# Preliminary Design and Verification of a Fuel Pin

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#### 1 Introduction

This report presents the preliminary design and verification of a fuel pin for a sodium-cooled fast reactor, as specified in the assignment.

The analysis involves calculations for material properties, thermal-hydraulic conditions, and mechanical stress limits.

We verify the robustness of our models and justify the assumptions made throughout the process.

## 2 Problem Description

The fuel pin design problem requires:

- Determining the cladding thickness, fuel-cladding gap size, and plenum height.
- Verifying the design against limits for fuel melting, cladding temperature, yielding, and rupture time.
- Identifying critical aspects if irradiation time is doubled.

The project specifications and material properties are summarized in Table 1.

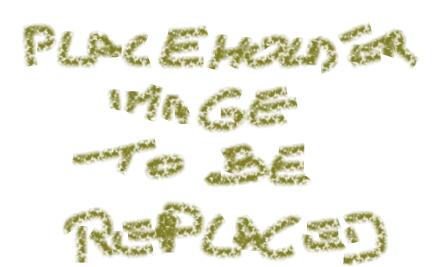


Table 1: Fuel pin design specifications.

# 3 Assumptions

To address the given problem, the following assumptions were made: Steady State Solution for Gas in Grains:

→ The rate equation for the gas remaining in the grains (PDE) was solved in steady state conditions, given that we just want to size the plenum for 1-year operation and are not interested in the specific behavior in time of the function.

#### **Fission Rate Calculation:**

- → The fission rate was calculated by using the formula (macroscopic cross section \* average flux).
- → The macroscopic cross section of fission was computed from data taken from the JANIS database.
- → The average flux was evaluated considering power and flux profile to be equal.

#### **Material Properties and Geometry:**

- → Material properties are temperature-dependent and were modeled using provided empirical correlations.
- → Axial power and neutron flux profiles remain constant over time.
- $\hookrightarrow\,$  Initial helium pressure and temperature in the fuel-cladding gap were assumed as specified.
- → Simplifications in geometry, such as neglecting axial deformation, were made to ease computation.

#### 4 Verification of Models

Each function used in the analysis was tested for expected behavior. Below are the key verification steps.

#### 4.1 Thermal-Hydraulics Analysis

Preliminary checks were conducted on coolant properties.

Density, viscosity, and thermal conductivity were validated at the coolant inlet temperature

The heat transfer coefficient between the coolant and cladding was computed using Nusselt number correlations.

Figure 1 shows the axial power profile and the computed heat transfer coefficient.

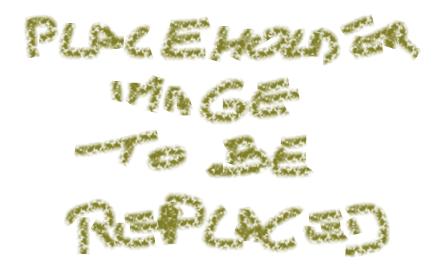


Figure 1: Thermal-hydraulics analysis results.

#### **4.2 Temperature Profiles**

Radial and axial temperature profiles were computed for the cold geometry to check if the shape of the profile made sense and if the values were reasonable.

The results provided an initial validation of the temperature distribution behavior before further analysis.

Figure 2 illustrates the temperature distributions.

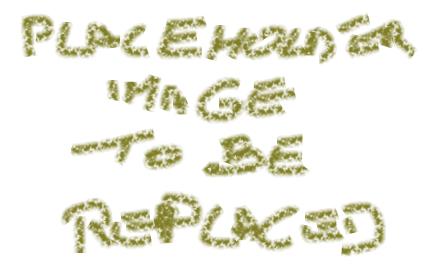


Figure 2: Radial and axial temperature profiles for cold geometry.

#### 4.3 Fission Gas Behavior

Rate theory equations were solved to estimate fission gas production and release over the fuel cycle.

The rate equation for the gas remaining in the grains was solved under steady state conditions, given that we are only interested in sizing the plenum for 1-year operation.

The fission rate was calculated as the product of the macroscopic cross section and the average flux.

The macroscopic cross section was obtained from data in the JANIS database, and the average flux was estimated by assuming the power and flux profiles were equivalent.

The concentration profiles are shown in Figure 3.

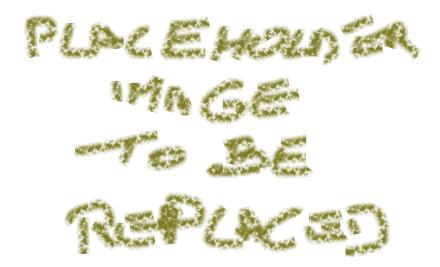


Figure 3: Fission gas concentration profiles.

# 5 Plenum Design

The relationship between plenum height and pressure was analyzed to ensure the pressure remains below 5 MPa.

Figure 4 shows the results.

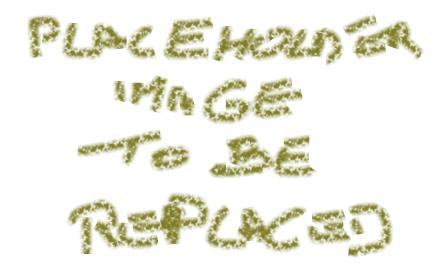


Figure 4: Plenum pressure as a function of height.

#### **6 Future Work**

In subsequent steps, we will develop a dimensioning loop to automate the iterative design process.

We will present final results, including optimized dimensions and safety margins, and comment on the design's robustness under extended irradiation.

# **A Code Listings**

Placeholder for code files.