

Analogue Devices

Experiment 2

ENG471

Shane REYNOLDS

October 31, 2019

Date Performed: April 7, 2016
Instructor: Dr Sina Vafi

1 Objective

Explore both the differential and common mode gains of a differential amplifier which is driven by a current mirror current source.

2 Process & Results

The differential amplifier implemented in software simulation can be seen in both Figures 1, which has been set up to find the differential gain, and Figure 2, which was used to find the common mode gain. In both cases, the circuit consists of a current mirror stage and the amplifier itself. A capacitor has been employed to decouple the small signal at the output, v_o , from DC sources. To determine the differential gain, the gate of transistor M1 was connected to a sinusoidal voltage source, and the gate for transistor M2 was grounded. This arrangement can be seen in Figure 1. To determine the common mode gain, the gate of transistor M2 was connected to the same sinusoidal voltage source as transistor M1. In both cases a frequency sweep was performed on the sinusoidal input voltage, v_1 , and the differential voltage gain, $\frac{v_o}{v_1 - v_2}$, or the common mode voltage gain, $\frac{v_o}{v_1 + v_2}$, was measured. These gains were measured for two different loads at the output: 10M Ω and 400k Ω . The results for the simulated gain can be seen in Table 1. Hand calculations which support the simulation can be found in calculations section of the report.

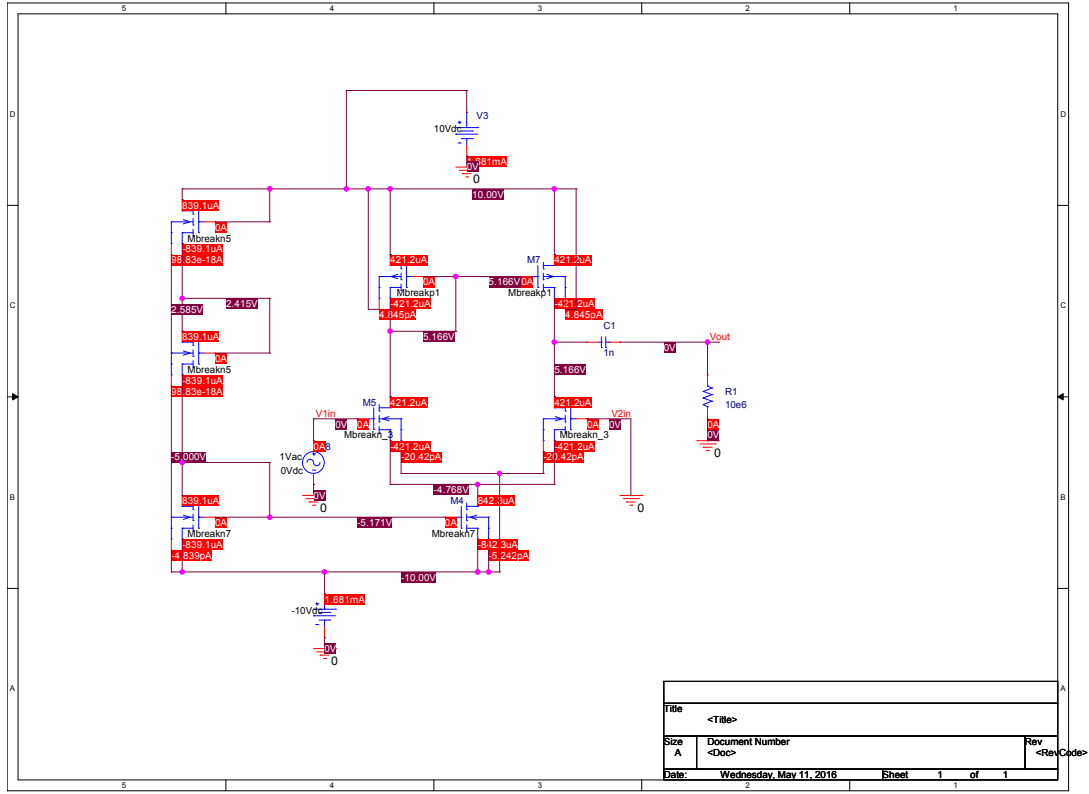


Figure 1: Simulation for calculating differential gain

3 Discussion

The hand calculations for the differential gain came to approximately 35.76 V/V for the $10\text{M}\Omega$ resistive load, and 27.07 V/V for the $400\text{k}\Omega$ resistive load. Further, the common mode gain for the $10\text{M}\Omega$ load was -0.0134 V/V , and the $400\text{k}\Omega$ load has -0.00847 V/V . These results closely match the simulated values for the differential gain and common mode gain. Figures 3 and 4 show the results of a simulated frequency sweep for the differential gain of the $10\text{M}\Omega$ and $400\text{k}\Omega$ loaded circuits, respectively. Further, 5 and 6 show the common mode gain for the $10\text{M}\Omega$ and $400\text{k}\Omega$ loaded circuits, respectively.

Table 1: Data for differential and common mode gain captured from simulations

Load Value (Ω)	A_d (V/V)	A_{cm} (V/V)
10×10^6	38.01	12.8×10^{-3}
400×10^3	29.16	9.8×10^{-3}

The DC bias values for which the amplifier's bias currents are derived are shown on the OrCAD schematics in Figure 1. These match the hand calculated results almost identically indicating that the simulation provides accurate results. In fact, error in the simulation is not discernible, however, further understanding of divergence between the hand calculated model and simulated model would require a working knowledge of the computational simulation methods employed by OrCAD. It must also be noted that the hand calculation relies on simplification of the non-linear transistor model and hence contains error of its own.

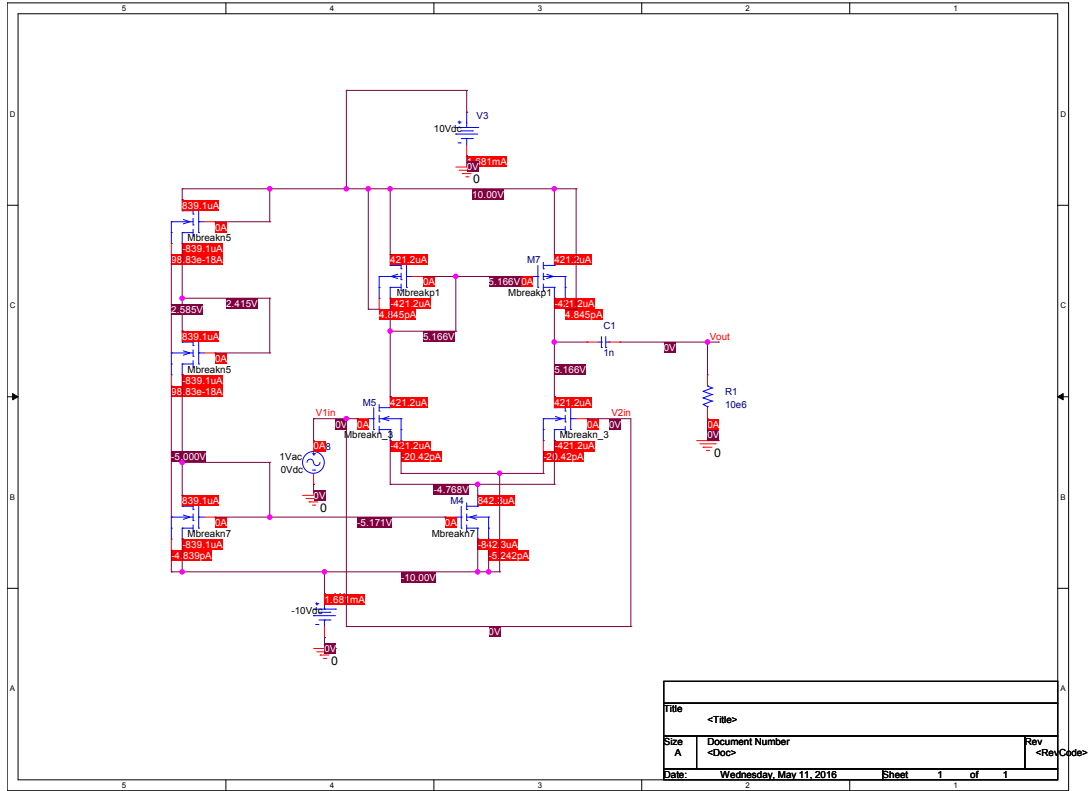


Figure 2: Simulation for calculating common mode gain

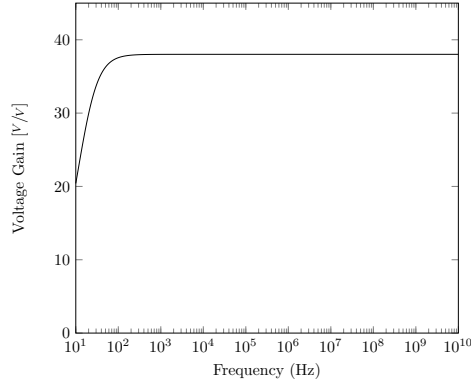


Figure 3: Differential gain:
 $R_L = 10\text{M}\Omega$

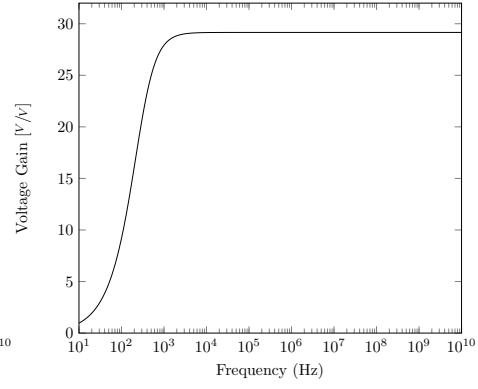


Figure 4: Differential gain:
 $R_L = 400\text{k}\Omega$

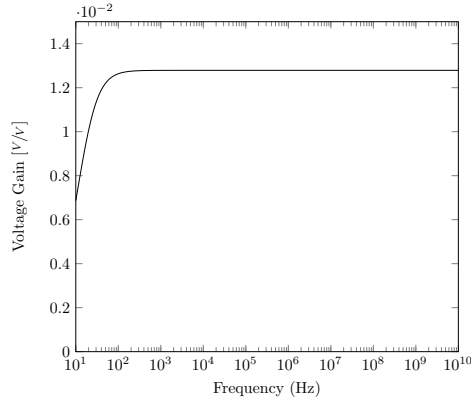


Figure 5: Common mode:
 $R_L = 10\text{M}\Omega$

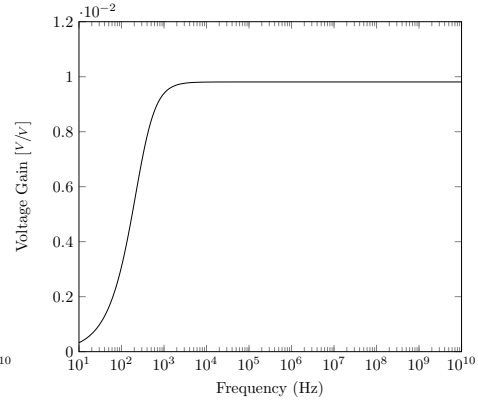


Figure 6: Common mode:
 $R_L = 400\text{k}\Omega$

4 Conclusion

The active loaded differential amplifier was analysed using both hand analysis and a computational approach using software to find the differential and common mode gains. Calculated and simulated results differ only marginally. This difference can be attributed to the approximations that are made in the hand calculations. The principal point of difference is that the software did not report an inverted small signal upon amplification.