

16 - The Rocket Equation, Chemical Propulsion, and Staging

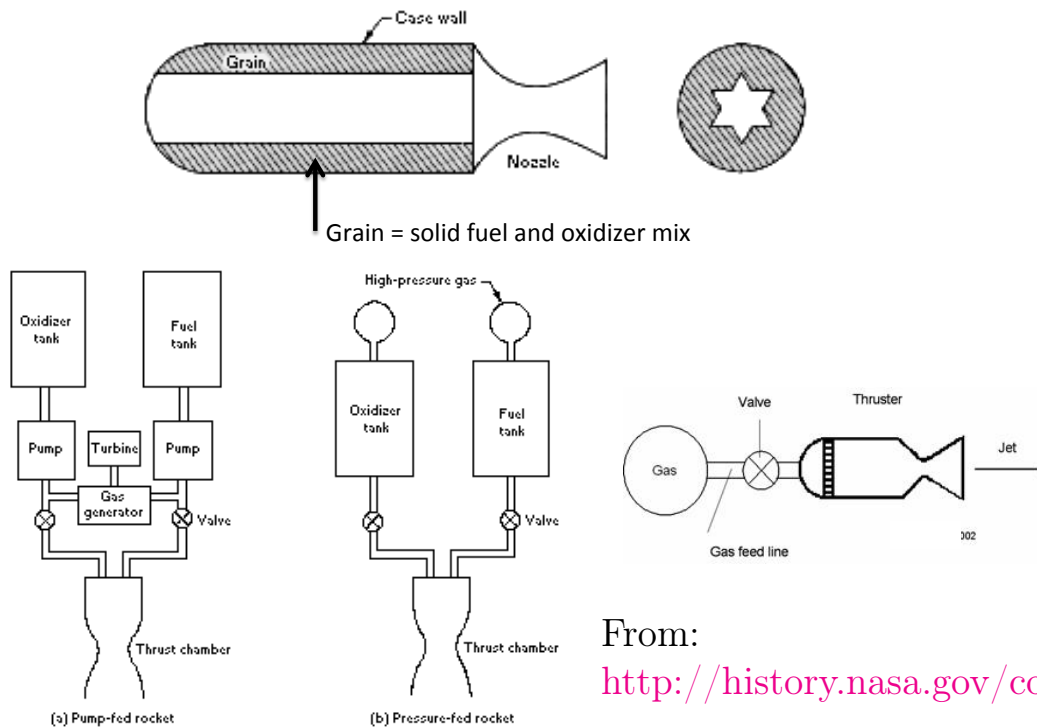
Dmitry Savransky

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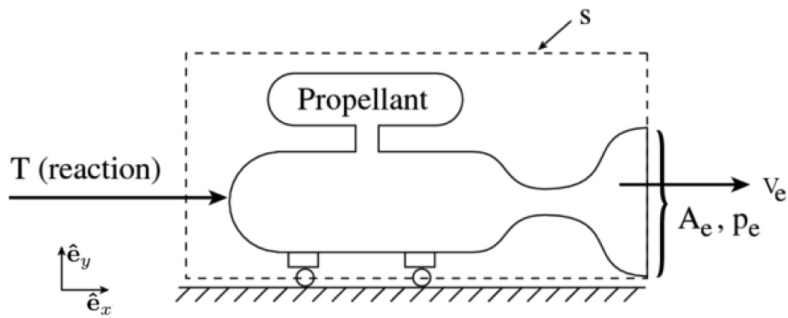
MAE 4060

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Chemical Rockets



Rocket Propulsion



From: <http://web.mit.edu/16.unified/www/FALL/thermodynamics/notes/node77.html>

$$\Delta \mathbf{p} = \dot{m} V_e$$

Change in Momentum Nozzle Exit Velocity
Mass Flow Rate

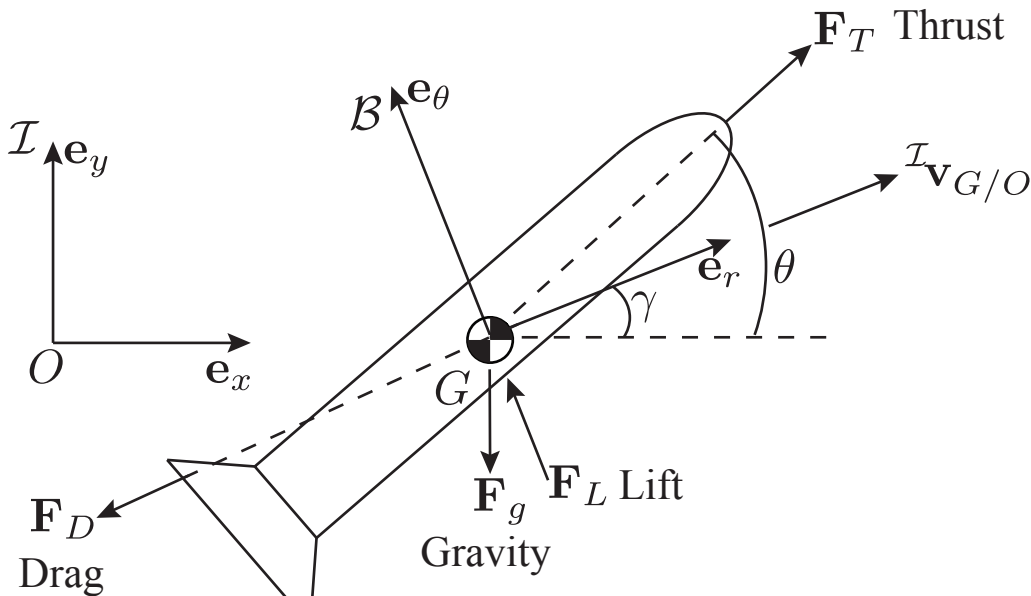
$$\sum \mathbf{F} \cdot \hat{\mathbf{e}}_x = T - A_e(p_e - p_a)$$

Thrust Force Nozzle Exit Ambient
Magnitude Exit Area Pressure Pressure

$$F_T = \dot{m} V_e + A_e(p_e - p_a)$$

$$v_{\text{eff}} \triangleq \frac{F_T}{\dot{m}} = V_e + \frac{A_e}{\dot{m}}(p_e - p_a)$$

Rocket Forces



NB: Rocket mass (m) is **not** constant

$$m \mathbf{a}_{G/O} = \sum \mathbf{F} = \mathbf{F}_g + \mathbf{F}_L + \mathbf{F}_D + \mathbf{F}_T$$

$$= -mg\mathbf{e}_y + F_L\mathbf{e}_\theta - F_D\mathbf{e}_r + F_T(\cos(\theta - \gamma)\mathbf{e}_r + \sin(\theta - \gamma)\mathbf{e}_\theta)$$

The Tsiolkovsky (Ideal) Rocket Equation

$$\mathcal{I}\mathbf{a}_{G/O} = \frac{\mathcal{B}}{dt} \underbrace{\mathcal{I}\mathbf{V}_{G/O}}_{\equiv v\mathbf{e}_r} + \underbrace{\mathcal{I}\boldsymbol{\omega}^{\mathcal{B}}}_{\equiv \dot{\gamma}\mathbf{e}_3} \times \underbrace{\mathcal{I}\mathbf{V}_{G/O}}_{\equiv v\mathbf{e}_r} = \frac{dv}{dt}\mathbf{e}_r + v\frac{d\gamma}{dt}\mathbf{e}_\theta$$

$$\mathbf{e}_r : \quad \frac{dv}{dt} = -g \sin \gamma - \frac{F_D}{m} + \frac{F_T}{m} \cos(\theta - \gamma)$$

$$\mathbf{e}_\theta : \quad v \frac{d\gamma}{dt} = -g \cos \gamma + \frac{F_L}{m} + \frac{F_T}{m} \sin(\theta - \gamma)$$

$$\Delta v \triangleq v(t_f) - v(t_0) = \int_{t_0}^{t_f} \left[-g \sin \gamma - \frac{F_D}{m} + \frac{F_T}{m} \cos(\theta - \gamma) \right] dt$$

Assuming gravity and drag are negligible:

$g = 0, F_D = 0, \theta = \gamma$, and v_{eff} is constant:

$$\Delta v = \int_{t_0}^{t_f} \frac{F_T}{m} dt = v_{\text{eff}} \int_{t_0}^{t_f} \frac{\dot{m}}{m} dt = -v_{\text{eff}} \int_{m_0}^{m_f} \frac{dm}{m}$$

$$\Delta v = v_{\text{eff}} \ln \left(\frac{m_0}{m_f} \right)$$

Specific Impulse

Assuming Constant Thrust
and Mass Flow Rate

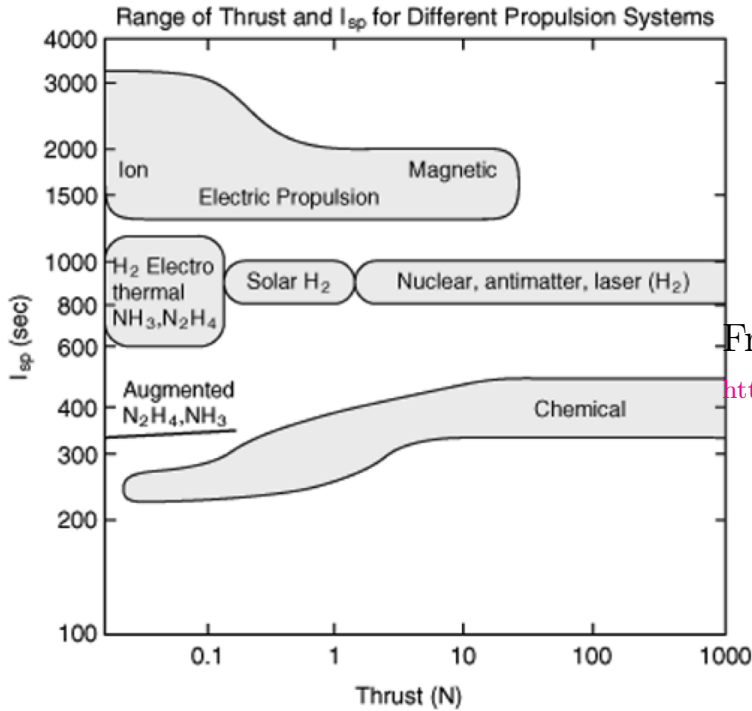
$$I_{sp} = \frac{1}{w_p} \overbrace{\int_{t_0}^{t_f} F_t dt}^{\text{Total Impulse}} = \frac{F_T}{\dot{m}g_0} = \frac{v_{\text{eff}}}{g_0}$$

Propellant Weight
“Standard Gravity”: Gravity at Earth’s Surface. $g_0 = 9.80665 \text{ m/s}^2$

$$\Delta v = I_{sp} g_0 \ln \left(\frac{m_0}{m_f} \right)$$

$$m_0 - m_f = m_0 \left(1 - e^{-\frac{\Delta v}{I_{sp} g_0}} \right)$$

Efficiency vs. Thrust

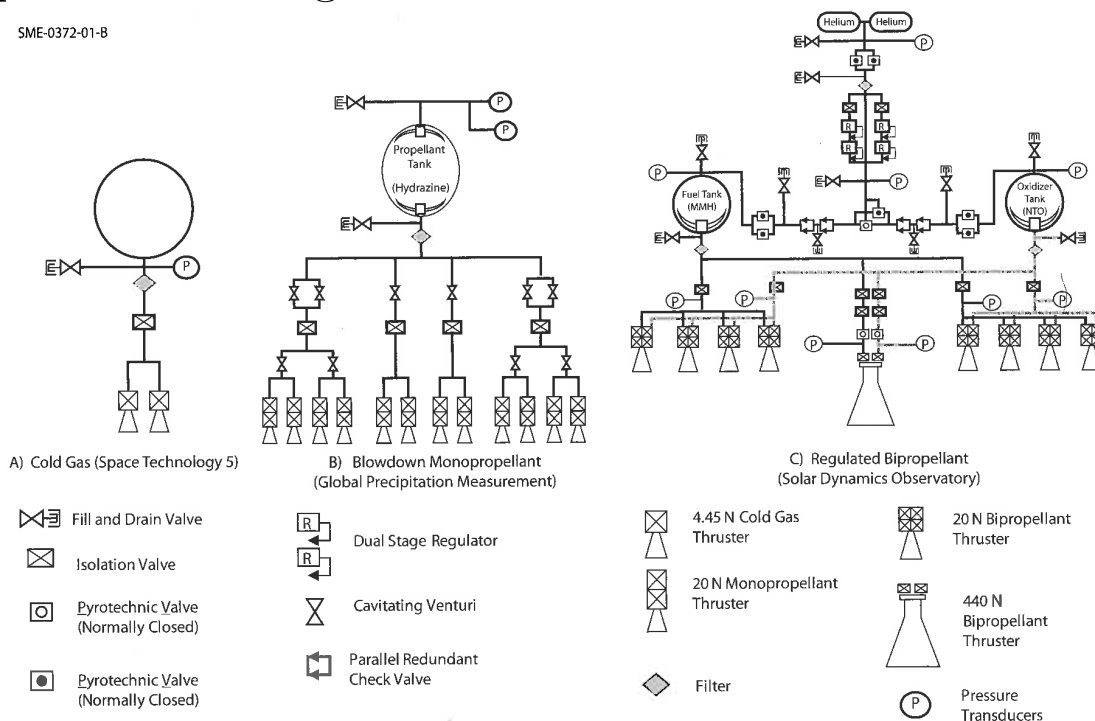


From:

http://dawn.jpl.nasa.gov/mission/ion_prop.asp

Space Plumbing

SME-0372-01-B



SMAD-SME
Fig. 8-18

An Illustrative Example

- You wish to launch an H₂-O₂ rocket ($v_{\text{eff}} = 4000 \text{ m/s}$) to a 600 km circular orbit:

$$\Delta v = v_{\text{circ}} = \sqrt{\frac{\mu}{r}} = \sqrt{\frac{3.986 \times 10^{14} \text{ m}^3\text{s}^{-2}}{600\text{km} + 6371\text{km}}} \approx 7.5\text{km/s}$$

- Typically require an additional 1.5 km/s for atmospheric drag and gravity compensation for a total of 9 km/s

$$\Delta v = v_{\text{eff}} \ln \left(\frac{m_0}{m_f} \right) \Rightarrow \frac{m_0}{m_f} = e^{\Delta v / v_{\text{eff}}} \approx 9.5$$

- Your rocket must be 89.5% fuel by mass (and we still haven't even included all other losses)

Staging

$$\Delta v = \sum_{i=1}^n \Delta v_i = \sum_{i=1}^n v_{\text{eff}_i} \ln \left(\frac{m_{0_i}}{m_{f_i}} \right)$$

- m_{0_i} : Total mass before stage i ignition
- m_{f_i} : Total mass after stage i fuel expended but **before** stage i separation

If all stages have the same effective exhaust velocity:

$$e^{\Delta v / v_{\text{eff}}} = \prod_{i=1}^n \frac{m_{0_i}}{m_{f_i}}$$

Stages can be optimized for thrust, or efficiency, or maximized payload mass

Another Illustrative Example

Consider a 2-stage rocket with a 6000 m/s Δv requirement and 4500 kg total launch mass. Both stages have the same thrusters: 300 s I_{sp} , 3000 m/s v_{eff} , and 0.88 fuel mass fraction (ξ). m_1, m_2 are the stage wet masses (with fuel).

$$m_{0_1} = m_1 + m_2 + m_{\text{payload}}$$

$$m_{0_2} = m_2 + m_{\text{payload}}$$

$$m_{f_1} = m_1(1 - \xi) + m_2 + m_{\text{payload}}$$

$$m_{f_2} = m_2(1 - \xi) + m_{\text{payload}}$$

Equal Mass Stages

$$m_1 = m_2 \triangleq m \quad m_{\text{tot}} = 2m + m_{\text{payload}}$$

$$c \triangleq e^{\Delta v / v_{\text{eff}}}$$

$$= \frac{m_{\text{tot}}}{m(1 - \xi) + m + m_{\text{payload}}} \left(\frac{m + m_{\text{payload}}}{m(1 - \xi) + m_{\text{payload}}} \right)$$

$$m_{\text{payload}} =$$

$$\frac{m_{\text{tot}}}{c\xi(\xi + 1)} \left(c(\xi^2 - \xi - 1) + \sqrt{c^2 + 4c\xi^2 - 2c + 1} + 1 \right)$$

$$\approx 300 \text{ kg}$$

Equal Mass-Ratio Stages

$$\frac{m_{0_1}}{m_{f_1}} = \frac{m_{0_2}}{m_{f_2}} \quad m_{\text{tot}} = m_1 + m_2 + m_{\text{payload}}$$

$$\frac{m_{\text{tot}}}{m_{\text{tot}} - \xi m_1} = \frac{m_2 + m_{\text{payload}}}{m_2(1 - \xi) + m_{\text{payload}}}$$

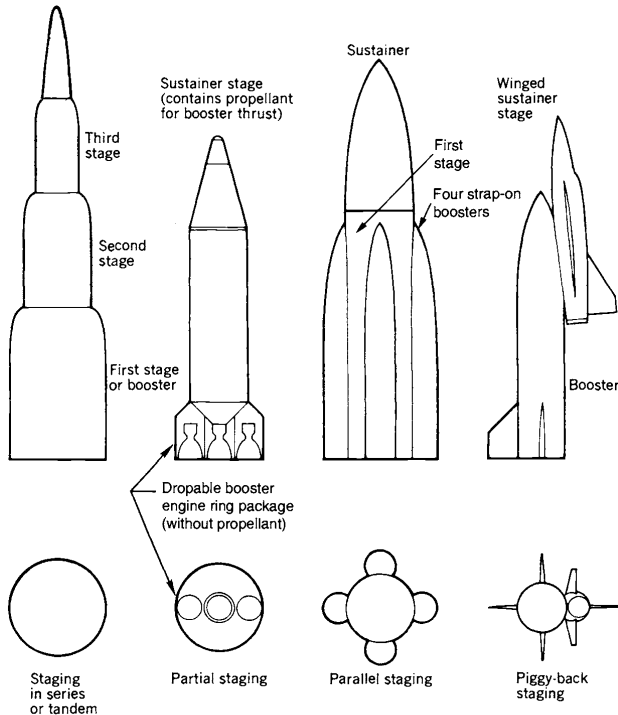
$$c \triangleq e^{\Delta v / v_{\text{eff}}} = \left(\frac{m_{\text{tot}}}{m_{\text{tot}} - m_1 \xi} \right)^2$$

$$m_{\text{payload}} = \frac{m_{\text{tot}}}{c^2 \xi^2} \left(c^2(\xi^2 - 2\xi + 1) + c + 2\sqrt{c^3}(\xi - 1) \right)$$

$$\approx 357 \text{ kg}$$

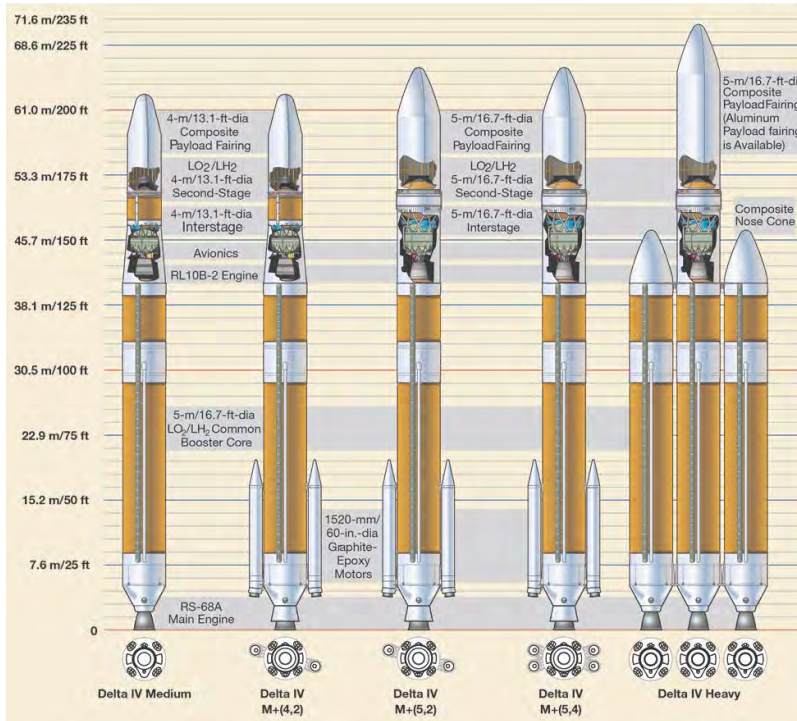
$\sim 20\% \text{ Gain!}$

Staging Options



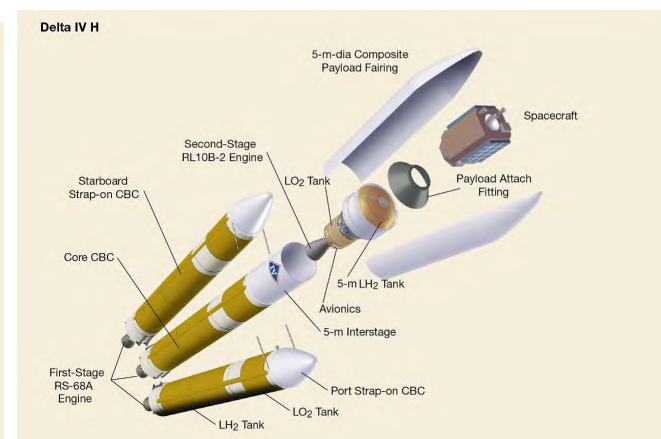
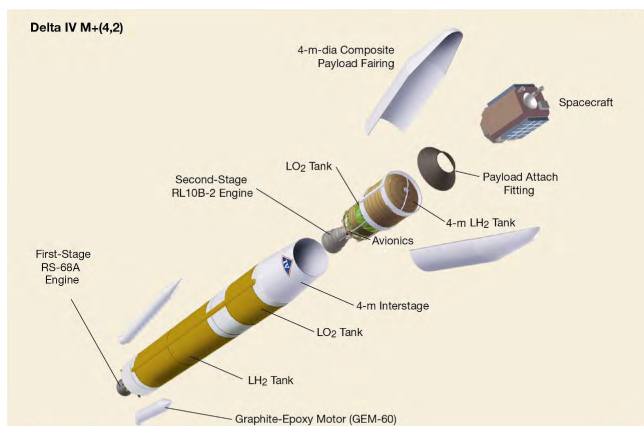
Sutton and Biblarz (2001) Fig. 4-14

Delta IV Configurations



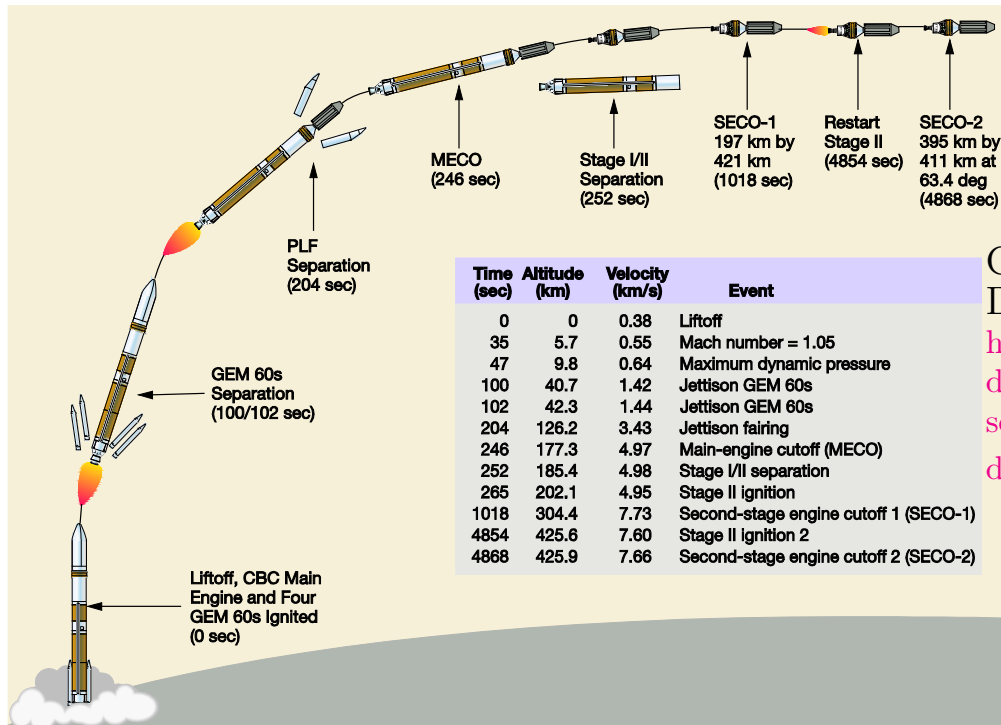
Credit: ULA
 Delta IV User's Guide
<https://www.ulalaunch.com/docs/default-source/rockets/delta-iv-user's-guide.pdf>

Delta IV Configurations



Credit: ULA, Delta IV User's Guide
<https://www.ulalaunch.com/docs/default-source/rockets/delta-iv-user's-guide.pdf>

Delta IV LEO Mission Profile



Credit: ULA
Delta IV User's Guide
<https://www.ulalaunch.com/docs/default-source/rockets/delta-iv-user's-guide.pdf>