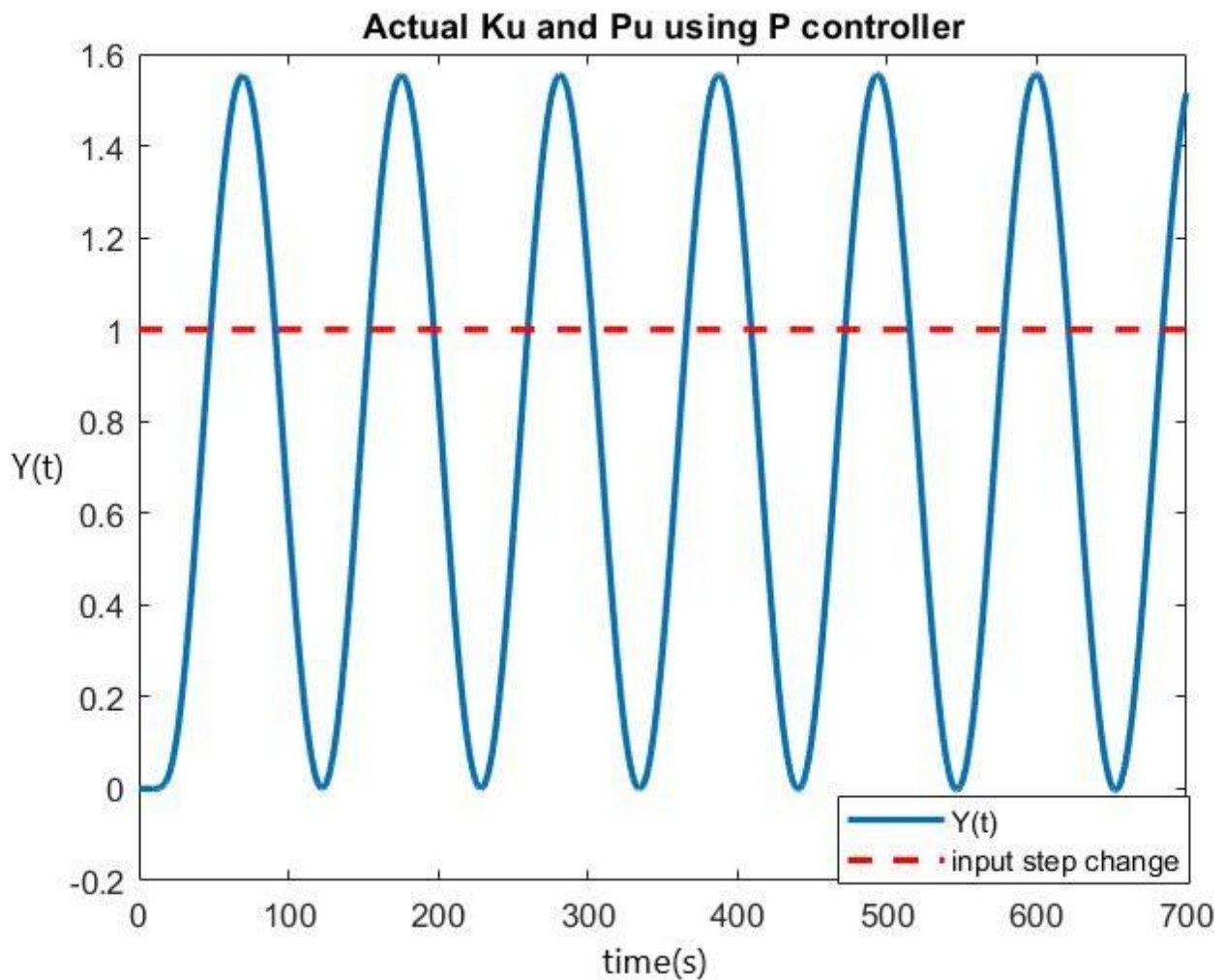


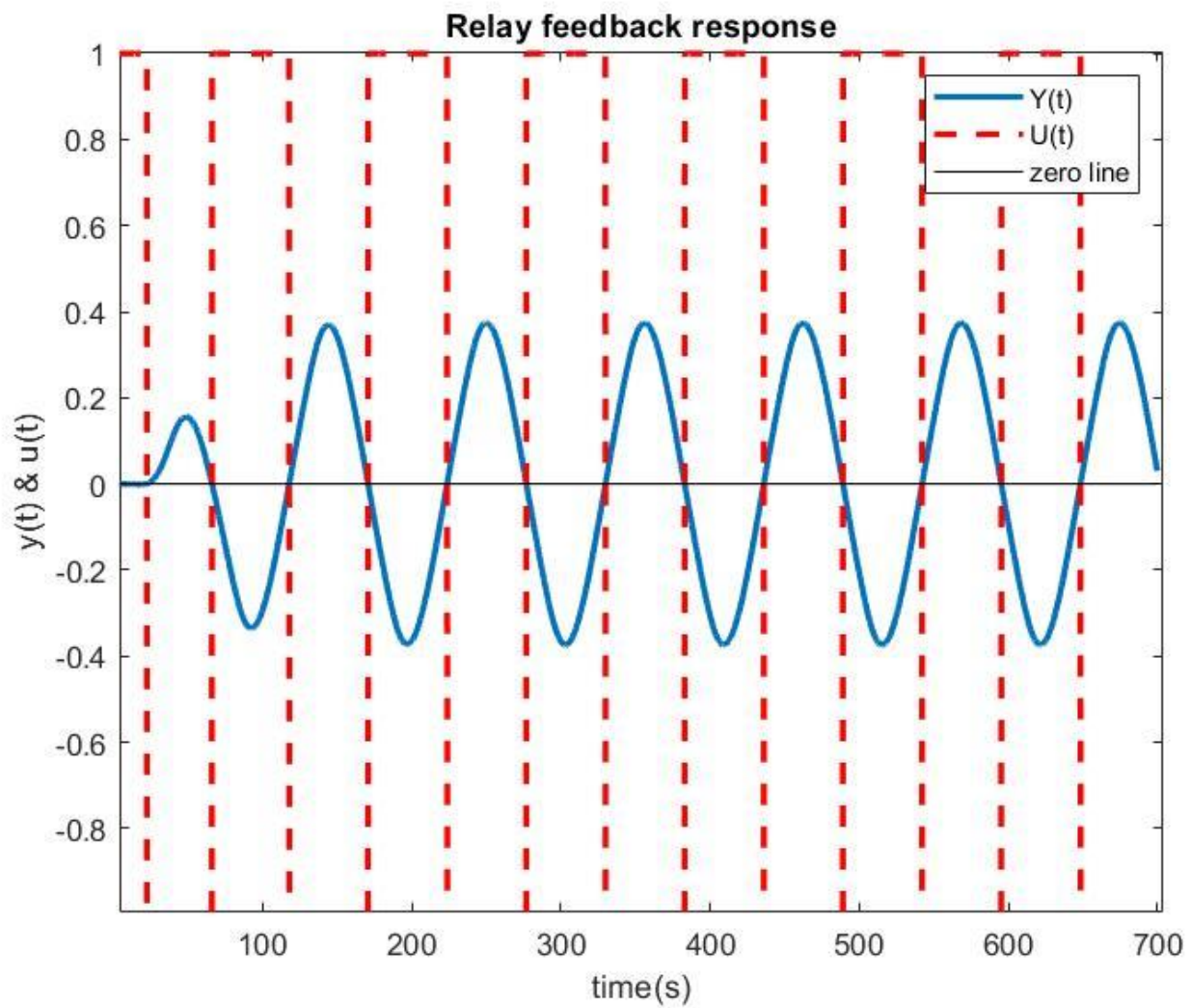
Lab Report 2(170747)

Using P controllers:



For sustained oscillations $K_c = K_u = 3.53$ & $P_u = 106.2$ s

Using Relay Feedback:



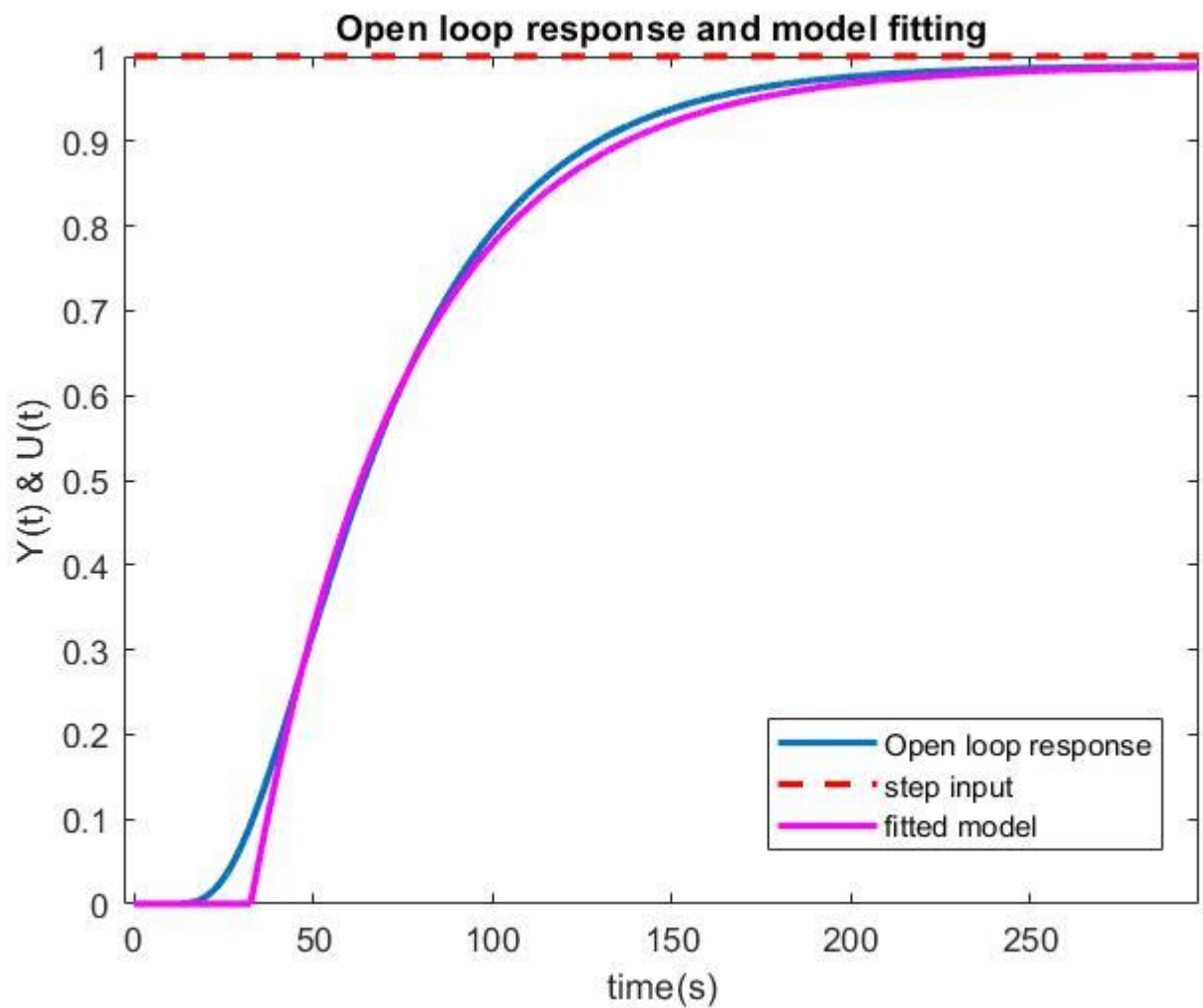
Height of Relay (H) = 1

Amplitude of Signal (A) = .3737

$K_u = (4H) / (\pi * A) = 3.4071$

$P_u = 356.6 - 250.4 = 106.2 \text{ sec}$

USING FIRST ORDER PLUS DEAD TIME MODEL:



Fitting First Order plus Dead Time to the Process

Calculations:

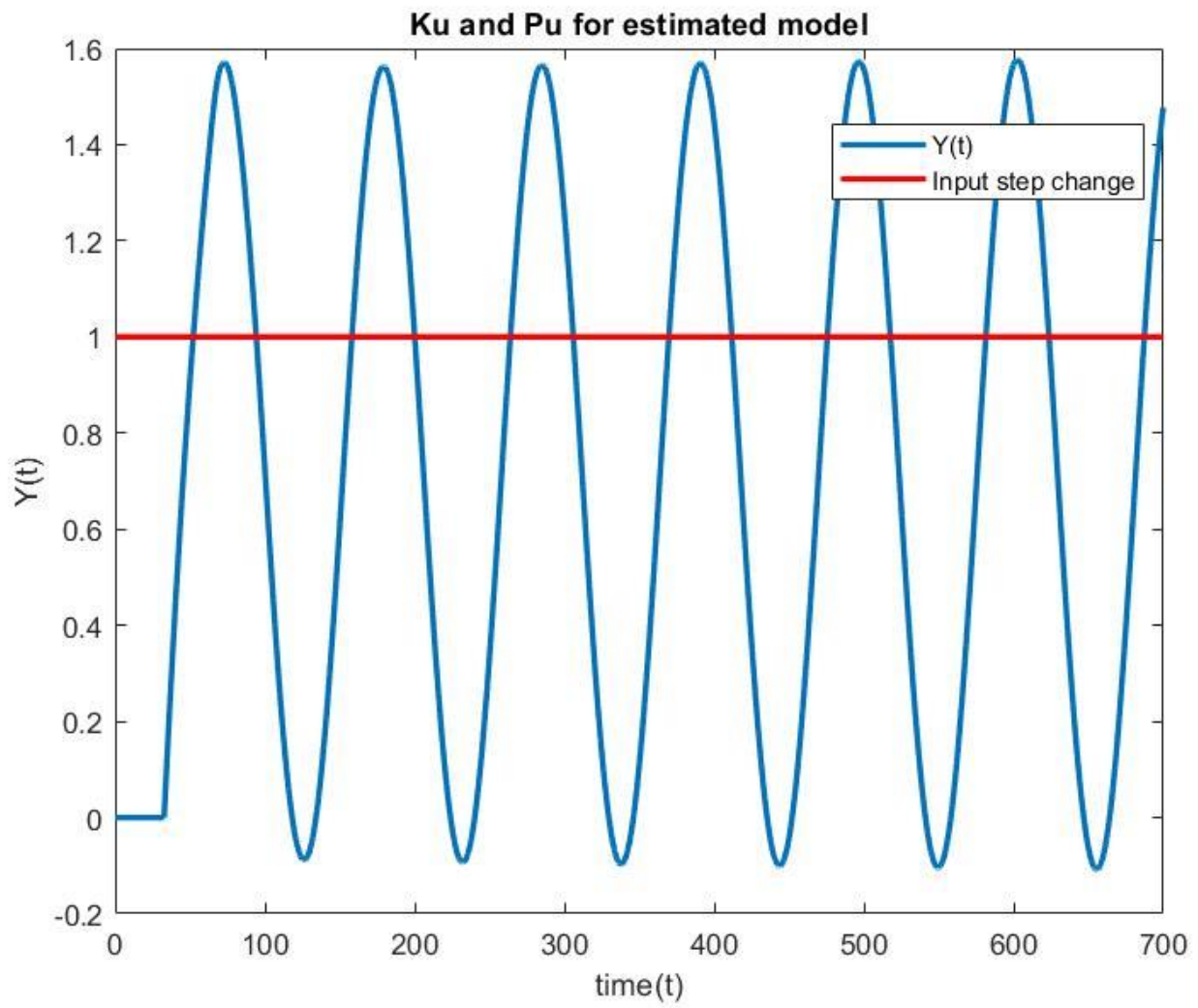
$$D + T = t_{63.2}$$

$$D + T/3 = t_{28.3}$$

$$D = 32.6856 \text{ s}$$

$$T = 43.6287 \text{ s}$$

$$K_m = .9894$$



Ku=2.81

Pu=106 s

Plotting Responses at recommended tuning

Using the K_u and P_u obtained from **Relay Feedback Test**.

$K_u = 3.4071$

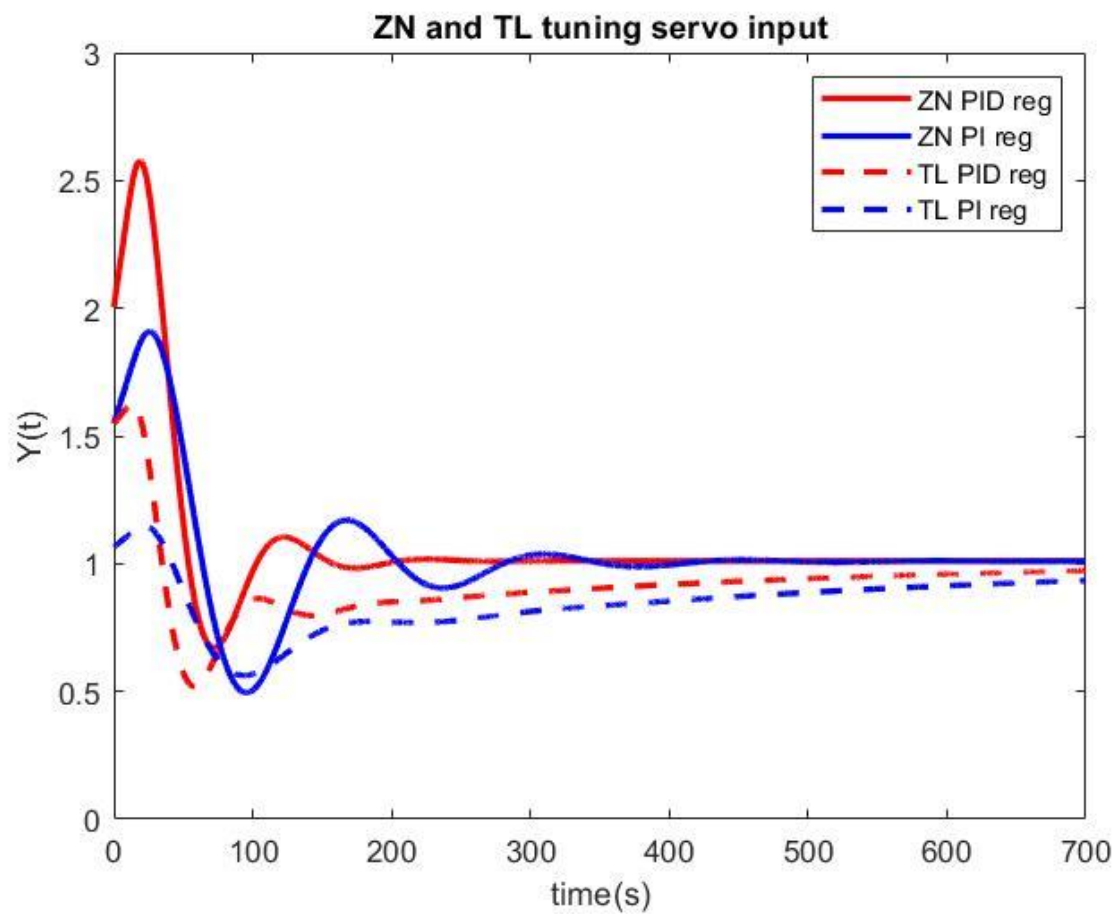
$P_u = 106.2 \text{ sec}$

Using Empirical Relations for Tuning:

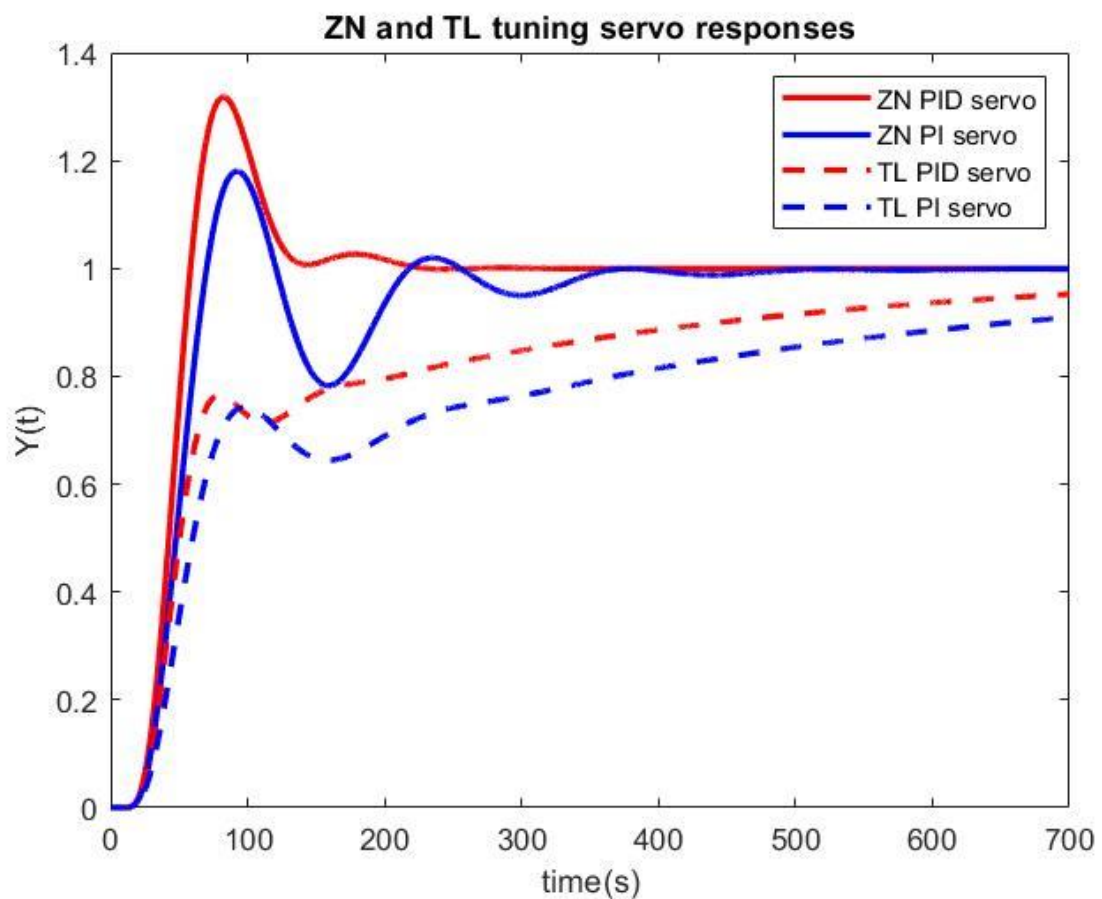
Zeigler Nichols	K_c	τ_i	τ_d
P	$K_u/2$	-	-
PI	$K_u/2.2$	$P_u/1.2$	-
PID	$K_u/1.7$	$P_u/2$	$P_u/8$
Tyres Luyben	K_c	τ_i	τ_d
P	-	-	-
PI	$K_u/3.2$	$2.2P_u$	-
PID	$K_u/2.2$	$2.2P_u$	$P_u/6.3$

Zeigler Nichols	K_c	τ_i	τ_d
P	1.70355	-	-
PI	1.54868	88.5	-
PID	2.00417	53.1	13.275
Tyres Luyben	K_c	τ_i	τ_d
P	-	-	-
PI	1.0647	233.64	-
PID	1.54868	233.64	16.857

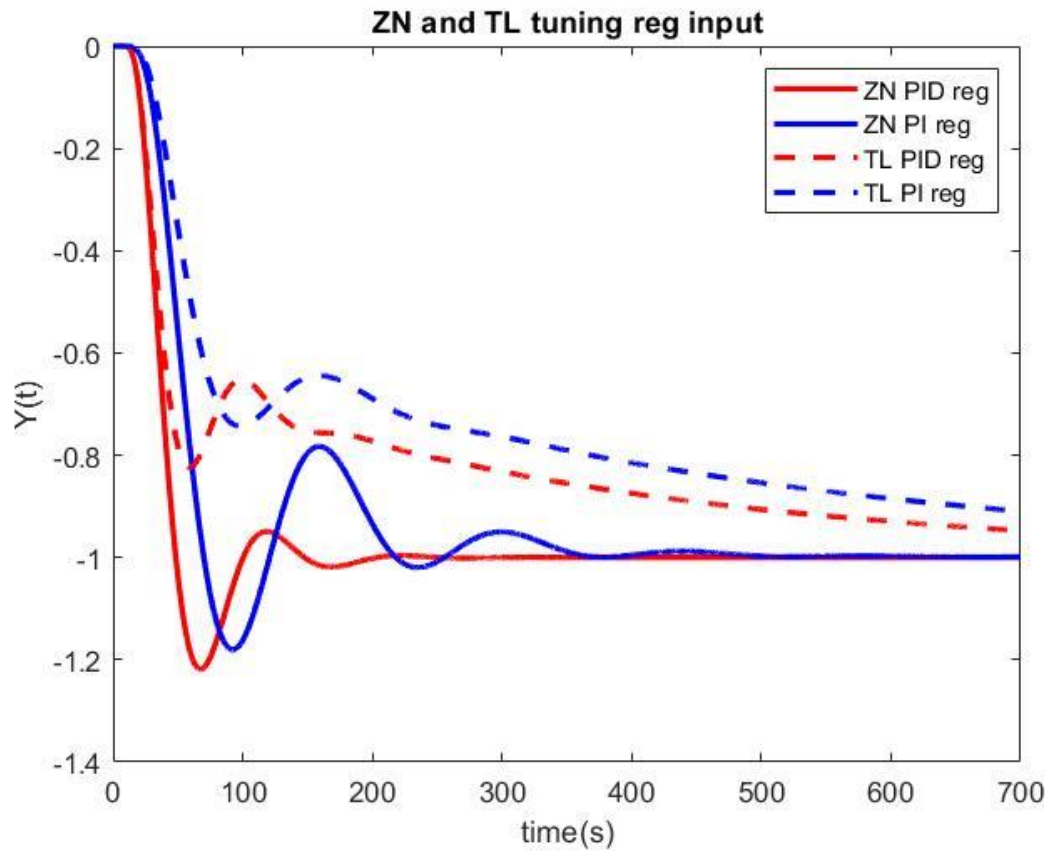
Servo Input



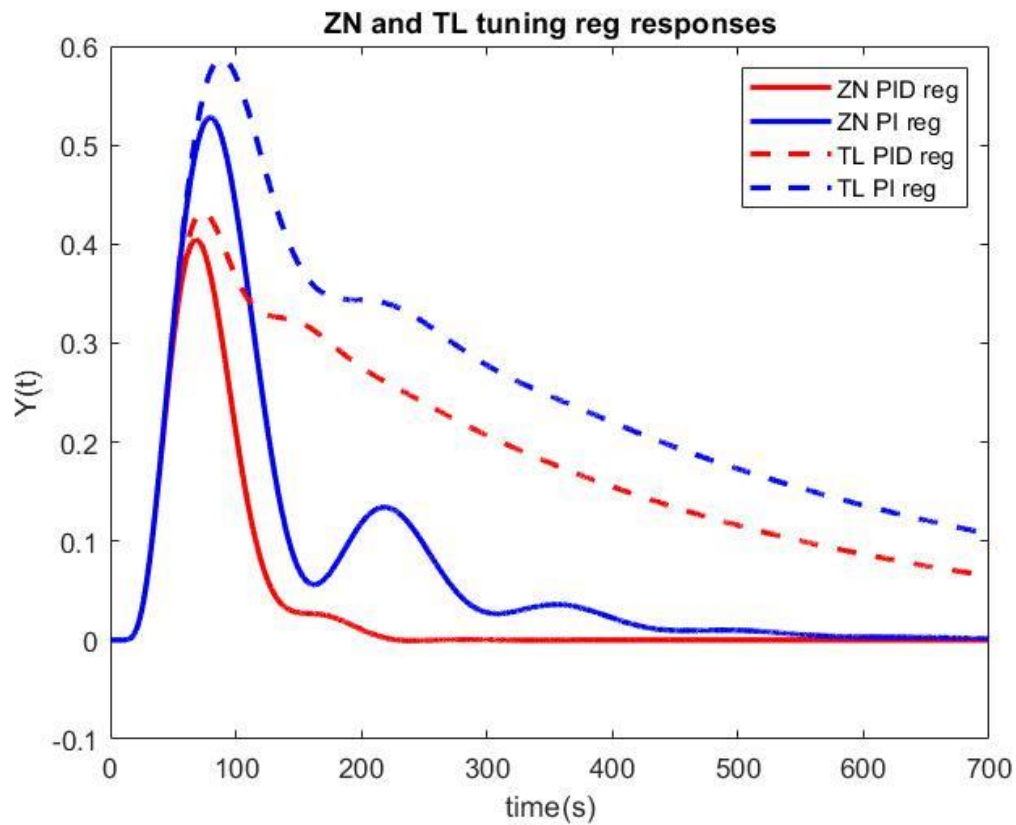
Servo Responses



Regulatory Input



Regulatory Response



Part 2

Anti-Reset Windup

Using the K_u and P_u obtained from **Relay Feedback Test**.

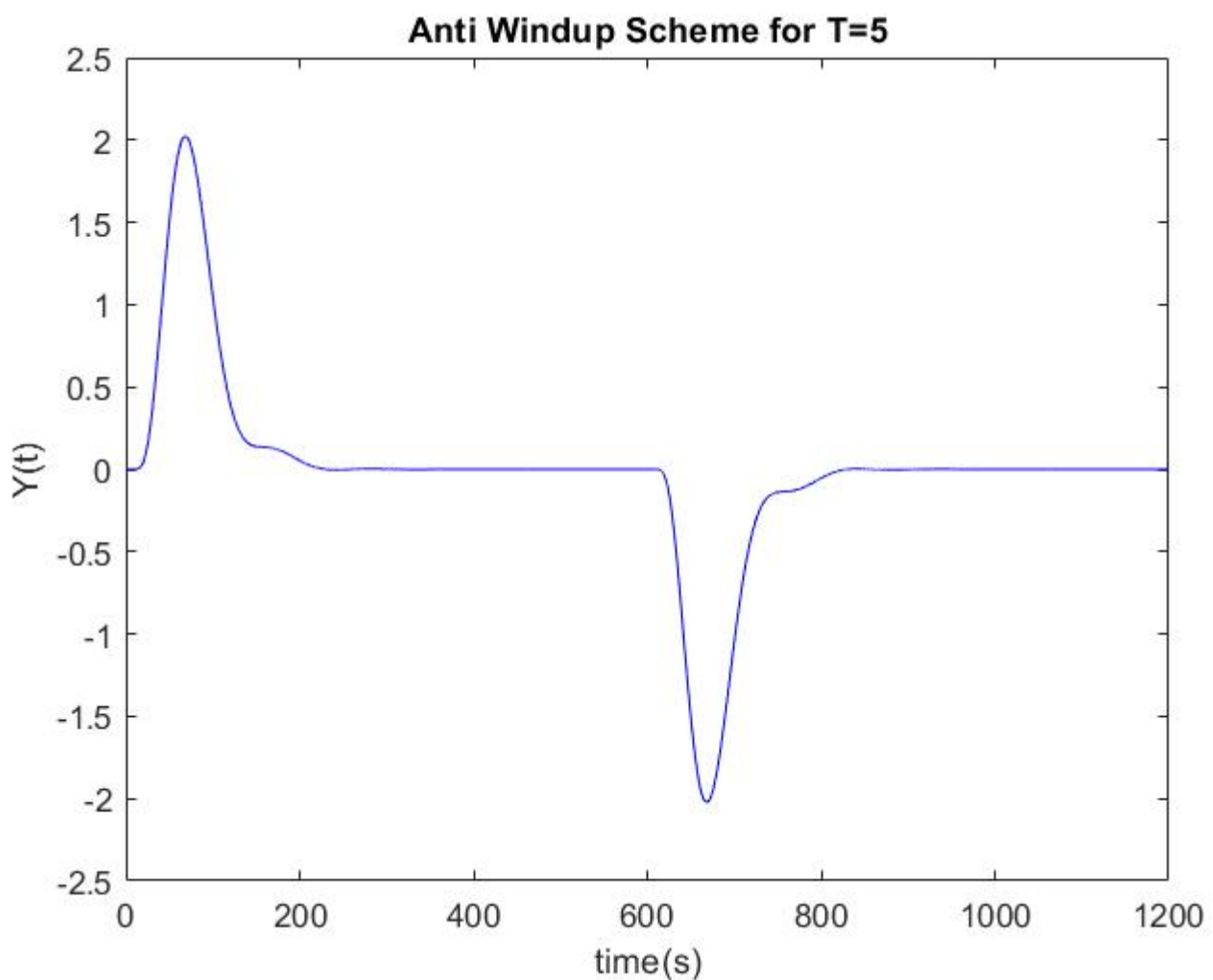
$K_u = 3.4071$

$P_u = 106.2 \text{ sec}$

Operating under zeigler nicholas tuning for PID controller

PID	$K_u/1.7$	$P_u/2$	$P_u/8$
PID	2.00417	53.1	13.275

For small disturbance amplitude of $T=5s$:



At small disturbance amplitude such as $T=5s$

- Saturation is not achieved
- U remains equal to U_{imp}
- All the anti-reset windup schemes give the same output.

For large disturbance amplitude of T=12s:

