Advanced & Intelligent Control

Digital PID Tunning tables

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$$C(z^{-1}) = \frac{U(z^{-1})}{E(z^{-1})} = K_e \frac{q_0 + q_1 z^{-1} + q_2 z^{-2}}{1 - z^{-1}} \; ; \; 1/10 \le K_e \le 1 \rightarrow recomended \rightarrow \begin{cases} 1 & Fast \\ 3/4 & Moderate \\ 1/2 & Slow \end{cases}$$
 For $q_0 > 0 \rightarrow q_1 < -q_2$, $-(q_0 + q_1) < q_2 < q_0$

Table 1. Digital Controllers							
Parameter	Forward rectangular method	Backward rectangular method	Trapezoidal method				
Parameter	FRM	BRM	TRAP				
q_0	$K_c\left(1+\frac{\tau_d}{T}\right)$	$K_c \left(1 + \frac{T}{\tau_i} + \frac{\tau_d}{T} \right)$	$K_c \left(1 + \frac{T}{2\tau_i} + \frac{\tau_d}{T} \right)$				
q_1	$-K_c\left(1-\frac{T}{\tau_i}+\frac{2\tau_d}{T}\right)$	$-K_c\left(1+\frac{2\tau_d}{T}\right)$	$-K_c\left(1-\frac{T}{2\tau_i}+\frac{2\tau_d}{T}\right)$				
q_2	$\frac{K_c \tau_d}{T}$	$\frac{K_c \tau_d}{T}$	$\frac{K_c \tau_d}{T}$				

Table 2. Ziegler-Nichols/Critic Gain					
Controller	K_c	$ au_i$	$ au_d$		
P	$(1/2)K_u$				
PI	$(9/20)K_u$	$(83/100)T_u$			
PID	$(3/5)K_u$	$(1/2)T_u$	$(1/8)T_u$		

Robust Ziegler-Nichols tunning

$$K_c = K_u G_m \cos(\emptyset)$$

$$\tau_i = \frac{T_u}{4\pi\alpha} \left(\tan(\emptyset) + \sqrt{4\alpha + \tan^2(\emptyset)} \right)$$

$$\tau_d = \alpha \tau_i$$

 \textit{G}_{m} : Desired inverse of gain margin (default = 0.5)

 \emptyset : Desired phase margin

lpha : Desing seletion of the ration au_d : au_i

Tables for FOR systems auto-tunning

$$\theta = \alpha + \frac{T}{2}$$
Table 3. Ziegler-Nichols/Reaction Curve
$$\frac{Controller}{P} = \frac{K_c}{K_\theta} = \frac{\tau_i}{K_\theta}$$

$$\frac{9\tau}{10K\theta} = \frac{10\theta}{3}$$

$$PID = \frac{6\tau}{10K_\theta} = \frac{1}{2}\theta$$

5*Κθ*

$G_p(s) = \frac{Ke^{-\alpha s}}{\tau s + 1} \to T \to G_p(z) = \frac{b_0 + b_1 z^{-1}}{1 + a_1 z^{-1}} z^{-d}$ $\theta = \alpha + \frac{T}{2}$	$K = \lim_{z \to 1} G_p(z) = \frac{b_0 + b_1}{1 + a_1}$ $\tau = -\frac{T}{\ln(a_1)} \qquad \theta = dT$
Table 3. Ziegler-Nichols/Reaction Curve	(1811)

Table 4. IMC							
Controller	K_c	$ au_i$	$ au_d$	λ			
PI	$\frac{ au}{K\lambda}$	τ		$\lambda \ge 1.7\alpha$ $\lambda \ge 0.2\tau$			
PID	$\frac{2\tau + \alpha}{K(2\lambda + \alpha)}$	$\frac{2\tau + \alpha}{2}$	$\frac{\tau\alpha}{2\tau+\alpha}$	$\lambda \ge 0.8\alpha$ $\lambda \ge 0.2\tau$			

Controller	K_c	$ au_i$	$ au_d$				
PI	$\frac{0.928}{K} \left(\frac{\theta}{\tau}\right)^{-0.946}$	$0.928\tau \left(\frac{\theta}{\tau}\right)^{0.503}$					
PID	$\frac{1.3070}{K} \left(\frac{\theta}{\tau}\right)^{-0.950}$	$0.740\tau \left(\frac{\theta}{\tau}\right)^{0.7380}$	$0.365\tau \left(\frac{\theta}{\tau}\right)^{0.950}$				

Table 6. Cohen-Coon/Reaction Curve					
Controller	K_c	$ au_i$	$ au_d$		
P	$\frac{\tau}{K\theta}\left(1+\frac{\theta}{3\tau}\right)$				
PI	$\frac{\tau}{K\theta} \left(\frac{9}{10} + \frac{\theta}{12\tau} \right)$	$\frac{\theta(30\tau+3\theta)}{9\tau+20\theta}$			
PID	$\frac{\tau}{K\theta} \left(\frac{4}{3} + \frac{\theta}{4\tau} \right)$	$\frac{\theta(32\tau+6\theta)}{13\tau+8\theta}$	$\frac{4\theta\tau}{11\tau + 2\theta}$		

			Tal	ole 7. C	liancon	e-Marli	n			
	PI			PID						
	K		τ	i	K	c C	τ	i	τ	d
	<u> </u>	<u>3</u> <u>7</u>	$\delta(\tau)$	+ θ)	<u>[</u> 	<u>{</u>	$\delta(\tau)$	+ θ)	$\varphi(\tau)$	+ θ)
Ø	Set-I	Point	Distui	rbance	S	et-Poin	it	Di	sturban	ice
$\alpha(\tau + \alpha)$	β	δ	β	δ	β	δ	φ	β	δ	φ
0.0	1.417	0.748	1.259	0.241	1.520	0.732	0.000	1.392	0.245	0.000
0.1	1.417	0.748	1.259	0.235	1.520	0.732	0.000	1.392	0.245	0.000
0.2	1.193	0.964	1.626	0.518	1.430	0.941	0.017	1.823	0.513	0.000
0.3	1.032	0.881	1.377	0.789	1.110	0.864	0.035	1.423	0.714	0.008
0.4	0.918	0.818	1.000	0.746	0.862	0.773	0.060	1.130	0.691	0.036
0.5	0.861	0.756	0.858	0.702	0.687	0.672	0.087	0.859	0.641	0.070
0.6	0.722	0.693	0.599	0.659	0.545	0.596	0.118	0.670	0.600	0.107
0.7	0.648	0.631	0.464	0.615	0.460	0.545	0.155	0.521	0.550	0.148
0.8	0.608	0.568	0.383	0.572	0.398	0.505	0.215	0.406	0.505	0.203
0.8	0.594	0.506	0.359	0.528	0.370	0.468	0.139	0.335	0.468	0.132
1.0	0.558	0.443	0.316	0.485	0.370	0.432	0.047	0.284	0.432	0.050

Table	Table 8. Error criterions			I	ICE		IAE		IAET	
Controller	K_c	$ au_i$	$ au_d$	а	b	а	b	а	b	
P	$\frac{a}{K} \left(\frac{\theta}{\tau}\right)^b$			1.411	-0.917	0.902	-0.985	0.940	-1.084	
DI	$\frac{a}{K} \left(\frac{\theta}{\tau}\right)^b$			1.305	-0.959	0.984	-0.986	0.859	-0.977	
PI		$\frac{\tau}{a} \left(\frac{\theta}{\tau}\right)^b$		0.492	0.739	0.608	0.707	0.674	0.680	
	$\frac{a}{K} \left(\frac{\theta}{\tau}\right)^b$			1.495	-0.945	1.435	-0.921	1.357	-0.947	
PID		$\frac{\tau}{a} \left(\frac{\theta}{\tau}\right)^b$		1.101	0.771	0.878	0.749	0.842	0.738	
			$a\tau \left(\frac{\theta}{\tau}\right)^b$	0.560	1.006	0.482	1.137	0.381	0.995	

Table 7. Parallel-Series PID Conversion					
Series to Parallel	Parallel to Series				
$K_c = K_c \frac{(\tau_i + \tau_d)}{\tau_i}$	$K_c = \frac{K_c}{2} \left(1 + \sqrt{1 - 4\frac{\tau_d}{\tau_i}} \right)$				
$\tau_i = \tau_i + \tau_d$	$\tau_i = \frac{\tau_i}{2} \left(1 + \sqrt{1 - 4 \frac{\tau_d}{\tau_i}} \right)$				
$\tau_d = \frac{\tau_i \tau_d}{\tau_i + \tau_d}$	$\tau_d = \frac{2\tau_d}{1 + \sqrt{1 - 4\frac{\tau_d}{\tau_i}}}$				