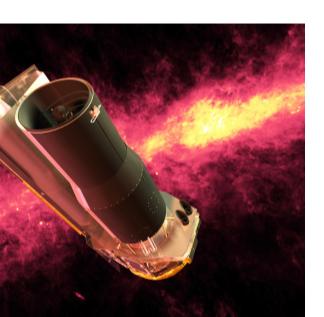


I. Background and Motivation

- Spacecraft serve a critical role in enabling and understanding modern life
- The Global Positioning System (GPS) is vital to navigation, commerce, and emergency services
- Scientific instruments such as the Hubble Space Telescope, Voyager missions, and the recent Rosetta mission have provided great insight into our solar system
- Designing spacecraft trajectories is a classic and ongoing topic of research
 - Predicting the motion of celestial bodies has motivated the likes of Newton, Euler, and Lagrange
 - The launch of Sputnik in 1957 shifted the focus to the motion of man-made objects
 - Incorporating additional perturbing forces increases the model accuracy at the expense of complexity
- The addition of propulsion devices enables the spacecraft to depart from the free motion trajectory
 - Previous work assume impulsive or instantaneous changes in spacecraft velocity (ΔV) to ease complexity
 - Continuous low thrust propulsion devices, such as electric propulsion, increase analysis complexity but improve capability
 - Electric Propulsion** has higher exhaust speeds and offers higher specific impulse than chemical propulsion methods
 - Can operate for extended periods which is ideal for deep space missions
- Miniaturization of electric propulsion enables their use on small satellites (1 – 100 kg)
- Several recent missions have exploited the system dynamics to enable very low energy orbital transfers



Genesis



Spitzer

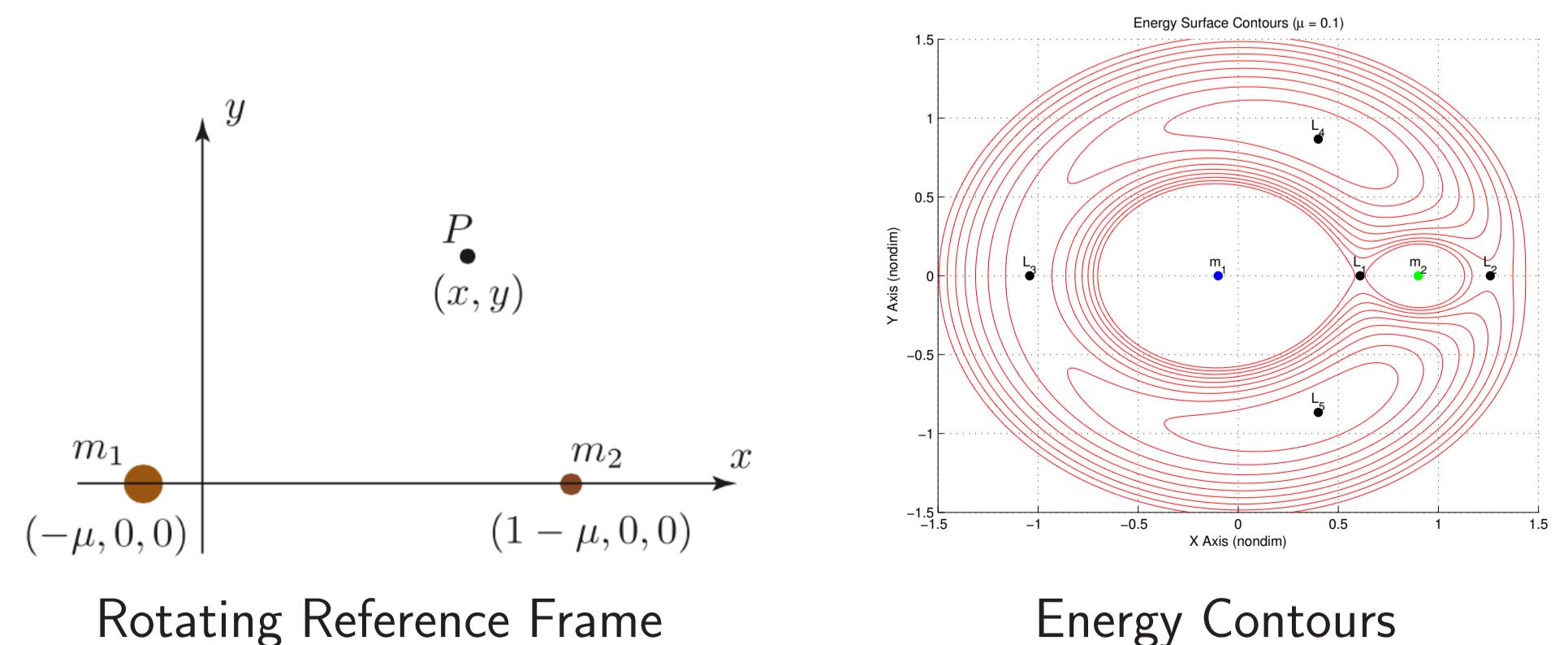


Ion Propulsion

II. Dynamic Model

- Circular Restricted Three Body Problem** describes the motion of a spacecraft under the gravitational force of two massive primaries
- No closed form analytic solutions available
- Use of a rotating reference frame allows for additional insight that produces an effective system for trajectory design in a multi-body environment
- The **Jacobi Integral**, is a scalar energy like term that divides realms of possible motion

$$E = \frac{1}{2} (\dot{x}^2 + \dot{y}^2 + \dot{z}^2) + \bar{U}(x, y, z)$$

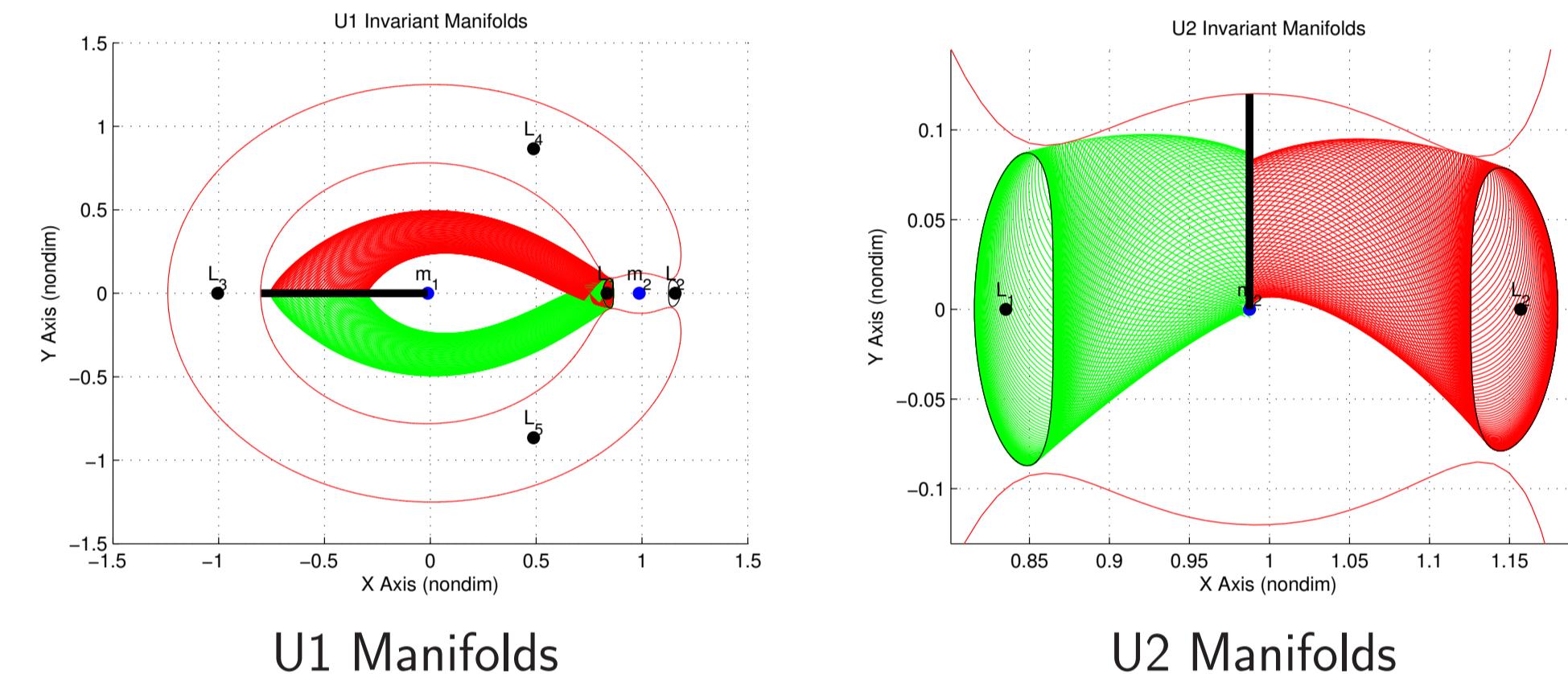


III. Dynamic Structure

- Equilibrium points classified by local stability properties
 - Collinear lagrange points (L_1, L_2, L_3) are dynamically unstable while equilateral (L_4, L_5) are stable
 - Numerical technique of **Differential correction** allows for infinite number of periodic solutions
- $\delta x(t) = \frac{\partial x}{\partial x_0} \delta x_0 = \Phi(t, t_0) \delta x_0$
- The **State Transition Matrix** gives the linear relationship between initial and final displacements

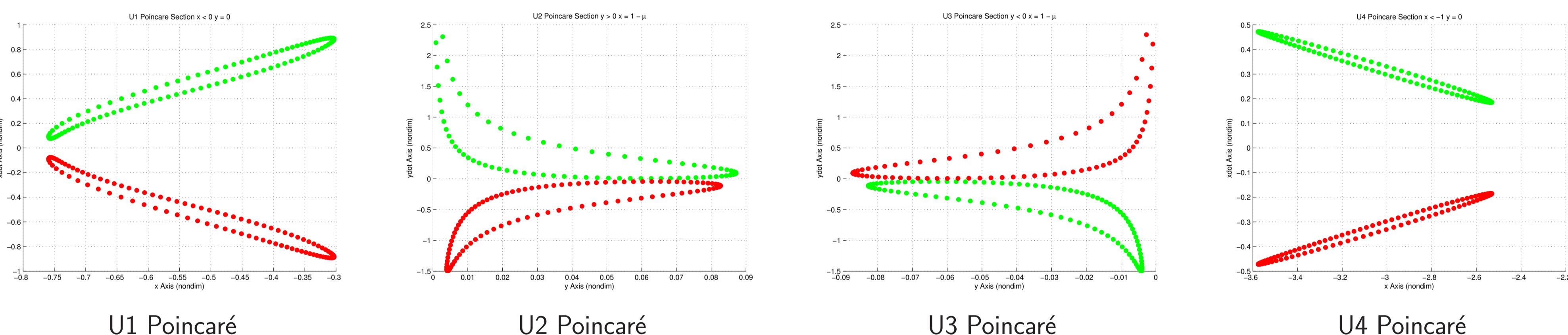
$$\Phi(t, t_0) = \frac{\partial f(x, u, t)}{\partial x} \Phi(t, t_0)$$
- The **Monodromy Matrix** of the periodic solutions allows insight into the local stability

$$M = \Phi(T)$$
- Globalization of the **Invariant Manifolds** define regions of the state space that asymptotically arrive or depart the periodic orbit



IV. Optimal Control Formulation

- Poincaré Section**, or return map, is an essential tool in examining the behavior of periodic orbits
 - Use of the Jacobi integral and intersection hyperplane reduces the problem dimensionality and allows for improved visualization

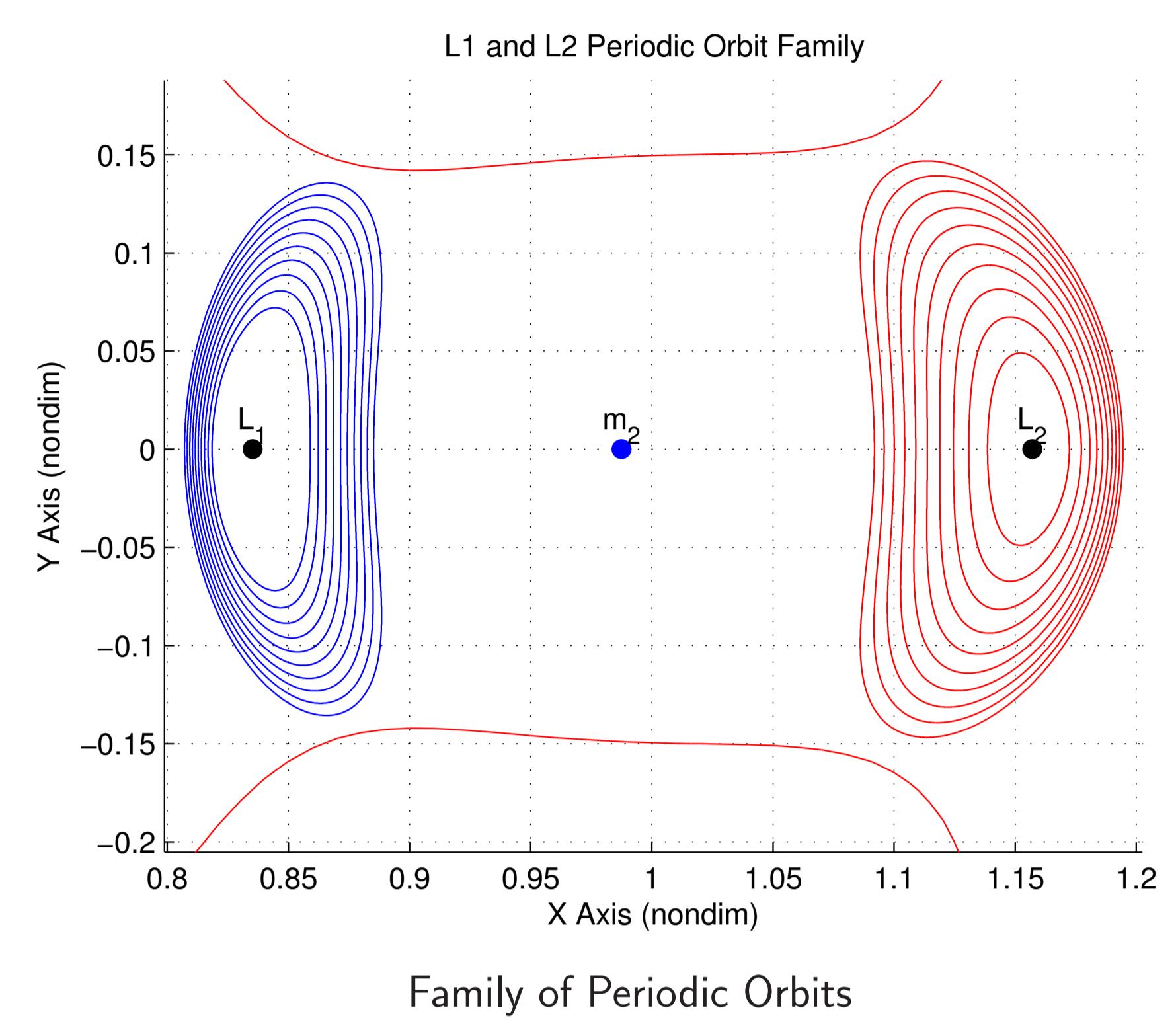


- Optimal Control** techniques enables the design of control histories that allow transfers between regions of space
- Incorporating control magnitude constraints lets us approximate the reachable set of the spacecraft
 - Calculus of variations leads to a two point boundary value problem with split boundary conditions

$$\min J = -\frac{1}{2} (\bar{x}(t_f) - \bar{x}_n(t_f))^T \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} (\bar{x}(t_f) - \bar{x}_n(t_f))$$

$$\begin{aligned} \frac{y(t_f) - L_1 y}{x(t_f) - L_1 x} - \tan \alpha_d &= 0 \\ \frac{\dot{x}(t_f) - \dot{x}_n(t_f)}{x(t_f) - x_n(t_f)} - \tan \theta_d &= 0 \\ \bar{u}^T \bar{u} - u_{max}^2 &\leq 0 \end{aligned}$$

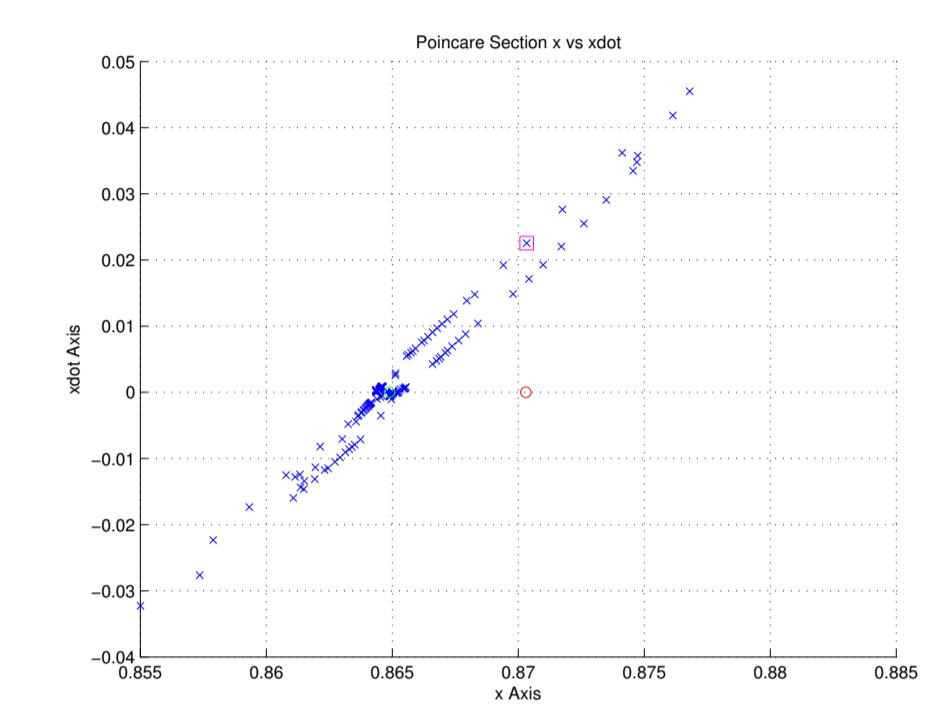
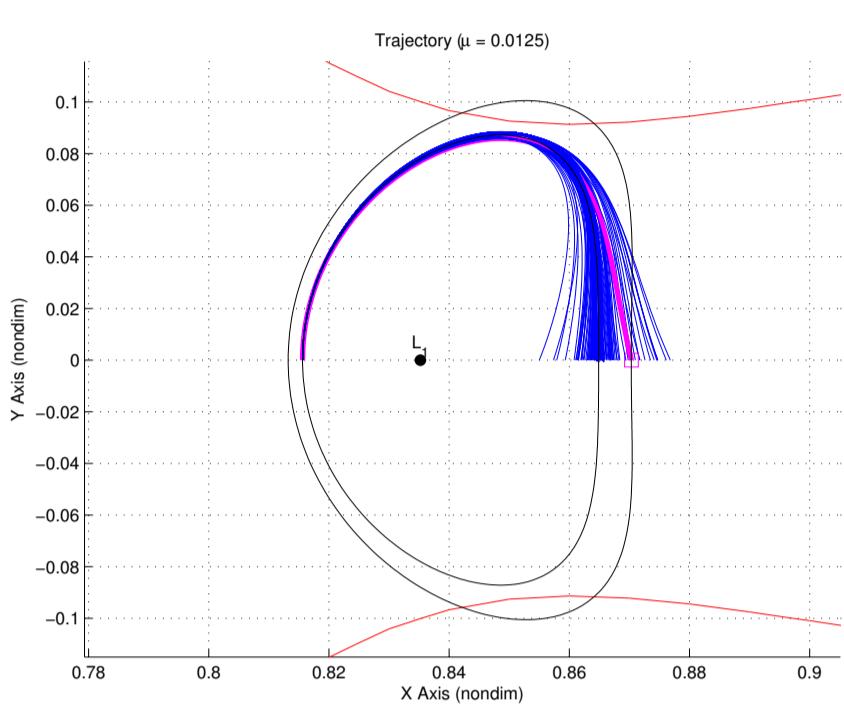
- Reachable set approximates state space that can be attained by spacecraft
- Constraints ensure trajectories intersect the return map and maximize the attainable state



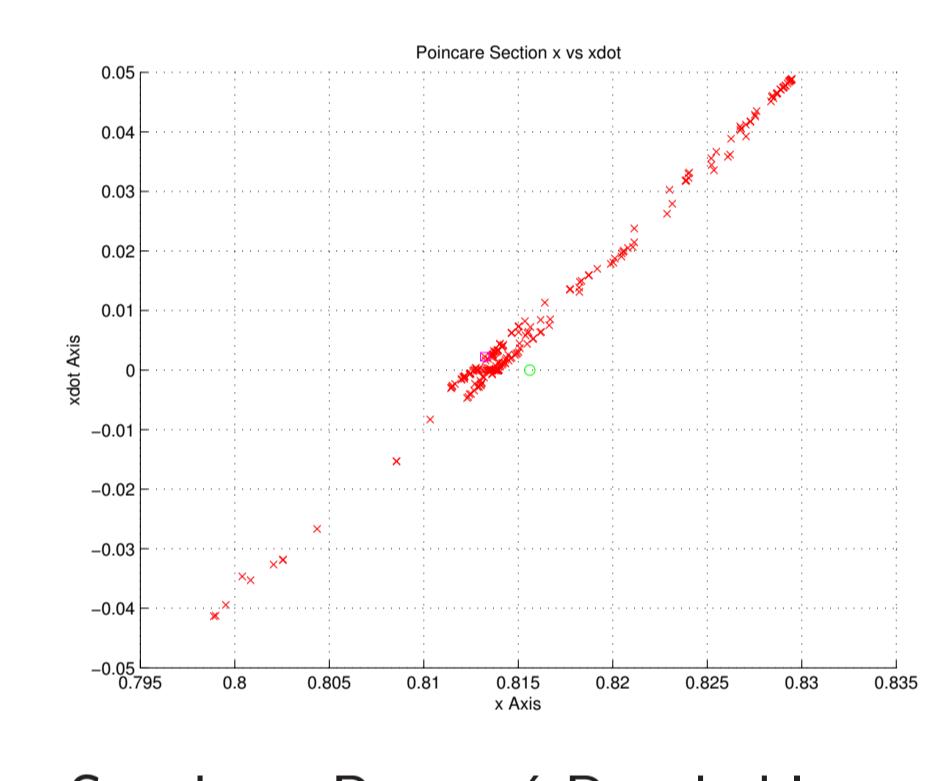
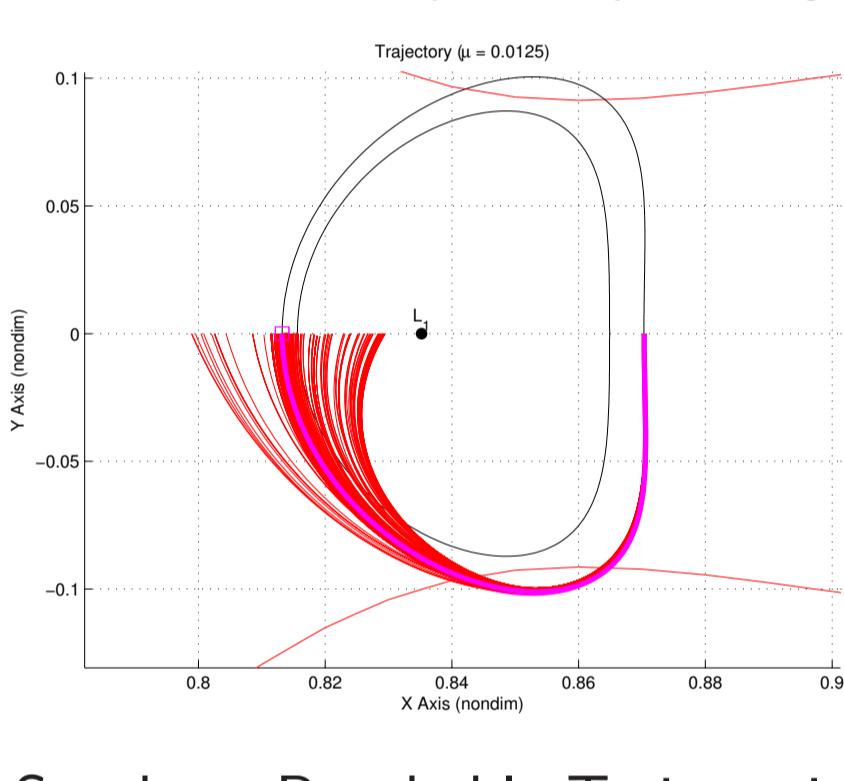
Family of Periodic Orbits

V. Experimental Results

- Design control history that transfers spacecraft between periodic orbits about the Earth-Moon L1 Lagrange point
- An algorithm is developed that approximates the reachable state space on a chosen Poincaré section
 - 2D Poincaré section allows straightforward visualization and decreases the problem complexity
- Variation of θ_d generates the reachable set which approximates the states that can be achieved subject to the bounded control input



- Multiple iterations of the reachable set computation allows for transfer trajectory design



- Poincaré section chosen such that periodic solutions will intersect the section twice per orbital period
- Projection of optimal trajectories onto the return map enables a decision making process in a lower dimensional space

VI. Conclusion

- Developed an optimal transfer design process which utilizes the concept of reachable sets on lower dimensional Poincaré maps
- Indirect optimal control formulation enables straightforward method of incorporating additional path and control constraints
- Current formulation is open loop and not robust to model uncertainties or disturbances
 - Nonlinear Lyapunov theory is being pursued to develop a feedback control algorithm that offers verifiable stability properties
- Planar assumption is a valid model for popular mission scenarios such as the Earth-Moon or Sun-Earth system
 - Extension to the spatial problem is necessary for more exotic missions, such as multi-moon orbit missions of the outer planets
 - Poincaré map representation would require extension from 2D to 4D
 - Innovative visualization techniques required to display higher dimensional state spaces