


Linear Matrix Inequalities

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Optimaliseringsbasert reguleringsdesign og analyse
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What are LMIs?

- A set of matrix-valued inequalities that are linear (or affine) in a set of variables
- Many design/analysis problems in control engineering can be formulated as LMIs
 - Natural connection to quadratic Lyapunov functions, energy storage functions, etc.
- Can be used to formulate problems involving several matrix variables
 - Different structures can be imposed on the matrix variables

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LMIs

- Unite many previous results in a common framework
 - H_∞ control design
 - H_2 control design
 - Mixed H_∞/H_2 control design
 - Pole placement
 - Robust MPC
 - ...
- These will not be presented (in any detail) here, see references if interested

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Definite matrices and sign-definite quadratic functions

- A real-valued, square, symmetric matrix is said to be positive definite if

$$x^T Q x > 0 \quad \forall x \neq 0$$
 - Positive semi-definite with \geq instead of $>$
 - Extension to complex-valued matrices is of less interest here
- Common to write $Q > 0$ ($Q \geq 0$) to indicate that a matrix is positive (semi-)definite.
 - Occasionally $> (\geq)$ is used to distinguish from sign-definiteness of the elements of Q .
 - $P > Q$ means $(P - Q) > 0$
- If Q is positive definite, $P = -Q$ is negative definite

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Definite matrices

- Any square matrix W can be decomposed into a symmetric and a skew-symmetric part

$$W = \left(\frac{W + W^T}{2} \right) + \left(\frac{W - W^T}{2} \right)$$
- Only the symmetric part contributes to the value of a quadratic function
 - I.e., when considering quadratic functions, it is non-restrictive to only consider symmetric matrices

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Some LMI basics

- Basic structure of an LMI


$$F(p) = F_0 + \sum_{i=1}^m p_i F_i > 0$$
- Several LMIs combine into one big LMI by simple diagonal augmentation

$F(p) > 0, G(p) > 0, \dots$
is equivalent to

$$\begin{bmatrix} F(p) & 0 & 0 \\ 0 & G(p) & 0 \\ 0 & 0 & \ddots \end{bmatrix} > \begin{bmatrix} 0 \\ 0 \\ \vdots \end{bmatrix}$$

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Types of LMI problems

- LMI feasibility problem
 - Is $\dot{x} = Ax$ stable?
 - Valid Lyapunov function $V(x) = x^T P x$, if there exists $P > 0$ such that $A^T P + P A < 0$
 - Formulated as an LMI:

$$\begin{bmatrix} A^T P + P A & 0 \\ 0 & -P \end{bmatrix} < 0$$

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Types of LMI problems


- Convex function minimization with LMI constraints
 - LMI constraints are convex, giving a convex overall problem
 - Consider the system

$$\begin{aligned} \dot{x} &= Ax + Bw \\ z &= Cx + Dw \end{aligned}$$
 - H_∞ norm of transfer function from w to z calculated from $\min \gamma$
 - s.t.

$$\begin{bmatrix} A^T P + P A & P B & C^T \\ B^T P & -\gamma I & D^T \\ C & D & -\gamma I \end{bmatrix} < 0$$

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Software for LMIs

- LMIs have appeared in control theory since the '60s or '70s
- Lots of developments in the '90s
- 'Reasonably' user friendly software have made these techniques fairly accessible since the 2000s.
- LMItools – integrated into Matlab Robust Control Toolbox
 - Some illustrations of use in Skogestad & Postlethwaite, Ch. 12.
- YALMIP
 - <http://users.isy.liu.se/johanl/yalmip/>
 - Integrated with Matlab
 - Need semidefinite programming solvers. Some available as freeware
 - SeDuMi <http://users.isy.liu.se/johanl/yalmip/pmwiki.php?n=Solvers.SEDUMI>
 - SDPT3 <http://users.isy.liu.se/johanl/yalmip/pmwiki.php?n=Solvers.SDPT3>
 - MOSEK <https://www.mosek.com/>

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LMI tricks – change of variables

- New variables may sometimes 'linearize' the problem.
- State feedback design problem. Find $u = Kx$ such that the closed loop is stable. Need to find $P > 0$ and K such that

$$(A + BK)^T P + P(A + BK) < 0$$
- Not an LMI due to nonlinear terms with products of P and K .
- Pre- and postmultiplication with $Q = P^{-1}$ does not change sign definiteness (see next slide). Pre- and postmultiplication with Q gives


$$QA^T + AQ + QK^T B^T + BKQ < 0$$
- Define $L = KQ$ to obtain

$$QA^T + AQ + L^T B^T + BL < 0$$

which is an LMI in $Q > 0$ and L . Furthermore, since Q is full rank, P and K can always be recovered from Q and L .

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LMI tricks – congruence transform

- If W is full rank, sign definiteness is not changed by pre-multiplication with W^T and post-multiplication by W . I.e.,

$$Q > 0 \Leftrightarrow W^T Q W > 0 \text{ for full rank } W$$
- Consider

$$Q = \begin{bmatrix} A^T P + PA & PBK + C^T V \\ * & -2V \end{bmatrix} < 0$$

in matrix variables $P > 0, V > 0$ and K .
- Choose the following full-rank W :


$$W = \begin{bmatrix} P^{-1} & 0 \\ 0 & V^{-1} \end{bmatrix}$$

$$W^T Q W = \begin{bmatrix} XA^T + AX & BL + XC^T \\ * & -2U \end{bmatrix}$$

which is an LMI in $X = P^{-1}, U = V^{-1}$, and $L = KV^{-1}$

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LMI tricks – Schur complement

- The following are equivalent

$$\Phi = \begin{bmatrix} \Phi_{11} & \Phi_{12} \\ \Phi_{12}^T & \Phi_{22} \end{bmatrix} < 0$$

and

$$\Phi_{22} < 0$$

$$\Phi_{11} - \Phi_{12} \Phi_{22}^{-1} \Phi_{12}^T < 0$$
- Riccati inequality: Given $Q \geq 0, R > 0$ find $P > 0$ such that


$$A^T P + PA + PBR^{-1}B^T P + Q < 0$$

From the Schur complement, and noting that $-R < 0$, this is equivalent to

$$\begin{bmatrix} A^T P + PA + Q & PB \\ * & -R \end{bmatrix} < 0$$

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LMI tricks – S-procedure

- Occasionally a criterion cannot be fulfilled globally – but we need it to be fulfilled in some region defined by the sign of some function.
- For example, we may want $F_0(x) \leq 0$ whenever $F_i(x) \geq 0$. This is fulfilled, provided

$$F_{aug}(x) = F_0(x) + \sum_{i=1}^q \tau_i F_i(x) \leq 0, \quad \tau_i \geq 0$$
- Note that $F_{aug}(x) \geq F_0(x)$ wherever $F_i(x) \geq 0, \forall i$
- $F_{aug}(x)$ is linear in τ_i .
- The S-procedure is generally conservative, except when $q = 1$.

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S-procedure example

- Find $P > 0$ such that


$$\begin{bmatrix} x \\ z \end{bmatrix}^T \begin{bmatrix} A^T P + PA & PB \\ * & 0 \end{bmatrix} \begin{bmatrix} x \\ z \end{bmatrix} < 0$$
 whenever

$$z^T z \leq x^T C^T C x \Leftrightarrow \begin{bmatrix} x \\ z \end{bmatrix}^T \begin{bmatrix} C^T C & 0 \\ * & -I \end{bmatrix} \begin{bmatrix} x \\ z \end{bmatrix} \geq 0$$
- From the S-procedure, we get

$$\begin{bmatrix} x \\ z \end{bmatrix}^T \begin{bmatrix} A^T P + PA + \tau C^T C & PB \\ * & -\tau I \end{bmatrix} \begin{bmatrix} x \\ z \end{bmatrix} < 0$$
 which is an LMI in $P > 0$ and $\tau \geq 0$.

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LMI tricks – Projection Lemma

- In some control problems, the following type of inequalities appear

$$\Psi(X) + G(X)\Lambda H^T(X) + H(X)\Lambda^T G^T(X) < 0$$
 where X and Λ are the matrix variables. $\Psi(\cdot)$, $G(\cdot)$ and $H(\cdot)$ are normally affine functions of X .
- The above inequality is satisfied, for some X , if and only of

$$W_{G(X)}^T \Psi(X) W_{G(X)} < 0$$


$$W_{H(X)}^T \Psi(X) W_{H(X)} < 0$$
 Where $W_{G(X)}$ and $W_{H(X)}$ are orthogonal complements to G and H , respectively, i.e.

$$W_{G(X)} G(X) = 0, \text{rank}(W_{G(X)}) + \text{rank}(G) = n$$

$$W_{H(X)} H(X) = 0, \text{rank}(W_{H(X)}) + \text{rank}(H) = n$$

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LMI tricks – Finsler's Lemma

- In some control problems, the following type of inequalities appear


$$\Psi(X) + G(X)\Lambda H^T(X) + H(X)\Lambda^T G^T(X) < 0$$
 where X and Λ are the matrix variables. $\Psi(\cdot)$, $G(\cdot)$ and $H(\cdot)$ are normally affine functions of X .
- This is equivalent to the following two inequalities

$$\Psi(X) - \sigma G(X)G(X)^T < 0$$

$$\Psi(X) - \sigma H(X)H(X)^T < 0$$
 for some real σ

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Example, Projection Lemma

- State feedback design problem

$$(A + BK)^T P + P(A + BK) < 0, P > 0$$
 transformed to


$$QA^T + AQ + L^T B^T + BL < 0, Q > 0$$
- Eliminate L using projection lemma:

$$W_B^T (AQ + QA^T) W_B < 0, Q > 0$$

$$W_I^T (AQ + QA^T) W_I < 0, Q > 0$$
- However, since the identity matrix is full rank, the second inequality is superfluous (in this case).
- First inequality has a nice intuitive interpretation: stabilization requires the system to be stable in the subspace where the inputs have no effect.

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Example, Finsler's Lemma

- State feedback design problem

$$(A + BK)^T P + P(A + BK) < 0, P > 0$$
 transformed to


$$QA^T + AQ + L^T B^T + BL < 0, Q > 0$$
- Eliminate L using Finsler's lemma:

$$AQ + QA^T - \sigma BB^T < 0, Q > 0$$

$$AQ + QA^T - \sigma I < 0, Q > 0$$
- However, can always find σ to fulfill second inequality, if Q, σ fulfilling first inequality is found

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Projection/Finsler's lemmas

- May allow for a linear formulation
- Gives 'smaller' problems, fewer variables for computation
- However, once X is determined, this must be used in the original formulation for calculating Λ .
 - (or Q and L in the example on previous slides)
- Skogestad & Postlethwaite warns against ill-conditioning in this two-step approach. If X is poorly conditioned, the calculation of Λ might be inaccurate.

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SOME APPLICATIONS

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Discrete-time state feedback stabilization

- With the quadratic LF $V(x_k) = x_k^T P x_k$, for $P > 0$, the Lyapunov difference inequality tells us that the system is stable provided

$$x_k^T P x_k - x_{k+1}^T P x_{k+1} > 0$$
- This corresponds to


$$P - (A + BK)^T P (A + BK) > 0$$
- Using the Schur complement:

$$\begin{bmatrix} P & (A + BK)^T P \\ P(A + BK) & P \end{bmatrix} > 0$$
- Congruence transform with $W = \begin{bmatrix} P^{-1} & 0 \\ 0 & P^{-1} \end{bmatrix}$ gives

$$\begin{bmatrix} P^{-1} & P^{-1}(A + BK)^T \\ (A + BK)P^{-1} & P^{-1} \end{bmatrix} > 0$$

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Discrete-time ...

- Change of variables: $Q = P^{-1}$, $L = KP^{-1}$

$$\begin{bmatrix} Q & QA^T + L^T B^T \\ AQ + BL & Q \end{bmatrix} > 0$$
- LMI in $Q > 0$ and L .

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Robust feedback stabilization


- Assume that the plant is not precisely known, only known to be a member of the set

$$\begin{bmatrix} A \\ B \end{bmatrix} \in Co \begin{bmatrix} A_1 & \cdots & A_q \\ B_1 & \cdots & B_q \end{bmatrix}$$
- That is, any possible A and B can be found as a convex combination of the 'extreme elements' of the set:

$$A = \sum_{i=1}^q a_i A_i, B = \sum_{i=1}^q a_i B_i, \sum_{i=1}^q a_i = 1, a_i \geq 0$$
- Can a controller that stabilizes all possible plants be found?

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Robust feedback stabilization

- A controller that stabilizes 'all possible' plants is found if the same Q and L solves the LMI's for all the q 'extreme plants'

$$\begin{bmatrix} A_i \\ B_i \end{bmatrix}$$
- This follows directly from the linearity of the LMI in the model matrices, and the convexity of the set of possible plants
- Remark: The controller thus found will also stabilize the system if the plant model changes arbitrarily fast inside the specified model set.

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Parameter dependent Lyapunov functions

- Above, we found a constant controller and prove with a constant LF that the system is stable for all possible uncertainties in a polytopic set.
- What if we can allow the LF to depend on the uncertain parameters?
- Will here only consider stability verification for autonomous systems ('A matrices only').

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Parameter dependent Lyapunov functions

- Express the model as

$$A = A_0 + \sum_{i=1}^q \delta_i A_i$$


with known bounds $\delta_i \in [\underline{\delta}_i \ \overline{\delta}_i]$
and rate of variation $\dot{\delta}_i \in [\underline{\lambda}_i \ \overline{\lambda}_i]$
- Define the sets

$$\Delta = \{\delta | \delta_i \in [\underline{\delta}_i \ \overline{\delta}_i] \forall i\}, \text{ with } \Delta_0 \text{ the set of vertices of } \Delta$$

$$\Lambda = \{\dot{\delta} | \dot{\delta}_i \in [\underline{\lambda}_i \ \overline{\lambda}_i] \forall i\}, \text{ with } \Lambda_0 \text{ the set of vertices of } \Lambda$$

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Parameter dependent LFs

- Will consider LFs of the form


$$V(\delta, x) = x^T P(\delta) x, P(\delta) = P_0 + \sum_{i=1}^q \delta_i P_i$$
- Note that

$$\frac{dP(\delta)}{dt} = \dot{\delta}_1 P_1 + \dot{\delta}_2 P_2 + \dots + \dot{\delta}_q P_q = P(\dot{\delta}) - P_0$$
- And therefore

$$\dot{V}(\delta, x) = x^T (A^T(\delta)P(\delta) + P(\delta)A(\delta) + P(\dot{\delta}) - P_0)x$$

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Parameter dependent LFs

- The system is stable if there exists matrices P_0, \dots, P_q such that


$$A^T(\delta)P(\delta) + P(\delta)A(\delta) + P(\dot{\delta}) < P_0, \forall \delta \in \Delta_0, \forall \dot{\delta} \in \Lambda_0$$

$$P(\delta) > I, \forall \delta \in \Delta_0$$

$$A_i^T P_i + P_i A_i \leq 0, i = 1, \dots, q$$
- Can be extended to
 - State feedback design
 - LPV controller design (if δ is available online)
 - See Scherer and Weiland for details

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Robustly stable ellipsoid for system with saturated inputs


- An ellipsoid can be defined in several ways. We use $\mathcal{E}(P) = \{x | xP^{-1}x \leq 1\}$
- We want to find a controller K such that
 - The system with the input $u = \text{sat}(Kx)$ is stable inside $\mathcal{E}(P)$
 - The system adheres to the constraints $X = \{x | -1 \leq F_i x \leq 1, \forall i = 1, \dots, n\}$
 - These conditions should hold for all plants in a polytopic uncertainty description

$$A = \sum_{i=1}^q a_i A_i, B = \sum_{i=1}^q a_i B_i, \sum_{i=1}^q a_i = 1, a_i \geq 0$$

- Will model saturation using a Linear Differential Inclusion approach

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LDI approach to modelling saturated inputs

- Single input, there exist β and v such that $\text{sat}(u) = \beta Kx + (1 - \beta)v$

$$\begin{aligned} u_l &\leq v \leq u_u \\ 0 &\leq \beta \leq 1 \end{aligned}$$
- Two inputs:


$$\begin{aligned} u_{1l} &\leq v_1 \leq u_{1u} \\ u_{2l} &\leq v_2 \leq u_{2u} \end{aligned}$$

$$\text{sat}(u) = \beta_1 \begin{bmatrix} K_1 x \\ K_2 x \end{bmatrix} + \beta_2 \begin{bmatrix} K_1 x \\ v_2 \end{bmatrix} + \beta_3 \begin{bmatrix} v_1 \\ K_2 x \end{bmatrix} + \beta_4 \begin{bmatrix} v_1 \\ v_2 \end{bmatrix}$$

$$\sum_{i=1}^4 \beta_i = 1, \beta_i \geq 0$$

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LDI approach...

- m inputs: Define D_m as the set of diagonal matrices whose diagonal elements are either 0 or 1. For example, for $m = 2$


$$D_2 = \left\{ \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}, \begin{bmatrix} 1 & 0 \\ 0 & 0 \end{bmatrix}, \begin{bmatrix} 0 & 0 \\ 0 & 1 \end{bmatrix}, \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \right\}$$
- Each element of D_m is denoted $E_j, j = 1, 2, \dots, 2^m$
- Define also $E_j^- = I - E_j$, then
$$\text{sat}(u) \in \text{Conv}\{E_j Kx + E_j^- v\}$$

for some v such that $u_{il} \leq v_i \leq u_{iu}$
- That is, there exist β_j, v_i such that
$$\beta_j \geq 0, \sum_{j=1}^{2^m} \beta_j = 1$$

$$\text{sat}(u) = \sum_{j=1}^{2^m} \beta_j (E_j Kx + E_j^- v)$$

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Robustly stable ellipsoid...

- The ellipsoid $\mathcal{E}(P) = \{x | x^T P^{-1} x \leq 1\}$ is invariant provided
$$\begin{bmatrix} P & \{A_i P + B_i (E_j K P + E_j^- Y)\} \\ * & P \end{bmatrix} \geq 0, \quad \forall i = 1, \dots, q \text{ and } \forall j = 1, \dots, 2^m$$


For discrete time dynamics
- State constraints are fulfilled, provided
$$\begin{bmatrix} 1 & F_i P \\ * & P \end{bmatrix} \geq 0, \quad \forall i = 1, \dots, n$$

Maximize $\det(P)$ subject to these constraints.
-Convex problem
-Maximizes the size of the stable ellipsoid.
- Input constraints (assuming $-u_{il} = u_{iu} = u_{i,max}$):
$$\begin{bmatrix} u_{i,max}^2 & Y_i \\ * & P \end{bmatrix} \geq 0, \quad \forall i = 1, \dots, m$$


Where Y_i is the i th row of the matrix Y .
- The input constraint conditions ensure that $-u_{i,max} \leq v_i \leq u_{i,max}$, and thus that the saturated input is included in the LDI, for $v_i = H_i x$, where $H_i P = Y_i$.

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Literature

- There is a lot of literature on LMI based analysis and design – including many issues not covered here. Much information is contained in the following two references (both freely available for personal use):
- Book by S. Boyd et al.: <http://www.stanford.edu/~boyd/lmibook/>
- Lecture notes by Carsten Scherer and Siep Weiland
<http://www.imng.uni-stuttgart.de/mst/files/LectureNotes.pdf>
- The more accessible presentation of the robust design with saturated inputs is probably in the thesis by Hoai-Nam Nguyen:
http://tel.archives-ouvertes.fr/docs/00/78/38/29/PDF/Nguyen_Hoai_Nam_these_VF.pdf
 although many of the main contributions are from other authors (see Nguyen's thesis for details).
- A quick and readable introduction to LMIs is given in Chapter 12 of
 S. Skogestad, I Postlethwaite: Multivariable Feedback Control. Analysis and Design (2nd ed.) John Wiley & Sons, 2005.

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