s), c = \frac{\alpha}{T}$
  - Using inverse Laplace transform:  $r(t) = h_{chan}(t) * u(t)$  where  $h_{chan}(t) = ce^{-ct}1_{[0,\infty)}(t)$
  - Filtered channel response:  $g(t) = p_{tx}(t) * p_{rx}(t) * h_{chan}(t) = cTe^{-ct}1_{[0,\infty)}(t)$
  - Discrete-time response:  $h[n] = g(nT) = cTe^{-cnT}1_{\{n \geq 0\}} = \alpha e^{-\alpha n}1_{\{n \geq 0\}}$

# Example 2: Exponential Illustrated

- Suppose that  $p_{tx}(t) = \delta(t), p_{rx}(t) = T\delta(t)$
- Baseband channel is:  $\frac{dr(t)}{dt} = \frac{\alpha}{T}(u(t) - r(t))$
- From previous slide:
  - Filtered channel response:  $g(t) = cTe^{-ct}1_{[0,\infty)}(t)$
  - Discrete-time response:  $h[n] = g(nT) = \alpha e^{-\alpha n}1_{\{n \geq 0\}}$





# Effective Discrete-Time Channel

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- ❑ Lack of synchronization causes channel of the form

$$r[n] = \sum_{k=-\infty}^{\infty} h[k]s[n-k]$$

- ❑  $h[k]$  called the effective discrete-time channel

- ❑ Inter-symbol interference:

- Whenever  $h[k] \neq 0$  for  $k \neq 0$
- Other symbols interfere with one another

- ❑ ISI occurs for many reasons:

- Lack of synchronization
- Channel impairments

# ISI and Equalization

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- Effective discrete-time channel is:

$$r[n] = \sum_{k=-\infty}^{\infty} h[k]s[n-k]$$

- System has **inter-symbol interference (ISI)**:

- Multiple symbols  $s[n-k]$  effect  $r[n]$


- The receiver must undo this ISI.

- This process is called equalization

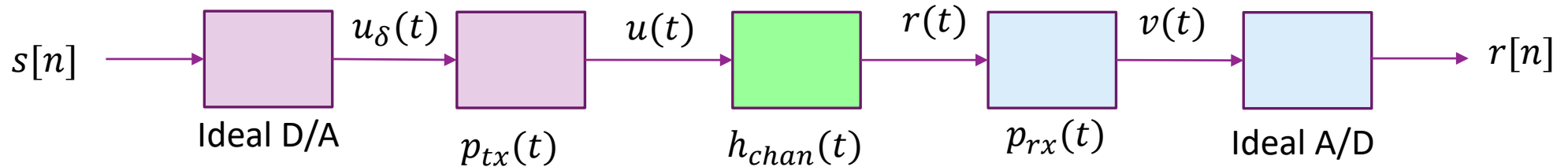
- We will discuss this later.

# Outline

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- ☐ Receiver filtering and sampling
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-  ☐ General channels: Frequency-domain analysis
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- ☐ Channel sounding

# Digital Channel Frequency Response



□ We saw that effective digital channel from  $s[n] \mapsto u[n]$  is:

$$r[n] = \sum_k h[k]s[n-k], \quad h[k] = g(kT), \quad g(t) = p_{rx}(t) * h_{chan}(t) * p_{tx}(t)$$

□ Question: What is the frequency response?

$$R(\Omega) = H(\Omega)S(\Omega)$$

# Frequency Response of DT Filter

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□ Fact from signals and systems: If  $h[n] = g(nT)$

$$H(\Omega) = \frac{1}{T} \sum_{k=-\infty}^{\infty} G\left(\left(\frac{\Omega}{2\pi} + k\right)\frac{1}{T}\right)$$

□ Shifted copies of  $G(f)$

□ Continuous frequency  $f$  mapped to DT frequency  $\Omega = 2\pi f / f_s$ ,  $f_s = 1/T$

□ Can obtain coefficients from inverse DTFT:

$$h[n] = \frac{1}{2\pi} \int_0^{2\pi} H(\Omega) e^{jn\Omega} d\Omega$$

# Computing Effective DT Frequency Response Summary

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□ Compute frequency response of channel with filtering  $G(f) = P_{rx}(f)H_{chan}(f)P_{tx}(f)$

□ Effective DT channel response is:

$$H(\Omega) = \frac{1}{T} \sum_{k=-\infty}^{\infty} G\left(\left(\frac{\Omega}{2\pi} + k\right)\frac{1}{T}\right)$$

- Scale  $G(f)$  vertically by  $1/T$
- Map continuous-time frequency  $f$  to  $\Omega = 2\pi fT = \frac{2\pi f}{f_s}$
- Create shifted versions every  $2\pi$
- Shifted versions may overlap if there is aliasing

# Bandlimited Channel

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□ Suppose one of  $P_{rx}$ ,  $P_{tx}$  or  $G$  bandlimited to  $|f| < \frac{1}{2T}$ ,

□ Effective discrete-time channel reduces to

- $H(\Omega) = \frac{1}{T} P_{rx} \left( \frac{\Omega}{2\pi T} \right) P_{tx} \left( \frac{\Omega}{2\pi T} \right) H_{chan} \left( \frac{\Omega}{2\pi T} \right)$  for  $|\Omega| < \pi$

□ If TX and RX filters are ideal low-pass:

- $P_{rx}(f) = P_{tx}(f) = \sqrt{T} \text{Rect}(fT)$
- $H(\Omega) = G \left( \frac{\Omega}{2\pi T} \right)$

# Example: Sinc Pulses

---

□ Suppose that

- $p_{rx}(t) = p_{tx}(t) = \frac{1}{\sqrt{T}} \text{sinc}\left(\frac{t}{T}\right)$
- $H_{chan}(f) = 1$  (no impairments)

□ Then,

- $P_{rx}(f) = P_{tx}(f) = \sqrt{T} \text{rect}(fT)$
- $H(\Omega) = 1$

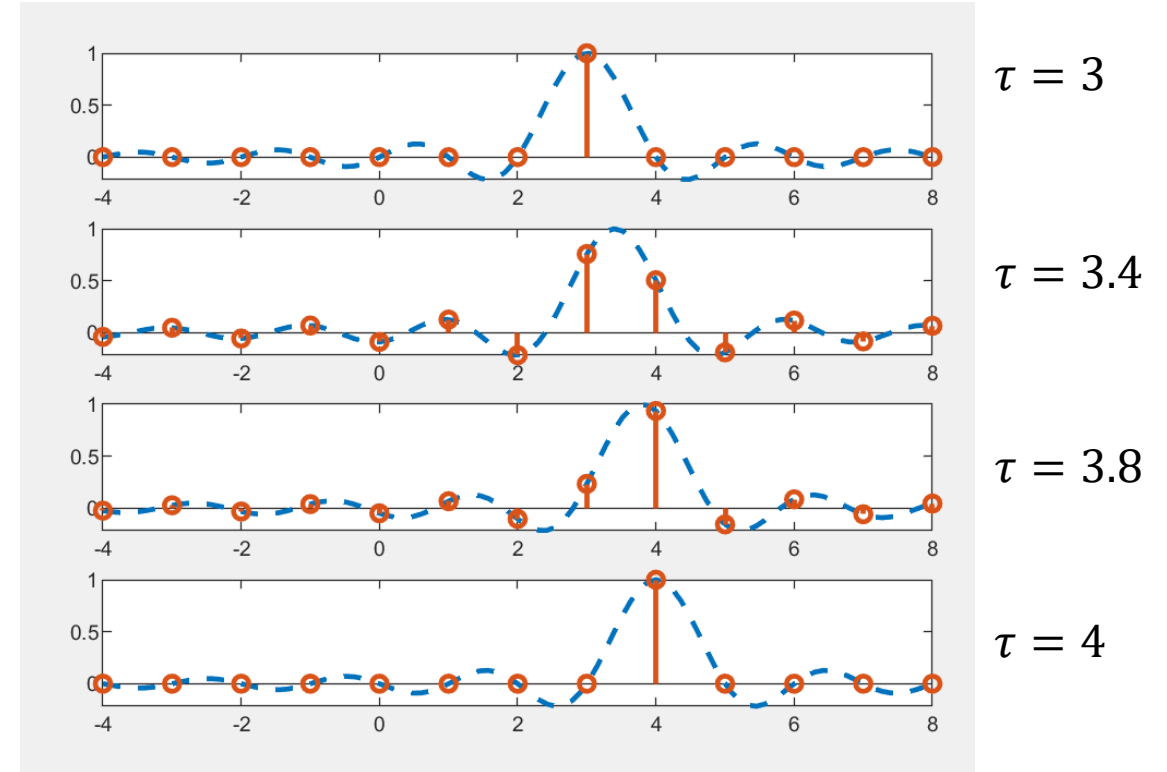
□ Hence,  $R(\Omega) = S(\Omega)$ .

□ Recover symbols exactly. No ISI



# Example: Sinc Pulses with Delay

- Suppose that  $p_{rx}(t) = p_{tx}(t) = \frac{1}{\sqrt{T}} \text{sinc}\left(\frac{t}{T}\right)$
- Channel has gain and delay:  $r(t) = Gu(t - \tau)$
- $H_{chan}(f) = Ge^{-2\pi jf\tau}$
- Then,
  - $P_{rx}(f) = P_{tx}(f) = \sqrt{T} \text{rect}(fT)$
  - $H(\Omega) = H_{chan}\left(\frac{\Omega}{2\pi T}\right) = Ge^{-j\Omega\tau/T}$
- Similar calculation as before:  $h[n] = \text{sinc}\left(\frac{\tau n}{T}\right)$



# Flat Channels

---

□ Suppose that

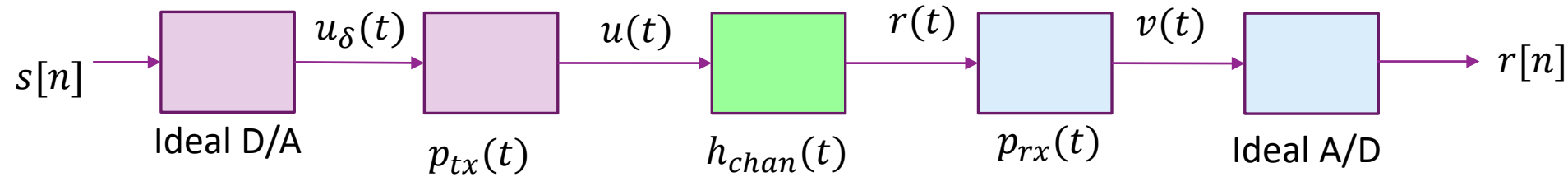
- $P_{rx}(f) = P_{tx}(f) = \sqrt{T} \text{rect}(fT)$
- $G(f) \approx G_0$  in  $|f| < \frac{1}{2T}$
- “Flat” over the channel.

□ Then, effective discrete-time channel is

- $H(f) = G_0$
- $r[n] = G_0 s[n]$
- No ISI

□ **Conclusion:** When channel is “flat” over band, equalization is not needed

# Numerically Computing the Channel



- ❑ For most real channels, we cannot analytically compute  $h[n]$ 
  - Transmit and receive filters have complex frequency response
  - Channels can have many taps at arbitrary delays
- ❑ But, we need  $h[n]$  for proper simulation of communication systems
- ❑ Common solution: Approximately compute  $h[n]$  numerically

# Numeric Computation via Discretization

□ Baseband channel frequency response with filtering:  $G(f) = P_{rx}(f)P_{tx}(f)H_{chan}(f)$

□ Effective discrete-time frequency response:  $H(\Omega) = \frac{1}{T} G\left(\frac{\Omega}{2\pi T}\right)$

- Assume no aliasing.

□ Discrete-time impulse response:  $h[n] = \frac{1}{2\pi} \int_0^{2\pi} H(\Omega) e^{i\Omega n} d\Omega$

□ Evaluate integral by discretization:

- Take  $N$  points

- $h[n] \approx \frac{1}{N} \sum_{k=-N/2+1}^{N/2} H(\Omega_k) e^{\frac{i2\pi kn}{N}}, \quad \Omega_k = \frac{2\pi k}{N}$

- Writing in terms of  $G(f)$ :  $h[n] \approx \frac{1}{NT} \sum_{k=-N/2+1}^{N/2} G(f_k) e^{\frac{i2\pi kn}{N}}, \quad f_k = \frac{k}{TN}$

- Summation can be computed via an IFFT

# Example: Two Path Channel

□ Sample rate =  $\frac{1}{T} = 8(120)(1.024) = 983.04$  MHz

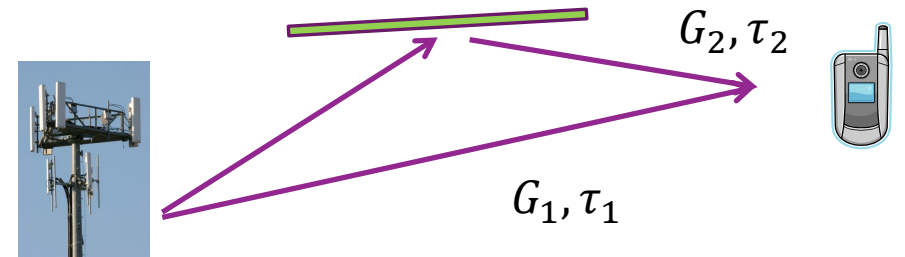
- Sample rate for an 8 channel 5G New Radio system at 120 sub-carrier spacing

□  $p_{rx}(t) = p_{tx}(t) = \frac{1}{\sqrt{T}} \text{Rect}\left(\frac{t}{T}\right)$  (zero-order hold ADCs)

□  $h_{chan}(t)$  has two paths:

- LOS path: Gain -10 dB, delay = 0
- NLOS path: Gain -15 dB, delay = 10 ns

□ In a wireless system, this would correspond to a path difference of  $10(10)^{-9}3(10)^8 = 3$  m



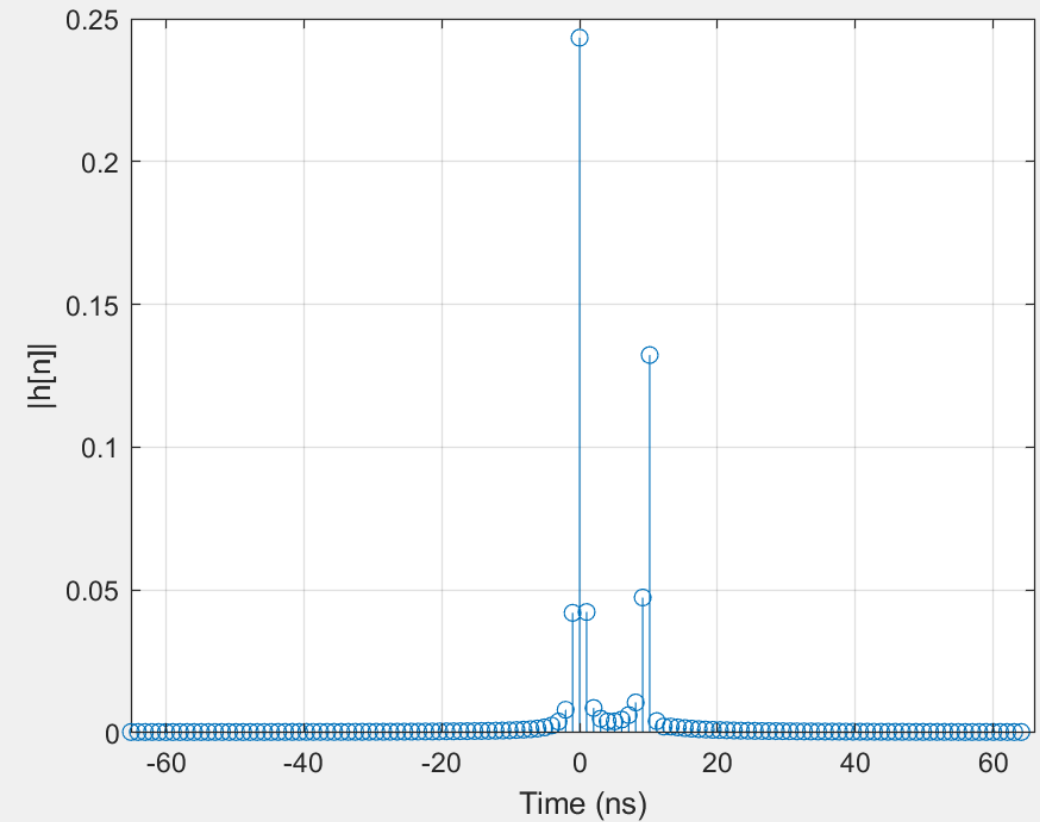
# MATLAB Code

```
% Parameters
fsampMHz = 8*120*1.024;
Tsamp = 1/fsampMHz;

% Freq discretization points
npts = 128;
f = fsampMHz*(-npts/2+1:npts/2)'/npts;

% TX and RX filter
Prx = sqrt(Tsamp)*sinc(f*Tsamp);
Ptx = Prx;


% Channel
gaindB = [-10,-15];
dlyus = [0,0.01];
npath = length(gaindB);
Hchan = zeros(npts,1);
for ip = 1:npath
    Hchan = Hchan + 10^(0.05*gaindB(ip))*exp(-1i*2*pi*f*dlyus(ip));
end
```



```
% Compute discrete-time channel
G = Hchan.*Prx.*Ptx;
t = (-npts/2+1:npts/2)*Tsamp;
h = 1/Tsamp*ifft(G);
h = fftshift(h);
stem(t,abs(h));
```

# Outline

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- ☐ Receiver filtering and sampling
- ☐ Perfect reconstruction with orthonormal modulation
- ☐ General channels: Time-domain analysis
- ☐ General channels: Frequency-domain analysis
-  ☐ PSD Analysis
- ☐ Practical RX filter design
- ☐ Channel sounding

# PSD of a Sampled Signal

---

□ Suppose that  $y[n] = x(nT)$

□ If there is no aliasing:  $Y(\Omega) = \frac{1}{T} X\left(\frac{\Omega}{2\pi T}\right)$

□ Now, look at auto-correlation:

$$R_y[m] = E(y[n]y^*[n-m]) = E(x(nT)x^*((n-m)T)) = R_x(mT)$$

□ Hence, if there is no aliasing

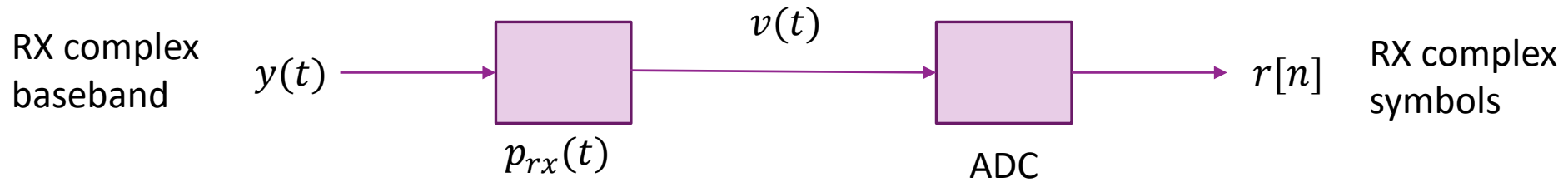
$$S_y(\Omega) = \frac{1}{T} S_x\left(\frac{\Omega}{2\pi T}\right)$$

□ With aliasing:

$$S_y(\Omega) = \frac{1}{T} \sum_{k=-\infty}^{\infty} S_x\left(\left(\frac{\Omega}{2\pi} + k\right)\frac{1}{T}\right)$$



# PSD of the Receiver



□ We have  $r[n] = v(nT)$

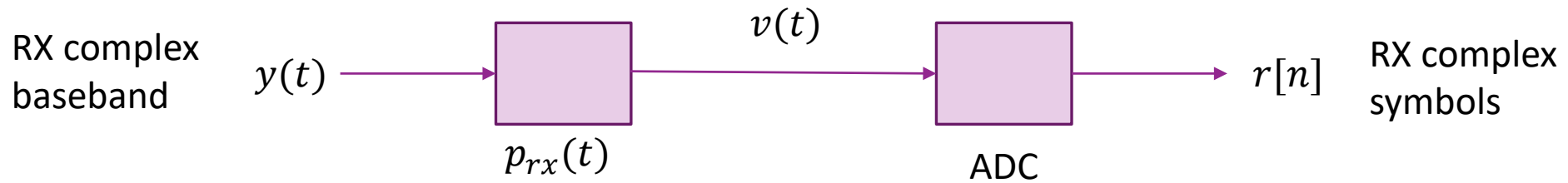
□ By sampling result, discrete-time PSD is:

$$S_r(\Omega) = \frac{1}{T} \sum_{k=-\infty}^{\infty} S_v(f_k) = \frac{1}{T} \sum_{k=-\infty}^{\infty} |P_{rx}(f_k)|^2 S_y(f_k)$$

◦  $f_k = \left(\frac{\Omega}{2\pi} + k\right) \frac{1}{T}$

□ Without aliasing:  $S_r(\Omega) = \frac{1}{T} \left| P_{rx} \left( \frac{\Omega}{2\pi T} \right) \right|^2 S_y \left( \frac{\Omega}{2\pi T} \right)$

# Units in RX Chain: Time Domain



□ In time-domain:  $v(t) = p_{rx}(t) * y(t)$ ,  $r[n] = v(nT)$

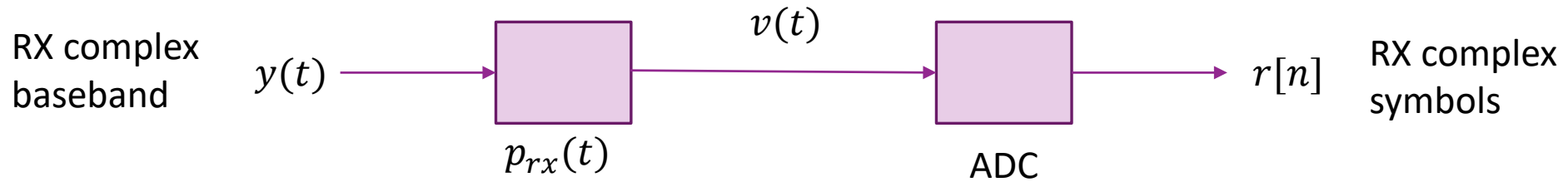
□ Units of  $|y(t)|^2$  = power = energy / time

□ We take convention:  $|p_{rx}(t)|^2 = 1 / (\text{time} * \text{sample})$

□ Then:  $r[n] = \int r(t) p_{rx}(nT - t) dt = \sqrt{\frac{\text{Energy}}{\text{Time}}} \times \sqrt{\frac{1}{\text{Samples} \times \text{Time}}} \times \text{Time} = \sqrt{\frac{\text{Energy}}{\text{Sample}}}$

□ Hence:  $|r[n]|^2 = \frac{\text{Energy}}{\text{Sample}}$

# Units in RX Chain: PSD



$$\square S_r(\Omega) = \frac{1}{T} \left| P_{rx} \left( \frac{\Omega}{2\pi T} \right) \right|^2 S_y \left( \frac{\Omega}{2\pi T} \right)$$

$$\square \text{Units of } S_y(f) = \text{power/Hz} = \text{energy}$$

$$\square \text{Units of } |p_{rx}(t)|^2 = 1/(\text{samples} \times \text{time})$$

$$\square \text{Units of } |P_{rx}(f)|^2 = 1/(\text{samples} \times \text{Hz})$$

$$\square \text{Units of } S_r(\Omega) = \frac{1}{\text{Time}} \times \text{Energy} \times \frac{\text{Time}}{\text{Sample}} = \text{Energy per radian}$$

# Sample problem (Solution on board)

Received PSD and filter as shown

Two components:

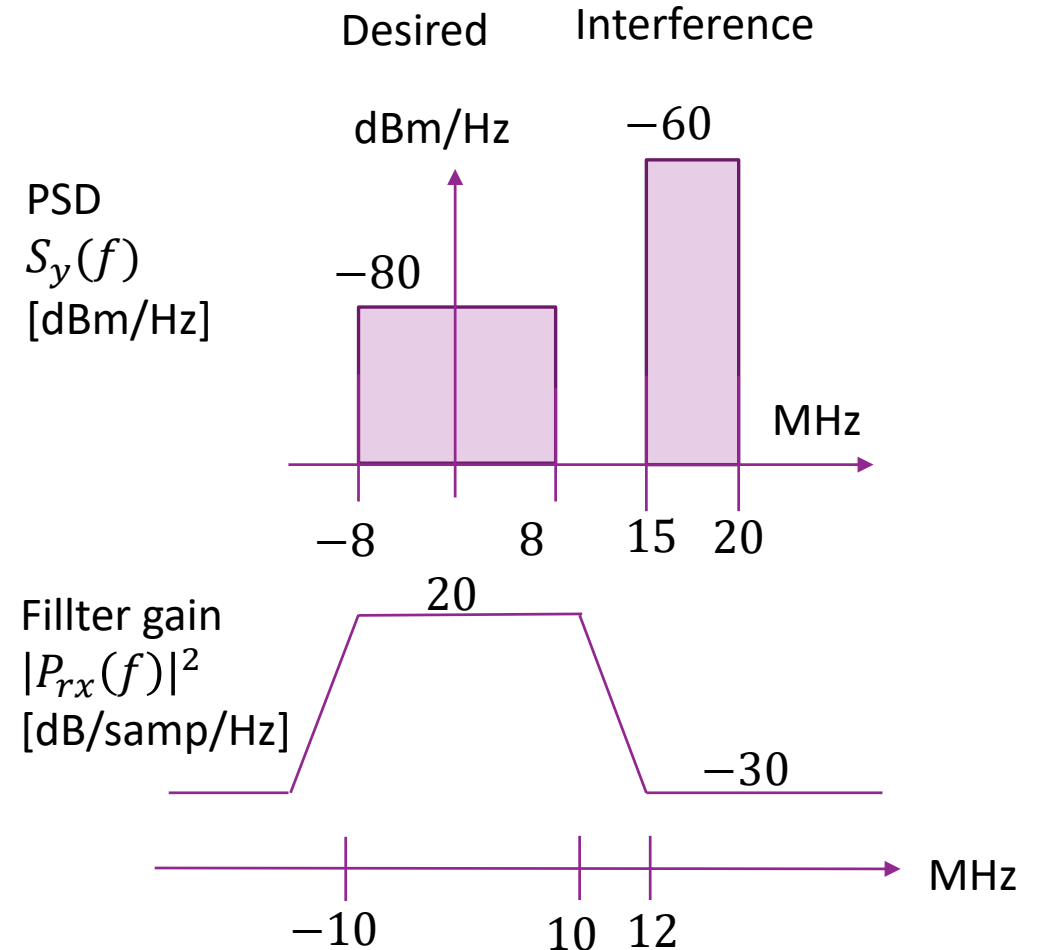
- Desired signal
- Nearby adjacent carrier signal

Assume they are uncorrelated

- Hence powers add.


Draw discrete-time PSD  $S_r(\Omega)$

- Sample rate = 80 Msamples / sec
- Sample rate = 20 Msamples / sec

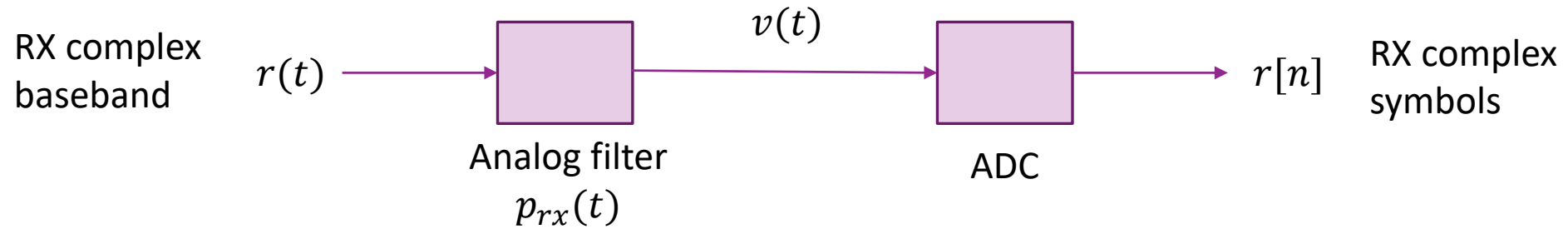


# Outline

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- ☐ Receiver filtering and sampling
- ☐ Perfect reconstruction with orthonormal modulation
- ☐ General channels: Time-domain analysis
- ☐ General channels: Frequency-domain analysis
- ☐ PSD Analysis
-  ☐ Practical RX filter design
- ☐ Channel sounding

# Problems with Analog Filtering



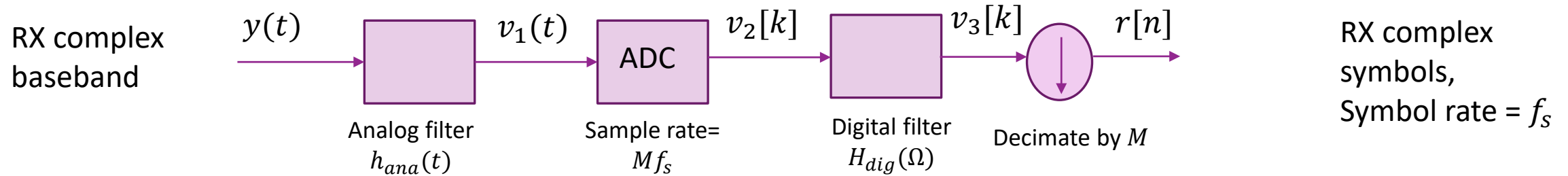
□ Up to now, we have considered two stage filtering

- Filtering:  $v(t) = p_{rx}(t) * r(t)$
- Sampling / ADC:  $r[n] = v(nT)$

□ Problem: Filtering is performed in analog

- Desire sharp filters to remove close adjacent carrier
- Difficult to design sharp filters

# Typical Digital Implementation of RX Filtering



- ❑ Use combination of analog and digital filtering in four steps:
- ❑ Step 1. Analog filtering  $v_1(t) = h_{ana}(t) * y(t)$
- ❑ Step 2. Sample at  $M$  times symbol rate:  $v_2[k] = v_1(kT/M)$ 
  - $M$  = oversampling ratio
- ❑ Step 3. Digitally filter:  $v_3[k] = h_{dig}[k] * v_2[k]$
- ❑ Step 4. Decimate:  $r[n] = v_3[nM]$ .
  - Takes one every  $M$  samples

# Frequency Domain Analysis

---

- Step 1:  $V_1(f) = H_{ana}(f)Y(f)$
- Step 2: Sampling at  $\frac{T}{M}$ :  $V_2(\Omega) = \frac{M}{T} \sum_{k=-\infty}^{\infty} V_1\left(\left(\frac{\Omega}{2\pi} + k\right)\frac{M}{T}\right)$
- Step 3: Digital filtering:  $V_3(\Omega) = V_2(\Omega)H_{dig}(\Omega)$
- Step 4: Decimate:  $R(\Omega) = \frac{1}{M} \sum_{m=0}^{M-1} V_3\left(\frac{\Omega + 2\pi m}{M}\right)$
  
- Assuming no aliasing: Effective RX pulse shape is  $P_{rx}(f) = H_{ana}(f)H_{dig}\left(\frac{2\pi f}{f_s M}\right)$



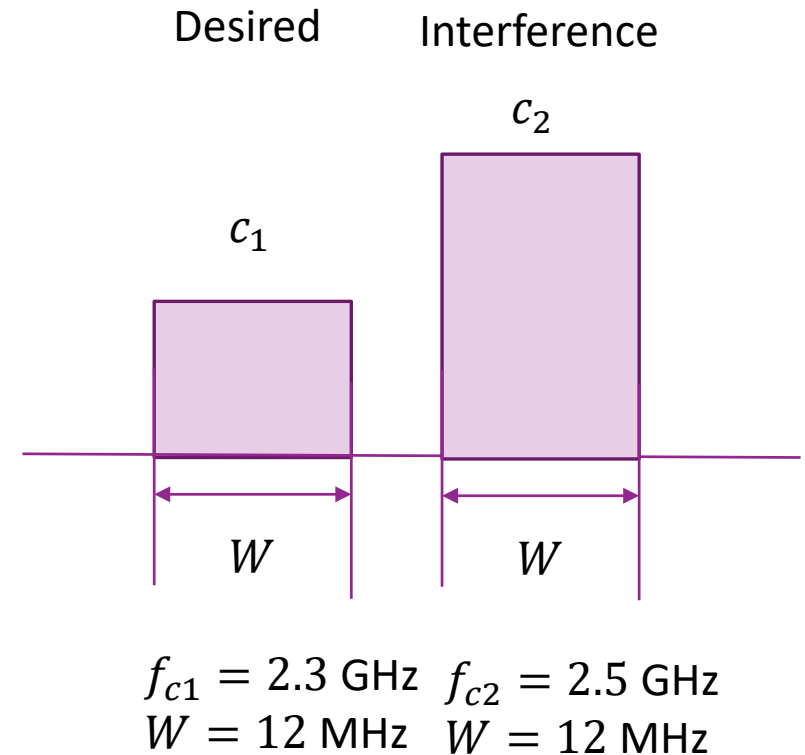
# Frequency Domain Analysis: PSD

---

- Step 1:  $S_1(f) = |H_{ana}(f)|^2 S_y(f)$
- Step 2: Sampling at  $\frac{T}{M}$ :  $S_2(\Omega) = \frac{M}{T} \sum_{k=-\infty}^{\infty} S_1\left(\left(\frac{\Omega}{2\pi} + k\right)\frac{M}{T}\right)$
- Step 3: Digital filtering:  $S_3(\Omega) = S_2(\Omega) |H_{dig}(\Omega)|^2$
- Step 4: Decimate:  $R(\Omega) = \frac{1}{M} \sum_{m=0}^{M-1} S_3\left(\frac{\Omega + 2\pi m}{M}\right)$
  
- Assuming no aliasing: Effective RX pulse shape is  $P_{rx}(f) = H_{ana}(f) H_{dig}\left(\frac{2\pi f}{f_s M}\right)$

# Sample problem (Solution on board)

- ❑ Received passband signal  $S_y(f)$  as shown
- ❑ Two components:
  - Desired signal
  - Nearby adjacent carrier signal
- ❑ Draw the following:
  - Complex baseband  $R(f)$  after mixing at  $f_{c1}$
  - Response after analog filtering with cutoff  $|f| \leq 20$  MHz
  - Sampling at 40 Ms/s
  - Digital filtering with  $|\Omega| \leq \pi/2$
  - Downsampling by 2



# Filter Design

---

- ❑ Effective pulse shape:  $P_{rx}(f) = H_{ana}(f)H_{dig}\left(\frac{2\pi f}{f_s M}\right)$
- ❑ Want  $P_{rx}(f)$  to be low-pass with cutoff  $f = \frac{1}{T}$
- ❑ Typical design for analog filter
  - $H_{ana}(f)$  passband up to  $\frac{1}{2T}$ , Stopband  $\frac{2M-1}{2T}$
  - Removes images before sampling
  - Large transition region. Easy to design
- ❑ Design spec for digital filter
  - Low pass with digital cut-off frequency  $\pi/M$
  - Typically very sharp to remove close adjacent carrier

# Summary of Sampling Relations


Operation	Time domain	Frequency-domain	PSD
Ideal DAC	$u(t) = \sum_n s[n]p(t - nT)$	$U(f) = P(f)S\left(\frac{2\pi f}{f_s}\right)$	$S_u(f) = \frac{1}{T}S_s(2\pi fT) P(f) ^2$
Digital upsampling	$s[n] = \begin{cases} x[k] & n = kM \\ 0 & \text{else} \end{cases}$	$S(\Omega) = X(M\Omega)$	$S_s(\Omega) = \frac{1}{M}S_x(M\Omega)$
Ideal ADC	$r[n] = v(nT)$	$R(\Omega) = \frac{1}{T} \sum_{k=-\infty}^{\infty} V(f_k)$ $f_k = \left(\frac{\Omega}{2\pi} + k\right)\frac{1}{T}$	$S_r(\Omega) = \frac{1}{T} \sum_{k=-\infty}^{\infty} S_v(f_k)$ $f_k = \left(\frac{\Omega}{2\pi} + k\right)\frac{1}{T}$
Ideal ADC. No aliasing	$r[n] = v(nT)$	$R(\Omega) = \frac{1}{T}V\left(\frac{\Omega}{2\pi T}\right)$	$S_r(\Omega) = \frac{1}{T}S_v\left(\frac{\Omega}{2\pi T}\right)$
Digital decimation	$r[n] = x(nM)$	$R(\Omega) = \frac{1}{M} \sum_{m=0}^{M-1} X\left(\frac{\Omega + 2\pi m}{M}\right)$	$S_r(\Omega) = \frac{1}{M} \sum_{m=0}^{M-1} S_x\left(\frac{\Omega + 2\pi m}{M}\right)$
Digital decimation. No aliasing	$r[n] = x(nM)$	$R(\Omega) = \frac{1}{M}X\left(\frac{\Omega}{M}\right)$	$S_r(\Omega) = \frac{1}{M}S_x\left(\frac{\Omega}{M}\right)$

# Summary of Units

Operation	Quantity	Time domain units	PSD units
TX symbols	$s[n]$	$ s[n] ^2$ : Energy per sample	$S_s(\Omega)$ : Energy per sample per radian
TX modulation	$u(t) = \sum p_{tx}(t - nT)s[n]$	$ p_{tx}(t) ^2$ : Samples / sec	$ P_{tx}(f) ^2$ : Samp / Hz = Samp x sec
		$ u(t) ^2$ : Energy / sec = power	$S_u(f)$ : Power / Hz = Energy
RX signal	$y(t)$	$ y(t) ^2$ : Energy / sec = power	$S_y(f)$ : Power / Hz = Energy
RX filtered & sampled	$v(t) = p_{rx}(t) * y(t)$ $r[n] = v(nT)$	$ p_{rx}(t) ^2$ : 1/(samp x time)	$ P_{rx}(f) ^2$ : 1/(samp x Hz)=time/samp
		$ r[n] ^2$ : Energy per sample	$S_r(\Omega)$ : Energy per sample per radian

# Outline

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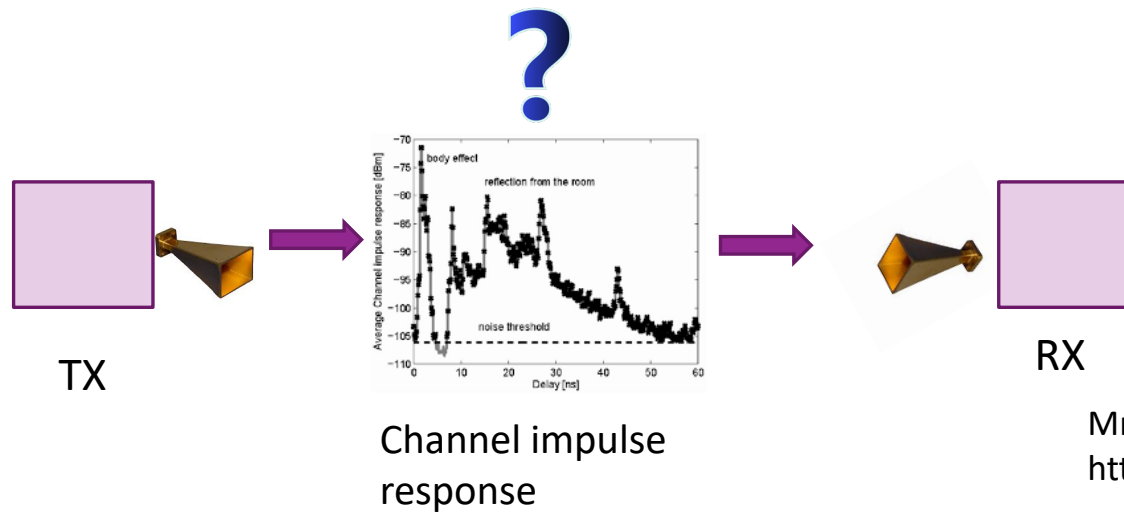
- ❑ Receiver filtering and sampling
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- ❑ General channels: Time-domain analysis
- ❑ General channels: Frequency-domain analysis
- ❑ PSD Analysis
- ❑ Practical RX filter design
-  Channel sounding

# Channel Sounder

□ Measure channel

□ Useful for:

- Wireless propagation analysis
- Measure multipath components, signal strengths, directions of arrival
- But, also good for debugging any front-end



MmWave and sub-THz channel sounder by Rappaport lab  
<https://wireless.engineering.nyu.edu/mmwave-5g-and-6g-channel-sounder/>

# FFT-Based Channel Sounding

- ❑ Effective discrete-time channel:  $r[n] = h[n] * s[n]$
- ❑ Select period  $N$
- ❑ Repeatedly transmit  $s[n] = \sum_{k=0}^{N-1} S_k e^{2\pi i k n / N} = \text{FFT}(S_k)$
- ❑ Receiver will get:  $r[n] = \sum_{k=0}^{N-1} R_k e^{2\pi i k n / N}$ ,  $R_k = S_k H\left(\frac{2\pi k}{N}\right)$
- ❑ Recover  $R_k = \text{IFFT}(r[n])$
- ❑ Get channel response:  $H\left(\frac{2\pi k}{N}\right) = \frac{R_k}{S_k} = H_{chan}\left(\frac{k}{NT}\right) P_{tx}\left(\frac{k}{NT}\right) P_{rx}\left(\frac{k}{NT}\right)$
- ❑ Learn  $P_{tx}\left(\frac{k}{NT}\right), P_{rx}\left(\frac{k}{NT}\right)$  from calibration
- ❑ Estimate  $H_{chan}\left(\frac{k}{NT}\right)$
- ❑ Provides a discrete estimate of the channel.
- ❑ More in the lab