

Figure 1: Background for the app

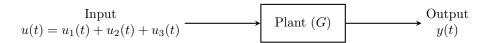
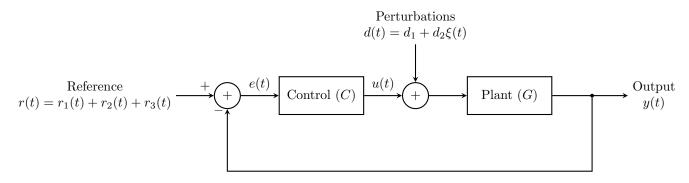
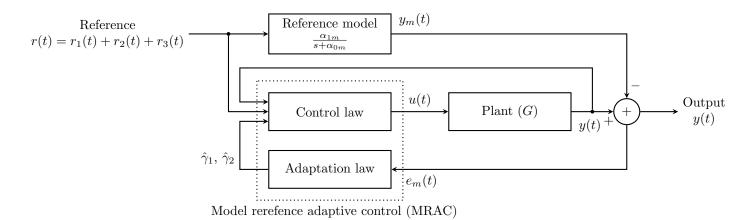


Figure 2: Open loop system



$$\begin{split} C(s) &= \frac{U(s)}{E(s)} = K_P + \frac{K_I}{s} + K_D s \\ C(z) &= \frac{U(z)}{E(z)} = K_P + K_I \frac{T_S(z+1)}{2(z-1)} + K_D \frac{z-1}{zT_S} \\ T_S \text{ is sampling time and } \xi(t) \text{ is white noise with zero mean power 1.} \end{split}$$

Figure 3: Closed loop system with a PID Controller



Control law:

$$u(t) = \hat{\gamma}_1(t)r(t) + \hat{\gamma}_2(t)y(t)$$

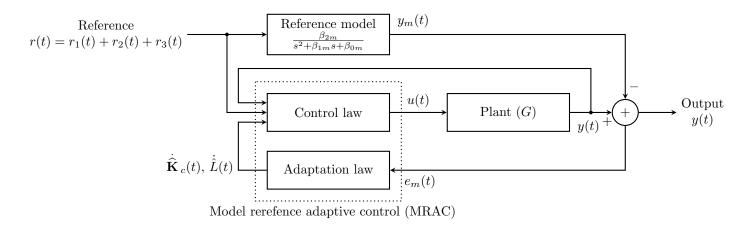
Adaptation law:

$$\dot{\hat{\gamma}}_1(t) = -\varrho e_m(t) r(t)$$

$$\dot{\hat{\gamma}}_2(t) = -\varrho e_m(t) y(t)$$

where $e_m = y - y_m$, $\varrho > 0$ is called adaptation gain and T_S is sampling time.

Figure 4: Adaptive control



Model:

$$\dot{\mathbf{x}}_{m}(t) = \widehat{\mathbf{A}}_{mc}\mathbf{x}_{m}(t) + \widehat{\mathbf{B}}_{mc}r(t)$$

$$\mathbf{A}_{mc} = \begin{bmatrix} 0 & 1 \\ -\beta_{0m} & -\beta_{1m} \end{bmatrix}, \quad \mathbf{B}_{mc} = \begin{bmatrix} 0 \\ \beta_{2m} \end{bmatrix}, \quad \mathbf{x}_{m}(t) = [y_{m}(t), \ \dot{y}_{m}(t)]^{T}$$

Control law:

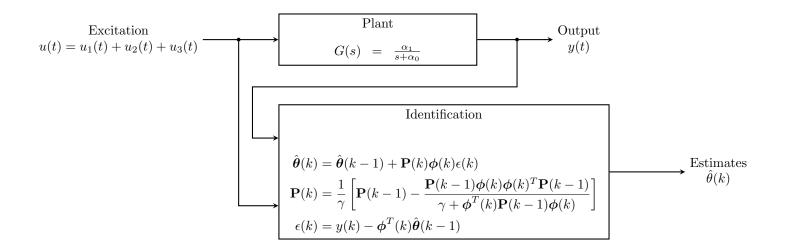
$$u(t) = \widehat{\mathbf{K}}_c(t)\mathbf{x}(t) + \widehat{L}(t)r(t)$$

Adaptation law:

$$\begin{split} & \dot{\hat{\mathbf{K}}}_{c}(t) = \gamma \mathbf{B}_{mc}^{T} \mathcal{P} \mathbf{E}(t) \mathbf{x}^{T}(t) \\ & \dot{\hat{L}}(t) = \gamma \mathbf{B}_{mc}^{T} \mathcal{P} \mathbf{E}(t) r(t) \end{split}$$

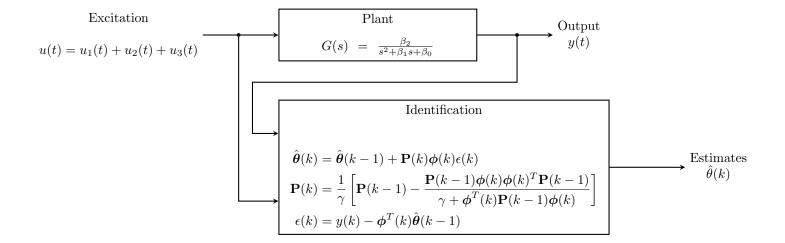
where T_S is sampling time, $\gamma > 0$ is the adaptation gain, $\mathbf{x}(t) = [y(t), \dot{y}(t)]^T$, $\mathbf{E}_m(t) = [e_m(t), \dot{e}_m(t)]^T$ and matrix $\mathcal{P} = \mathcal{P}^T$.

Figure 5: Adaptive control



$$\begin{split} \mathbf{P}(0) &= \mathbf{P_0} = \mathbf{P_0}^\mathsf{T} > 0, \, \mathbf{P_0} = \rho \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}, \, \boldsymbol{\phi} = \begin{bmatrix} y(k-1) & u(k-1) \end{bmatrix}^\mathsf{T}, \\ \boldsymbol{\theta} &= \begin{bmatrix} \theta_1 & \theta_2 \end{bmatrix}^\mathsf{T}, \, \hat{\boldsymbol{\theta}} = \begin{bmatrix} \hat{\theta}_1 & \hat{\theta}_2 \end{bmatrix}^\mathsf{T}, \, \hat{\alpha}_0 = \frac{-\ln \hat{\theta_1}}{T_S}, \, \hat{\alpha}_1 = \frac{\hat{\alpha}_0 \hat{\theta_2}}{1 - \hat{\theta_1}}, \, \text{and} \\ T_S \text{ is sampling time.} \end{split}$$

Figure 6: First order system identification



Discretized plant model: $y(k) = \theta_1 y(k-1) + \theta_2 y(k-2) + \theta_3 u(k-1) + \theta_4 u(k-2) = \boldsymbol{\phi}^T(k) \boldsymbol{\theta},$ $\boldsymbol{\theta} = [\theta_1, \ \theta_2, \ \theta_3, \ \theta_4]^T,$ $\boldsymbol{\phi}(k) = [y(k-1), \ y(k-2), \ u(k-1), \ u(k-2)]^T,$ $\hat{\boldsymbol{\theta}}(k) = [\hat{\theta}_1(k), \ \hat{\theta}_2(k), \ \hat{\theta}_3(k), \ \hat{\theta}_4(k)]^T,$ T_S is sampling time,

$$P(0) = P_0 = P_0^{\mathsf{T}} > 0, P_0 = \rho \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}.$$

Discretized plant model in state space:

$$\mathbf{x}(k+1) = \hat{\mathbf{A}}_d \mathbf{x}(k) + \hat{\mathbf{B}}_d u(k)$$
$$y(k+1) = \hat{\mathbf{C}}_d \mathbf{x}(k)$$

where

$$\hat{\mathbf{A}}_d = \begin{bmatrix} 0 & 1 \\ -\hat{\theta}_2 & -\hat{\theta}_1 \end{bmatrix}, \qquad \hat{\mathbf{B}}_d = \begin{bmatrix} 0 \\ 1 \end{bmatrix}, \qquad \hat{\mathbf{C}}_d = [\hat{\theta}_4, \ \hat{\theta}_3]$$

. Estimated continuous model is:

$$\dot{\mathbf{x}}(t) = \hat{\mathbf{A}}_c x(t) + \hat{\mathbf{B}}_c u(t)$$
$$y(t) = \hat{\mathbf{C}}_c \mathbf{x}(t)$$

where

$$\widehat{\mathbf{A}}_{c} = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} = \frac{2}{T} \mathbf{R} \left[\mathbf{I}_{2x2} - \frac{8}{21} \mathbf{R}^{2} - \frac{4}{105} \mathbf{R}^{4} \right] \left[\mathbf{I}_{2x2} - \frac{5}{7} \mathbf{R}^{2} \right]^{-1}$$

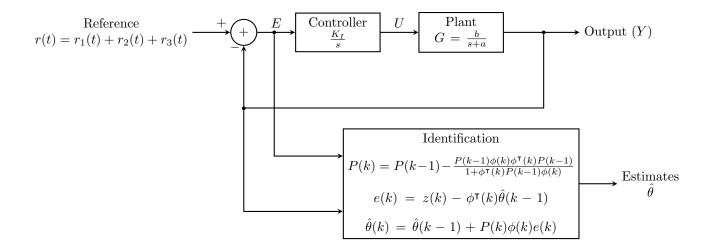
$$\widehat{\mathbf{B}}_{c} = \begin{bmatrix} b_{11} \\ b_{21} \end{bmatrix} = \widehat{\mathbf{A}}_{c} \left[\widehat{\mathbf{A}}_{d} - \mathbf{I}_{2x2} \right]^{-1} \widehat{\mathbf{B}}_{d}, \qquad \widehat{\mathbf{C}}_{c} = [c_{11}, c_{12}] = \widehat{\mathbf{C}}_{d}$$

$$\mathbf{R} = \left[\widehat{\mathbf{A}}_{d} - \mathbf{I}_{2x2} \right] \left[\widehat{\mathbf{A}}_{d} + \mathbf{I}_{2x2} \right]^{-1}$$

So, we calculate:

$$\hat{\beta}_0(k) = a_{11}a_{22} - a_{12}a_{21}, \quad \hat{\beta}_1 = -(a_{11} + a_{22}), \quad \hat{\beta}_2 = c_{11}(b_{21}a_{12} - b_{11}a_{22}) + c_{12}(b_{11}a_{21} - b_{21}a_{11})$$

Figure 7: Second order system identification



$$P(0) = P_0 = P_0^{\mathsf{T}} > 0, P_0 = \rho \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}, z = y(k) - y(k-1),$$

$$\phi = \begin{bmatrix} e(k-1) + e(k-2) \\ y(k-1) - y(k-2) \end{bmatrix}, \theta = \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix}, \hat{a} = -\frac{\ln \hat{\theta}_2}{T_S}, \hat{b} = \frac{2\hat{\theta}_1 \hat{a}}{T_S(1-\hat{\theta}_2)K_I},$$
and T_S is sampling time.

Figure 8: Parameter estimation of a first order system with integral controller