

Paper-1Convex MPC:-

* Abstract:- MPC \rightarrow to determine GRFs \rightarrow torque controlled quadruped robot.

simplified robot dynamics \rightarrow to convert/formulate problem as convex optimization.
 (what does this mean?)

\Rightarrow With the simplified model, GRF planning problems are formulated for prediction horizons of up to 0.5 seconds, and are solved to optimality in under 1ms at a rate of 20-30 Hz.

* Swing leg controller:-

$$\tau_i = J_i^T [K_p ({}_B p_{i,ref} - {}_B p_i) + K_d ({}_B v_{i,ref} - {}_B v_i)] + \tau_{i,ff}$$

* $J_i \in \mathbb{R}^{3 \times 3}$; foot Jacobian.

* $K_p, K_d \in \mathbb{R}^{3 \times 3}$; diag. +ve definit proportional & derivative gain.

* ${}_B p_i, {}_B v_i \in \mathbb{R}^3$; foot position & velocity in body frame. (of i th foot).
 (matrices)

* ${}_B p_{i,ref}, {}_B v_{i,ref} \in \mathbb{R}^3$; ref. for pos. & vel.

* $\tau_{i,ff} \in \mathbb{R}^3$ is a feedforward torque

$$\tau_{i,ff} = J_i^T \Delta_i ({}_B q_{i,ref} - \dot{J}_i \dot{q}_i) + C_i \dot{q}_i + G_i$$

$\Delta_i \in \mathbb{R}^{3 \times 3}$ space inertia matrix.

Manipulator Dynamics ??

★ Desired foot location calculation :-

$$p^{des} = p^{ref} + v^{com} \Delta t / 2$$

↙
↘ world frame

Δt - time the foot will spend on the ground.
 p^{ref} - location on the ground beneath the hip of the robot.

★ Ground force control :-

$$\tau_i = J_i^T R_i^T f_i$$

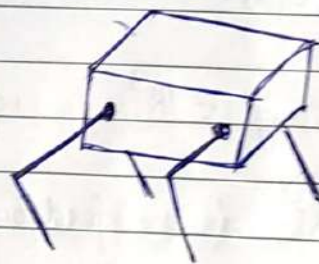
R is the rotation mat. which transforms from body to world coordinates

J is foot Jacobian.

f_i is the vector of forces calc. from MPC.

★ Simplified Robot Dynamics :-

* SRB model :-



$$\Rightarrow \ddot{p} = \frac{\sum_{i=1}^n f_i}{m} - g$$

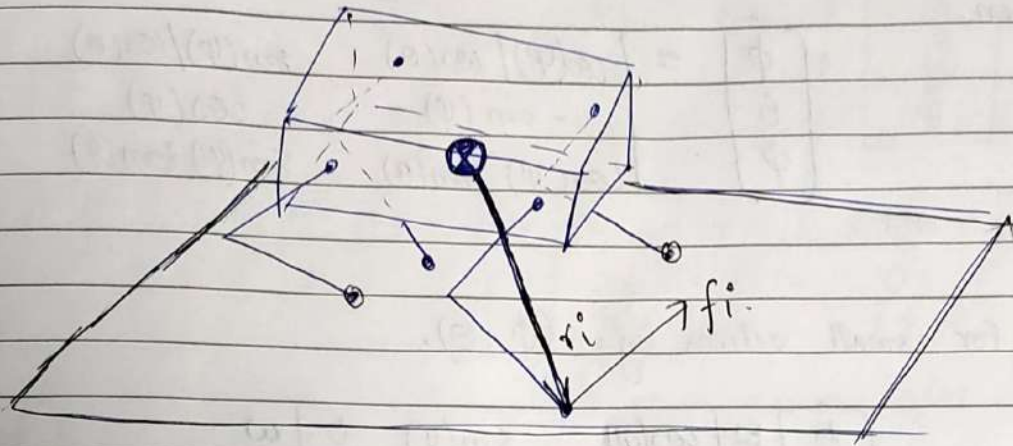
$$\Rightarrow \frac{d}{dt}(I\omega) = \sum_{i=1}^n (r_i \times f_i)$$

$$\Rightarrow \dot{R} = \hat{\omega} R$$

} Non-linear.

for every GRF, $f_i \in \mathbb{R}^3$, the vector from the centre of mass

to the pt. where the force is applied is $r_i \in \mathbb{R}^3$.



where $p \in \mathbb{R}^3$ is robot's position.
 m is robot's mass.

g is acc. of gravity.

$I \in \mathbb{R}^3$; is robot's inertia tensor.

$\omega \in \mathbb{R}^3$; is the robot's angular velocity.

R , is the rotation matrix; Body \rightarrow World.

* Approximated angular velocity dynamics:-

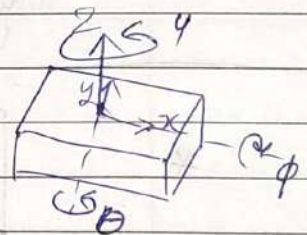
Robot's orientation is expressed as a vector of Z-Y-X.

Euler angles $\theta = [\phi \ \theta \ \psi]^T$

ϕ - roll

θ - pitch

ψ - Yaw



$$R = R_z(\psi)R_y(\theta)R_x(\phi)$$

* Angular velocity in world coordinate frame.

$$\omega = \begin{bmatrix} \cos(\theta) \cdot \cos(\psi) & -\sin(\psi) & 0 \\ \cos(\theta) \sin(\psi) & \cos(\psi) & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix}$$

* If robot is not pointed vertically (ie $\cos(\theta) \neq 0$)

$$-\begin{bmatrix} \cdot \\ \cdot \end{bmatrix}$$

then

$$\begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} = \begin{bmatrix} \cos(\psi)/\cos(\theta) & \sin(\psi)/\cos(\theta) & 0 \\ -\sin(\psi) & \cos(\psi) & 0 \\ \cos(\psi)\tan(\theta) & \sin(\psi)\tan(\theta) & 1 \end{bmatrix} \omega$$

* For small values of (ϕ, θ) ,

$$\begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} \approx \begin{bmatrix} \cos(\psi) & \sin(\psi) & 0 \\ -\sin(\psi) & \cos(\psi) & 0 \\ 0 & 0 & 1 \end{bmatrix} \omega$$

$$\begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} \approx R_2(\psi) \cdot \omega$$

Note:- Order of Euler angle rotations are imp.

* For alternate seq of rot. approx. will be inaccurate.

Why??

*

$$\frac{d}{dt}(I\omega) = I\dot{\omega} + \omega \times (I\omega) \approx I\dot{\omega}$$

discards the effects of precession and nutation of the rotating body.

The inertia tensor in World coordinate frame is given by:-

$$I = R_0 I R^T$$

classmate

$$\Rightarrow \hat{I} = [R_2(\psi)][I][R_2(\psi)^T]$$

* Simplified Robot Dynamics:-

$$\frac{d}{dt} \begin{bmatrix} \hat{\theta} \\ \hat{p} \\ \hat{\omega} \\ \hat{\dot{p}} \end{bmatrix} = \begin{bmatrix} 0_3 & 0_3 & R_2(\psi) & 0_3 \\ 0_3 & 0_3 & 0_3 & I_3 \\ 0_3 & 0_3 & 0_3 & 0_3 \\ 0_3 & 0_3 & 0_3 & 0_3 \end{bmatrix} \begin{bmatrix} \hat{\theta} \\ \hat{p} \\ \hat{\omega} \\ \hat{\dot{p}} \end{bmatrix} + \begin{bmatrix} 0_3 & \dots & 0_3 \\ 0_3 & \dots & 0_3 \\ \hat{I}(\hat{r}_1) & \dots & \hat{I} \hat{r}_n \\ I_3/m & \dots & I_3/m \end{bmatrix} \begin{bmatrix} g_1 \\ g_2 \\ 0 \\ \hat{f}_n \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ g \end{bmatrix}$$

above eqⁿ can be rewritten with "g" as additional state to get state-space form. —??

$$\dot{x}(t) = A_c(\psi) x(t) + B_c(x_1, \dots, x_n, \psi) u(t)$$

$$A_c \in \mathbb{R}^{13 \times 13}, B_c \in \mathbb{R}^{13 \times 3n}$$