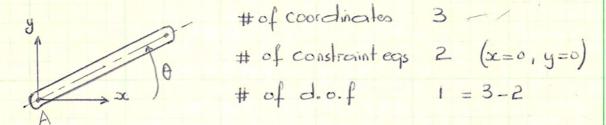
### I Introduction

1. Definitions and Examples

Def: The number of degrees-of-freedom (d.o.f) associated with a given mechanical system is equal to the number of coordinates used to describe its configuration minus the number of independent equations of constraints

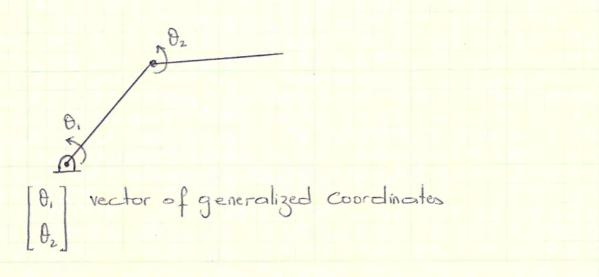
Ex: Planar One-Link-Robot

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Def: Any set of parameters which gives an unambiguous representation of the configuration of the system will serve as a system of coordinates in a more general sense. These parameters are known as generalized coordinates.

Ex: Planor Two-Link robot



Owban Amban

### 2. Eulez Lagrange Equations

A very well known method for deriving the dynamic equations of mechanical systems is by using the Euler-Lagrange equations

[in] acting on the system.

(n-d.o.f) robot manipulators have two special features:

- . The potential energy P=P(9) is independent of 9
- . The kinetic energy is a quadratic function of q

where D(9) is an nxn matrix called the inertia matrix.

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The inertia matrix D(q) has two properties:

- . D(q) is symmetric: dij(q) = dii(q) + q eR" i,j=1,...,n
- D(9) is positive definite (PD): xTD(9) x >0 ∀x≠0, ∀q∈R°, or equivalently all eigenvalues of D(9), Ai(9) >0 ∀q∈R° i=1,-,n

We now derive the Euler - Lagrange equations as follows:

$$L = K - P$$

$$= \frac{1}{2} \sum_{i=1}^{n} \sum_{j=1}^{n} d_{ij}(q) \dot{q}_{i} \dot{q}_{j} - P(q)$$

$$\frac{\partial L}{\partial \dot{q}_{k}} = \sum_{j=1}^{n} d_{kj}(q) \dot{q}_{j}$$

$$\frac{1}{Jt} \frac{\partial L}{\partial \dot{q}_{k}} = \sum_{j=1}^{n} d_{kj} (q) \overset{\circ}{q}_{j} + \sum_{j=1}^{n} \frac{1}{Jt} d_{kj} (q) \overset{\circ}{q}_{j} \\
= \sum_{j=1}^{n} d_{kj} (q) \overset{\circ}{q}_{j} + \sum_{i=1}^{n} \sum_{j=1}^{n} \frac{1}{2} \frac{1$$

Hence, the Euler-Lagrange equations can be written as follows

$$\sum_{j=1}^{n} d_{kj}(q) \ddot{q}_{j} + \sum_{i=1}^{n} \sum_{j=1}^{n} \left[ \frac{\partial d_{kj}(q)}{\partial q_{i}} - \frac{1}{2} \frac{\partial d_{ij}}{\partial q_{k}} \right] \dot{q}_{i} \ddot{q}_{j} + \frac{\partial P}{\partial q_{k}} = \mathcal{T}_{k}$$

$$k = 1, \dots, n.$$

No that

$$\sum_{i=1}^{n} \sum_{j=1}^{n} \frac{\partial d_{kj}}{\partial q_{i}} \dot{q}_{i} \dot{q}_{j} = \frac{1}{2} \sum_{i=1}^{n} \sum_{j=1}^{n} \left\{ \frac{\partial d_{kj}}{\partial q_{i}} + \frac{\partial d_{ki}}{\partial q_{j}} \right\} \dot{q}_{i} \dot{q}_{j} \quad \text{why?}$$

It follows that

$$\sum_{i=1}^{n} \sum_{j=1}^{n} \left\{ \frac{\partial d_{kj}}{\partial q_{i}} - \frac{1}{2} \frac{\partial d_{kj}}{\partial q_{k}} \right\} \dot{q}_{i} \dot{q}_{j}$$

$$= \sum_{i=1}^{n} \sum_{j=1}^{n} \frac{1}{2} \left\{ \frac{\partial d_{kj}}{\partial q_{i}} + \frac{\partial d_{ki}}{\partial q_{j}} - \frac{\partial d_{kj}}{\partial q_{k}} \right\} \dot{q}_{i} \dot{q}_{j}$$

The coefficients

one known as Christoffel symbols.

Now set 
$$Q_k = \frac{\partial P}{\partial q_k}$$

Then the equations of motion, the Euler-Lagrange equations, can be written as

$$\sum_{j=1}^{n} d_{kj}(q) \ddot{q}_{j} + \sum_{i=1}^{n} \sum_{j=1}^{n} C_{ijk}(q) \ddot{q}_{i} \dot{q}_{j} + \Phi_{k}(q) = t_{k}, k=1,2,..,n$$

There are three types of terms in this equation

- Terms involving the second derivative of the generalized coordinates
- Quadratic terms in the first derivatives of q where the coefficients may depend on q. These are further classified into two types

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- Terms involving a product of the type 92 are called centrifugal

\_Terms involving a product of the type qiqi where i +j are called Coriolis terms

- Terms involving only q but not q. These arise from differentiating the potential energy.

We commonly write the equations of motion in matrix form as follows

where the elements a of the matrix C(9,9) are defined here as

$$Ck_{j} = \sum_{i=1}^{c} C_{ijk}(q) \dot{q}_{i}$$

$$= \sum_{i=1}^{c} \frac{1}{2} \left\{ \frac{\partial dk_{j}}{\partial q_{i}} + \frac{\partial dk_{i}}{\partial q_{j}} - \frac{\partial dk_{j}}{\partial q_{k}} \right\} \dot{q}_{i}$$

Note: Other choices of the C(q,q) matrix are possible.

4. Fundamental Properties of the Equations of Motion

The equations of motion are generally complex nonlinear equations but they have several fundamental properties which are exploited to facilitate control system design.

Property 1:

The inertia matrix D(q) is symmetric, positive definite, and both D(q) and D'(q) are bounded as a function of  $q \in \mathbb{R}^n$ .

Properly 2: In general There is an independent control input for each d.o.f.

Properly 3:

All of the constant parameters of interest such as link masses, moments of inertia, etc., appear as coefficients of known functions of the generalized coordinates. By defining each coefficient as a separate parameter, a linear relationship results so that we may write the dynamic equations as

 $D(9)\ddot{q} + C(9,\dot{q})\dot{q} + g(9) = \gamma(9,\dot{q},\ddot{q})\theta = \tau$ where

Y(9,9,9) is an nxr matrix of known functions, known as the regressor and D is an r-dimensional vector of parameters.

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### Aside:

Daf: A matrix S is said to be skew symmetric iff:

$$5^{T}+S=0$$

S is skew symmetric with components Sij, I If
Sij + Sji = 0 i.e. Sij = - Sji

Notethat: S is skew symmetric > x Sx = 0 +x

HW: Prove (\*)

Property 4:

Define the matrix N(9,9) = D(9) -2 C(9,9).

Then N(9,9) is skew symmetric, i.e. the components Tik of

N(9,9) satisfy Mik = - Mkj

Proof: Given the inextia matrix D(q), the kith component of D(q) is given by the chain rule as

Therefore, the kith component of N=D-2C is given by  $n_k = d_{kj} - 2 c_{kj}$ 

It follows that 
$$\Pi_{jk} = \sum_{i=1}^{n} \left[ \frac{\partial d_{ik}}{\partial q_{j}} - \frac{\partial d_{ii}}{\partial q_{k}} \right] \dot{q}_{i}$$

$$= \sum_{i=1}^{n} \left[ \frac{\partial d_{ki}}{\partial q_{j}} - \frac{\partial d_{ij}}{\partial q_{k}} \right] \dot{q}_{i} \quad \text{(used symmetry of D(q))}$$

$$= -\Pi_{kj}$$

Remark 1:

$$N(q,\dot{q}) = \dot{D}(q) - 2C(q,\dot{q})$$
 is skew symmetric

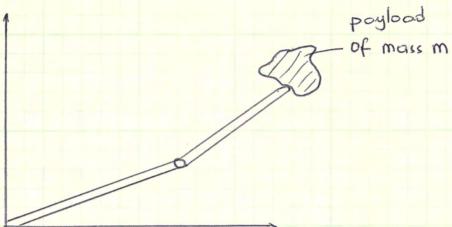
$$\Rightarrow \qquad \qquad \mathring{q}^{T} \left[ \mathring{D}(q) - 2C(q, \mathring{q}) \right] \mathring{q} = 0$$

Remark 2:

It turns out that it is always true that gr [D-2C]g=0

no matter how C is chosen. However [D-2C] is skew-symmetric only in the case the C matrix is as defined aarlier.

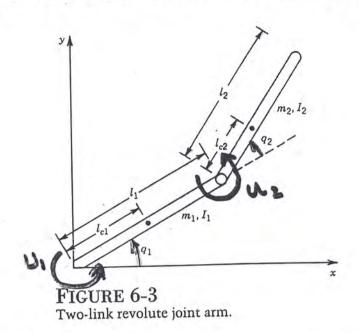
HW: Suppose all the system ponometers in the 2 d.o.f planer manipulator are completely known. Suppose now that we attack an unknown payload of mass m to the tip of the second link



Write the equations of motions in the following form

where Y, D, and Yz one known and Oz is a vector of unknown ponometers

## Example: A two d.o.f Planar Manipulator



$$M\ddot{\mathbf{q}} + C\dot{\mathbf{q}} + \mathbf{g} = \mathbf{u}$$

$$\mathbf{q} = \left[egin{array}{c} q_1 \ q_2 \end{array}
ight], \quad \ \mathbf{u} = \left[egin{array}{c} u_1 \ u_2 \end{array}
ight]$$

$$C_i \triangleq Cos(q_i)$$
  
 $S_i \triangleq S_{in}(q_i)$   
 $C_{ij} \triangleq Cos(q_i+q_i)$ 

$$M = \left[ \begin{array}{c|c} m_1 l_{c_1}^2 + m_2 (l_1^2 + l_{c_2}^2 + 2 l_1 l_{c_2} C_2) + I_1 + I_2 \\ \hline m_2 (l_{c_2}^2 + l_1 l_{c_2} C_2) & \hline \end{array} \right] \begin{array}{c|c} m_2 (l_{c_2}^2 + l_1 l_{c_2} C_2) + \overline{I_2} \\ \hline \end{array}$$

$$C = \begin{bmatrix} -m_2 l_1 l_{c_2} S_2 \dot{q}_2 & -m_2 l_1 l_{c_2} S_2 (\dot{q}_2 + \dot{q}_1) \\ m_2 l_1 l_{c_2} S_2 \dot{q}_1 & 0 \end{bmatrix}$$

$$\mathbf{g} = \left[ egin{array}{c} (m_1 l_{c_1} + m_2 l_1) g C 1 + m_2 l_{c_2} g C_{12} \\ m_2 l_{c_2} C_{12} \end{array} 
ight].$$

#### Note that

$$\dot{M} - 2C = \begin{bmatrix} 0 & m_2 l_1 l_{c_2} S_2(\dot{q}_2 + 2\dot{q}_1) \\ -m_2 l_1 l_{c_2} S_2(\dot{q}_2 + 2\dot{q}_1) & 0 \end{bmatrix}$$

which is skew symmetric

# Example: A two d.o.f Planar Manipulator (Continued)

Define

$$egin{array}{ll} heta_1 &= m_1 l_{c_1}^2 & heta_4 &= m_2 l_1 l_{c_2} & heta_7 &= m_1 l_{c_1} g \ heta_2 &= m_2 l_1^2 & heta_5 &= I_1 & heta_8 &= m_2 l_1 g \ heta_3 &= m_2 l_{c_2}^2 & heta_6 &= I_2 & heta_9 &= m_2 l_{c_2} g \end{array}$$

 $\Rightarrow$ 

- choice of parameters in above is not unique and dimension of parameter space may depend on particular choice of parameters
- some of the parameters may be known

Example: Inverted Pendulum (M+m) = + mlast 0 \_ mlosing = u mlcosd i + ml2 0 - melsing =0  $\begin{bmatrix} M+m & ml\cos\theta \end{bmatrix} \begin{bmatrix} \dot{s}\dot{c} \\ ml\cos\theta & ml^2 \end{bmatrix} \begin{bmatrix} \dot{o} \\ \dot{\theta} \end{bmatrix} + \begin{bmatrix} 0 & -ml\theta\sin\theta \end{bmatrix} \begin{bmatrix} \dot{s}\dot{c} \\ \dot{\theta} \end{bmatrix} + \begin{bmatrix} -mgl\sin\theta \end{bmatrix} \begin{bmatrix} 0 \\ 0 \end{bmatrix}$ D(9) Symmetric [M+n)ml2-ml2639 (Mml2 VP. d: 1 1 = [M+n)ml2-ml2639 (Mml2  $\begin{array}{c} \left( \overrightarrow{D} - 2 \overrightarrow{C} \right) = \begin{bmatrix} 0 & -m (\partial S in \theta) \\ -m (\partial S in \theta) \end{bmatrix} - 2 \begin{bmatrix} 0 & -m (\partial S in \theta) \\ -m (\partial S in \theta) \end{bmatrix} \end{array}$ = [-mlåsma o] Sken Symmetris D(9)9 = 70 (9,9) 00  $D(9)\ddot{0} = \left[ (M+m)\ddot{x} + ml\cos\theta \dot{\theta} \right] = \left[ \ddot{x} \cos\theta \dot{\theta} \right] = \left[ M+m \cos\theta \dot{x} + ml\cos\theta \dot{x} \right]$ · C(919)9 = Ye De  $= \begin{bmatrix} -ml \hat{\theta}^2 s m \theta \end{bmatrix} = \begin{bmatrix} -\hat{\theta}^2 s m \theta \end{bmatrix} ml$   $\frac{1}{\theta c}$  $9(9) = \frac{1}{3} \cdot \frac{1}{3} = \frac{1}{3}$ Henre

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Heno,
$$D(q)\ddot{q} + C(q,\dot{q})\dot{q} + g(q) = Y_{d}(q,\dot{q})\partial_{0} + Y_{c}(q,\dot{q})\partial_{c} + Y_{g}(q)\partial_{g} = Y(q,\dot{q},\dot{q})\partial_{0}$$

$$[\ddot{x} \quad cos\theta\dot{\partial}_{-}\dot{\theta}_{s}^{*}\sin\theta \quad 0 \quad 0][M+m]$$

$$[o \quad cos\theta\dot{x} \quad \ddot{\theta} \quad -\sin\theta][m]^{2}$$

$$[mg]$$

J 1 + m



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Given a constant matrix A E R", The norm of a matrix, denoted | All is a measure of the size of A. We can define many norms. In porticular the so-called 2-norm >min(A) < |A||<sub>2</sub> = √ \lambda max [ATA] < \lambda max [A]

For a positive definite matrix (i.e hi >0 or all minors one >0)

i) 0 < \(\lambda\_{\text{min}}(A)\)

λmax(A) <∞

IF A = A(sc) where \$ x EIR, then

 $(ic)_{nim} k = nim k (i)$ 

Amax = Amax (31)

ii) Amax (x) < 00

iii) if A(x) is positive definite then

Def: A(x) is bounded if all element of A are bounded => Amax (x) < 00 Def: A(a) is uniformly positive definite if I a constant c>0 s.t.

 $0 < c < \sigma_{(\alpha)} \leq ||A||_2 \quad \forall x \in \mathbb{R}$