Kevin Zhang Macroscapic Physical Chem Reading Assignment 7 7.1: Real Gases and Ideal Go Das molecules are point masses Moleules orupy a finite volume. - a real gas cornot be compressed to a volume less than total molecular volume Second assumption is that gas molecules do not interact but gas molecules do interact through a potential The molecular volume is neglible compared w/ the volume the gas oupies The P-V-T relationship b/w a ideal gas is the same as that of a real gus. 7.2: Equations of state for real gases and their range of applicability. Real gas equations of state are list viewed as empirical equations whose functional form has been chosen to fit experimentally P-V-T data Van der Waals Equation

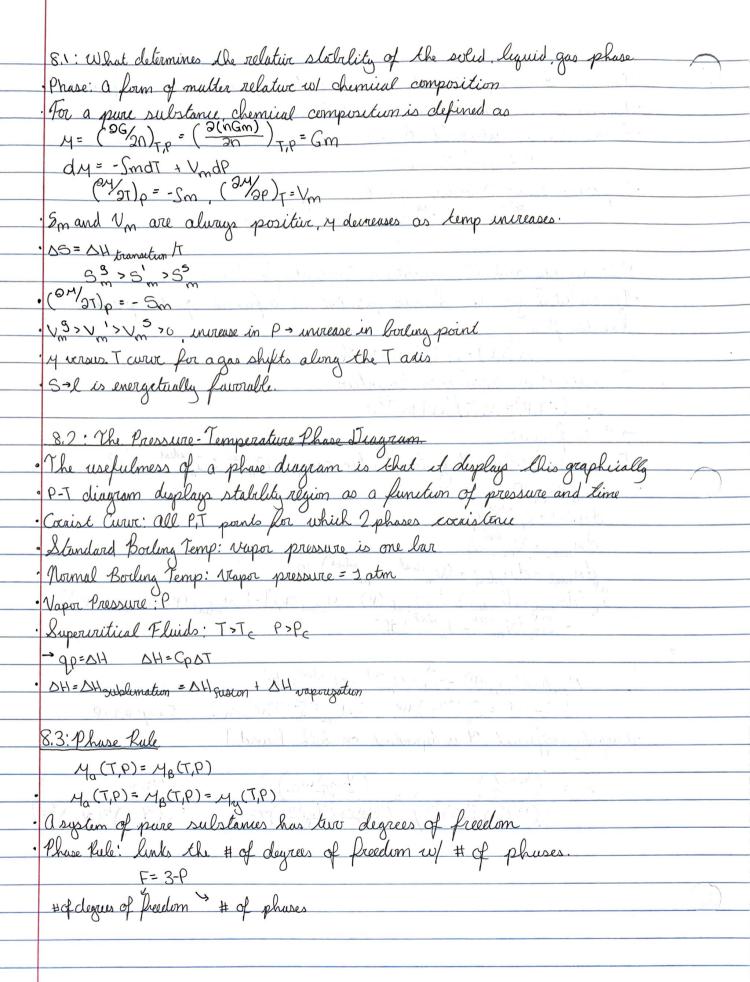
P= PX - b - 42 = "IKTY - nb -Redlich - Kwong Equation of State P= 87/m-6-(-457) /m(vm+6))= · Beuttie - Bridgeman Equation P= R/2 (1- / -3) (VMB) - A/2 L= A= A0 (1-9/m), B=B(1-6/m) · Virul Equation of State P= RT[1/m + B(T) + - always valid in convergence runge Value of V when P busines constant depends on T. V - decrease P - increases Vapor Pressure - temperature - dependent equilibrium les pressure further increases, system becomes single phase $\mathcal{O}_2(l)$ Critical Temperature: The temp at which the range of Im shunks to single phase.

 $(\frac{\partial P}{\partial V_m})_{T=T_c} = 0$ and $(\frac{\partial P}{\partial V_m})_{T=T_c} = 0$ · Tele Ve are the critical constants eln the Maxwell Construction, the oscillating region is replaced by the horizontal lines to which the orea above and below are equal 7.3. The Compression Factor Compression factor 3, is determined by Z = Vm / ideal = PVm / 25- a function of temperature · We use the Van der Waals equation to understand the low pressure value $Z = Vm/\sqrt{1000}$ ideal = VVm/PTTo and the corresponding values Known as Boyle's TB · B/c the parameters a and b are temp dependent, To is different for each gas. at Boyle temp, 2 > 2 and (22/2P) -0 The inequalities provides criterium to predict whether Z increases or devicases w/ pressure. lim (32/2P) is always positive @ high temp eff T<<TB, lim(22/28), will always be negative If $\lim_{z \to 2/2P} < 0$, the attracture part of gas dominates 7.4. The Law of Cornesponding & tates · Different gases have the same equation of state of each gas is described by the dimensionless reduced variables - law of Corresponding States P.V.T variables of two gases can be different for corresponding states Variables a and B are eliminated

PRP = RT, Tc/mr/mc b - 2mr/mc Pc = 9/2762 Vmc = 30 and Tc = 80/27Rb $aP_{c} = \frac{8aT_{c}}{27b^{2}} = \frac{8aT_{c}}{270(3bV_{mr}-b)} = \frac{ab^{2}V^{2}_{mr}}{ab^{2}V^{2}_{mr}}$

_	
•	The law of corresponding states assumes two parameters are sufficient
	assumes spheres b/c orientation would be neglible
	Errors can be calculated through
	% ENTOL = Z-1/Z . 100%
	Compression Partor @ critical point.
	Compression factor @ critical point \[\frac{210}{270} = \times \frac{2180}{80} = \frac{3}{8} \]
	75 Englite and the envelopment Constant Do Real Das
-	7.5: Fugauty and the equilibrium Constant for Real Das. For an ideal gas, the chemical potential as a function of the pressure has the form
- /-	1 to an rate gas, she chemine potential as a familiar que se que
	has the form
	$M(T,P) = M^{\circ}(T) + RT \ln(\%)$
•	To construct an analogous Equation
	$\mathcal{A} \left(\mathbf{x} \mathbf{T}, \mathbf{p} \right) = \mathcal{A}_{o}(\mathbf{T})^{O} + R\mathbf{T} \ln \frac{\mathbf{p}}{2} \mathbf{p}$
_	is fuguety
•	For densitues corresponding to attractive range $G_m^{real} < G_m^{real} < G_m^{rea$
•	dGm=VmdP
	dGm=VmdP wheat dp
_	de real = Vm de (v real - V udul) de
	dyreal - dyreal = (Vmenl - Vm) dP
	Sp. (dr neal - drideal) = [y real (P) - Mideal (P)] - [y ideal (P) - Mideal (P)] = Sp. (V meal - V ideal) dp ²
	- Sp. (V new - v ideal) dp2
	- TADONA HAS
	Mread(P) = -Sp (Nm real - Vm ideal) dp!
	Inf-InP + Se (z-1/p) dp', &= Pexp[St(z-1/p))dp'], f=y(p,T)p
	Fuguety Cofficient. Y is dependent on both Pand T
	(970 k × 60 71 k
	$\chi_{c} = \frac{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \frac{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \frac{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \frac{\chi_{b} + \frac{3}{2} + \frac{3}{2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \frac{\chi_{b} + \frac{3}{2} + \frac{3}{2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \frac{\chi_{b} + \frac{3}{2} + \frac{3}{2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \frac{\chi_{b} + \frac{3}{2} + \frac{3}{2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \frac{\chi_{b} + \frac{3}{2} + \frac{3}{2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \frac{\chi_{b} + \frac{3}{2} + \frac{3}{2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \frac{\chi_{b} + \frac{3}{2} + \frac{3}{2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \frac{\chi_{b} + \frac{3}{2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \frac{\chi_{b} + \frac{3}{2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \frac{\chi_{b} + \frac{3}{2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \frac{\chi_{b} + \frac{3}{2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \frac{\chi_{b} + \frac{3}{2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \frac{\chi_{b} + \frac{3}{2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \frac{\chi_{b} + \frac{3}{2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \frac{\chi_{b} + \frac{3}{2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \frac{\chi_{b} + \frac{3}{2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \frac{\chi_{b} + \frac{3}{2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \frac{\chi_{b} + \frac{3}{2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \frac{\chi_{b} + \frac{3}{2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \frac{\chi_{b} + \frac{3}{2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \frac{\chi_{b} + \frac{3}{2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \frac{\chi_{b} + \frac{3}{2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \frac{\chi_{b} + \frac{3}{2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \frac{\chi_{b} + \frac{3}{2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \frac{\chi_{b} + \frac{3}{2}}{\left(\frac{1}{2} \ln \frac{3}{2} + \frac{3}{2}\right)^{3/2}} = \chi_{b} = \chi_$
	(FN2/Cox FH2)3/2) (4N20N2) (4N20H2)3/2 KP (4) 1/2 (4) 3/2)
	and the language to the first the fi
	page of the training of the standard of the st

is all my our or existence in the si



8.4: The P-V and P-V-T phase diagrams Cong diagram must contain all 3 to be complete g-l corristence region is broader than 5-l phase In P-V phase diagram, the process involves large change in volume P-V-T diagram displays the value of U, P,T P-T diagram is a projection of 3-D surface. on the P-T plane 8.5. Providing a theoretically busis for the P-T phase deagram 4 (P,T) = MB(P,T) P,T -> P + dP, T + dT such that pressure + lemp still lie within coexistens curuc Ma(P,T) + dMa = MB(P,T) + dMB In order for the two phases to remain in equilibrium dya = dya dMa = - Sma dT + VmadP and dys = - SubdT + Vmb dP - Smadt + VmadP = - SmbdT + VmBdP (SmB-Sma)dT=(VmB-Vma)dP ASm = Smp AVm = VmB - Vma dP/ DS vae/ = DH vap/ gas = PDH vap/ RT2

dP/p = DH vap/B dT/2 · Variation of vapor pressure is given by

SRE dP/p = SHap/R . STE dT/-2

In PE/p = - DHap/R . (14 - 17;) 8.7: The Vapor Pressure of pure substance depends on the applied Pressure · Neiping T constant, enough argon gas is introduced into cylinder such that aryon + H20 = 1 bar. To calculate the partial pressure of water; $(\frac{2m_e(T,P)}{2P})_T = (\frac{2M_e(T,P)}{2P})_T (\frac{2P}{2P})_T$ · Vm (8) (9) (98/28) 7 or (38/28) 7 = Vm(6) / (9) Vapor pressure encreases if total pressure increase

RT/p dp = Vm dP or RTSP dP'p' = Vm Spo dp'

Hop of the noduced is its hack tensile strungth The property of water that amounts for the water supply to the the weight of the externit in the grantinal full part. Capillary ruse and depression are other consequences of pressence - 6-6= 24 (18-18) 47117 day Parter + STILLE = 47117 Pinner pressure and the base arising from the surfuse tonsion · elmend outing force is the sum of forces switted by the external 16-47172 do=87174=0 Europus Lensin hus runico sufurd aby=Ab as Thus V surd is . The work associated we the creation of orlitional surfuse onces @ 8.8; Surface Tension P-OIX POLL = 09 01. (318.0.1)(1 10m m OIX 18.1) satur to saw willings soft.

P-OIX POLL = (3/2)(1)(1 - 10m m OIX 18.1) = (3/2)(1), mV = (3/2)(1) (°9-9) (X) (9-9°)