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Problem set 4

Macroscopic Physical Chemistry

Analytical Problems:

1. ideal gas expanded reversibly, adiabatically $(v_i, T_i) \rightarrow (v_f, T_f)$
Prove $\Delta S = 0$?

Entropy Transfer takes place through interactions of heat
$$\Delta S = \int \frac{dq_{rev}}{T}$$

Adiabatic Process means no heat can leave or enter the system

$$\text{so, } dq_{rev} = 0$$

so this means for a reversible adiabatic process $\Delta S = 0$

2. a. $\Delta U, \Delta H$, and ΔS for the entire cycle are going to be equal to zero because since they are state functions, they are not path dependent, and only depend on final and initial states. For a cyclic process initial and final states are the same, therefore the change in state is zero, so all $\Delta U, \Delta H$, and $\Delta S = 0$.

b. steps: $a \rightarrow b$, Temperature is constant so $\Delta U = 0$

steps: $b \rightarrow c$ and $d \rightarrow a$ are adiabatic so $q = 0$

work done by system is carried out from heat supplied to the system

$$w = -nRT_h \ln\left(\frac{v_b}{v_a}\right); \Delta U = q + w = 0$$

$$q = -w = -nRT_h \ln\left(\frac{v_b}{v_a}\right) \Rightarrow q = nRT_h \ln\left(\frac{v_b}{v_a}\right)$$

Heat absorbed from step $a \rightarrow b$

$$c. \text{ } W_{\text{total}} = W_{ab} + W_{bc} + W_{cd} + W_{da}$$

$$W_{\text{total}} = -nRT_h \ln\left(\frac{V_b}{V_a}\right) - nRT_c \ln\left(\frac{V_d}{V_c}\right)$$

$$W_{\text{total}} = -(T_h - T_c) nR \ln\left(\frac{V_b}{V_a}\right)$$

Total work is negative = system does work on surroundings

d. Efficiency = $\frac{\text{net work done by heat engine}}{\text{heat absorbed by heat engine}}$
 (ϵ)

$$\epsilon = \frac{-W}{Q} = - \frac{[-(T_h - T_c) nR \ln(V_b/V_a)]}{nRT_h \ln(V_b/V_a)}$$

$$\epsilon = \frac{T_h - T_c}{T_h} = 1 - \frac{T_c}{T_h}, \text{ therefore } \epsilon < 1$$

3. a. (T, C_p, α, β) , and no derivatives
 $\left(\frac{\partial S}{\partial T}\right)_P, \left(\frac{\partial S}{\partial P}\right)_T$

$$S(T, P)$$

$$dS = \left(\frac{\partial S}{\partial T}\right)_P dT + \left(\frac{\partial S}{\partial P}\right)_T dP$$

$$\left(\frac{\partial S}{\partial P}\right)_P = \frac{C_p}{T} \text{ and } \left(\frac{\partial S}{\partial T}\right)_P = \frac{1}{T} \left[\left(\frac{\partial H}{\partial P}\right)_T - V \right]$$

$$\text{Maxwell's relation: } \left(\frac{\partial S}{\partial P}\right)_T = - \left(\frac{\partial V}{\partial T}\right)_P = -V\beta$$

$$dS = \frac{C_p}{T} dT - \left(\frac{\partial V}{\partial T}\right)_P dP$$

$$\underline{b.} \quad ds = \left(\frac{\partial s}{\partial T}\right)_P dT + \left(\frac{\partial s}{\partial P}\right)_T dP$$

$$dU = Tds - PdV = dH - PdV - VdP$$

$$ds = \frac{1}{T} dH - \frac{V}{T} dP$$

$$dH = \left(\frac{\partial H}{\partial T}\right)_P dT + \left(\frac{\partial H}{\partial P}\right)_T dP = (PdT + \left(\frac{\partial H}{\partial P}\right)_T dP$$

$$ds = \frac{CP}{T} dT + \frac{1}{T} \left[\left(\frac{\partial H}{\partial P}\right)_T - V \right] dP = \left(\frac{\partial s}{\partial T}\right)_P dT + \left(\frac{\partial s}{\partial P}\right)_T dP$$

$$\left(\frac{\partial s}{\partial T}\right)_P = \frac{CP}{T} \text{ and } \left(\frac{\partial s}{\partial P}\right)_T = \frac{1}{T} \left[\left(\frac{\partial H}{\partial P}\right)_T - V \right]$$

$$\left(\frac{\partial}{\partial T} \left(\frac{\partial s}{\partial P}\right)_T\right)_P = \left(\frac{\partial}{\partial P} \left(\frac{\partial s}{\partial T}\right)_P\right)_T$$

$$\left(\frac{\partial}{\partial T} \left(\frac{\partial s}{\partial P}\right)_T\right)_P = \frac{1}{T} \left(\frac{\partial CP}{\partial P}\right)_T = \frac{1}{T} \left(\frac{\partial}{\partial P} \left(\frac{\partial H}{\partial T}\right)_P\right)_T$$

$$\left(\frac{\partial}{\partial T} \left(\frac{\partial s}{\partial P}\right)_T\right)_P = \frac{1}{T} \left[\left(\frac{\partial}{\partial T} \left(\frac{\partial H}{\partial P}\right)_T\right)_P - \left(\frac{\partial V}{\partial T}\right)_P \right] - \frac{1}{T^2} \left[\left(\frac{\partial H}{\partial P}\right)_T - V \right]$$

$$\frac{1}{T} \left(\frac{\partial}{\partial T} \left(\frac{\partial H}{\partial P}\right)_T\right)_P = \frac{1}{T} \left[\left(\frac{\partial}{\partial T} \left(\frac{\partial H}{\partial P}\right)_T\right)_P - \left(\frac{\partial V}{\partial T}\right)_P \right] - \frac{1}{T^2} \left[\left(\frac{\partial H}{\partial P}\right)_T - V \right]$$

$$\left(\frac{\partial H}{\partial P}\right)_T - V = -T \left(\frac{\partial V}{\partial T}\right)_P$$

$$\left(\frac{\partial s}{\partial P}\right)_T = - \left(\frac{\partial V}{\partial T}\right)_P = -V\beta$$

$$ds = \frac{CP}{T} dT - V\beta dP$$

$$\Delta S = \int_{T_i}^{T_f} \frac{CP}{T} dT - \int_{P_i}^{P_f} V\beta dP$$

Numerical Problems:

$$1. \Delta H^{\circ}_{\text{reaction}} = \sum \Delta H^{\circ}_{\text{products}} - \sum \Delta H^{\circ}_{\text{reactants}} \\ = [(-1364 - 278 - 394) - (-1273)] \text{ kJ/mol}$$

$$\Delta H^{\circ}_{\text{reaction}} = -763 \text{ kJ/mol}$$

$$\Delta S^{\circ}_{\text{reaction}} = \sum S^{\circ}_{\text{products}} - \sum S^{\circ}_{\text{reactants}} \\ = [(192 + 161 + 213) - (209)] \text{ J/mol}\cdot\text{K}$$

$$\Delta S^{\circ}_{\text{reaction}} = 357 \text{ J/mol}\cdot\text{K}$$

$$\Delta S^{\circ}_{\text{surroundings}} = -\frac{\Delta H^{\circ}_{\text{reaction}}}{T} = -\frac{(-763 \text{ kJ/mol})}{298 \text{ K}} = 2.56 \times 10^3 \frac{\text{J}}{\text{mol}\cdot\text{K}}$$

$$\Delta S^{\circ}_{\text{surrounding}} = 2.56 \times 10^3 \text{ J/mol}\cdot\text{K}$$

$$\Delta S^{\circ}_{\text{universe}} = \Delta S^{\circ}_{\text{reaction}} + \Delta S^{\circ}_{\text{surroundings}} = 357 \text{ J/mol}\cdot\text{K} + 2.56 \times 10^3 \text{ J/mol}\cdot\text{K}$$

$$\Delta S^{\circ}_{\text{universe}} = 2917 \text{ J/mol}\cdot\text{K}$$

This reaction is spontaneous because $\Delta S^{\circ}_{\text{universe}} > 0$

$$2. \Delta_{\text{vap}}H_m(25.0^{\circ}\text{C}) = 42.3 \text{ kJ/mol}$$

$$C_p^g = 65.6 \text{ J/mol}\cdot\text{K} + 2.38 \times 10^{-4} \text{ T J/mol}\cdot\text{K}^{-2}$$

$$C_p^l = 112. \text{ J/mol}\cdot\text{K}$$

$$\Delta H_m(78.3^{\circ}\text{C}) = \Delta_{\text{vap}}H_m(25^{\circ}\text{C}) + \int_{298 \text{ K}}^{351.3 \text{ K}} \Delta C_p dT$$

$$\Delta C_p = C_{p,\text{product}} - C_{p,\text{react}} = (C_p^{\text{gas}} - C_p^{\text{liq}}) \\ = (65.6 \text{ J/mol}\cdot\text{K} + 2.38 \times 10^{-4} \text{ T J/mol}\cdot\text{K}) - 112 \text{ J/mol}\cdot\text{K} \\ = -46.4 \text{ J/mol}\cdot\text{K} + 2.38 \times 10^{-4} \text{ T J/mol}\cdot\text{K}$$

$$\int_{298 \text{ K}}^{351.3 \text{ K}} C_p dT = \int_{298 \text{ K}}^{351.3 \text{ K}} (-46.4 \text{ J/mol}\cdot\text{K} + 2.38 \text{ T J/mol}\cdot\text{K}) dT$$

$$= -46.4 \left[\frac{\text{J}}{\text{mol}} \right] \left| \frac{351.3 \text{ K}}{298 \text{ K}} \right| + 2.38 \times 10^{-4} \left[\frac{\text{J}}{\text{mol}} \right] \left| \frac{351.3 \text{ K}}{298 \text{ K}} \right|^2$$

$$= -46.4(351.3 - 298) + 1.19 \times 10^{-4}(351.3^2 - 298^2)$$

$$= -2473.12 \text{ J/mol} + 4.1183 \text{ J/mol}$$

$$= -2469 \text{ J/mol} = -2.469 \text{ kJ/mol}$$

$$\boxed{\Delta H_m = -2.469 \text{ kJ/mol}}$$

$$\Delta_{\text{vap}} H_m(78.3^\circ \text{C}) = \Delta_{\text{vap}} H_m(25^\circ \text{C}) + \int_{298 \text{ K}}^{351.3 \text{ K}} (p \, dT)$$

$$= 42.3 \text{ kJ/mol} - 2.469 \frac{\text{kJ}}{\text{mol}}$$

$$\boxed{\Delta_{\text{vap}} H_m = 39.831 \text{ kJ/mol}}$$

$$\Delta_{\text{vap}} S_m(78.3^\circ \text{C}) = \frac{\Delta_{\text{vap}} H_m(78.3^\circ \text{C})}{T \ln(T)} = \frac{39.831 \text{ kJ/mol}}{351.3 \text{ K}}$$

$$\boxed{\Delta_{\text{vap}} S_m = 113.38 \text{ J/mol/K}}$$

Graphical Problems :

3. $S_m(70 \text{ K})$, calculate $S_m(150 \text{ K})$, $\Delta S_{70 \text{ K} \rightarrow 150 \text{ K}}$

$$S_m(70 \text{ K}) = \int_0^{23.66} \frac{C_{p,m}^{\text{solid III}}(T)}{T} dT + \frac{93.80 \text{ J}}{23.66 \text{ K}} + \int_{23.66}^{43.76} \frac{C_{p,m}^{\text{solid II}}(T)}{T} dT + \frac{743 \text{ J}}{43.76 \text{ K}}$$

$$+ \int_{43.76}^{54.39} \frac{C_{p,m}^{\text{solid I}}(T)}{T} dT + \frac{445.0 \text{ J}}{54.39 \text{ K}} + \int_{54.39}^{70.0 \text{ K}} \frac{C_{p,m}^{\text{liquid}}(T)}{T} dT$$

$$= 8.182 \text{ J/K} + 3.964 \text{ J/K} + 17.61 \text{ J/K} + 16.98 \text{ J/K} + 10.13 \text{ J/K} + 8.182 \text{ J/K}$$

$$+ 13.323$$

$$= 180.37 \text{ J/mol/K}$$

$$\begin{matrix} 70\text{K} & & 298 \\ 80.37 & \longrightarrow & 205 \end{matrix}$$

$$\begin{aligned} S_m^{\circ} 150\text{K} = & \int_0^{29.66} \frac{C_{p,m}^{\text{solid III}}}{T} dT + \frac{43.80\text{J}}{29.66\text{K}} + \int_{29.66}^{43.76} \frac{C_{p,m}^{\text{solid II}}}{T} dT + \frac{743\text{J}}{43.76\text{K}} \\ & + \int_{43.76}^{54.39} \frac{C_{p,m}^{\text{solid I}}}{T} dT + \frac{445\text{J}}{54.39\text{K}} + \int_{54.39}^{90.20} \frac{C_{p,m}^{\text{liquid}}}{T} dT + \frac{6815\text{J}}{90.20\text{K}} \\ & + \int_{90.20\text{K}}^{150\text{K}} \frac{C_{p,m}^{\text{gas}}}{T} dT \end{aligned}$$

$$\begin{aligned} = & 8.182\text{J/K} + 3.964\text{J/K} + 19.61\text{J/K} + 16.98\text{J/K} + 16.13\text{J/K} \\ & + 8.181\text{J/K} + 27.06\text{J/K} + 75.59\text{J/K} + 14.973 \end{aligned}$$

$$S_m^{\circ} 150\text{K} = 184.67\text{J/molK}$$

$$\begin{aligned} \Delta S_{70\text{K} \rightarrow 150\text{K}} &= 184.67\text{J/molK} - 80.37\text{J/molK} \\ &= 104.3\text{J/molK} \end{aligned}$$