CODE OF PRACTICE

FOR

OVERALL THERMAL TRANSFER VALUE

IN BUILDINGS

1995

BUILDING AUTHORITY HONG KONG

April 1995

Foreword

A consultancy study in 1991 found that if the envelope of a building was constructed to a suitable overall thermal transfer value (OTTV), electricity demand from air-conditioning and thus the emission of greenhouse gases from power generation could be reduced. The Government's aim is to establish a comprehensive building energy code to control the total energy consumption of a building, of which OTTV controls would form a part. As a first step, legislative control over OTTV has been introduced in the Building (Energy Efficiency) Regulation (Cap. 123 sub. leg.).

This Code of Practice provides technical guidance for authorized persons, registered structural engineers and other persons responsible for the design and construction of buildings. Compliance with the provisions in this Code may be deemed to satisfy the requirement of a suitable OTTV for a building under the Building (Energy Efficiency) Regulation.

This Code will be regularly reviewed. The Building Authority welcomes suggestions for improving this Code or for enhancing the energy efficiency of buildings in general.

Other options for achieving equivalent and better performance standards are available and will of course be considered in isolation or in combination for the purpose of establishing acceptability.

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1. General Principles of Control of Overall Thermal Transfer Value

1.1 For the design and planning of energy - efficient buildings, Government is developing a comprehensive energy code to cover inter alia lighting and air-conditioning. Overall thermal transfer value (OTTV) is one aspect of energy conservation.

General approach

- 1.2 An OTTV is a measure of the energy consumption of a building envelope. Its formulation allows authorized persons, registered structural engineers and other persons responsible for the design and construction of buildings freedom to innovate and vary important envelope components such as type of glazing, window size, external shading to windows, wall colour and wall type to meet the maximum OTTV criteria. Any measure to improve energy efficiency or to save energy should be considered in planning a building.
- 1.3 Siting a building to avoid extensive glazed facades with a southerly aspect or introducing shades to window areas can reduce solar heat gain. Appropriate choice of windows with a low thermal transmittance characteristic will also minimize solar heat transmission.
- 1.4 Artificial lighting consumes electricity and creates heat. This increases the cooling load of a building and in turn increases energy consumption. Consequently, when determining the size and location of windows as well as choice of glass in the envelope of a building, efforts should be made to provide as much natural lighting into the building as possible. For example, with glazing, the visible lighting transmittance should be acknowledged in addition to its thermal transmittance properties; daylight can supplement artificial lighting and consequently reduce the cooling load.
- 1.5 Other measures include more extensive use of energy-efficient building services equipment and appliances, e.g. energy-saving lamps, low-loss luminaries and high-efficiency air-conditioning and more sophisticated building services control systems.

Scope

- 1.6 The provisions in this Code apply to all hotels and commercial buildings as defined in the Building (Energy Efficiency) Regulation. They aim at reducing heat transfer through the building envelope and thus the electricity required for airconditioning.
- 1.7 The concept of OTTV is based on the assumption that the envelope of a building is completely enclosed.
- 1.8 In the OTTV formulation, the following factors are not addressed or allowed for :
- (a) Internal shading devices, such as draperies and blinds.
- (b) Solar reflection or shading from adjacent buildings.

2. **Definitions**

In this Code, unless otherwise stated, words and expressions have the meaning attributed to them by the Building (Energy Efficiency) Regulation. It should also be noted that:

"building tower" means that part of a building above the podium of the building;

"fenestration" means any glazed aperture in the building envelope;

"lightwell" means a vertical shaft of open air enclosed on all sides by parts of a building;

"opaque" wall or roof means that solid part of the wall or roof which is not part of the fenestration;

"podium" means that part of a building which,

- (a) if having a site coverage exceeding the permitted percentage site coverage,is -
 - (i) within 15 m above ground level as permitted under Building (Planning) Regulation 20(3); or
 - (ii) within such height as is permitted by the Building Authority by way of a modification of that regulation granted under section 42 of the Buildings Ordinance; and
- (b) if having a site coverage within the permitted percentage site coverage, is within 15 m above ground level.
- "refuge floor" has the meaning assigned to it in the Code of Practice for Means of Escape and means a protected floor that serves as a refuge for the occupants of the building to assemble in case of fire.

3. **Suitable OTTV**

- 3.1 The external walls and roofs of a building to which the Building (Energy Efficiency) Regulation applies should be designed and constructed to have the following OTTV:
- (a) in the case of a building tower; the OTTV should not exceed 35 W/m²; and
- (b) in the case of a podium; the OTTV should not exceed 80 W/m².
- 3.2 The maximum OTTV specified in paragraph 3.1 should apply to the overall building envelope, i.e. all the external walls and roofs, as the case may be, in average and do not apply to the individual wall or roof.

3.3 The OTTV of the external walls and roofs of a building tower or podium should be assessed in accordance with methods set out in this Code. A sample of OTTV calculations for a typical commercial building is set out in Appendix for illustration.

4. **Principles of OTTV Calculations**

External walls and roofs not included in OTTV calculations

- 4.1 All external walls and roofs of a building should be included in OTTV calculations except -
- (a) an external wall of a refuge floor;
- (b) an external wall or roof of a carparking floor;
- (c) an external wall of a lightwell having an area on plan not exceeding 21 m²; and
- (d) any wall on any roof.

Party wall

4.2 An external wall of a building which is a party wall should be included in OTTV calculations whether an adjoining building exists or not. Shading to the party wall from adjoining buildings should not be considered in calculating the OTTV.

5. OTTV of External Walls

The OTTV of the external walls of a building tower or a podium, $OTTV_{W_1}$ should be calculated using the following formula -

$$OTTV_{W} = \frac{(A_{W} \times U \times \alpha \times TD_{EQW}) + (Af_{W} \times SC \times ESM \times SF)}{Ao_{W}}$$

where

 A_w = Area of opaque wall, m^2

U = Thermal transmittance of opaque wall, W/m^2 °C (See para 7.1)

 α = Absorptivity of the opaque wall (Table 4)

TD_{EOw} = Equivalent temperature difference for wall, °C (Table 5)

 Af_{W} = Area of fenestration in wall, m^2

SC = Shading coefficient of fenestration in wall (See para 7.5)

ESM = External shading multiplier (Table 6 and 7)

SF = Solar factor for the vertical surface, W/m² (Table 8)

 Ao_W = Gross area of external walls, i.e. $A_W + Af_W$, m^2

6. **OTTV of Roofs**

The OTTV of the roofs of a building tower or a podium, $OTTV_{r,}$ should be calculated using the following formula:-

$$OTTV_r = \frac{(A_r \times U \times \alpha \times TD_{EQr}) + (Af_r \times SC \times SF)}{Ao_r}$$

Where

 A_r = Area of opaque roof, m^2

U = Thermal transmittance of opaque roof, W/m^2 °C (See para 7.1)

 α = Absorptivity of the opaque roof (Table 4)

 TD_{EQr} = Equivalent temperature difference for roof, °C (Table 9)

 Af_r = Area of fenestration in roof, m^2

SC = Shading coefficient of fenestration in roof (See para 7.5)

SF = Solar factor for horizontal surface, W/m² (Table 8)

 Ao_r = Gross area of roof, i.e. $Ar + Af_r$, m^2

7. Calculation of Component Coefficients and Parameters of OTTV

Thermal transmittance of opaque construction (U)

7.1 Opaque walls and roofs usually involve a composite of materials. The thermal transmittance of an opaque wall or roof should be derived by the following formula:

$$U = \frac{1}{R_{i} + \frac{x_{1}}{k_{1}} + \frac{x_{2}}{k_{2}} + \dots + \frac{x_{n}}{k_{n}} + R_{a} + R_{o}}$$

x = Thickness of building material of the wall or roof or part thereof, m

k = Thermal conductivity of the building material, W/m°C (Table 1)

 R_i = Surface film resistance of internal surface of the wall or roof, m^2 °C/W (Table 2)

 R_O = Surface film resistance of external surface of the wall or roof, m^2 °C/W (Table 2)

 R_a = Air space resistance, m^2 °C/W (Table 3)

Component coefficients and parameters of thermal transmittance

- 7.2 The component coefficients and parameters used in calculating the thermal transmittance of opaque construction should be assessed as follows:
- (a) Thermal conductivity of building materials (k)

The thermal conductivity of the building materials of walls and roofs should be obtained from Table 1.

- 7 -

Table 1 Thermal Conductivity of Building Materials

Material	Density kg/m ³	Thermal Conductivity (k) W/m°C
Asphalt, mastic with 20% grit	2350	1.15
Boards a) cork b) hardboard high density c) mineral fibre d) plasterboard	145 1010 265 950	0.042 0.144 0.053 0.16
Brick (common)	1900	0.95
Concrete a) normal weight aggregate b) lightweight aggregate c) flat roof tiles or slabs	2400 1300 2100	2.16 0.44 1.10
Glass	2500	1.05
Mosaic tile cladding	2500	1.50
Insulating materials a) glass fibre mat or quilt b) mineral wool felt c) polystyrene expanded d) polyurethane foam	32 50 25 30	0.035 0.039 0.034 0.026
Metals a) aluminium alloy typical b) copper commercial c) steel, carbon	2800 8900 7800	160 200 50
Plaster/render a) gypsum b) gypsum, sand aggregate c) cement/sand	1120 1570 1860	0.38 0.53 0.72
Screeding a) cement sand b) terrazzo	1860 2435	0.72 1.59
Stone a) granite b) marble	2650 2500	2.9 2.0

Note:

If other materials are used the thermal conductivity values should be subject to the acceptance of the Building Authority and the source of the information from which the thermal conductivity values are obtained should be submitted for his consideration for this purpose.

(b) Surface film resistance for walls and roofs (R_i , R_o)

The surface film resistance for walls and roofs should be obtained from Table 2.

Table 2 Surface Film Resistance for Walls and Roofs

Type of surface	Surface film resistance m ² °C/W
Surface film resistance for walls	
1. Internal surface (R _i)	
(a) Absorptivity (0.5 and above)(b) Absorptivity (below 0.5)	0.120 0.299
2. External surface (R ₀)	0.044
Surface film resistance for roofs	-
1. Internal surface (R _i)	
(a) Absorptivity (0.5 and above) (i) Flat roof (ii) Sloped roof 22½° (iii) Sloped roof 45°	0.162 0.148 0.133
 (b) Absorptivity (below 0.5) (i) Flat roof (ii) Sloped roof 22½° (iii) Sloped roof 45° 2. External surface (R ₀)	0.801 0.595 0.391 0.055

(c) Air space resistance for walls and roofs (R_a)

The air space resistance for walls and roofs should be obtained from Table 3.

Table 3 Air Space Resistance for Walls and Roofs

		Air space resistance (Ra) m ² °C/W						
Type of air space	5 mm	10 mm	20 mm	50 mm	75 mm	100 mm		
Air space resistance for walls								
Vertical air space (heat flows horizontally)								
(a) Absorptivity (0.5 and above)	0.110	0.123	0.148	0.153	0.156	0.160		
(b) Absorptivity (below 0.5)	0.250	0.359	0.578	0.589	0.597	0.606		
Air space resistance for roofs								
Horizontal or sloping air space (heat flows downward)								
(a) Absorptivity (0.5 and above)								
(i) horizontal air space (ii) sloped air space 22½° (iii) sloped air space 45°	0.110 0.110 0.110	0.123 0.123 0.123	0.148 0.148 0.148	0.158 0.154 0.152	0.166 0.160 0.155	0.174 0.165 0.158		
(b) Absorptivity (below 0.5)								
(i) horizontal air space (ii) sloped air space 22½° (iii) sloped air space 45°	0.250 0.250 0.250	0.357 0.357 0.357	0.572 0.571 0.570	0.891 0.768 0.644	1.157 0.931 0.706	1.423 1.095 0.768		

Absorptivity (α)

7.3 Energy simulation studies for Hong Kong have shown that the external surface and colour of walls and roofs, and therefore their absorptivity, have a significant effect on chiller energy used. This should be included in the heat gain calculation as a multiplication constant to the equivalent temperature difference. The absorptivity for wall and roof surfaces should be obtained from Table 4.

Table 4 Absorptivity for wall and roof surfaces

Material	Absorptivity α	Paint	Absorptivity α
Black glass	1.0	Optical flat black paint	0.98
Black concrete	0.91	Flat black paint	0.95
Stafford blue brick	0.89	Black lacquer	0.92
Red brick	0.88	Dark grey paint	0.91
Bituminous felt	0.88	Dark blue lacquer	0.91
Blue grey slate	0.87	Black oil paint	0.90
Roofing, green	0.86	Dark olive drab paint	0.89
Brown concrete	0.85	Azure blue or dark green lacquer	0.88
Asphalt pavement, weathered	0.82	Dark brown paint	0.88
Wood, smooth	0.78	Dark blue-grey paint	0.88
Uncoloured concrete	0.65	Medium brown paint	0.84
White marble	0.58	Medium light brown paint	0.80
White mosaic tiles	0.58	Brown or green lacquer	0.79
Light buff brick	0.55	Medium rust paint	0.78
Built-up roof, white	0.50	Light grey oil paint	0.75
Bituminous felt, aluminized	0.40	Red oil paint	0.74
Gravel	0.29	Medium dull green paint	0.59
White on galvanized iron	0.26	Medium orange paint	0.58
White glazed brick	0.25	Medium yellow paint	0.57
Polished aluminium reflector sheet	0.12	Medium blue paint	0.51
Aluminized mylar film	0.10	Medium kelly green paint	0.51
Tinned surface	0.05	Light green paint	0.47
		Aluminium paint	0.40
		White semi-gloss paint	0.30
		White gloss paint	0.25
		Silver paint	0.25
		White lacquer	0.21
		Laboratory vapour deposited coatings	0.02

Note:

Absorptivity for other materials or surfaces should be subject to the acceptance of the Building Authority and the source of the information from which the absorptivity values are obtained should be submitted for his consideration.

Equivalent temperature difference for walls (TDEOw)

7.4 Energy simulation studies for Hong Kong have indicated that thermal mass affects the total heat flow through walls sufficiently to warrant its inclusion in the formulation of an OTTV. The equivalent temperature difference for walls should take into account the wall mass, density and orientation. Heavyweight construction gives a better performance than lightweight construction because it resists the passage of heat. The equivalent temperature difference for walls should be obtained from Table 5.

 Table 5
 Equivalent Temperature Difference for Walls

		Density of wall construction								
Orientation	less than 22 kg/m ²	23-199 kg/m²	200-379 kg/m²	380-569 kg/m²	570 kg/m ² or greater					
N	3.70	3.38	2.72	2.05	1.70					
NNE	4.65	4.21	3.30	2.36	1.88					
NE	5.60	5.03	3.86	2.67	2.05					
ENE	6.55	5.86	4.44	2.98	2.23					
Е	7.50	6.68	5.01	3.28	2.40					
ESE	7.05	6.26	4.65	3.00	2.15					
SE	6.60	5.85	4.30	2.71	1.90					
SSE	6.15	5.43	3.95	2.43	1.65					
S	5.70	5.01	3.60	2.15	1.40					
SSW	6.15	5.42	3.92	2.37	1.58					
SW	6.60	5.82	4.23	2.59	1.75					
WSW	6.55	5.81	4.29	2.73	1.93					
W	6.50	5.79	4.35	2.86	2.10					
WNW	5.80	5.19	3.94	2.66	2.00					
NW	5.10	4.59	3.54	2.45	1.90					
NNW	4.40	3.98	3.13	2.25	1.80					

Shading coefficient of fenestration (SC)

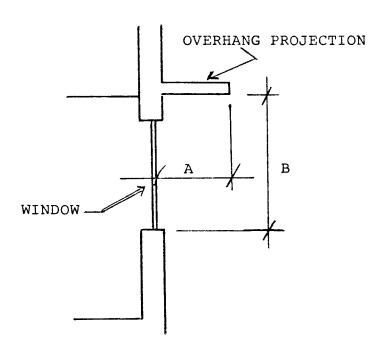
7.5 The shading coefficient of fenestration is the ratio of the solar heat gain through a particular type of glass under a specific set of conditions to the solar heat gain through double strength sheet clear glass under the same conditions. Allowances for Hong Kong's latitude and solar effects have been taken into account in the solar factor and therefore the shading coefficient of glass published by glass manufacturers in Hong Kong or overseas can be used without modification provided that the calculations have been based on a normal angle of incidence.

External shading multiplier (ESM)

7.6 Shading of windows is of paramount importance in reducing solar heat gain to the building. This shading can be provided by projections over the window, at the side of the window, or a combination of both. For the purpose of simplicity in OTTV calculations this shading effect is taken into account as an external shading multiplier which should be assessed as follows:

(a) Overhang projections to windows

The external shading multiplier for overhang projections to windows should be obtained from Table 6 according to the overhang projection factor (OPF) and the orientation of the window. The OPF should be calculated as follows:



$$OPF = \frac{A}{B}$$

Table 6 External Shading Multiplier for Overhang Projections to Windows

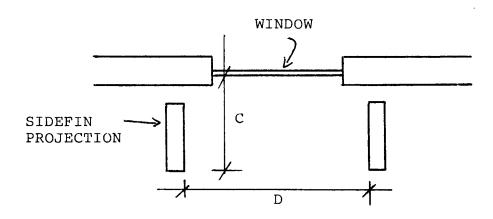
		E:	SM	
OPF	N	NE/NW	S/E/W	SE/SW
0.00	1.000	1.000	1.000	1.000
0.05	0.975	0.969	0.962	0.962
0.10	0.951	0.939	0.926	0.926
0.15	0.928	0.909	0.890	0.890
0.20	0.905	0.880	0.856	0.856
0.25	0.883	0.853	0.823	0.823
0.30	0.861	0.826	0.790	0.790
0.35	0.840	0.800	0.759	0.759
0.40	0.820	0.774	0.729	0.729
0.45	0.800	0.750	0.700	0.700
0.50	0.781	0.726	0.672	0.672
0.55	0.762	0.704	0.645	0.645
C.60	0.744	0.682	0.620	0.620
0.65	0.726	0.661	0.595	0.595
0.70	0.710	0.641	0.572	0.572
0.75	0.693	0.621	0.549	0.549
0:80	0.678	0.603	0.528	0.528
0.85	0.663	0.585	0.507	0.507
0.90	0.648	0.568	0.488	0.488
0.95	0.634	0.552	0.470	0.470
1.00	0.621	0.537	0.453	0.453

Notes:

- (i) Should the OPF value fall in between increments, adopt the multiplier related to the next larger OPF value.
- (ii) OPF values above 1.0 are considered to produce too great an error in estimation.
- (iii) ESM for South, East and West orientations are combined since the figures are very similar.

(b) Sidefin projections to windows

The external shading multiplier for sidefin projections to windows should be obtained from Table 7 according to the sidefin projection factor (SPF) and the orientation of the window. The SPF should be calculated as follows:



$$SPF = \frac{C}{D}$$

Table 7 External Shading Multiplier for Sidefin Projections to Windows

	ESM									
SPF	N	NE	Е	SE	S	SW	w	NW		
0.00	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000		
0.05	0.955	0.964	0.974	0.968	0.962	0.968	0.968	0.964		
0.10	0.911	0.929	0.948	0.937	0.925	0.936	0.947	0.929		
0.15	0.869	0.896	0.923	0.906	0.890	0.906	0.922	0.895		
0.20	0.828	0.863	0.898	0.877	0.855	0.876	0.897	0.863		
0.25	0.789	0.832	0.875	0.848	0.822	0.848	0.873	0.831		
0.30	0.751	0.801	0.852	0.821	0.790	0.820	0.850	0.800		
0.35	0.714	0.772	0.829	0.794	0.759	0.793	0.828	0.771		

(Cont'd)

Table 7 External Shading Multiplier for Sidefin Projections to Windows (Cont'd)

				E.	SM			
SPF	N	NE	Е	SE	S	SW	W	NW
0.40	0.679	0.743	0.807	0.768	0.729	0.767	0.806	0.742
0.45	0.645	0.716	0.786	0.743	0.700	0.743	0.785	0.715
0.50	0.613	0.690	0.766	0.719	0.673	0.719	0.765	0.689
0.55	0.582	0.664	0.746	0.696	0.646	0.696	0.746	0.664
0.60	0.553	0.640	0.727	0.674	0.621	0.674	0.727	0.640
0.65	0.525	0.617	0.709	0.653	0.596	0.653	0.709	0.617
0.70	0.499	0.595	0.691	0.632	0.573	0.633	0.692	0.595
0.75	0.473	0.574	0.674	0.613	0.551	0.613	0.675	0.574
0.80	0.450	0.554	0.658	0.594	0.531	0.595	0.660	0.555
0.85	0.428	0.535	0.642	0.577	0.511	0.578	0.645	0.536
0.90	0.407	0.517	0.627	0.560	0.493	0.561	0.630	0.519
0.95	0.388	0.500	0.613	0.544	0.475	0.546	0.617	0.502
1.00	0.370	0.484	0.599	0.529	0.459	0.531	0.604	0.487
1.05	0.354	0.470	0.586	0.515	0.444	0.518	0.592	0.473
1.10	0.339	0.456	0.574	0.502	0.430	0.505	0.581	0.460
1.15	0.325	0.444	0.562	0.490	0.417	0.494	0.570	0.448
1.20	0.313	0.432	0.551	0.478	0.406	0.483	0.560	0.437
1.25	0.302	0.422	0.541	0.468	0.395	0.473	0.551	0.427
1.30	0.293	0.412	0.531	0.458	0.386	0.464	0.543	0.418
1.35	0.286	0.404	0.522	0.450	0.377	0.456	0.535	0.410
1.40	0.279	0.396	0.514	0.442	0.370	0.449	0.528	0.404
1.45	0.274	0.390	0.506	0.435	0.364	0.443	0.522	0.398
1.50	0.271	0.385	0.499	0.429	0.359	0.438	0.517	0.394

Notes:

- (i) SPF values above 1.5 are considered to produce too great an error in estimation.
- (ii) Should the SPF value fall in between increments, adopt the multiplier related to the next larger SPF value.

(c) Combination of overhang and sidefin projections

For windows with both overhang and sidefin projections each external shading multiplier should be calculated separately as described in (a) and (b) and the smaller of the two values obtained should be used as the external shading multiplier in the OTTV calculations.

Solar factor (SF)

7.7 The solar factor for vertical surfaces at various orientations and that for horizontal surfaces should be obtained from Table 8. The solar factors have been calculated for the Hong Kong climate. Any sloping or angled wall or roof can be resolved into vertical and horizontal components. The vertical components of the sloping or angled wall or roof can be treated as a vertical surface with a solar factor at that respective orientation; whereas the horizontal component can be treated as a horizontal surface.

Table 8 Solar Factor

orientation	N	NE	Е	SE	S	SW	W	NW
SF for vertical surface	104	138	168	197	191	202	175	138
orientation	NNE	ENE	ESE	SSE	SSW	wsw	WNW	NNW
SF for vertical surface	121	153	183	194	197	189	157	121
SF for horizontal surface	264							

Equivalent temperature difference for roofs (TD_{EQr})

7.8 The equivalent temperature difference for roofs should take into account the roof mass and density and should be obtained from Table 9.

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Table 9 Equivalent Temperature Difference for Roofs

Density of roof construction	less than 22 kg/m ²	23-199 kg/m²	200-379 kg/m²	380-569 kg/m²	570 kg/m ² or above
TD _{EQr}	18.60	16.88	13.37	9.75	7.90

8. Windows and doors

Buildings should not have unenclosed doorways and entrances. For commercial buildings where heavy traffic of people is anticipated, self-closing doors without restrainers, revolving doors or other similar means of minimizing heat gain should be employed. Careful attention should also be paid to the sealing of windows to guard against leakage during service.

9. Submission of Information

- 9.1 Information and calculations required by the Building Authority are specified in the Building (Energy Efficiency) Regulation. Simplified version of OTTV calculations can be included in the first submission of building plans, provided that detailed calculations have to be submitted before consent to commence works will be granted. The following information and calculations should be submitted on the standard forms set out in the schedule to this Code:
- (a) Calculation of 'U' value of composite wall and roof and details of other component coefficients and parameters of OTTV on Form OTTV 1.
- (b) Window and rooflight schedule on Form OTTV 2.
- (c) OTTV calculations on Form OTTV 3 and Form OTTV 4.
- 9.2 OTTV calculations should be made to two places of decimals.

Schedule of Standard Forms

Form OTTV 1

Form OTTV 2

Form OTTV 3

Form OTTV 4

Building (Energy Efficiency) Regulation Form OTTV 1

Calculation of 'U' Value of Composite Wall/Roof and Details of Other Values

Sheet No. A		BD Re	t 2/_	/_	/_	
Building address						
Physical data of Opaque *Wall/Roof						
Facade Orientation facing	Solar 1	Factor	(SF)	is _		

*Wall/Roof Code No.	T *W /D	*W /D	±₩ /D	*¼ /D
Location of Wall/Roof	*W ₁ /R ₁	*W2/R2	*W ₃ /R ₃	*W ₄ /R ₄
External Finish Material				
	<u> </u>			
Conductivity W/m°C				
Density kg/m ³				
Thickness m				
Absorptivity (a)				
Intermediate component	ļ			
Conductivity W/m°C				
Density kg/m ³				
Thickness m				
Intermediate component			24444-4-724-124-4-144-144-144-144-144-144-144-144	
Conductivity W/m°C				
Density kg/m ³				
Thickness m				
Intermediate component				
Conductivity W/m°C				
Density kg/m ³				
Thickness m				
Intermediate component				
Conductivity W/m°C				
Density kg/m ³				
Thickness m				
Internal Finish Material				
Conductivity W/m°C				
Density kg/m ³				
Thickness m				
Absorptivity a				
`U' value of composite *Wall/Roof				
Area of *Wall/Roof m ²				
Density of composite *Wall/Roof kg/m ²				
Equivalent temperature difference (TD_{EQ})				

Building (Energy Efficiency) Regulation Form OTTV 2

Window/Rooflight Schedule

eet No. B BD Ref 2//_			2//		
Building address					
Physical data on *window/rooFacade Orientation facing _		Solar Factor (SF) is _			
Window/Rooflight Code No.	*F ₁ /RL ₁	*F ₂ /RL ₂	*F ₃ /RL ₃	*F ₄ /RL ₄	
Location of *Window/ Rooflight					
Glazing type					
Thickness m					
Shading Coefficient (SC)					
Type of shading device					
External Shading Multiplier (ESM)					
Area of glazing m ²					
Physical data on *window/ro Facade Orientation facing _ Window/Rooflight Code No.		*F ₂ /RL ₂	Solar Fact	or is *F ₄ /RL ₄	
Location of *Window/ Rooflight					
Glazing type					
Thickness m					
Shading Coefficient (SC)					
Type of shading device					
External Shading Multiplier (ESM)					
Area of glazing m ²					

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^{*} Delete as appropriate

Building (Energy Efficiency) Regulation Form OTTV 3

Calculation of OTTV of Individual Facade in Building Envelope

	С				BD Ref 2/_		
uilding a	address						
acade Or	ientation facing		•				
		<u>Opaque</u>	*Walls/Ro	ofs			
Code No.	Description	*A _w /A _r	Ų	α	TD _{EQ}	Sum	
_	Subtotals		(A)	H e	eat Gain		((
Code	Description	*Af _w /Af _r	estration SC	ESM	SF	Sum	7
No.		wr					_
	Subtotals		(B)	Не	eat Gain		(
ross Hea	t Gain (C + D)						
	a (A + B)						
	: + D	พ	/m²				
	+ B		,				

* Delete as appropriate

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Building (Energy Efficiency) Regulation Form OTTV 4

Summary of OTTV of Building Envelope

Sheet No. D	BD Ref. 2//			
Building address				
Total Envelope Heat Gain	(* Tower/Podium)			
Facade Orientation	Gross Area from Form OTTV 3	Gross Heat Gain from Form OTTV3		
a. b. c. d.				
f.				
Subtota1	(E)	(G)		
Roof				
a. b.				
Subtota1	(F)	(н)		
* Tower/Podium Walls OTTV =	=			
* Tower/Podium Roofs OTTV =	= H F = W/n	12		

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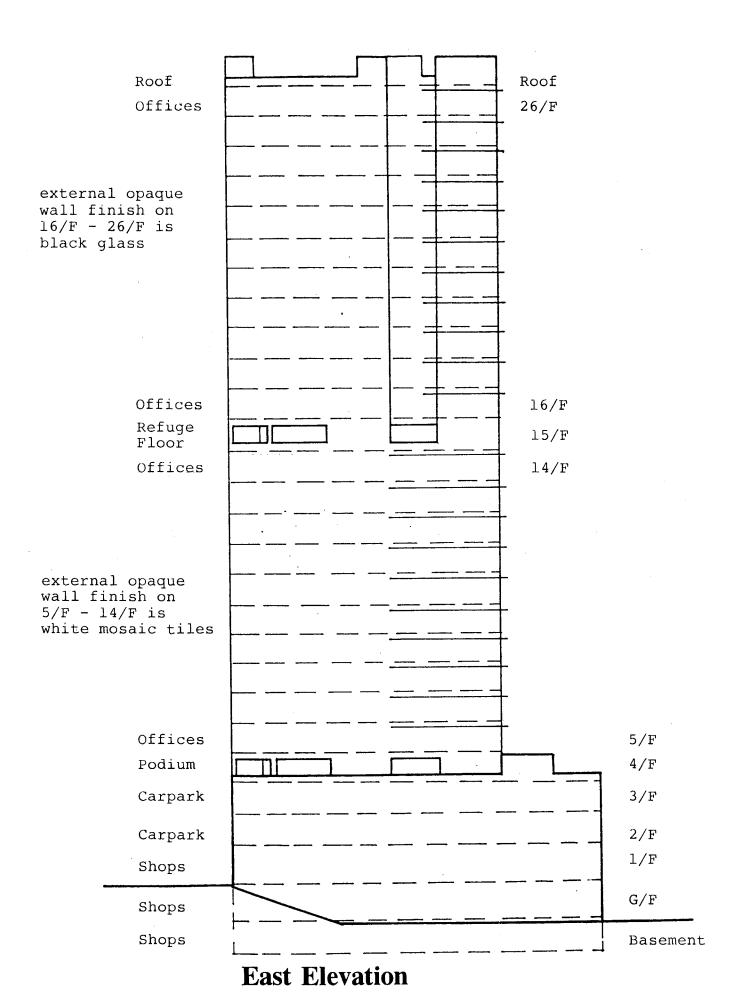
* Tower/Podium OTTV

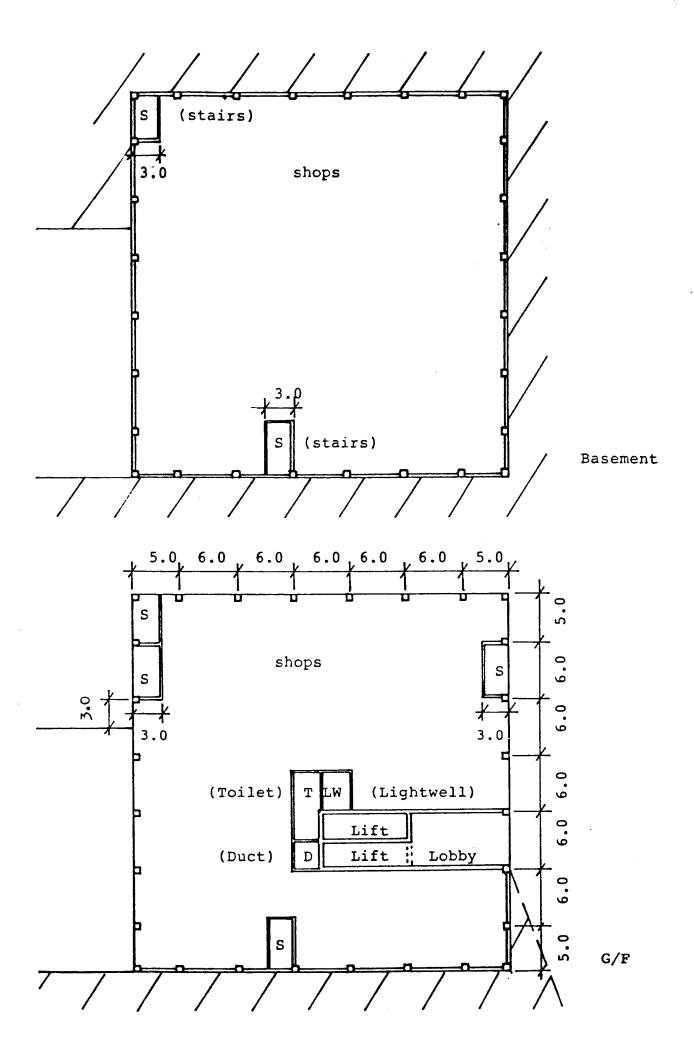
^{*} Delete as appropriate

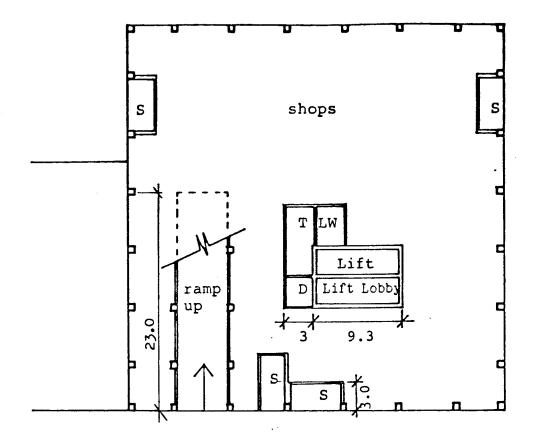
Appendix A

A sample of OTTV calculation for a typical commercial building

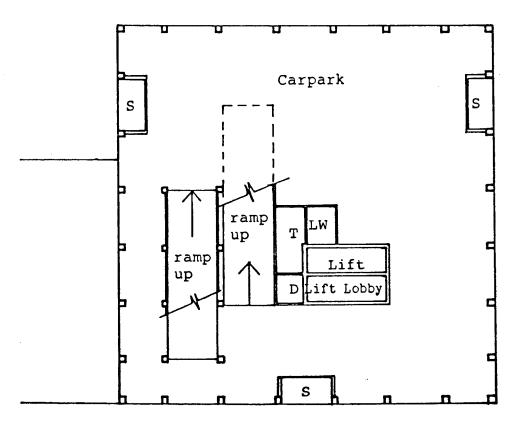
Plans and Elevation of a Typical Commercial Building



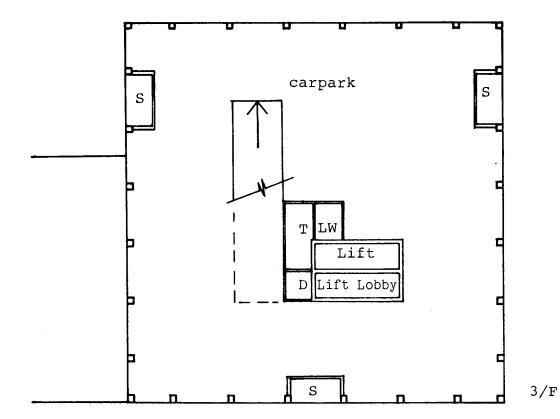


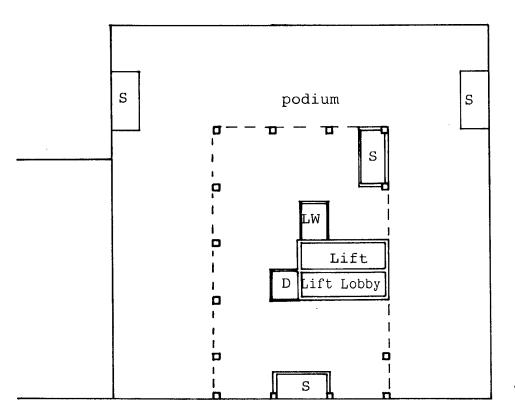




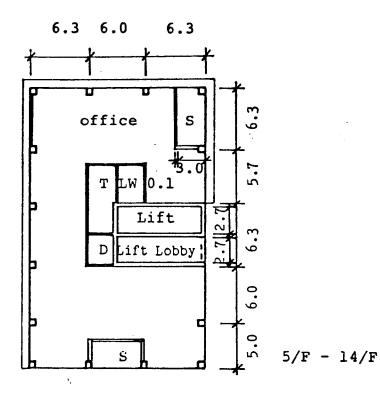


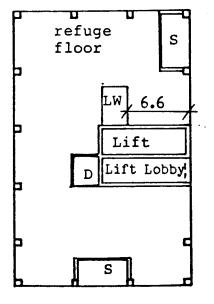
2/F



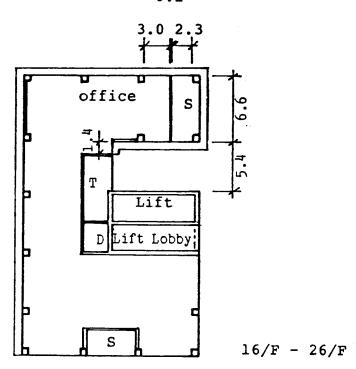


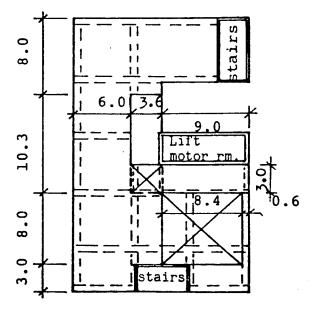
4/F





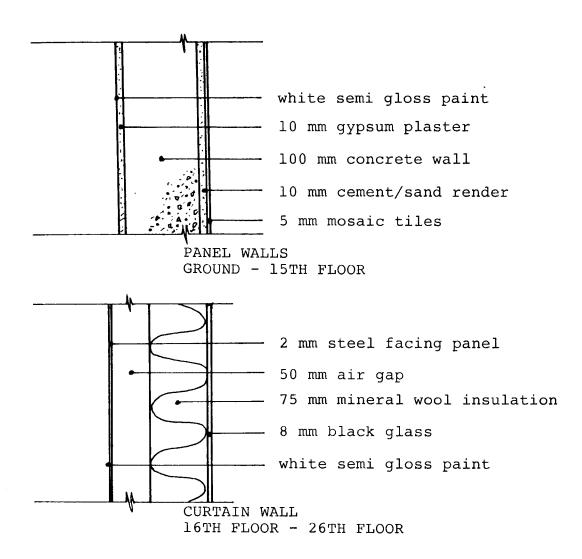
15/F

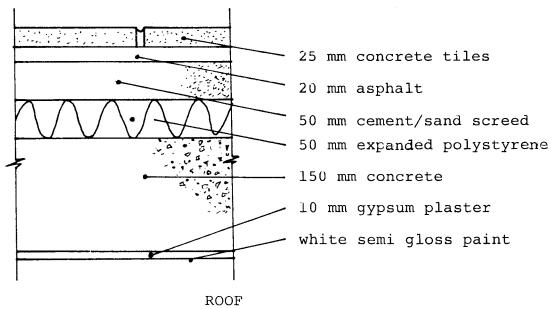


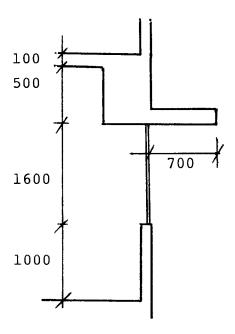


Roof

Construction of Walls and Roof







TYPICAL SECTION
5TH FLOOR - 26TH FLOOR

Gross Wall Calculations

Storey heights:

Ground and First Floors 4.0 m 2nd & 3rd floors 3.5 m 4th to 26th floors 3.2 m

All columns 600 x 600 mm

All beams 600 x 600 mm

East Elevation

P G/F $11.0 \times 4.0 \div 2 + 29 \times 4.0$ 138.00 m² = 1/F $40 \times 4.0 + 23 \times 4 \times 0.5$ 206.00 m² 344.00 m² 23.0 x 3.2 x 10 T 5/F-14/F $736.00 \, m^2$ = 16/F-26/F 23.0 x 3.2 x 11 809.60 m² $1,545.60 \text{ m}^2$ 5/F-14/F $6.3 \times 3.2 \times 10$ = 201.60 m² 16-26/F 6.3 x 3.2 x 11 =: 221.76 m² 423.36 m²North Elevation

P G/F 40.0×4.0 160.00 m² 1/F 40.0 x 4.0 160.00 m² 320.00 m² T 5-14/F 18.6 x 3.2 x 10 595.20 m² 16-26/F $(18.6 + 9) \times 3.2 \times 11$ 971.52 m² $1,566.72 \text{ m}^2$

West Elevation

P G/F 40 x 4.0 160.00 m² 1/F $40 \times 4.0 + 23 \times 4 \times 0.5$ $206.00 \, m^2$ 366.00 m² 29.3 x 3.2 x 10 T 5/F-14/F 937.60 m² 16/F-26/F 29.3 x 3.2 x 11 $1,031.36 \text{ m}^2$ $1,968.96 \text{ m}^2$

South Elevation

P G/F Ni1 = 1/F 40 x 4.0 + (5.4x23.35-5.4x4.0) = 264.49 m^2 264.49 m^2

T 5/F-14/F 18.6 x 3.2 x 10 = 595.20 m² 16/F-26/F (18.6 + 9) x 3.2 x 11 = 971.52 m² 1,566.72 m²

Window Schedule

Building Address

Typical Commercial Building

Orientation of Facade	Floor	Class Thickness m	Туре	Sizes and no./floor	Total area per floor m ²
East	G/F	0.012	plain	(5.4 x 4 + 4.1) 3.4	87.38
	1/F	0.012	plain	(4.1x2 + 5.4x5) 3.4	119.68
	2-4/F	Nil	Nil		
	5-14/F	0.008	tinted	(4.1+5.7+5.4x2) 1.6	32.96
	5-14/F	0.008	tinted	2.7 x 1.6	4.32
	15/F	Nil	tinted	_	
	16-26/F	0.008	tinted	(4.1+5.7+1.4+5.4) 1.6 +3.9x0.8	29.68
	16-26/F	0.008	tinted	2.7 x 1.6	4.32
North	G/F	0.012	plain	(4.1+5.4x5+1.7+2.3) 3.4	119.34
	1/F	0.012	plain	(4.1x2+5.4x5) 3.4	119.68
	2-4/F	Nil	Nil	-	-
	5-14/F	0.008	tinted	(2.3+3.0+5.4x2) 1.6	25.76
	15/F	Nil	Nil	-	-
	16-26/F	0.008	tinted	(2.3+3.0+5.4x2) 1.6	25.76
West	G/F	0.012	plain	(4.1+5.4+2.7) 3.4	41.48
	1/F	0.012	plain	(4.1+5.4+2.7) 3.4	41.48
	2-4/F	Nil	Nil	-	-
	5-14/F	0.008	tinted	(5.4x3+4.1) 1.6	32.48
	15/F	Nil	Nil	-	-
	16-26/F	0.008	tinted	(5.4x3+4.1) 1.6	32.48
South	G/F	Nil	Nil	-	-
	1/F	0.012	plain	(4.1x2+2.7+2.6+5.4x3) 3.4	100.98
	2-4/F	Nil	Nil	-	_
	5-14/F	0.008	tinted	(5.4x3) 1.6	25.92
	15/F	Nil	Nil	-	-
	16-26/F	0.006	reflect- ive	(5.4x3) 1.6	25.92
	16-26/F	0.008	tinted	(3.0 + 2.3) 1.6	8.48

```
East Elevation (Tower) Gross Wall Area 1,545.60 + 423.36 =
                                                                               1,968.96 \text{ m}^2
Wall composite areas
Beams and Column Areas
5/F - 14/F
                  [0.6 (11.0+5.7+6.3)+(0.6x2.6x4)] 10 = 200.40 m<sup>2</sup>
15/F
                       Nil
16/F - 26/F
                  [0.6 (11.0+5.4+6.6)+(0.6x2.6x4)] 11
                                                                = 220.44 \text{ m}^2
                                                                                  420.84 m<sup>2</sup>
Glazing Areas in 100 mm panel/curtain wall from Window Schedule
5/F - 14/F
                  32.96 x 10
                                                                    329.60 \, m^2
15/F
                       Nil
16/F - 26/F
                  29.68 x 11
                                                                    326.48 \, m^2
                                                                                 656.08 m<sup>2</sup>
Glazing Area in 300 mm Structural Walls from Window Schedule
5/F - 14/F
                  4.32 \times 10
                                                                    43.20 \ m^2
15/F
                  4.32 x 11
                                                               =
                                                                    47.52 m<sup>2</sup>
                                                                                   90.72 \text{ m}^2
100 mm Panel/Curtain Wall Areas
5/F - 14/F
                  736.00 - (200.40 + 329.60)
                                                                    206.00 m<sup>2</sup>
15/F
                       Nil
16/F - 26/F
                  809.60 - (220.44 + 326.48)
                                                                    262.68 m<sup>2</sup>
                                                                                 468.68 m<sup>2</sup>
300 mm Structural Walls to Lift & Lift Lobby
5/F - 14/F
                  0.3 \times 3.2 \times 3 \times 10
                                                                     28.80 m<sup>2</sup>
16/F - 26/F
                  0.3 \times 3.2 \times 3 \times 11
                                                               =
                                                                     31.68 \, m^2
                                                                                  60.48 \, m^2
300 mm Panel Walls to Lift & Lift Lobby
5/F - 14/F
                  201.60 - (43.20 + 28.80)
                                                                  129.60
16/F - 26/F
                  221.76 - (47.52 + 31.68)
                                                                   142.56 m<sup>2</sup>
                                                                                 272.16 \text{ m}^2
Lift shaft walls without gypsum plaster
5/F - 14/F
                  2.7 x 3.2 x 10
                                                                    86.40 m<sup>2</sup>
16/F - 26/F
                  2.7 x 3.2 x 11
                                                               =
                                                                    95.04 \text{ m}^2
                                                                                 181.44 m<sup>2</sup>
Fenestration between 5/F - 14/F
                  Total Glazing in 100 mm panel walls
                                                                    329.60
                  (4.1 + 5.7) 1.6 \times 10
                                                                    156.80
                                                                               unshaded
                                                                    172.80
                                                                               shaded
Fenestration between 16/F - 26/F
                 Total Glazing in curtain wall
                                                                    326.48
                  [(4.1+5.7)1.6+(3.9x0.8)] 11
                                                                    206.80
                                                                               unshaded
                                                                    119.68
                                                                              shaded
```

'U' value of composite wall of columns and beams :-G/F, 1/F, 5/F-14/F

W _l for beam and column		Weight
external surface film	Ro = 0.044	
5 mm white mosaic tiles	$\frac{0.005}{1.5} = 0.003$	0.005 x 2500 = 12.50
10 mm cement/sand render	$\frac{0.01}{0.72} = 0.014$	0.01 x 1860 = 18.60
600 mm concrete beam & column	$\frac{0.60}{2.16} = 0.278$	0.60 x 2400 = 1440.00
10 mm gypsum plaster	$\frac{0.01}{0.38} = 0.026$	0.01 x 1120 = 11.20
Internal surface film (absorptivity below 0.5)	Ri = 0.299	
Totals	0.664	1482.30 kg/m²

$$U_W = \frac{1}{0.664} = 1.51 \text{ W/m}^2 \text{ °C}$$

'U' value of composite wall panels :-G/F, 1/F, 5/F-14/F

W ₃ for wall panel		Weight
external surface film	Ro = 0.044	
5 mm white mosaic tiles	= 0.003	$0.005 \times 2500 = 12.50$
10 mm cement/sand render	= 0.014	$0.01 \times 1860 = 18.60$
100 mm concrete panel	$\frac{0.1}{2.16} = 0.046$	0.10 x 2400 = 240.00
10 mm gypsum plaster	= 0.026	$0.01 \times 1120 = 11.20$
Internal surface film	Ri = 0.299	
Totals	0.432	282.30 kg/m²

$$U_W = \frac{1}{0.432} = 2.32 \text{ W/m}^2 \text{ °C}$$

 $U_W = \frac{1}{0.432} = \frac{2.32}{2.32}$ W/m²°C (for west podium wall without tiles and render 'U' value is 2.41 W/m²°C)

 ${}^{`U'}$ value of composite columns and beams :- 16/F - 26/F

W ₂ for beam and column		Weight
External surface film	Ro = 0.044	
8 mm black glass	$\frac{0.008}{1.05} = 0.0076$	0.008 x 2500 = 20.00
50 mm Air space resistance (absorptivity above 0.5)	Ra = 0.153	
600 mm concrete beam and column	$\frac{0.60}{2.16} = 0.278$	0.6 x 2400 = 1440.00
10 mm gypsum plaster	$\frac{0.01}{0.38} = 0.026$	0.01 x 1120 = 11.20
Internal surface film	Ri = 0.299	
Totals	0.808	1471.20 kg/m²

$$U_W = \frac{1}{0.808} = \frac{1.24}{---} \text{ W/m}^2 \text{ °C}$$

'U' value of composite curtain wall panels :- 16/F - 26/F

W ₄ for panel wall		Weight
External surface film	Ro = 0.044	
8 mm black glass	$\frac{0.008}{1.05} = 0.0076$	0.008 x 2500 = 20.00
75 mm mineral wool felt insulation	$\frac{0.075}{0.039} = 1.923$	0.075 x 50 = 3.75
50 mm Air space resistance (absorptivity above 0.5)	Ra = 0.153	-
2 mm pressed steel panel	$\frac{0.002}{50} = 0.00004$	0.002 x 7800 = 15.60
Internal surface film	Ri = 0.299	
Totals	2.427	39.35 kg/m²

$$U_W = \frac{1}{2.427} = 0.41 \text{ W/m}^2 \text{ °C}$$

'U' value of structural walls :G/F, 1/F, 5/F-14/F

W ₅ for wall panel		Weight
external surface film	Ro = 0.044	
5 mm white mosaic tiles	$\frac{0.005}{1.5} = 0.003$	$0.005 \times 2500 = 12.50$
10 mm cement/sand render	$\frac{0.01}{0.72} = 0.014$	0.01 x 1860 = 18.60
300 mm concrete wall	$\frac{0.30}{2.16} = 0.139$	$0.30 \times 2400 = 720.00$
10 mm gypsum plaster	$\frac{0.01}{0.38} = 0.026$	0.01 x 1120 = 11.20
Internal surface film (absorptivity below 0.5)	Ri = 0.299	
Totals	0.525	762.3 kg/m²

$$U_W = \frac{1}{0.525} = \frac{1.91}{0.525} \text{ W/m}^2 \text{°C}$$

(for carpark ramp and walls without tiles or render 'U' value is 1.97 W/m²°C) (for lift wall without gypsum plaster 'U' value is 3.13 W/m²°C)

<u>'U' value of structural walls</u> :- 16/F-26/F

W ₆ for beam and column		Weight
external surface film	Ro = 0.044	
8 mm black glass	$\frac{0.008}{1.05} = 0.0076$	0.008 x 2500 = 20.00
50 mm Air space resistance (absorptivity above 0.5)	Ra = 0.153	
300 mm concrete wall	$\frac{0.30}{2.16} = 0.139$	$0.3 \times 2400 = 720.00$
10 mm gypsum plaster	$\frac{0.01}{0.38} = 0.026$	0.01 x 1120 = 11.20
Internal surface film	Ri = 0.299	
Totals	0.669	751.20 kg/m²

$$U_W = \frac{1}{0.669} = 1.50 \text{ W/m}^2 \text{°C}$$

(for lift wall without gypsum plaster 'U' value is 2.16 W/m2°C)

'U' value of Lift Lobby wall :-

5/F - 14/F

W7 for beam and column			Weight
External surface film	Ro	= 0.044	
5 mm white mosaic tiles		= 0.003	$0.005 \times 2500 = 12.50$
10 mm cement/sand render		= 0.014	0.01 x 1860 = 18.60
*3.0 m concrete lobby wall	$\frac{3.00}{2.16}$	= 1.389	3.00 x 2400 = 7200.00
Totals		1.450	7231.10 kg/m²

$$U_W = \frac{1}{1.45} = 0.69 \text{ W/m}^2 \text{°C}$$
 * 3.0 m length assumed for simplicity

'U' value of Lift Lobby wall :-

16/F - 26/F

Wg for beam and column			Weight
External surface film	Ro	= 0.044	
8 mm black glass		= 0.0076	0.008 x 2500 = 20.00
50 mm Air space resistance (absorptivity above 0.5)	Ra	= 0.153	
*3.0 m concrete lobby wall		= 1.389	3.00 x 2400 = 7200.00
Totals		= 1.594	7220.00 kg/m ²

$$U_W = \frac{1}{1.594} = 0.63 \text{ W/m}^2 \circ \text{C}$$

Sheet No. A $\phantom{aaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaa$	BD Ref 2//
Building address <u>Typical Commercial Building</u>	
Physical data of Opaque *Wall/Roof	
Facade Orientation facing <u>East (Tower)</u>	Solar Factor (SF) is <u>168</u>

*Wall/Roof Code N	io.	*W ₁ /R ₁	*W2/R2	*W ₃ /R ₃	*W ₄ /R ₄
Location of Wall		Beams & Cols	Reams & Cols	Panel Curtain Walls5/F-14/F	Panel Curtain
External Finish N		5/F-14/F	10/1-20/1	Walls J/1 - 1-7/1	WCLL 10/1 LOVE
Conductivity	W/m°C	1.50	1.05	1.50	1.05
Density	kg/m ³	2500	2500	2500	2500
Thickness	m	0.005	0.008	0.005	0.008
Absorptivity	(a)	0.58	1.00	0.58	1.00
Intermediate com	ponent	cement render	air gap	cement render	mineral wool
Conductivity	W/m°C	0.72		0.72	0.039
Density	kg/m ³	1860		1860	50
Thickness	m	0.01	0.05	0.01	0.075
Intermediate com	ponent	r. concrete	r. concrete	r. concrete	air gap
Conductivity	W/m°C	2.16	2.16	2.16	
Density	kg/m ³	2400	2400	2400	
Thickness	m	0.60	0.60	0.10	0.05
Intermediate com	ponent				
Conductivity	W/m°C				
Density	kg/m ³				
Thickness	m				
Intermediate com	ponent				
Conductivity	W/m°C				
Density	kg/m ³				
Thickness	m	N	hite semi glo		white semi gloss paint o
Internal Finish	Material		on gypsum p		steel panel
Conductivity	W/m°C	0.38	0.38	0.38	50
Density	kg/m ³	1120	1120	1120	7800
Thickness	m	0.01	0.01	0.01	0.002
Absorptivity	α	0.30	0.30	0.30	0.30
`U' value of com *Wall/Roof	nposite	1.51	1.24	2.32	0.41
Area of *Wall/Ro	oof m²	200.40	220.44	206.00	262.68
Density of compo	osite kg/m²	1482	1471	282	39
Equivalent tempo difference	erature (TD _{EQ})	2.40	2.40	5.01	6.68

^{*}Delete as appropriate First issue April 1995

Calculation of 'U' Value of Composite Wall/Roof and Details of Other Values

Sheet No. Al(A)	BD Ref 2//
Building address <u>Typical Commercial Building</u>	
Physical data of Opaque *Wall/Roof	
Facade Orientation facing <u>East (Tow</u> er)	Solar Factor (SF) is 168

*Wall/Roof Code	No.	*W ₅ /R ₅	*W ₆ /R ₆	*W7/R7	*W ₈ /R ₈
Location of Wal	l/Roof	L	· · · · · · · · · · · · · · · · · · ·	Lift Lobby Wall 5/F-14/F white mosaic	Lift Lobby Wall 16/F-26/F
External Finish	Material	White mosaic tiles	black glass	white mosaic tiles	black glass
Conductivity	W/m°C	1.50	1.05	1.50	1.05
Density	kg/m ³	2500	2500	2500	2500
Thickness	m	0.005	0.008	0.005	0.008
Absorptivity	(a)	0.58	1.00	0.58	1.00
Intermediate co	mponent	cement render	air gap	cement render	air gap
Conductivity	W/m°C	0.72		0.72	
Density	kg/m ³	1860		1860	
Thickness	m	0.01	0.05	0.01	0.05
Intermediate co	mponent	r. concrete	r. concrete	r. concrete	r. concrete
Conductivity	W/m°C	2.16	2.16	2.16	2.16
Density	kg/m ³	2400	2400	2400	2400
Thickness	m	0.30	0.30	3.00	3.00
Intermediate co	mponent				
Conductivity	W/m°C				
Density	kg/m ³				
Thickness	m				
Intermediate co	mponent				
Conductivity	W/m°C				
Density	kg/m ³				
Thickness	m				
Internal Finish	Material	white semi glo on gypsum pl	ss paint aster		
Conductivity	W/m°C	0.38	0.38		
Density	kg/m ³	1120	1120		
Thickness	m	0.01	0.01		
Absorptivity	a.	0.30	0.30		
`U' value of comes *Wall/Roof	mposite	1.91(3.13)	1.50(2.16)	0.69	0.63
Area of *Wall/R	oof m²	43.20(86.4)	47.52(95.04)	28.80	31.68
Density of comp *Wall/Roof	osite kg/m²	762(751)	751(740)	7231	7220
Equivalent temp	erature (TD _{EQ})	2.40	2.40	2.40	2.40

() Lift shaft walls without gypsum plaster

^{*}Delete as appropriate First issue April 1995

Window/Rooflight Schedule

Sheet No. B <u>l</u>	BD Rei 2//
Building address <u>Typical Commercial Building</u>	
Physical data on *window/rooflight	
Facade Orientation facing <u>East (Tower)</u>	Solar Factor (SF) is <u>168</u>

Window/Rooflight Code No.	*F ₁ /RL ₁	*F ₂ /RL ₂	*F3/RL3	*F ₄ /RL ₄
Location of *Window/ Rooflight	5/F-14/F shaded	5/F-14/F unshaded	16/F-26/F shaded	16/F-26/F unshaded
Glazing type	tinted	tinted	tinted	tinted
Thickness m	0.008	0.008	0.008	0.008
Shading Coefficient (SC)	0.70	0.70	0.70	0.70
Type of shading device	solid overhang	_	aluminium foils	_
External Shading Multiplier (ESM)	0.7	-	0.7	-
Area of glazing m²	172.80	156.80	119.68	206.80

Physical data on *window/rooflight

Facade Orientation facing <u>East (Tower)</u>

Solar Factor is <u>168</u>

Window/Rooflight Code No.	*F ₅ /RL ₅	*F ₆ /RL ₆	*F7/RL7	*F ₈ /RL ₈
Location of *Window/ Rooflight	5/F-14/F unshaded	16/F-26/F unshaded		
Glazing type	tinted	tinted		
Thickness m	0.008	0.008		
Shading Coefficient (SC)	0.70	0.70		
Type of shading device		-		
External Shading Multiplier (ESM)		-		
Area of glazing m²	43.20	47.52		

^{*} Delete as appropriate

Calculation of OTTV of Individual Facade in Building Envelope

Sheet No. Cl	BD	Ref	2/_	/	, 	/
Building address <u>Typical Commercial Building</u>						
Facade Orientation facing <u>East (Tower)</u> .						

Opaque *Walls/Roofs

Code No.	Description	*A _w /A _r	U	α	$^{\mathrm{TD}}_{\mathrm{EQ}}$	Sum	
W1	Beams & Cols 5/F-14/F	200.40	1.51	0.58	2.40	421.22	
W2	Beams & Cols 16/F-26/F	220.44	1.24	1.00	2.40	656.03	
W3	Panel Curtain Walls 5/F-14/F	206.00	2.32	0.58	5.01	1,388.74	
W4	Panel Curtain Walls 16/F-26/F	262.68	0.41	1.00	6.68	719.43	
W 5	300 Panel Walls 5/F-14/F	43.20	1.91	0.58	2.40	114.86	
W5A	300 Lift Walls	86.40	3.13	0.58	2.40	376.44	
W 6	300 Panel Walls 16/F-26/F	47.52	1.50	1.00	2.40	171.07	
W6A	300 Lift Walls	95.04	2.16	1.00	2.40	492.69	
W7	Lift/Lobby wall 5/F-14/F	28.80	0.69	0.58	2.40	27.66	
W8	Lift/Lobby wall 16/F-26/F	31.68	0.63	1.00	2.40	47.90	
	Subtotals	1,222.16	(A)	Не	eat Gain	4,416.04	(c

Fenestration

Code No.	Description	*Af _w /Af _r	SC	ESM	SF	Sum
Fl	5/F - 14/F shaded	172.80	0.70	0.7	168	14,224.90
F2	5/F - 14/F unshaded	156.80	0.70	-	168	18,439.68
F3	16/F - 26/F shaded	119.68	0.70	0.7	168	9,852.06
F4	16/F - 26/F unshaded	206.80	0.70	-	168	24,319.68
F5	5/F-14/F unshaded	43.20	0.70	-	168	5,080.32
F6	16/F - 26/F unshaded	47.52	0.70	-	168	5,588.35
	Subtotals	746.80	(B)	Н	eat Gain	77,504.99
		L				L

Gross Heat Gain (C + D) 81,921.03 Gross Area (A + B) 1,968.96 OTTV = $\frac{C + D}{A + B}$ = 41.61 W/m²

* Delete as appropriate

Gross Wall Area

 $1.566.72 \text{ m}^2$

Wall composite areas

Beams and Column Areas

5/F - 14/F (0.6 x 18.6 + 0.6 x 2.6 x 4) 10 = 174.00 m²

15/F Nil = -

16/F - 26/F (0.6 x 18.6 + 0.6 x 2.6 x 4) 11 = 191.40 m² 365.40 m²

300 mm Structural Wall to Lift

16/F-26/F 0.3 x 3.2 x 11 = 10.56 m²

300 mm Structural Panel Walls to Lift

16/F-26/F 9.0 x 3.2 x 11 - 10.56 = 306.24 m² 316.80 m²

Glazing Areas

 $5/F - 14/F = 25.76 \times 10$ = 257.60 m²

15/F Nil = -

16/F - 26/F 25.76 x 11 = 283.36 m² 540.96 m²

100 mm Staircase Wall

5/F - 14/F 0.1 x 2.6 x 10 = 2.60 m²

16/F - 26/F 0.1 x 2.6 x 11 = 2.86 m² 5.46 m²

100 mm Wall Panel Areas

5/F - 14/F 595.20 - (174.00 + 257.60 + 2.60) = 161.00 m²

15/F Nil = -

16/F - 26/F 971.52-(191.40+316.80+283.36+2.86) = 177.10 m² 338.10 m²

Sheet No. A2	BD Ref 2//
Building address <u>Typical Commercial Building</u>	
Physical data of Opaque *Wall/Roof	
Facade Orientation facing North (Tower)	Solar Factor (SF) is 104

*Wall/Roof Code N	No.	*W ₁ /R ₁	*W2/R2	*W ₃ /R ₃	*W ₄ /R ₄
Location of Wall,	/Roof	Beams & Cols 5/F-14/F	Beams & Cols 16/F-26/F	Panel Walls	Curtain Wall panel 16/F-26/F
External Finish	Material	White mosaic tiles	black glass	white mosaic tiles	black glass
Conductivity	W/m°C	1.50	1.05	1.50	1.05
Density	kg/m ³	2500	2500	2500	2500
Thickness	m	0.005	0.008	0.005	0.008
Absorptivity	(a)	0.58	1.00	0.58	1.00
Intermediate comp	onent	cement render	air gap	cement render	air gap
Conductivity	W/m°C	0.72		0.72	0.039
Density	kg/m ³	1860		1860	50
Thickness	m	0.01	0.05	0.01	0.075
Intermediate comp	ponent	r. concrete	r. concrete	r. concrete	air gap
Conductivity	W/m°C	2.16	2.16	2.16	
Density	kg/m ³	2400	2400	2400	
Thickness	m	0.60	0.60	0.10	0.05
Intermediate com	ponent				
Conductivity	W/m°C				
Density	kg/m ³				
Thickness	m				
Intermediate comp	ponent				
Conductivity	W/m°C				
Density	kg/m ³				
Thickness	m	white	semi gloss p	int on	white semi gloss paint on
Internal Finish !	Material		gypsum plast	r	steel panel
Conductivity	W/m°C	0.38	0.38	0.38	50
Density	kg/m ³	1120	1120	1120	7800
Thickness	m	0.01	0.01	0.01	0.002
Absorptivity	α	0.30	0.30	0.30	0.30
`U' value of comp *Wall/Roof	posite	1.51	1.24	2.32	0.41
Area of *Wall/Roo	of m ²	174.00	191.40	161.00	177.10
Density of compose *Wall/Roof	site kg/m²	1482	1471	282	39
Equivalent temper difference	rature (TD _{EQ})	1.70	1.70	2.72	3.38

^{*}Delete as appropriate First issue April 1995

Sheet No. A3	BD Ref 2//
Building address <u>Typical Commercial B</u>	uilding
Physical data of Opaque *Wall/Roof	
Facade Orientation facing North (Tower) Solar Factor (SF) is 104

*Wall/Roof Code N	0.	*W6 ^{/R} 6	*W ₇ /R ₇	*W ₈ /R ₈	*W _{8A} /R _{8A}
Location of Wall/		300mm Structural Panel Walls 16/F—26/F	100mm Staircase wall 5/F-14/F	100mm Stair wall 16/F—26/F	300mmStructural Lift Walls 16/F-26/F
External Finish M	aterial	black glass	white mosaic tiles	black glass	black glass
Conductivity	W/m°C	1.05	1.50	1.05	1.05
Density	kg/m ³	2500	2500	2500	2500
Thickness	m	0.008	0.005	0.008	0.008
Absorptivity	(a)	1.00	0.58	1.00	1.00
Intermediate comp	onent	air gap	cement render	air gap	air <i>g</i> ap
Conductivity	W/m°C		0.72		
Density	kg/m ³		1860		
Thickness	m	0.05	0.01	0.05	0.05
Intermediate comp	onent	r. concrete	r. concrete	r. concrete	r. concrete
Conductivity	W/m°C	2.16	2.16	2.16	2.16
Density	kg/m ³	2400	2400	2400	2400
Thickness	m	0.30	3.00	3.00	3.00
Intermediate comp	onent				
Conductivity	W/m°C				
Density	kg/m ³				
Thickness	m				
Intermediate comp	onent				
Conductivity	W/m°C				
Density	kg/m ³				
Thickness	m				
Internal Finish M	aterial				
Conductivity	W/m°C				
Density	kg/m ³				
Thickness	m				
Absorptivity	α				
`U' value of comp *Wall/Roof	osite	2.16	0.69	0.63	0.63
Area of *Wall/Roo	of m ²	306.24	2.60	2.86	10.56
Density of compos *Wall/Roof	site kg/m²	740	7231	7220	7220
Equivalent temper difference	rature (TD _{EQ})	1.70	1.70	1.70	1.70

^{*}Delete as appropriate First issue April 1995

Window/Rooflight Schedule

sneet No. BZ	_		BD Ref	2//
Building address <u>Typical</u>	Commercial Bu	ilding		
Physical data on *window/ro	ooflight			
Facade Orientation facing _	North (Tower)	Sol	ar Factor (SF) is <u>104</u>
Window/Rooflight Code No.	*F ₁ /RL ₁	*F ₂ /RL ₂	*F3/RL3	*F ₄ /RL ₄
Location of *Window/ Rooflight	5/F-14/F shaded	16/F-26/F shaded		
Glazing type	tinted	tinted		
Thickness m	0.008	0.008		
Shading Coefficient (SC)	0.70	0.70		
Type of shading device	solid overhang	aluminium foils		
External Shading Multiplier (ESM)	0.80	0.80		
Area of glazing m²	257.60	283.36		
Physical data on *window/ro	_		Solar Factor	r is
Window/Rooflight Code No.	*F ₁ /RL ₁	*F ₂ /RL ₂	*F3/RL3	*F ₄ /RL ₄
Location of *Window/ Rooflight				
Glazing type				
Thickness m				
Shading Coefficient (SC)				
Type of shading device				
External Shading Multiplier (ESM)				

m²

First issue April 1995

Area of glazing

^{*} Delete as appropriate

Calculation of OTTV of Individual Facade in Building Envelope

Sheet No. C	2	_		BD	Ref	2//
Building address	Typical	Commercial Bui	lding		•	
Facade Orientatio	n facing	North (Tower)	•			

Opaque *Walls/Roofs

Code No.	Description	*A _w /A _r	U	α	$^{\mathrm{TD}}_{\mathrm{EQ}}$	Sum
Wl	Beams & Col. 5/F-14/F	174.00	1.51	0.58	1.70	259.06
W2	Beams & Col. 16/F-26/F	191.40	1.24	1.00	1.70	403.47
W3	Panels Walls 5/F-14/F	161.00	2.32	0.58	2.72	589.27
W4	Panels Walls 16/F-26/F	177.10	0.41	1.00	3.38	245.43
W6	300 mm Structural Panel 16/F-26/F	306.24	2.16	1.00	1.70	1,124.51
W 7	100 mm Stair wall 5/F-14/F	2.60	0.69	0.58	1.70	1.77
W8	100 mm Stair wall 16/F-26/F	2.86	0.63	1.00	1.70	3.06
W8A	300 mm Lift wall 16/F-26/F	10.56	0.63	1.00	1.70	11.31
	Subtotals	1,025.76	(A)	Не	eat Gain	2,637.88

Fenestration

Code No.	Description	*Af _w /Af _r	sc	ESM	SF	Sum	
Fl	5/F - 14/F	257.60	0.70	0.80	104	15,002.62	
F2	16/F - 26/F	283.36	0.70	0.80	104	16,502.89	
	Subtotals	540.96	(B)	Не	eat Gain	31,505.51	(D

Gross Heat Gain (C + D)
$$34,143.39$$

Gross Area (A + B) $1,566.72$

OTTV = $\frac{C + D}{A + B}$ = $\frac{21.79}{W/m^2}$

* Delete as appropriate

West Elevation (Tower)

Gross Wall Area

1,968.96 m²

Wall composite areas

Beams and Column Areas

5/F - 14/F (0.6 x 29.3 + 0.6 x 2.6 x 6) 10 = 269.40 m²

15/F Nil = -

16/F - 26/F (0.6 x 29.3 + 0.6 x 2.6 x 6) 11 = 296.34 m² 565.74 m²

Glazing Areas

5/F - 14/F 32.48 x 10 = 324.80 m²

15/F Nil = -

16/F - 26/F 32.48 x 11 = 357.28 m² 682.08 m²

Wall Panel Areas

5/F - 14/F = 937.60 - (269.40 + 324.80) = 343.40 m²

15/F Nil = -

16/F - 26/F 1,031.36 - (296.34 + 357.28) = 377.74 m² 721.14 m²

Sheet No. A3	BD Ref 2//
Building address <u>Typical Commercial Building</u>	
Physical data of Opaque *Wall/Roof	
Facade Orientation facing <u>West</u> (Tower)	Solar Factor (SF) is 175

*Wall/Roof Code	No.	*W ₁ /R ₁	*W2/R2	*W ₃ /R ₃	*W ₄ /R ₄
Location of Wal	l/Roof	Beams & Cols 5/F-14/F	Beams & Cols 16/F-26/F	Panel Walls	Curtain Wall panel 16/F-26/F
External Finish	Material	5/F-14/F White mosaic tiles	black glass	5/F-14/F white mosaic tiles	black glass
Conductivity	W/m°C	1.50	1.05	1.50	1.05
Density	kg/m ³	2500	2500	2500	2500
Thickness	m	0.005	0.008	0.005	0.008
Absorptivity	(a)	0.58	1.00	0.58	1.00
Intermediate co	mponent	cement render	air gap	cement render	mineral felt
Conductivity	W/m°C	0.72		0.72	0.039
Density	kg/m ³	1860		1860	50
Thickness	m	0.01	0.05	0.01	0.075
Intermediate co	mponent	r. concrete	r. concrete	r. concrete	air gap
Conductivity	W/m°C	2.16	2.16	2.16	
Density	kg/m ³	2400	2400	2400	
Thickness	m	0.60	0.60	0.10	0.05
Intermediate co	mponent				
Conductivity	W/m°C				
Density	kg/m ³				
Thickness	m				
Intermediate co	mponent				
Conductivity	W/m°C				
Density	kg/m ³				
Thickness	m	white	semi gloss par	nt on	white semi gloss paint or
Internal Finish	Material		gypsum plaster		steel panel
Conductivity	W/m°C	0.38	0.38	0.38	50
Density	kg/m ³	1120	1120	1120	7800
Thickness	m	0.01	0.01	0.01	0.002
Absorptivity	α	0.30	0.30	0.30	0.30
`U' value of co *Wall/Roof	mposite	1.51	1.24	2.32	0.41
Area of *Wall/R	oof m²	269.40	296.34	343.40	377.74
Density of comp *Wall/Roof	osite kg/m²	1482	1471	282	39
Equivalent temp difference	erature (TD _{EQ})	2.10	2.10	4.35	5.79

^{*}Delete as appropriate First issue April 1995

Window/Rooflight Schedule

Sheet No. B3	_		BD Ref	2//
Building address <u>Typical</u>	Commercial Bu	ilding		
Physical data on *window/ro	ooflight			
Facade Orientation facing _	West (Tower)	Sol	ar Factor (SI	?) is <u>175</u>
Window/Rooflight Code No.	*F ₁ /RL ₁	*F ₂ /RL ₂	*F3/RL3	*F ₄ /RL ₄
Location of *Window/ Rooflight	5/F-14/F shaded	16/F-26/F shaded		
Glazing type	tinted	tinted		
Thickness m	0.008	0.008		
Shading Coefficient (SC)	0.70	0.70		
Type of shading device	solid overhang	aluminium foils	•	
External Shading Multiplier (ESM)	0.70	0.70		
Area of glazing m²	324.80	357.28		
Physical data on *window/ro			Solar Facto	r is
Window/Rooflight Code No.	*F ₁ /RL ₁	*F ₂ /RL ₂	*F ₃ /RL ₃	*F4/RL4
Location of *Window/ Rooflight				
Glazing type				
Thickness m				
Shading Coefficient (SC)				
Type of shading device				
External Shading Multiplier (ESM)				
Area of glazing m ²				

^{*} Delete as appropriate

Calculation of OTTV of Individual Facade in Building Envelope

Sheet No. C3	BD Ref 2//
Building address <u>Typical Commercial Building</u>	
Facade Orientation facing West (Tower) .	

Opaque *Walls/Roofs

Code No.	Description	*A _w /A _r	U	α	TD _{EQ}	Sum
Wl	Beams & Col. 5/F-14/F	269.40	1.51	0.58	2.10	495.48
W2	Beams & Col. 16/F-26/F	296.34	1.24	1.00	2.10	771.67
W3	Panels Walls 5/F-14/F	343.40	2.32	0.58	4.35	2,010.04
W4	Curtain Wall Panels 16/F-26/F	377.74	0.41	1.00	5.79	896.72
	Subtotals	1,286.88	(A)	He	eat Gain	4,173.91

Fenestration

Code No.	Description	*Af _w /Af _r	SC	ESM	SF	Sum
Fl	5/F - 14/F	324.80	0.70	0.70	175	27,851.60
F2	16/F - 26/F	357.28	0.70	0.70	175	30,636.76
	Subtotals	682.08	(B)	He	eat Gain	58,488.36

Gross Heat Gain (C + D)
$$62,662.27$$

Gross Area (A + B) $1,968.96$

OTTV = $\frac{C + D}{A + B}$ = $\frac{31.83}{W/m^2}$

* Delete as appropriate

South Elevation (Tower)

Gross Wall Area

 $1,566.72 \text{ m}^2$

Wall composite areas

Beam and Column Areas

 $(0.6 \times 18.6 + 0.6 \times 2.6 \times 4) \ 10 = 174.00 \ m^2$ 5/F - 14/F

15/F

Nil

16/F - 26/F

 $[(0.6 \times (18.6+9)+0.6 \times 2.6 \times 6)] 11 = 285.12 \text{ m}^2$

459.12 m²

<u>Glazing Areas</u>

5/F - 14/F

16/F - 26/F

25.92 x 10

 8.48×11

 $= 259.20 \text{ m}^2$

15/F

Nil

16/F - 26/F 25.92 x 11

285.12 m²

93.28 m²

 $637.60 \, m^2$

100 mm Stair case wall

16/F - 26/F 0.1 x 2.6 x 11

2.86 m²

 $2.86 \, m^2$

Wall Panel Areas

$$5/F - 14/F$$

$$595.20 - (174.00 + 259.20)$$

 $= 162.00 \text{ m}^2$

15/F

Nil

$$16/F - 26/F$$

$$16/F - 26/F$$
 971.52 - (285.12+285.12+93.28+2.86) = 305.14 m²

467.14 m²

Fenestration between 16/F - 26/F

Total Glazing
$$285.12 + 93.28 = 378.40 \text{ m}^2$$

 $(5.4 \times 3) \times 1.6 \times 11 = 285.12 \text{ m}^2$

Unshaded

93.28 m²

Shaded

$\begin{array}{c} \textbf{Building (Energy Efficiency) Regulation} \\ \underline{ \qquad \qquad \qquad \qquad \qquad } \\ \textbf{Form OTTV 1} \end{array}$

Sheet No. A	BD Ref 2//
Building address <u>Typical Commercial Building</u>	
Physical data of Opaque *Wall/Roof	
Facade Orientation facing South (Tower)	Solar Factor (SF) is 191

*Wall/Roof Code No).	*W ₁ /R ₁	*W ₂ /R ₂	*W ₃ /R ₃	*W ₄ /R ₄
Location of Wall/	Roof	Beams & Col 5/F-14/F	Beams & Cols 16/F-26/F	Panel Walls 5/F-14/F	Curtain Wall panel 16/F - 26/F
External Finish Ma	aterial	white mosaic tiles	black glass	white mosaic tiles	black glass
Conductivity	W/m°C	1.50	1.05	1.50	1.05
Density	kg/m ³	2500	2500	2500	2500
Thickness	m	0.005	0.008	0.005	0.008
Absorptivity	(a)	0.58	1.00	0.58	1.00
Intermediate compo	onent	cement render	air gap	cement render	mineral felt
Conductivity	W/m°C	0.72		0.72	0.039
Density	kg/m ³	1860		1860	50
Thickness	m	0.01	0.05	0.01	0.075
Intermediate compo	onent	r. concrete	r. concrete	r. concrete	air gap
Conductivity	W/m°C	2.16	2.16	2.16	
Density	kg/m ³	2400	2400	2400	
Thickness	m	0.60	0.60	0.10	0.05
Intermediate comp	onent				
Conductivity	W/m°C				
Density	kg/m ³				
Thickness	m				
Intermediate comp	onent				
Conductivity	W/m°C				
Density	kg/m ³				
Thickness	m	white	semi gloss pa	nt on	white semi gloss paint on
Internal Finish M	aterial		gypsum plaste:		steel panel
Conductivity	W/m°C	0.38	0.38	0.38	50
Density	kg/m ³	1120	1120	1120	7800
Thickness	m	0.01	0.01	0.01	0.002
Absorptivity	α	0.30	0.30	0.30	0.30
'U' value of comp *Wall/Roof	osite	1.51	1.24	2.32	0.41
Area of *Wall/Roo	f m²	174.00	285.12	162.00	305.14
Density of compos *Wall/Roof	ite kg/m²	1482	1471	282	39
Equivalent temper difference	ature (TD _{EQ})	1.40	1.40	3.60	5.01

^{*}Delete as appropriate First issue April 1995

Sheet No. A4	BD Ref 2//
Building address <u>Typical Commercial Building</u>	
Physical data of Opaque *Wall/Roof	
Facade Orientation facing <u>South (Tower)</u>	Solar Factor (SF) is 191

[13 /B 6 3		
*Wall/Roof Code		*W ₈ /R ₈
Location of Wall	16/F - 26/F	
External Finish		Staircase wall black glass
Conductivity	W/m°C	1.05
Density	kg/m ³	2500
Thickness	m	0.008
Absorptivity	(a)	1.00
Intermediate comp	ponent	air gap
Conductivity	W/m°C	
Density	kg/m ³	
Thickness	m	0.05
Intermediate comp	onent	r. concrete
Conductivity	W/m°C	2.16
Density	kg/m ³	2400
Thickness	m	3.00
Intermediate comp	onent	
Conductivity	W/m°C	
Density	kg/m ³	***
Thickness	m	
Intermediate comp	onent	
Conductivity	W/m°C	
Density	kg/m ³	
Thickness	m	
Internal Finish M	laterial	
Conductivity	W/m°C	
Density	kg/m ³	
Thickness	m	
Absorptivity	α	
`U' value of comp *Wall/Roof	osite	0.63
Area of *Wall/Roo	f m²	2.86
Density of compos *Wall/Roof	ite kg/m²	7220
Equivalent temper difference	ature (TD _{EQ})	1.40

^{*}Delete as appropriate First issue April 1995

Window/Rooflight Schedule

Sheet No. B4	•		BD Ref 2	2//
Building address <u>Typical</u>	Commercial Bu	uilding		
Physical data on *window/ro	oflight			
Facade Orientation facing _	South (Tower)	<u>S</u> ol	ar Factor (SF) is <u>191</u>
Window/Rooflight Code No.	*F ₁ /RL ₁	*F2/RL2	*F ₃ /RL ₃	*F ₄ /RL ₄
Location of *Window/ Rooflight	5/F-14/F unshaded	16/F-26/F unshaded	16/F-26/F shaded	
Glazing type	tinted	reflective	tinted	
Thickness m	0.008	0.006	0.008	
Shading Coefficient (SC)	0.70	0.40	0.70	
Type of shading device			aluminium foils	
External Shading Multiplier (ESM)			0.70	
Area of glazing m ²	259.20	285.12	93.28	
Physical data on *window/ro	_		Solar Factor	r is
Window/Rooflight Code No.	*F ₁ /RL ₁	*F2/RL2	*F3/RL3	*F ₄ /RL ₄
Location of *Window/ Rooflight				
Glazing type				
Thickness m				
Shading Coefficient (SC)				
Type of shading device				
External Shading Multiplier (ESM)				
Area of glazing m ²				

^{*} Delete as appropriate

Calculation of OTTV of Individual Facade in Building Envelope

Sheet No. C4	BD Ref 2//
Building address <u>Typical Commercial Building</u>	
Facade Orientation facing <u>South (Tower)</u> .	

Opaque *Walls/Roofs

Code No.	Description	*A _w /A _r	U	α	$^{\mathrm{TD}}$ EQ	Sum
Wl	Beams & Col. 5/F-14/F	174.00	1.51	0.58	1.40	213.34
W2	Beams & Col. 16/F-26/F	285.12	1.24	1.00	1.40	494.97
W3	Panels Walls 5/F-14/F	162.00	2.32	0.58	3.60	784.75
W4	Panels Walls 16/F-26/F	305.14	0.41	1.00	5.01	626.79
W8	Stair Walls 16/F-26/F	2.86	0.63	1.00	1.40	2.52
	Subtotals	929.12	(A)	He	eat Gain	2,122.37

Fenestration

Code No.	Description	*Af _w /Af _r	SC	ESM	SF	Sum
F1	5/F - 14/F unshaded	259.20	0.70		191	34,655.04
F2	16/F - 26/F unshaded	285.12	0.40		191	21,783.17
F3	16/F - 26/F shaded	93.28	0.70	0.70	191	8,730.08
	Subtotals	637.60	(B)	Не	eat Gain	65,168.29

Gross Heat Gain (C + D)
$$67,290.66$$

Gross Area (A + B) $1,566.72$

OTTV = $\frac{C + D}{A + B}$ = $\frac{42.95}{A + B}$ W/m²

* Delete as appropriate

Summary of OTTV of Building Envelope

Sheet No. D		BD	Ref.	2//		
Building address	Typical Commercial Bu	uilding				

Total Envelope Heat Gain (*Tower/Podium)

Facade Orientation	Gross Area from Form OTTV 3	Gross Heat Gain from Form OTTV 3
a. East	1,968.96	81,921.03
b. North	1,566.72	34,143.39
c. West	1,968.96	62,662.27
d. South	1,566.72	67,290.66
е.		
f.		
Subtotal	7,071.36 (E)	246,017.35 (G)
Roof		
a.	391.80	13,185.05
b.	,	
Subtotal	(F)	(H)

Tower/Podium Walls OTTV =
$$\frac{G}{E}$$
 = $\frac{34.79}{E}$ W/m²

Tower/Podium Roofs OTTV = $\frac{H}{F}$ = $\frac{33.65}{E}$ W/m²

Tower/Podium OTTV = $\frac{G+H}{E+F}$ = $\frac{34.73}{E+F}$ W/m²

^{*} Delete as appropriate

Accountable Roof Areas

Roof

Gross Area =
$$6.0 \times 6.6 + 9.6 \times 8.0 + 6 \times 10.3 + 9.0 \times 3.0 + 18.6 \times 8.0 + (6.3 \times 3.0 \times 2)$$
 = 391.80 m^2
Glazed area = 8.4×8.0 = 67.20 m^2
Beam area = $[(15.6 \times 2) + (6.0 \times 2) + 18.6 + (6.3 \times 2) + (5.4 \times 9) + 1.4 + (4.1 \times 2) + (1.7 \times 2) + (2.4 \times 2 \times 0.5) + (3.6 \times 0.5)] 0.6$ = 84.12 m^2
Lift Lobby walls = $0.3 (9+2.7)$ = 3.51 m^2
Panel area = $391.80 - 67.2 - 84.12 - 3.51$ = 236.97 m^2

15/F

Gross Area	=	6.6 x 5.4 + 2.4 x 1.4	=	39.00 m ²
Glazed area			=	Nil
Beam area	=	0.6 (5.4 x 2)	=	6.48 m ²
Panel area	=	39.00 - 6.48	=	32.52 m ²

Podium Roof

Carpark under non-accountable

Nil

A36

'U' value of composite roof beams (and panels) :-

15/F and Roof

R_1 (R_2) for beams (panels)	r	Weight
External surface film	Ro = 0.055	
25 mm concrete tiles	$\frac{0.025}{1.10} = 0.023$	0.025 x 2100 = 52.50
20 mm asphalt	$\frac{0.02}{1.15} = 0.017$	0.02 x 2350 = 47.00
50 mm cement/sand screed	$\frac{0.05}{0.72} = 0.069$	0.05 x 1860 = 93.00
50 mm polystyrene insulation	$\frac{0.05}{0.034} = 1.471$	0.05 x 25 = 1.25
600 mm r. concrete	= 0.278	0.6 x 2400 = 1440.00
10 mm gypsum plaster	= 0.026	0.01 x 1120 = 11.20
Internal surface film	Ri = 0.801	
Totals	2.740	1644.95 kg/m

$$U_R = \frac{1}{2.740} = 0.37 \text{ W/m}^2 \text{ °C}$$

for 150 mm slab 'U' value is 0.40 W/m²°C and weight = 564.95 kg/m for lift lobby walls say 3.0 m deep for ease of calculation, 'U' value is 0.33 W/m²°C and weight = 7,393.75 kg/m

Sheet No. A5	BD Ref 2//
Building address <u>Typical Commercial Building</u>	
Physical data of Opaque *Wall/Roof	
Facade Orientation facing Roof (Tower)	Solar Factor (SF) is 264

*Wall/Roof Code	No.	*W ₁ /R ₁	*W2/R2	*W3/R3
Location of Wall	/Roof	Tower Roof Beam	Tower Roof Panels	Tower Roof Lift Walls
External Finish	Material	concrete tiles	concrete tiles	concrete tiles
Conductivity	W/m°C	1.10	1.10	1.10
Density	kg/m ³	2100	2100	2100
Thickness	m	0.025	0.025	0.025
Absorptivity	(a)	0.65	0.65	0.65
Intermediate com	ponent	asphalt	asphalt	asphalt
Conductivity	W/m°C	1.15	1.15	1.15
Density	kg/m ³	2350	2350	2350
Thickness	m	0.02	0.02	0.02
Intermediate com	ponent	cemei	t/sand screed	
Conductivity	W/m°C	0.72	0.72	0.72
Density	kg/m ³	1860	1860	1860
Thickness	m	0.05	0.05	0.05
Intermediate com	ponent	ex	panded polystyre	ne
Conductivity	W/m°C	0.034	0.034	0.034
Density	kg/m ³	25	25	25
Thickness	m	0.05	0.05	0.05
Intermediate com	ponent	r. concrete	r. concrete	r. concrete
Conductivity	W/m°C	2.16	2.16	2.16
Density	kg/m ³	2400	2400	2400
Thickness	m	0.60	0.15	3.00
Internal Finish	Material	white semi g gypsum	loss paint on plaster	
Conductivity	W/m°C	0.38	0.38	
Density	kg/m ³	1120	1120	
Thickness	m	0.01	0.01	
Absorptivity	α	0.30	0.30	
`U' value of com *Wall/Roof	posite	0.37	0.40	0.33
Area of *Wall/Roo	of m²	84.12	236.97	3.51
Density of compos *Wall/Roof	site kg/m²	1645	565	7394
Equivalent tempe difference	rature (TD _{EQ})	7.90	9.75	7.90

^{*}Delete as appropriate First issue April 1995

Window/Rooflight Schedule

sneet No. B	-		pp ket	4///
Building address <u>Typical</u>	Commercial Bu	ilding		· · · · · · · · · · · · · · · · · · ·
hysical data on *window/ro	oflight			
acade Orientation facing _	Roof (Tower)	_ So	lar Factor (S	F) is <u>264</u>
Window/Rooflight Code No.	*F ₁ /RL ₁	*F2/RL2	*F3/RL3	*F ₄ /RL ₄
Location of *Window/ Rooflight	Roof			
Glazing type	tinted			
Thickness m	0.008			
Shading Coefficient (SC)	0.70			
Type of shading device	_			
External Shading Multiplier (ESM)				
Area of glazing m ²	67.20			
hysical data on *window/ro acade Orientation facing _	_		Solar Facto	or is
Window/Rooflight Code No.	*F1/RL1	*F2/RL2	*F3/RL3	*F ₄ /RL ₄
Location of *Window/ Rooflight				
Glazing type				
Thickness m				
Shading Coefficient (SC)				
Type of shading device				

External Shading

Area of glazing

(ESM)

m 2

Multiplier

^{*} Delete as appropriate

Calculation of OTTV of Individual Facade in Building Envelope

Sheet No. C5	BD	Ref	2/_	/	·	_/_	
Building address <u>Typical Commercial Building</u>							
Facade Orientation facing <u>Roof (Tower)</u> .							

Opaque *Walls/Roofs

Code No.	Description	*A _w /A _r	U	a	TD _{EQ}	Sum	
R ₁	Tower Roof Beams	84.12	0.37	0.65	7.90	159.82	
R ₂	Tower Roof Panels	236.97	0.40	0.65	9.75	600.72	
R ₃	Tower Roof Stair & Lift Walls	3.51	0.33	0.65	7.90	5.95	
	Subtotals	324.60	(A)	Не	eat Gain	766.49	(c

<u>Fenestration</u>

Code No.	Description	*Af _w /Af _r	SC	ESM	SF	Sum	
\mathtt{RL}_1	Rooflight	67.20	0.70	_	264	12,418.56	
	Subtotals	67.20	(B)	He	eat Gain	12,418.56	([

Gross Heat Gain (C + D) 13,185.05

Gross Area (A + B) 391.80

OTTV =
$$\frac{C + D}{A + B}$$
 = 33.65 W/m²

* Delete as appropriate

Sheet No. A5(A)	BD Ref 2//	/
Building address <u>Typical Commercial Building</u>		
Physical data of Opaque *Wall/Roof		
Facade Orientation facing Roof (15/F)	Solar Factor (SF) is $_$	264

*Wall/Roof Code No.		*W ₁ /R ₁	*W2/R2	
Location of Wall/Roo	of	15/F Beams	15/F Panels	
External Finish Mate	erial	concrete tiles	concrete tiles	
Conductivity V	V/m°C	1.10	1.10	
Density 1	kg/m ³	2100	2100	
Thickness	m	0.025	0.025	
Absorptivity	(a)	0.65	0.65	
Intermediate compone	ent	asphalt	asphalt	
Conductivity	W/m°C	1.15	1.15	
Density	kg/m ³	2350	2350	
Thickness	m	0.02	0.02	
Intermediate compone	ent	cement/sand scr	eed	
Conductivity	W/m°C	0.72	0.72	
Density	kg/m ³	1860	1860	
Thickness	m	0.05	0.05	
Intermediate compon	ent	expanded polystyrene		
Conductivity	W/m°C	0.034	0.034	
Density	kg/m ³	25	25	
Thickness	m	0.05	0.05	
Intermediate compon	ent	r. concrete	r. concrete	
Conductivity	W/m°C	2.16	2.16	
Density	kg/m ³	2400	2400	
Thickness	m	0.60	0.15	
Internal Finish Mat	erial	white semi gloss pair	nt on gypsum plaster	
Conductivity	W/m°C	0.38	0.38	
Density	kg/m ³	1120	1120	
Thickness	m	0.01	0.01	
Absorptivity	α	0.30	0.30	
`U' value of compos *Wall/Roof	ite	0.37	0.40	
Area of *Wall/Roof	m²	6.48	32.52	
Density of composit *Wall/Roof	e kg/m²	1645	565	
Equivalent temperat difference	ure (TD _{EQ})	7.90	9.75	

^{*}Delete as appropriate First issue April 1995

Calculation of OTTV of Individual Facade in Building Envelope

Sheet No. C5(A)	BD Ref 2//
Building address <u>Typical Commercial Building</u>	
Facade Orientation facing <u>Roof (15/F)</u> .	

Opaque *Walls/Roofs

Code No.	Description	*A _w /A _r	U	α	TD _{EQ}	Sum	
R_3	15/F Beams	6.48	0.37	0.65	7.90	12.31	
R ₄	15/F Panels	32.52	0.40	0.65	9.75	82.44	
	Subtotals	39.00	(A)	He	eat Gain	94.75	

Fenestration

Code No.	Description	*Af _w /Af _r	sc	ESM	SF	Sum	
						1177	
	Subtotals		(B)	H	l eat Gain		(

Gross Heat Gain (C +	D) 94.75
Gross Area (A + B)	39.00
$OTTV = \frac{C + D}{$	2.43 W/m
A + B	

* Delete as appropriate

344.00 m²

Wall Composite Areas

Beam and Column Areas

 $0.6 \times 40.0 + 0.6 (3.4 \times 6 + 3.4 \times 0.5^*) = 37.26 \text{ m}^2$ G/F

 $= 40.32 \text{ m}^2$ $0.6 \times 40.0 + 0.6 (3.4 \times 8)$ 1/F

1/F (Ramp) 0.6 x 23.0 + 0.6 (3.4 x 5 x 0.5) = 18.90 m^2

 96.48 m^2 2/F - 4/F Nil

Glazing Areas

G/F 87.38 m² $= 87.38 \text{ m}^2$

1/F 119.68 m² $= 119.68 \text{ m}^2$

= - 207.06 m^2 2/F - 4/F Nil

300 mm Retaining Wall

 $= 13.36 \text{ m}^2$ G/F 138.00 - (37.26 + 87.38)

300 mm Ramp Wall

1/F 23 x 4 x 0.5 - 18.90 $= 27.1 \text{ m}^2$

^{*} Only half column considered to contribute

Sheet No. A6	BD Ref 2//
Building address <u>Typical Commercial Building</u>	
Physical data of Opaque *Wall/Roof	
Facade Orientation facing <u>East (Podium)</u>	Solar Factor (SF) is 168

*Wall/Roof Code N	0.	*W ₁ /R ₁	*W ₅ /R ₅	*W _{5A} /R _{5A}	*W /R
Location of Wall/	Roof	Beams & Cols G/F & 1/F	Retaining Wall G/F	Ramp Wall	
External Finish M	aterial	white mosai		1/ F	
Conductivity	W/m°C	1.50	1.50	2.16	
Density	kg/m ³	2500	2500	2400	
Thickness	m	0.005	0.005	0.30	
Absorptivity	(a)	0.58	0.58	0.65	
Intermediate compo	onent	cement re	nder		
Conductivity	W/m°C	0.72	0.72		
Density	kg/m ³	1860	1860		
Thickness	m	0.01	0.01		
Intermediate compo	onent	Reinforced	concrete		
Conductivity	W/m°C	2.16	2.16		
Density	kg/m ³	2400	2400		
Thickness	m	0.60	0.30		
Intermediate compo	onent				
Conductivity	W/m°C				
Density	kg/m ³				
Thickness	m				774
Intermediate compo	onent				
Conductivity	W/m°C				
Density	kg/m ³				
Thickness	m	white semi g	oss paint		
Internal Finish Ma	iterial	on gypsum	plaster		
Conductivity	W/m°C	0.38	0.38	0.38	
Density	kg/m ³	1120	1120	1120	
Thickness	m	0.01	0.01	0.01	
Absorptivity	α	0.30	0.30	0.30	
`U' value of compo *Wall/Roof	site	1.51	1.91	1.97	
Area of *Wall/Roof	m²	96.48	13.36	27.1	
Density of composi *Wall/Roof	te kg/m²	1482	762	731	
Equivalent tempera difference	ture (TD _{EQ})	2.40	2.40	2.40	

^{*}Delete as appropriate First issue April 1995

Window/Rooflight Schedule

Sheet No. B6	-		BD Ref	2///
Building address <u>Typical</u>	Commercial Bui	ilding		
Physical data on *window/ro	oflight			
Facade Orientation facing _		\$o.	lar Factor (SF	') is <u>168</u>
Window/Rooflight Code No.	*F ₁ /RL ₁	*F ₂ /RL ₂	*F3/RL3	*F ₄ /RL ₄
Location of *Window/ Rooflight	G/F&1/F unshaded			
Glazing type	plain			
Thickness m	0.012			
Shading Coefficient (SC)	0.90			
Type of shading device	-			
External Shading Multiplier (ESM)	-			
Area of glazing m ²	207.06		·	
Physical data on *window/ro		-	Solar Facto	or is
Window/Rooflight Code No.	*F ₁ /RL ₁	*F ₂ /RL ₂	*F3/RL3	*F ₄ /RL ₄
Location of *Window/ Rooflight				
Glazing type				
Thickness m				
Shading Coefficient (SC)				
Type of shading device				
External Shading Multiplier (ESM)				

Area of glazing

m²

^{*} Delete as appropriate

Calculation of OTTV of Individual Facade in Building Envelope

Sheet No. C6	BD Ref 2//
Building address <u>Typical Commercial Building</u>	
Facade Orientation facingEast (Podium) .	

Opaque *Walls/Roofs

Code No.	Description	*A _w /A _r	U	α	TD _{EQ}	Sum	
Wl	Beams & Col. G/F&1/F	96.48	1.51	0.58	2.40	202.79	
W 5	Panels G/F&l/F	13.36	1.91	0.58	2.40	35.52	
W 5	Ramp Wall 1/F	27.10	1.97	0.65	2.40	83.28	
	Subtotals	136.94	(A)	Не	eat Gain	321.59	(0

Fenestration

Code No.	Description	*Af _w /Af _r	SC	ESM	SF	Sum
Fl	G/F & 1/F	207.06	0.90	_	168	31,307.47
	Subtotals	207.06	(B)	l He	l eat Gain	31,307.47

Gross Heat Gain (C + D) 31,629.06

Gross Area (A + B) 344.00

OTTV =
$$\frac{C + D}{A + B}$$
 = 91.95 W/m²

* Delete as appropriate

North Elevation (Podium)

Gross Wall Area

 $320.00 \, m^2$

Wall Composite Areas

Beam and Column Areas

G/F 0.6 x 40 + 0.6 x 3.4 x 8

 $= 40.32 \text{ m}^2$

1/F

 $0.6 \times 40 + 0.6 \times 3.4 \times 8$

 $= 40.32 \text{ m}^2$

80.64 m²

100 mm Stair Wall

G/F Stair Wall 0.1 x 3.4

 $= 0.34 \text{ m}^2$

Glazing Areas

G/F 119.34

 $= 119.34 \text{ m}^2$

1/F

119.68

 $= 119.68 \text{ m}^2$

 239.02 m^2

Panel Areas

G/F 160.00 - (40.32 + 119.34 + 0.34) =

1/F 160.00 - (40.32 + 119.68)

0

0

Calculation of 'U' Value of Composite Wall/Roof and Details of Other Values

Sheet No. A	BD Ref 2//
Building address <u>Typical Commercial Building</u>	
Physical data of Opaque *Wall/Roof	
Facade Orientation facing North (Podium)	Solar Factor (SF) is104

*Wall/Roof Code No	ο.	*W ₁ /R ₁	*W7/R7	*W ₃ /R ₃	*W ₄ /R ₄
Location of Wall/	Roof	Beams & Cols G/F & 1/F	Stair Wall G/F		
External Finish Ma	aterial	white mo	șaic tiles		
Conductivity	W/m°C	1.50	1.50		
Density	kg/m ³	2500	2500		
Thickness	m	0.005	0.005		
Absorptivity	(a)	0.58	0.58		
Intermediate compo	onent	cement	render		
Conductivity	W/m°C	0.72	0.72		
Density	kg/m ³	1860	1860		
Thickness	m	0.01	0.01		
Intermediate compo	onent	Reinforced	concrete		
Conductivity	W/m°C	2.16	2.16		
Density	kg/m ³	2400	2400		
Thickness	m	0.60	3.00		
Intermediate compo	onent				····
Conductivity	W/m°C				
Density	kg/m ³				
Thickness	m				
Intermediate compo	nent				
Conductivity	W/m°C				
Density	kg/m ³				
Thickness	m	white semi g	oss paint		
Internal Finish Ma	terial	on gypsum	plaster		
Conductivity	W/m°C	0.38			
Density	kg/m ³	1120			
Thickness	m	0.01			
Absorptivity	α	0.30			
`U' value of compo	site	1.51	0.69		
Area of *Wall/Roof	m 2	80.64	0.34		
Density of composi *Wall/Roof	te kg/m²	1482	7231		
Equivalent tempera difference	ture (TD _{EQ})	1.70	1.70		

^{*}Delete as appropriate First issue April 1995

Window/Rooflight Schedule

Sheet No. B7			BD Ref 2	//
Building address <u>Typical</u>	Commercial Bui	ilding		
Physical data on *window/roFacade Orientation facing No.		Sol	ar Factor (SF) is <u>104</u>
Window/Rooflight Code No.	*F ₁ /RL ₁	*F ₂ /RL ₂	*F ₃ /RL ₃	*F ₄ /RL ₄
Location of *Window/ Rooflight	G/F&1/F unshaded			
Glazing type	plain			
Thickness m	0.012			
Shading Coefficient (SC)	0.90			
Type of shading device	-			
External Shading Multiplier (ESM)	-			
Area of glazing m ²	239.02			
Physical data on *window/ro		-	Solar Facto	r is
Window/Rooflight Code No.	*F ₁ /RL ₁	*F ₂ /RL ₂	*F3/RL3	*F ₄ /RL ₄
Location of *Window/ Rooflight				
Glazing type	·			
Thickness m				
Shading Coefficient (SC)				
Type of shading device				
External Shading Multiplier (ESM)				

 m^2

Area of glazing

^{*} Delete as appropriate

Calculation of OTTV of Individual Facade in Building Envelope

Sheet No. C	BD	Ref	2/	_/	_/
Building address <u>Typical Commercial Building</u>			·		
Facade Orientation facing <u>North (Podium)</u> .					

Opaque *Walls/Roofs

Code No.	Description	*A _w /A _r	U	а	TD _{EQ}	Sum	
W1 W7	Beams & Cols. G/F&1/F Stair Wall G/F	80.64	1.51	0.58 0.58	1.70 1.70	120.06	1
	Subtotals	80.98	(A)	He	eat Gain	120.29	

Fenestration

Code No.	Description	*Af _w /Af _r	sc	ESM	SF	Sum
Fl	G/F & 1/F	239.02	0.90	-	104	22,372.27
	Subtotals	239.02	(B)	Не	eat Gain	22,372.27

Gross Heat Gain (C + D)
$$22,492.56$$

Gross Area (A + B) 320.00

OTTV = $\frac{C + D}{A + B} = 70.29$ W/m²

* Delete as appropriate

West Elevation (Podium)

Gross Wall Area

366.00 m²

(With tiles = 112 m^2) (Party wall = 208 m^2)

Wall Composite Areas

Beam and Column Areas (with tiles)

G/F

 $0.6 \times 14 + 0.6 (3.4 \times 3)$

 $= 14.52 \text{ m}^2$

1/F

 $0.6 \times 14 + 0.6 (3.4 \times 3)$

 $= 14.52 \text{ m}^2$

29.04 m²

300 mm Ramp Wall

1/F

23 x 4 x 0.5 - 18.9

= 27.1 m²

Glazing Areas

G/F

41.48

= 41.48 m²

1/F

41.48

 $= 41.48 \text{ m}^2$

82.96 m²

Beam and Column Areas (Party Wall and Ramp)

G/F

 $0.6 \times 26 + 0.6 (3.4 \times 5)$

 $= 25.80 \text{ m}^2$

1/F

 $0.6 \times 26 + 0.6 (3.4 \times 5)$

 $= 25.80 \text{ m}^2$

1/F Ramp

 $0.6 \times 23 + 0.6 (3.4 \times 5 \times 0.5)$

 $= 18.90 \text{ m}^2$

 $70.50 \, m^2$

Panel Areas (with tiles)

G/F and 1/F

112.00 - (29.04 + 82.96)

= -

Panel Areas in Party Wall

G/F and 1/F

208 - 51.60

 $= 156.40 \text{ m}^2$

 156.40 m^2

Calculation of 'U' Value of Composite Wall/Roof and Details of Other Values

Sheet No. A8	BD Ref 2//
Building address <u>Typical Commercial Building</u>	
Physical data of Opaque *Wall/Roof	
Facade Orientation facing <u>West (Podium)</u>	Solar Factor (SF) is175

*Wall/Roof Code N	0.	*W ₁ /R ₁	*W _{1A} /R _{1A} .	*W3/R3	*W ₅ /R ₅
Location of Wall/	Roof	Beams & Cols	Beams & Cols G/F & 1/F	Panels	Ramp Wall 1/F
External Finish M	aterial	G/F & 1/F White mosaic tiles	Reinforced	G/F & 1/F Concrete	Reinforced
Conductivity	W/m°C	1.50	2.16	2.16	Concrete 2.16
Density	kg/m ³	2500	2400	2400	2400
Thickness	m	0.005	0.60	0.10	0.30
Absorptivity	(a)	0.58	0.65	0.65	0.65
Intermediate comp	onent	cement render		-	
Conductivity	W/m°C	0.72			
Density	kg/m ³	1860			
Thickness	m	0.01			
Intermediate comp	onent	Reinforced o	oncrete		
Conductivity	W/m°C	2.16			
Density	kg/m ³	2400			
Thickness	m	0.60			
Intermediate compo	onent				
Conductivity	W/m°C				
Density	kg/m ³				
Thickness	m				
Intermediate compo	onent				
Conductivity	W/m°C				
Density	kg/m ³				
Thickness	m	white semi gl	oss paint		
Internal Finish Ma	aterial	on gypsum	plaster		
Conductivity	W/m°C	0.38	0.38	0.38	0.38
Density	kg/m ³	1120	1120	1120	1120
Thickness	m	0.01	0.01	0.01	0.01
Absorptivity	a	0.30	0.30	0.30	0.30
`U' value of compo *Wall/Roof	site	1.51	1.55	2.41	1.97
Area of *Wall/Roof		29.04	70.50	156.40	27.1
Density of composi *Wall/Roof	te kg/m²	1482	1451	250	731
Equivalent tempera difference	ture (TD _{EQ})	2.10	2.10	4.35	2.10

^{*}Delete as appropriate First issue April 1995

Window/Rooflight Schedule

Sheet No. B8			BD Ref 2	//
Building address <u>Typical (</u>	Commercial Bui	lding		
Physical data on *window/ro		gal	on Eagton (CE)	ic 175
Facade Orientation facing <u> </u>	west (Podlum)	201	ar Factor (SF)	15 <u>173</u>
Window/Rooflight Code No.	*F ₁ /RL ₁	*F ₂ /RL ₂	*F3/RL3	*F ₄ /RL ₄
Location of *Window/ Rooflight	G/F&1/F unshaded			
Glazing type	plain			
Thickness m	0.012			
Shading Coefficient (SC)	0.90			
Type of shading device	-			
External Shading Multiplier (ESM)	-			
Area of glazing m ²	82.96			
Physical data on *window/ro		-	Solar Factor	
Window/Rooflight Code No.	*F ₁ /RL ₁	*F ₂ /RL ₂	*F3/RL3	*F ₄ /RL ₄
Location of *Window/ Rooflight				
Glazing type				
Thickness m				
Shading Coefficient (SC)				
Type of shading device				

External Shading

Area of glazing

Multiplier

(ESM)

m²

^{*} Delete as appropriate

Calculation of OTTV of Individual Facade in Building Envelope

Sheet No. C	8	BD	Ref	2/	_/	_/
Building address _	Typical Commercial Building				···	
Facade Orientation	facing <u>West (Podium)</u> .					

Opaque *Walls/Roofs

Code No.	Description	*A _w /A _r	U	α	TD _{EQ}	Sum	
Wl	Beams & Cols. G/F&l/F	29.04	1.51	0.58	2.10	53.41	
WlA	Beams & Cols. G/F&1/F	70.50	1.55	0.65	2.10	149.16	
W3	Panels G/F&1/F	156.40	2.41	0.65	4.35	1,065.75	
W 5	Ramp Wall 1/F	27.10	1.97	0.65	2.10	72.87	
	Subtotals	283.04	(A)	He	eat Gain	1,341.19	(

Fenestration

Code No.	Description	*Af _w /Af _r	SC	ESM	SF	Sum	
Fl	G/F & 1/F	82.96	0.90	_	175	13,066.20	
	Subtotals	82.96	(B)	Н	eat Gain	13,066.20	(1

Gross Heat Gain (C + D) 14,407.39Gross Area (A + B) 366.00OTTV = $\frac{C + D}{A + B}$ = 39.36 W/m²

* Delete as appropriate

South	Flovat	ion ((Podium)	
DOULH	nievat	TOHE 1	L P O O 1 UIII /	

Gross Wall Area

264.49 m²

Wall Composite Areas

Beam and Column Areas

G/F = -

1/F 0.6 x 34.6 + 0.6 (3.4 x 8) = 37.08 m² 37.08 m².

1/F Stair Wall 0.1 x 3.4 = 0.34 m² 0.34 m²

Glazing Areas

G/F = -

1/F 100.98 m² 100.98 m²

Ramp

1/F 5.4 x 23.35 = 126.09 m² 126.09 m²

External wall at ramp omitted 5.4 x 40 = 21.60 m^2

Panel Areas

G/F = -

1/F 160.00 - (37.08 + 0.34 + 100.98 + 21.60) = - -

Calculation of 'U' Value of Composite Wall/Roof and Details of Other Values

Sheet No. A9	BD Ref 2//
Building address <u>Typical Commercial Building</u>	
Physical data of Opaque *Wall/Roof	
Facade Orientation facing South (Podium)	Solar Factor (SF) is191

*Wall/Roof Code No	•	*W ₁ /R ₁	*W ₅ /R ₅	*W ₇ /R ₇	*W /R
Location of Wall/Re	oof	Beams & Cols	Ramp 1/F	Stair Wall	
External Finish Ma	terial	1/F white mosaic tiles	r. concrete	1/F white mosaic tiles	· · · · · · · · · · · · · · · · · · ·
Conductivity	W/m°C	1.50	2.16	1.50	
Density	kg/m ³	2500	2400	2500	
Thickness	m	0.005	0.30	0.005	
Absorptivity	(a)	0.58	0.65	0.58	
Intermediate compo	nent	cement render		cement render	
Conductivity	W/m°C	0.72		0.72	
Density	kg/m ³	1860		1860	
Thickness	m	0.01		0.01	
Intermediate compo	nent	Reinforced Concrete		Reinforced Concrete	
Conductivity	W/m°C	2.16		2.16	· · · · · · · · · · · · · · · · · · ·
Density	kg/m ³	2400		2400	
Thickness	m	0.60		3.00	
Intermediate compo	nent				
Conductivity	W/m°C				
Density	kg/m ³				
Thickness	m				
Intermediate compo	nent				
Conductivity	W/m°C				•
Density	kg/m ³				
Thickness	m	white semi g	loss paint		
Internal Finish Ma	terial	on gypsum	plaster		
Conductivity	W/m°C	0.38	0.38		
Density	kg/m ³	1120	1120		
Thickness	m	0.01	0.01		
Absorptivity	α	0.30	0.30		
`U' value of compo *Wall/Roof	site	1.51	1.97	0.69	
Area of *Wall/Roof	m²	37.08	126.09	0.34	
Density of composi *Wall/Roof	te kg/m²	1482	731	7231	
Equivalent tempera difference	ture (TD _{EQ})	1.40	4.10	1.40	

^{*}Delete as appropriate First issue April 1995

Window/Rooflight Schedule

Sheet No. B9			BD Ref	2//
Building address <u>Typical</u>	Commercial Bui	lding		
Physical data on *window/ro	oflight			
Facade Orientation facing <u>S</u>	outh (Podium)	Sol	lar Factor (SF	') is <u>191</u>
Window/Rooflight Code No.	*F1/RL1	*F2/RL2	*F ₃ /RL ₃	*F ₄ /RL ₄
Location of *Window/ Rooflight	1/F unshaded			
Glazing type	plain			
Thickness m	0.012			
Shading Coefficient (SC)	0.90			
Type of shading device	-			
External Shading Multiplier (ESM)	-			
Area of glazing m ²	100.98			
Physical data on *window/ro			Solar Facto	or is
Window/Rooflight Code No.	*F ₁ /RL ₁	*F ₂ /RL ₂	*F ₃ /RL ₃	*F ₄ /RL ₄
Location of *Window/ Rooflight				
Glazing type				
Thickness m				
Shading Coefficient (SC)				
Type of shading device				

External Shading

Area of glazing

Multiplier

(ESM)

m 2

^{*} Delete as appropriate

Calculation of OTTV of Individual Facade in Building Envelope

Sheet No. C 9	BD 1	Ref	2//
Building address <u>Typical Commercial Building</u>			
Facade Orientation facing <u>South (Podium)</u> .			

Opaque *Walls/Roofs

Code No.	Description	*A _w /A _r	U	α	$^{\mathrm{TD}}$ EQ	Sum	
W1 W2 W3	Beams and Cols G/F&1/F Stair Wall 1/F Ramp 1/F	37.08 0.34 126.09	1.51 0.69 1.97	0.58 0.58 0.65	1.40 1.40 4.10*	45.46 0.19 611.98	
	Subtotals	163.51	(A)	Не	eat Gain	657.63	

^{*} Value interpolated from vert. and horizontal components.

Fenestration

Code No.	Description	*Af _w /Af _r	sc	ESM	SF	Sum	
F1	1/F	100.98	0.90	-	191	17,358.46	
<u> </u>	Subtotals	100.98	(B)	H.	l eat Gain	17,358.46	(D)

* Delete as appropriate

Summary of OTTV of Building Envelope

Sheet No. D	1	BD Ref. 2//	′/
Building address	Typical Commercial Bu	uilding	

Total Envelope Heat Gain (*Tower/Podium)

Facade Orientation	Gross Area from Form OTTV3	Gross Heat Gain from Form OTTV3
a. East	344.00	31,629.06
b. North	320.00	22,492.56
c. West	366.00	14,407.39
d. South	264.49	18,016.09
e.		
f.		
Subtotal	1,294.49 (E)	86,545.10 (G)
Roof	Carpark under - no	on accountable
a. Main		
b. 15/F		
Subtotal	(F)	(H)

*Tower/Podium Walls OTTV =
$$\frac{G}{E}$$
 = $\frac{66.86}{E}$ W/m²

*Tower/Podium Roofs OTTV =
$$\frac{H}{F}$$
 = $\frac{W/m^2}{F}$

*Tower/Podium OTTV =
$$\frac{G + H}{E + F}$$
 = _____ W/m²

^{*} Delete as appropriate