Conjunction Assessment Risk Analysis



Evaluating Probability of Collision (Pc) Uncertainty

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- Conjunction Assessment Basics
- Probability of Collision (Pc) calculation outline
- Pc uncertainty overview
- Pc uncertainty component: covariance uncertainty
 - Covariance realism assessment
 - Covariance realism PDF generation
- Pc uncertainty component: hard-body radius uncertainty
 - Primary objects using projected-area sampling
 - Secondary objects using radar cross-section values
- Pc uncertainty component: natural variation in Pc calculation
- Example output
- Conclusions and future work





How are Satellite Collision Risks Determined/Mitigated?

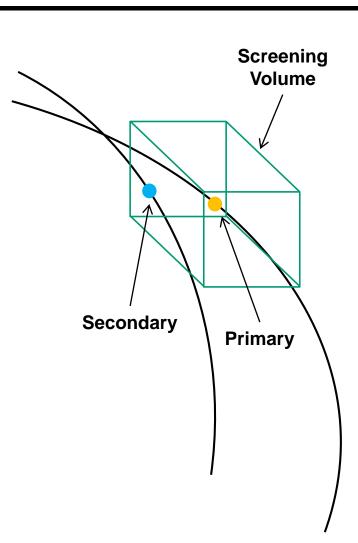
- Certain spacecraft are determined to be "defended assets"
 - Will be evaluated for collision risk with other objects
- For seven days into the future, the expected positions of the defended asset and the rest of the objects in the space catalogue are determined
- "Keep-out volume" box drawn around the defended asset at each time-step
 - Typically 5km x 5km x 25km in size, with the longer dimension along the orbit path
- Any satellite that penetrates the keep-out volume during the 7-day analysis is considered a possible "conjunctor"
- Particulars of the close approach analyzed to determine actual conjunction risk





"Fly By" Ephemeris Comparison

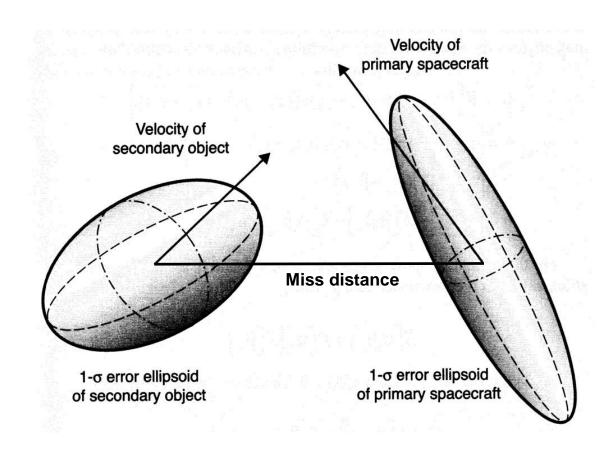
- Ephemerides generated for primary and secondaries that are possible threats
- Screening volume box (or ellipsoid) constructed about primary
- Box "flown" along the primary's ephemeris
- Any penetrations of box constitute possible conjunctions
- For these conjunctions, Conjunction Data Message (CDM) generated
 - State estimates and covariances at TCA
 - Relative encounter information
 - OD information
- CDM data used to calculate probability of collision (Pc)

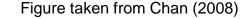






Calculating Probability of Collision (Pc): 3D Situation at Time of Closest Approach (TCA)









Calculating Pc: 2-D Approximation (1 of 3) **Combining Error Volumes**

Assumptions

- Error volumes (position random variables about the mean) are uncorrelated

Result

- All of the relative position error can be centered at one of the two satellite positions
 - Secondary satellite is typically used
- Relative position error can be expressed as the additive combination of the two satellite position covariances (proof given in Chan 2008)
 - $C_a + C_b = C_c$
- Must be transformed into a common coordinate system, combined, and then transformed back

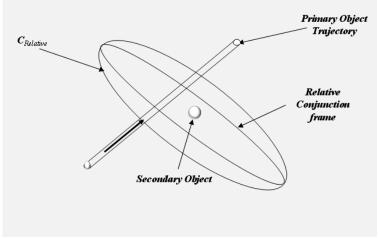




Calculating Pc: 2-D Approximation (2 of 3) **Projection to Conjunction Plane**

- Combined covariance centered at position of secondary at TCA
- Primary path shown as "soda straw"
- If conjunction duration is very short
 - Motion can be considered to be rectilinear—soda straw is straight
 - Conjunction will take place in 2-d plane normal to the relative velocity vector and containing the secondary position
 - Problem can thus be reduced in dimensionality from 3 to 2

 Need to project covariance and primary path into "conjunction plane"

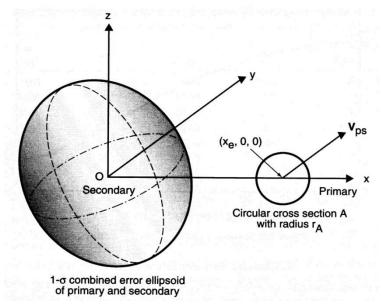






Calculating Pc: 2-D Approximation (3 of 3) Conjunction Plane Construction

- Combined covariance projected into plane normal to the relative velocity vector and placed at origin
- Primary placed on x-axis at (miss distance, 0) and represented by circle of radius equal to sum of both spacecraft circumscribing radii ("hard-body radius" or HBR")
- Z-axis perpendicular to x-axis in conjunction plane





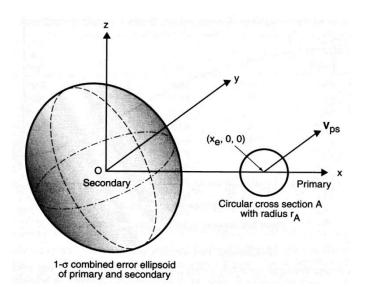




2-D Probability of Collision Computation

- Rotate axes until they align with principal axes of projected covariance ellipse
- Pc is then the portion of the density that falls within the HBR circle
 - r is [x z] and C* is the projected covariance

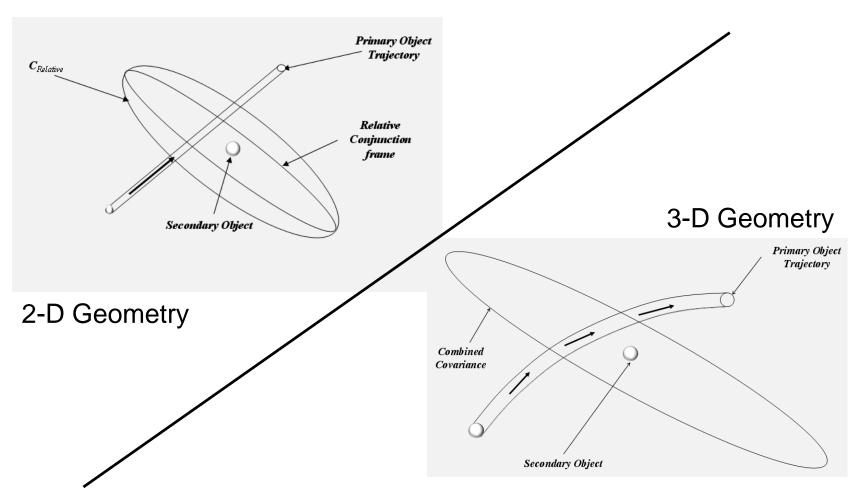
$$P_{C} = \frac{1}{\sqrt{(2\pi)^{2} |C^{*}|}} \iint_{A} \exp\left(-\frac{1}{2}\vec{r}^{T}C^{*-1}\vec{r}\right) dXdZ$$







2-D vs. 3-D Conjunction Geometry







Low Relative Velocity or Long Conjunction Duration Situation

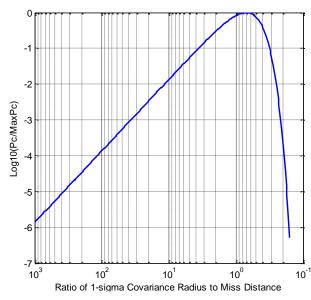
- 2-D approximation not valid
- Can attempt 3-D integral
 - Messy, but Coppola (2012) outlines methodology with Lebedev quadrature
- Can use Monte Carlo
 - From TCA
 - Propagate both satellites' states and covariances to nominal TCA
 - Take position (and maybe velocity) perturbations from each covariance to define new states for primary and secondary
 - Find new TCA and record miss distance
 - Tabulate all miss distances; percent that are smaller than HBR is Pc
 - From epoch
 - Similar procedure to above, but perturbations performed at epoch
 - Perturbed states propagated forward to new TCA with full non-linear dynamics





Conjunction Event Canonical Progression

- Conjunction typically first discovered 7 days before TCA
 - Covariances large, so typically Pc below maximum
- As event tracked and updated, changes to state estimate are relatively small, but covariance shrinks
 - Because closer to TCA, less uncertainty in projecting positions to TCA
- Theoretical maximum Pc encountered when 1-sigma covariance size to miss distance ratio is $1/\sqrt{2}$
 - After this, Pc usually decreases rapidly
- Behavior shown in graph at right
 - X-axis is covariance / miss distance
 - Y-axis is $log_{10} (P_c/max(P_c))$
 - Order of magnitude change in Pc considered significant, thus log-space more appropriate







Probability of Collision Calculation

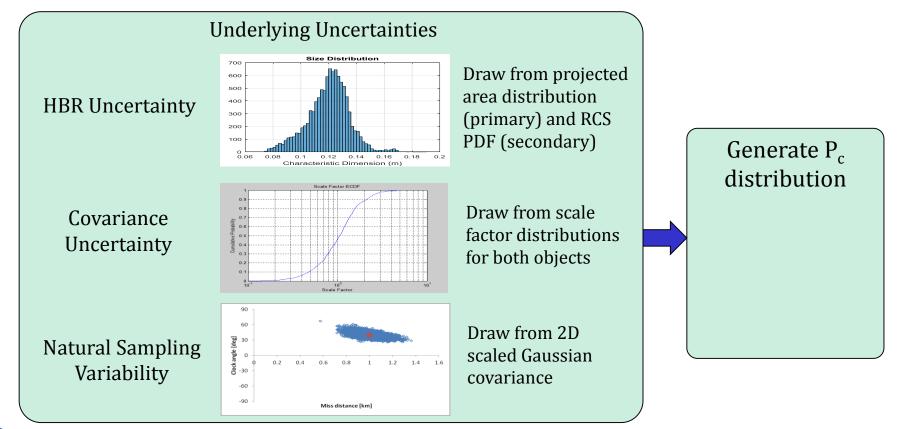
- Pc is only a nominal solution for the conjunction
 - Derived from estimates of the mean
 - If underlying distributions not symmetric, then this is not an expression of central tendency
 - Does not include uncertainties on the inputs
 - "Uncertainty of uncertainty volumes" or uncertainty in HBR
- Thus, while representing the risk, nominal Pc is just a point estimate
- Want to know how much variation or uncertainty in the Pc calculated for any given conjunction
 - Determine uncertainty PDFs for the Pc calculation inputs
 - Through Monte Carlo trials, vary above inputs to the Pc calculation
 - Include a resampling technique to determine natural variation in the calculation
 - Generate a probability density of resultant Pc values
 - Characterize this distribution empirically





Uncertainty in the Probability

- Generate a Pc distribution, using Monte Carlo (MC) trials of the underlying uncertainties
 - Determine uncertainty for each of the Pc parameters







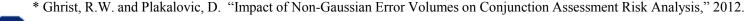
COVARIANCE REALISM AND SCALE FACTORS





Covariance Realism

- Ways a typical covariance can be unrealistic
 - Much larger or smaller than the "real" error volume
 - Differently oriented from the "real" error volume
 - Representing a different distribution from the "real" error distribution
- This last item not addressed in present study
 - Current form of covariance promotes Gaussian assumption
 - A priori arguments for presuming component error distributions close to Gaussian
 - A posteriori evidence for component errors following a symmetric distribution
 - Study indicates large-Pc events not affected by "bending" covariances*
- Large covariances not inherently problematic
 - Rather, quite appropriate if errors themselves are large
- Covariance realism assessment approach is combined evaluation of size and orientation, presuming error volume is Gaussian ellipsoid







JSpOC State and Covariance Accuracy Utility

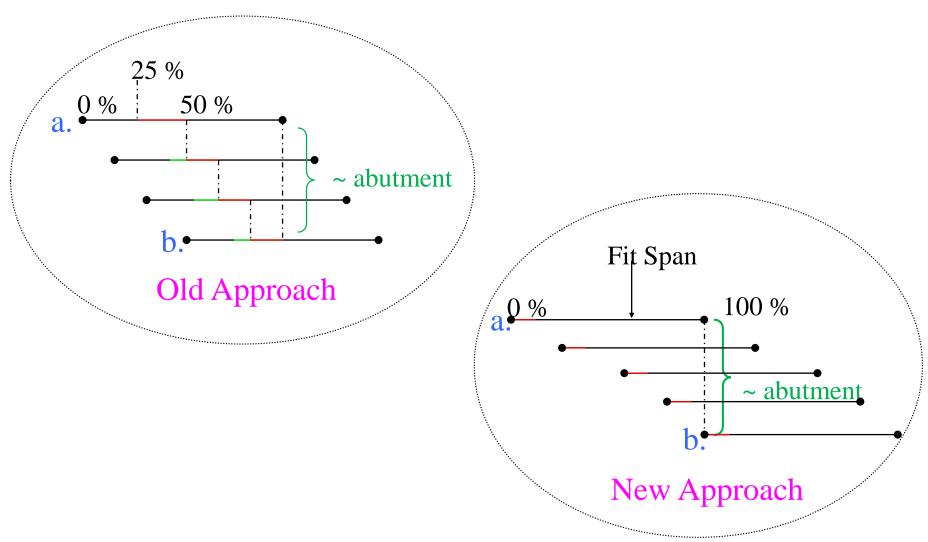
Truth ephemeris produced for every satellite

- Similar to methodology used for generating precision satellite laser ranging orbits
- "Stitched together" pieces of ephemeris from a "judiciously chosen" portion of the fit-spans of subsequent batch ODs
 - Methodology to minimize overlap of portions drawing from same observation base
- Covariance for reference orbit also preserved (epoch covariances from generating ODs)
- Each produced precision vector for each object compared to its reference orbit at propagation states of interest
 - Position comparisons at 6, 12, 18, 24, 36, 48, 72, 120, and 168 hrs
 - Propagated position covariance also calculated and retained at each comparison point
- Raw materials for covariance realism investigations thus available:
 - State errors
 - Propagated covariance at point of comparison and reference orbit covariance





Reference Orbit Formation Approaches: Previous and Present







Normal Deviates and Chi-squared Variables

- Let q and r be vectors of values that conform to a Gaussian distribution
 - Commonly called *normal deviates*
- A normal deviate set can be transformed to a standard normal deviate by subtracting the mean and dividing by the standard deviation
 - This produces the so-called Z-variables

$$Z_q = \frac{q - \mu_q}{\sigma_q}$$
, $Z_r = \frac{q - \mu_r}{\sigma_r}$

 The sum of the squares of a series of standard normal deviates produces a chi-squared distribution, with the number of degrees of freedom equal to the number of series combined

$$Z_q^2 + Z_r^2 = \chi_{2dof}^2$$





Covariance Realism: Normal Deviates in State Estimation

- In a state estimate, the errors in each component (u, v, and w here) are expected to follow a Gaussian distribution
 - If all systematic errors have been solved for, only random error should remain
- These errors can be standardized to the Z-formulation
 - Mean presumed to be zero (OD should produce unbiased results), so no need for explicit subtraction of mean

$$Z_u = \frac{u}{\sigma_u}, \quad Z_v = \frac{v}{\sigma_v}, \quad Z_w = \frac{w}{\sigma_w}$$

 Sum of squares of these standardized errors should follow a chisquared distribution with three degrees of freedom

$$Z_u^2 + Z_v^2 + Z_w^2 = \chi_{3dof}^2$$





Covariance Realism: State Estimation Example Calculation

- Let us presume we have a precision ephemeris, state estimate, and covariance about the state estimate
 - For the present, further presume covariance aligns perfectly with uvw frame (no off-diagonal terms)
- Error vector ε is position difference between state estimate and precision ephemeris, and covariance consists only of variances along the diagonal
 - Inverse of covariance matrix is straightforward

$$\varepsilon = \begin{bmatrix} \varepsilon_u \\ \varepsilon_v \\ \varepsilon_w \end{bmatrix}, \quad C = \begin{bmatrix} \sigma_u^2 & 0 & 0 \\ 0 & \sigma_v^2 & 0 \\ 0 & 0 & \sigma_w^2 \end{bmatrix} \qquad C^{-1} = \begin{bmatrix} 1/\sigma_u^2 & 0 & 0 \\ 0 & 1/\sigma_v^2 & 0 \\ 0 & 0 & 1/\sigma_w^2 \end{bmatrix}$$

$$C^{-1} = \begin{bmatrix} 1/\sigma_u^2 & 0 & 0\\ 0 & 1/\sigma_v^2 & 0\\ 0 & 0 & 1/\sigma_w^2 \end{bmatrix}$$

Resultant simple formula for chi-squared variables

$$\varepsilon C^{-1} \varepsilon^{T} = \frac{\varepsilon_{u}^{2}}{\sigma_{u}^{2}} + \frac{\varepsilon_{v}^{2}}{\sigma_{v}^{2}} + \frac{\varepsilon_{u}^{2}}{\sigma_{w}^{2}} = \chi_{3 \, dof}^{2}$$





Covariance Realism: Non-Diagonal Covariances

- Mahalanobis distance formulary naturally accounts for correlation terms
- Two-dimensional example:

$$\varepsilon C^{-1} \varepsilon^{T} = \frac{1}{1 - \rho^{2}} \left(\frac{\varepsilon_{x}^{2}}{\sigma_{x}^{2}} + \frac{\varepsilon_{y}^{2}}{\sigma_{y}^{2}} - \frac{2\rho \varepsilon_{x} \varepsilon_{y}}{\sigma_{x} \sigma_{y}} \right)$$

- Conforms to intuition
 - As ρ approaches zero, diagonal case recovered





Covariance Realism: Testing for Realism

- Mahalanobis distance set should conform to 3-DoF χ^2 distribution
- Expected value for each calculation is DoF, 3 in this case
- Each Mahalanobis point in principle produces a scale factor
 - mCm sizes covariance such that $\varepsilon C^{-1} \varepsilon^{T}$ will have a value of 3
 - m² thus the proper factor by which to scale the covariance in order to produce the expected value
- However, not every Mahalanobis calculation expected to equal expected value
 - Instead, a chi-squared distribution with expected value of 3
- To set scale factor(s), choose factor that brings entire Mahalanobis distance set into conformity with expected distribution

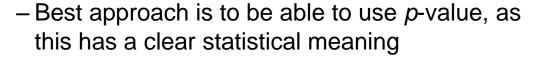


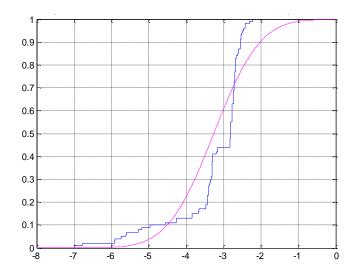


Empirical Distribution Function (EDF) GOF: Exquisite Solution

- Sum of vertical differences between "ideal" and "real" behavior
 - Hypothetical graph at left
- Cramér von Mises formulation the most appropriate for current situation
 - Equations at right
 - Weighting function (ψ) set to unity a better choice for outlier-infused situations







$$Q = n \int_{-\infty}^{\infty} [F_n(x) - F(x)]^2 \psi(x) dx$$

$$\psi(x) = 1$$

 But what if we want a distribution of scale factors?





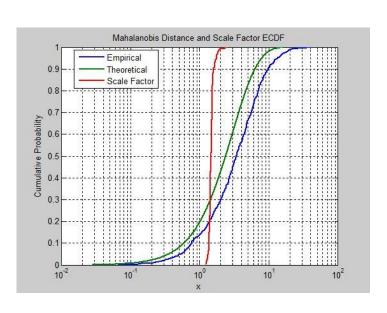
Covariance Realism: Distribution of Scale Factors

Rank-ordering of results can give reasonable PDF of scale factors

- Presume 100 squared Mahalanobis distance values (M2)
 - Derived from JSpOC covariance realism data
- Rank order list
- Align each entry with the 3-DoF χ^2 value that corresponds to that percentile
- Quotient of two terms is (square of) scale factor that produces the χ^2 value expected for that particular percentile

Examples:

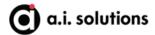
		Square of	
Percentile	x2	M Distance	Quotient
1 (0.01)	0.115	0.183	1.594
2 (0.02)	0.185	0.245	1.326
3 (0.03)	0.245	0.353	1.440
4 (0.04)	0.300	0.418	1.393







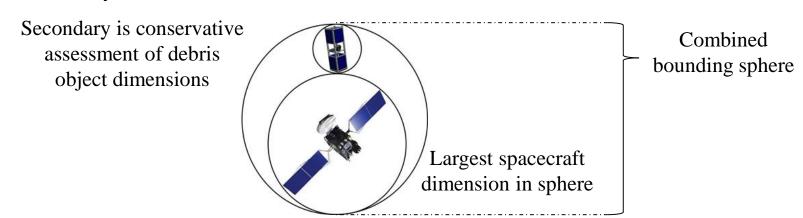
HARD-BODY RADIUS





Hard-Body Radius: Introduction

- HBR is typically found by circumscribing both objects in spheres and combining the objects into one bounding sphere
 - Size of the secondary is typically not known, so added as a large estimate of debris object dimensions

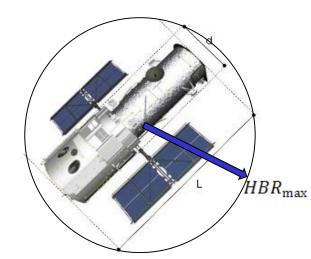


- HBR uncertainties that follow represent a more realistic estimate of the area in the conjunction plane
 - The combined uncertainties are much smaller than the bounding sphere





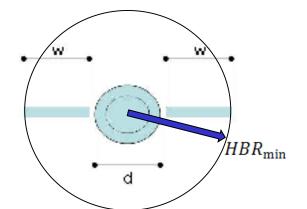
Hard-Body Radius: Min and Max Using Approximation Equations



$$HBR_{\text{max}} = \frac{\sqrt{L^2 + (2w + d)^2}}{2} \approx 8.1 \text{m}$$

$$L = 13.2 \text{m}$$

 $d = 4.2 \text{m}$
 $w = 2.6 \text{m}$



$$HBR_{\min} = \frac{2w + d}{2} \approx 4.7$$
m

Could presume uniform distribution between these values as first-order approximation of PDF, but seems rather arbitrary

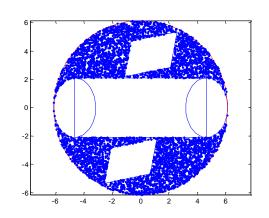


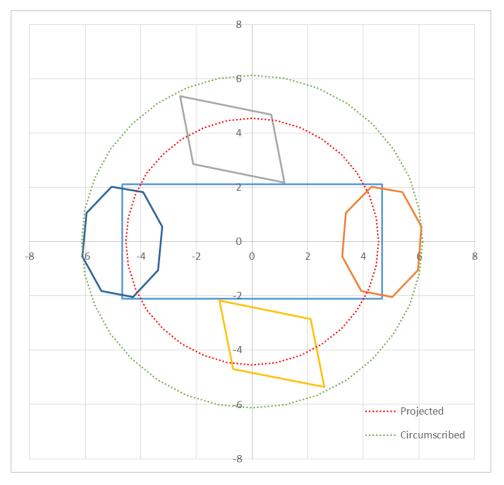


Hard-Body Radius: Projected Area Approach

- Randomized orientation of primary satellite to capture the average area
 - Ball-and-stick model to be created for each primary asset
 - Includes rotating solar panels
- Projected radius
 - Actual hit area of the satellite expressed as a circular radius

$$-r = \sqrt{\frac{A}{\pi}}$$



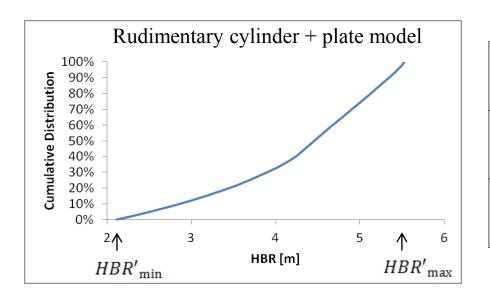






Hard-Body Radius: Projected Area Approach Performance

- NASA/JSC Orbital Debris Program Office (ODPO) has sophisticated satellite model and full Euler angle rotation software to generate projected area PDFs
- Comparison of results for Hubble Space Telescope between ODPO software and ball-and-stick model:



	Average Area [m²]	Average Effective HBR [m]
Crude HST model (corresponding to chart)	60.3	4.3
Sophisticated HST model (Matney*)	63.7	4.5

Good agreement

^{*} M. Matney, "How to Calculate the Average Cross Sectional Area," Orbital Debris Quarterly Newsletter, Vol. 8, issue 2.





Hard-Body Radius: Projected Area Approach Implementation

- Assemble ball-and-stick model of primary satellite
- Rotate through all Euler angles and project into plane
- Create empirical PDF of projected areas
- Express as PDF of radii of circles of equivalent area
- If satellite orientation is known at TCA, then area can be projected directly into conjunction plane
 - Can then perform integration by means of a contour integral
 - Lingering problem of how to incorporate area for secondary object





Hard-Body Radius: Secondary Object HBR Uncertainty

- For intact spacecraft, possible to use published dimensions
 - For payloads, these are often not precise enough to be useful, and at least some canonical models would have to be imposed
 - Error in all of this great enough that approach is questionable
 - For rocket bodies, published dimensions are probably adequate
 - But many booster types lack published dimensions
- Most common secondaries are debris objects, for which no size information is available
- Thus, forced to estimate size from radar cross-section (RCS) value
 - Objects do not have single RCS value but PDF of values, depending on radar response and object aspect function
 - PDFs of individual objects' RCS values not available, only averaged values
 - As proxy could use canonical distribution
 - Swerling III distribution is most common for debris, and also most conservative in terms of size*

^{*} Hejduk, M. D. and DePalma, D. "Comprehensive Radar Cross-Section "Target Typing" Investigation for Spacecraft," 2010.





Hard-Body Radius: Swerling Distribution Family

Swerling distributions derive from the gamma distribution family

- Location parameter (y) = 0
- Shape parameter (m) fixed
- Scale parameter (β) estimated from sample (MLE)

Swerling I/II is gamma with m=1

- Exponential distribution
- Presumes Rayleigh scattering

Swerling III/IV is gamma with m=2

- Erlang distribution
- Presumes correlation with object orientation; more correct assumption

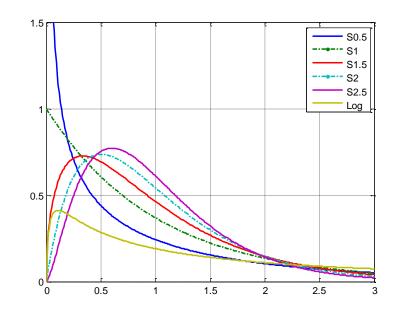
S-notation is gamma with m given

-S1.5 = gamma with m=1.5 &c.

$$f(x; \gamma, \beta, m) = \frac{1}{\beta^{m} \Gamma(m)} (x - \gamma)^{m-1} \exp\left(\frac{-(x - \gamma)}{\beta}\right)$$

$$f(x; \beta) = \frac{1}{\beta} \exp\left(\frac{-x}{\beta}\right)$$

$$f(x; \beta) = \frac{1}{\beta^2} x \exp\left(\frac{-x}{\beta}\right)$$

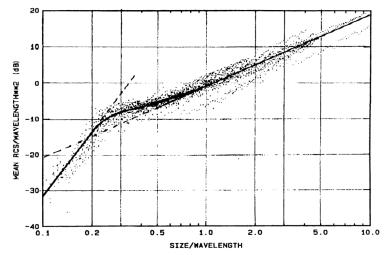






Hard-Body Radius: Radar OSEM Basic Rubric

- Simulated hyperkinetic destruction of satellite in vacuum chamber
- Collected pieces and subjected them to individual analysis
 - "Observed" each piece with radar in anechoic chamber
 - Articulated full range of aspect angles and full range of radar frequencies
 - Recorded resultant RCS of each aspect/frequency configuration
- Collected results and plotted in dimensionless format
 - $-RCS/\lambda^2$; size $/\lambda$
 - Results follow basic theory of Rayleigh, Mie, and optical regions

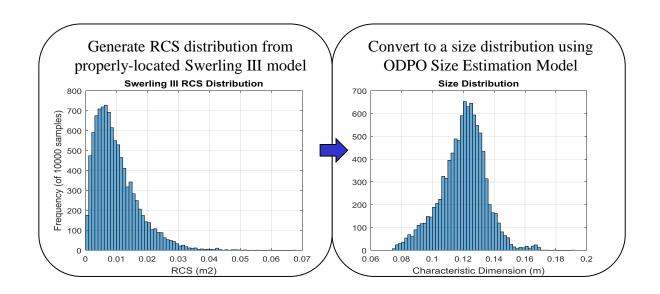






Hard-Body Radius: Full Process for Secondary Object

- Begin with average RCS
- Produce RCS PDF using Swerling III distribution
 - Scale parameter estimated by mean RCS divided by shape parameter
- Send distribution through ODPO size estimator to generate size PDF
 - Certified only for objects smaller than 20cm, but this is most debris







PC CALCULATION RESAMPLING





Pc Calculation Resampling

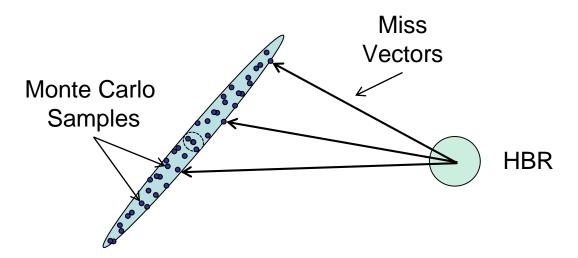
- Resampling/bootstrap methods often used to generate confidence intervals when calculation final distribution unknown
- Early attempts at this with Pc used resampling with invariant covariances
 - Take position draw on primary and secondary covariance at TCA
 - Find new TCA; this defines new nominal miss vector
 - Recompute Pc with this new miss vector and unaltered covariances
 - Problem: covariance is clearly correlated with conjunction geometry
 - Cannot produce new miss distance from covariance-based sampling and then recompute Pc using those same covariances
- Need approach that considers miss distance / covariance linkage





Pc Calculation Resampling Proposed Approach

- J.H. Frisbee proposed a resampling technique that would also address the correlation problem
 - Choose samples from the combined covariance to generate m miss vectors
 - Take mean of m miss vectors—this is new nominal miss
 - Take sample covariance of *m* miss vectors—this is new combined covariance
 - Compute Pc using this mean miss distance and sample combined covariance
 - Repeat procedure *n* times—this produces bootstrap dataset







Resampling Approach Issues

- In this framework, covariances are considered representatives of parent distributions, here further characterized by resampling
- Issue: what should be the value of m?
 - In bootstrapping, want the bootstrap sample size to equal the single-sample size that would have been used (or was used) to estimate the parameter
 - Thus, want the number of samples (DoF) of the bootstrap resampling (m) to equal the DoF that produced the covariance in the first place
 - That is, the DoF of the generating OD





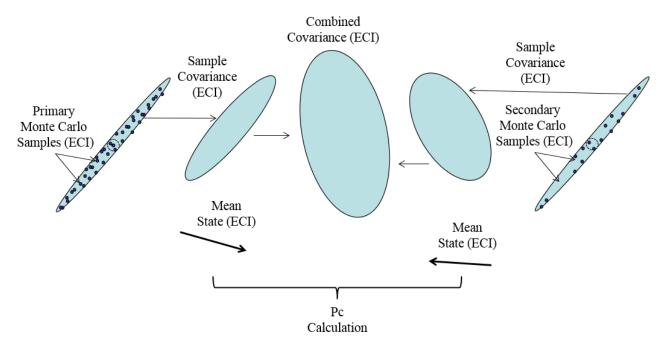
Tracking Levels and Degrees of Freedom

- DoF is usually calculated as the number of data points minus the number of estimated parameters
 - JSpOC ODs calculated with SSN obs (usually have range, azimuth, and elevation—three observables)
 - Obs provided in "tracks"—group of obs taken during one tracking session
- Thus, tabulation issues arise
 - Each ob provides 3 DoF, minus the estimated parameters
 - However, rather little information content in interior obs of a track
 - JSpOC "track weighting" confirms this—all tracks weighted the same in the OD, regardless of length
 - Better tabulation to count each track as equivalent of one state estimate
 - Longish track about enough data to execute a single state estimate, to first order
 - Total estimated parameters in OD would thus be only one—one state estimated
 - DoF calculation is thus "# of tracks 1"
 - Would need to be amended for DS, where obs report only two parameters, and needs more work in general





Resampling Approach Schematic



- Repeated thousands of times to calculate distribution of Pc values
- Benefits
 - Correlation of the miss vector and the covariance
 - Maintains an equivalent sampling level to the original OD
 - Naturally responds to variations in tracking density



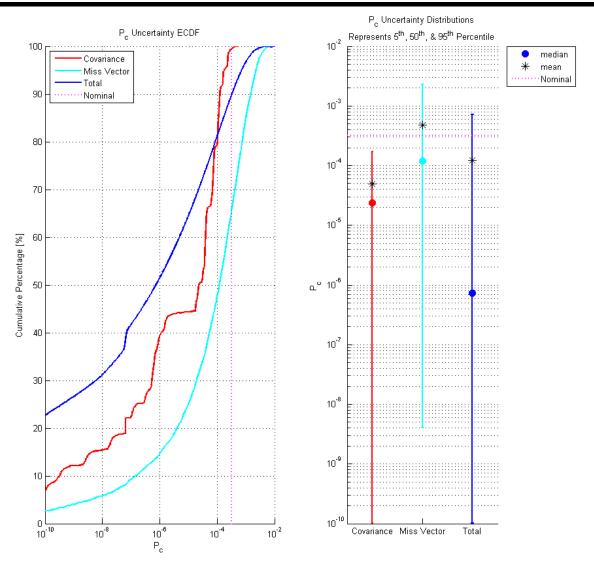


PROCESS RESULTS





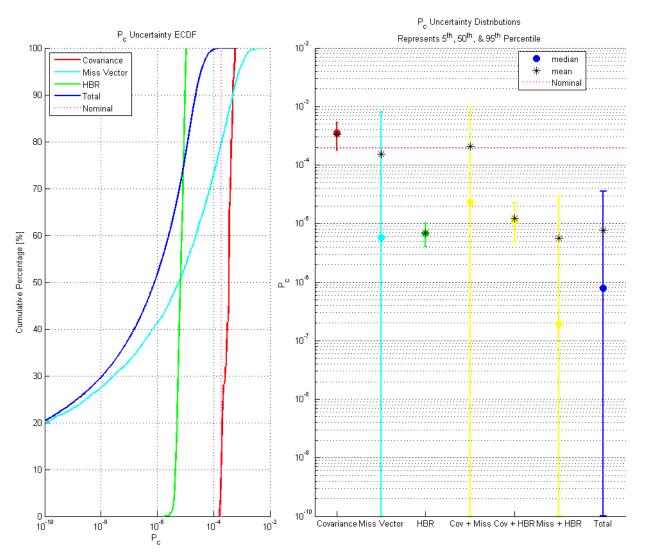
Example #1







Example #2







Conclusions and Future Work

Proposed method

- Characterizes the PDF that can represent the Pc from a particular conjunction, given the uncertainties in covariances, HBR and natural variation in the Pc calculation
- Gives a sense of the dynamic range of the Pc and allow maneuver decisions to be based on percentile points of this range rather than the nominal value alone
- Provides a mechanism for obtaining a better expression of the calculation's central tendency (here the median)

Future Work

- Refine DoF calculation and generate expansion for angles-only cases
- Survey results from runs of large datasets
 - Stability studies of simplifying assumptions for faster processing
- Examine potential as a Pc forecaster

