#### Simulazione in continua

- Determinazione del punto di lavoro circuiti con dispositivi a semiconduttore, non lineari
- Analisi a regime con eccitazioni costanti
   Si opera su un circuito senza memoria (resistivo), in genere, non lineare.
- E' usata anche nella simulazione della risposta temporale di circuiti dinamici metodi di discretizzazione

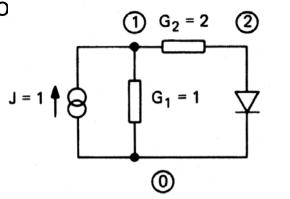
• MNA (o Tableau) —> sistema algebrico non lineare

Caso Scalare:

$$f(x) = 0$$

iterazione:

$$x^{k+1} = x^k + \Delta x^k = x^k - f(x^k)/f'(x^k)$$



$$i_D = e^{40\nu_D} -$$

equazioni ai nodi:

$$3v_1 - 2v_2 = 1$$
$$-2v_1 + 2v_2 + (e^{40v_2} - 1) = 0$$

$$v_1 = \frac{1}{3} + \frac{2}{3} v_2$$

$$f(v_2) = \frac{2}{3} v_2 + e^{40v_2} - \frac{5}{3} = 0$$

$$f'(v_2) = \frac{2}{3} + 40e^{40v_2}$$

$$v_2^0 = 0.1 \text{ V}$$

#### iterazioni:

k	$v_2^k$	$\Delta v_2^{k-1}$	
1	0.75740D - 01	-0.24260D - 01	
2	0.52712D - 01	-0.23029D - 01	
3	0.32705D - 01	-0.20007D - 01	
4	0.18883D - 01	-0.13822D - 01	
5	0.13356D - 01	-0.55267D - 02	
6	0.12654D - 01	-0.70199D - 03	
7	0.12644D - 01	-0.99424D - 05	
8	0.12644D - 01	-0.19579D - 08	

$$f(x) = 0$$

$$f_1(x_1, x_2, ..., x_n) = 0$$
  
 $f_2(x_1, x_2, ..., x_n) = 0$   
 $\vdots$   
 $f_n(x_1, x_2, ..., x_n) = 0$ 

espansione in serie di Taylor (1° ordine, linearizzazione):

$$\begin{cases} f_{1}(x_{1}, x_{2}, \dots, x_{n}) = 0 \\ f_{2}(x_{1}, x_{2}, \dots, x_{n}) = 0 \\ \vdots \\ f_{n}(x_{1}, x_{2}, \dots, x_{n}) = 0. \end{cases}$$

$$\begin{cases} f_{1}(\mathbf{x}^{*}) = f_{1}(\mathbf{x}) + \frac{\partial f_{1}}{\partial x_{1}}(x_{1}^{*} - x_{1}) + \frac{\partial f_{1}}{\partial x_{2}}(x_{2}^{*} - x_{2}) + \cdots \\ + \frac{\partial f_{1}}{\partial x_{n}}(x_{n}^{*} - x_{n}) + \cdots \\ \vdots \\ \vdots \\ f_{n}(\mathbf{x}^{*}) = f_{n}(\mathbf{x}) + \frac{\partial f_{n}}{\partial x_{1}}(x_{1}^{*} - x_{1}) + \frac{\partial f_{n}}{\partial x_{2}}(x_{2}^{*} - x_{2}) + \cdots \\ + \frac{\partial f_{n}}{\partial x_{n}}(x_{n}^{*} - x_{n}) + \cdots \end{cases}$$

$$\mathbf{f}(\mathbf{x}^*) \approx \mathbf{f}(\mathbf{x}) + \mathbf{M}(\mathbf{x}^* - \mathbf{x})$$

Jacobiana

$$\mathbf{f}(\mathbf{x}^*) \approx \mathbf{f}(\mathbf{x}) + \mathbf{M}(\mathbf{x}^* - \mathbf{x}) \qquad \qquad \mathbf{f}(\mathbf{x}^k) + \mathbf{M}(\mathbf{x}^{k+1} - \mathbf{x}^k) = \mathbf{f}(\mathbf{x}^k) + \mathbf{M}(\mathbf{x}^k) + \mathbf{M}(\mathbf{x}^$$

$$\mathbf{x}^{k+1} = \mathbf{x}^k - \mathbf{M}^{-1}\mathbf{f}(\mathbf{x}^k)$$

$$\Delta \mathbf{x}^k = \mathbf{x}^{k+1} - \mathbf{x}^k$$

$$\mathbf{M}\Delta \mathbf{x}^k = -\mathbf{f}(\mathbf{x}^k)$$

$$\mathbf{x}^{k+1} = \mathbf{x}^k + \Delta \mathbf{x}^k$$

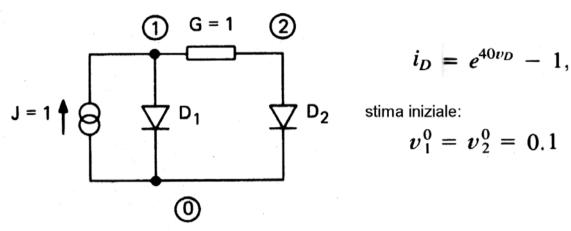
per ottenere, ad ogni iterazione:

$$\|\mathbf{f}(\mathbf{x}^{k+1})\| \leqslant \|\mathbf{f}(\mathbf{x}^k)\|$$

si usa:

$$\mathbf{x}^{k+1} = \mathbf{x}^k + t^k \Delta \mathbf{x}^k$$

$$0 < t^k \leqslant 1$$



equazioni ai nodi:

$$i_{D1} + G(v_1 - v_2) = j$$

$$G(-v_1 + v_2) + i_{D2} = 0$$

$$f_1(v_1, v_2) = e^{40v_1} + v_1 - v_2 - 2 = 0$$

$$f_2(v_1, v_2) = -v_1 + v_2 + e^{40v_2} - 1 = 0$$

Jacobiano: 
$$\mathbf{M} = \begin{bmatrix} 40e^{40v_1} + 1 & -1 \\ -1 & 40e^{40v_2} + 1 \end{bmatrix}$$

prima iterazione:

$$f_1 = 52.59815$$
  
 $f_2 = 53.59815$ 

$$\mathbf{M} = \begin{bmatrix} 2184.926 & -1 \\ -1 & 2184.926 \end{bmatrix}$$

$\Delta v_1^0 =$	-0.0240844
$\Delta v_2^0 =$	-0.0245419

$$v_1^1 = 0.0759156$$

$$v_2^1 = 0.07545810$$

k	$\Delta v_1^k$	$\Delta v_2^k$	$v_1^{k+1}$	$v_2^{k+1}$
0	-0.02408	-0.02454	0.07592	0.07546
1	-0.02260	-0.02378	0.05331	0.05168
2	-0.01909	-0.02182	0.03423	0.02986
3	-0.01234	-0.01736	0.02188	0.01250
4	-0.00432	-0.00962	0.01757	0.00289
5	-0.00044	-0.00236	0.01712	0.00053
6	-0.00001	-0.00012	0.01712	0.00041
7	-0.00000	-0.00000	0.01712	0.00041

#### Formulazione Nodale

supponiamo:

solo gen. indipendenti di corrente nonlinearità costitutite da resistori controllati in tensione:

$$i_b = g(v_b)$$

KVL: 
$$\mathbf{v}_b = \mathbf{A}^t \mathbf{v}_n$$

KCL:  $\mathbf{A}\mathbf{i}_b = -\mathbf{A}_J \mathbf{j}_b = \mathbf{j}_n$ 

$$\mathbf{A}\mathbf{g}(\mathbf{v}_b) = \mathbf{j}_n$$

$$\mathbf{A}\mathbf{g}(\mathbf{A}^t \mathbf{v}_n) = \mathbf{j}_n$$

#### Formulazione Nodale

Newton-Raphson:

$$\mathbf{f}(\mathbf{v}_n) \equiv \mathbf{A}\mathbf{g}(\mathbf{A}^t\mathbf{v}_n) - \mathbf{j}_n = \mathbf{0}.$$

$$\mathbf{M} = \frac{\partial \mathbf{f}}{\partial \mathbf{v}_n} = \mathbf{A} \frac{\partial \mathbf{g}}{\partial \mathbf{v}_b} \frac{\partial \mathbf{v}_b}{\partial \mathbf{v}_n}.$$

$$\frac{\partial \mathbf{g}}{\partial \mathbf{v}_b} = \mathbf{G}_b \qquad \frac{\partial \mathbf{v}_b}{\partial \mathbf{v}_n} = \mathbf{A}^t$$

$$\mathbf{M} = \mathbf{A}\mathbf{G}_b \mathbf{A}^t$$

### Tableau (MNA)

conduttanza nonlineare tra i nodi k ed l:

$$i_b = g(v_b).$$

equazioni ai nodi:

$$k: \quad \cdot \cdot \cdot + g(v_k - v_l) \cdot \cdot \cdot = 0$$

k: 
$$\cdot \cdot \cdot + g(v_k - v_l) \cdot \cdot \cdot = 0$$
l: 
$$\cdot \cdot \cdot - g(v_k - v_l) \cdot \cdot \cdot = 0.$$

Jacobiano:

variable 
$$\longrightarrow v_k \qquad v_l$$

row  $k \begin{bmatrix} \cdot \cdot \cdot \cdot & \partial g/\partial v_b \cdot \cdot \cdot -\partial g/\partial v_b \cdot \cdot \cdot \\ \cdot \cdot \cdot & -\partial g/\partial v_b \cdot \cdot \cdot & \partial g/\partial v_b \cdot \cdot \cdot \end{bmatrix}$ 

Lo Jacobiano ha esattamente la stessa forma della matrice nodale delle conduttanze.

Le conduttanze lineari restano invariate, al posto delle conduttanze nonlineari c'è la derivata della r.c., calcolata alla tensione dell'iterazione.

## Tableau (MNA)

#### Tableau

Equazioni del Tableau:

$$\mathbf{v}_b - \mathbf{A}^t \mathbf{v}_n = \mathbf{0}$$
$$\mathbf{p}(\mathbf{v}_b, \mathbf{i}_b) = \mathbf{w}$$
$$\mathbf{A}\mathbf{i}_b = \mathbf{0}.$$

Formulazione per Newton-Raphson:

$$\mathbf{f}(\mathbf{x}) \equiv \begin{bmatrix} \mathbf{v}_b - \mathbf{A}^t \mathbf{v}_n \\ \mathbf{p}(\mathbf{v}_b, \mathbf{i}_b) - \mathbf{w} \\ \mathbf{A}\mathbf{i}_b \end{bmatrix} = \mathbf{0}$$

Jacobiano alla k-esima iterazione:

$$\mathbf{M} = \begin{bmatrix} \mathbf{1} & \mathbf{0} & -\mathbf{A}^t \\ \mathbf{G}^k & \mathbf{R}^k & \mathbf{0} \\ \mathbf{0} & \mathbf{A} & \mathbf{0} \end{bmatrix}$$

ove: 
$$\mathbf{G}^k = \frac{\partial \mathbf{p}}{\partial \mathbf{r}}$$

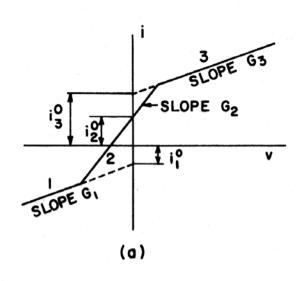
$$\Delta \mathbf{x}^k = \begin{bmatrix} \Delta \mathbf{v}_b \\ \Delta \mathbf{i}_b \\ \Delta \mathbf{v} \end{bmatrix}.$$

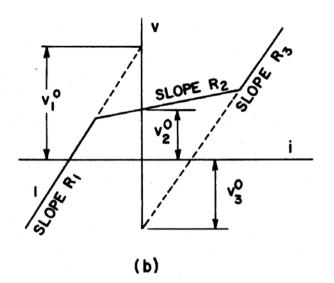
 $\mathbf{M}^k \Delta \mathbf{x}^k = -\mathbf{f}(\mathbf{x}^k)$ 

dove:

$$\mathbf{G}^{k} = \frac{\partial \mathbf{p}}{\partial \mathbf{v}_{h}} \bigg|_{\mathbf{v}_{k}}; \qquad \mathbf{R}^{k} = \frac{\partial \mathbf{p}}{\partial \mathbf{i}_{h}} \bigg|_{\mathbf{v}_{k}}$$

## Tecniche PWL





$$v = v_l^0 + R_l i$$

$$i = i_l^0 + G_l v$$

$$\mathbf{G}_l \mathbf{v}_b + \mathbf{R}_l \mathbf{i}_b = \mathbf{w}_l.$$

#### tableau

$$\begin{bmatrix} \mathbf{1} & \mathbf{0} & -\mathbf{A}^t \\ \mathbf{G}_l & \mathbf{R}_l & \mathbf{0} \\ \mathbf{0} & \mathbf{A} & \mathbf{0} \end{bmatrix} \begin{bmatrix} \mathbf{v}_b \\ \mathbf{i}_b \\ \mathbf{v}_n \end{bmatrix} = \begin{bmatrix} \mathbf{0} \\ \mathbf{w}_l \\ \mathbf{0} \end{bmatrix} + \begin{bmatrix} \mathbf{0} \\ \mathbf{w} \\ \mathbf{0} \end{bmatrix}$$

$$\mathbf{T}_l \mathbf{x}_l = \mathbf{w}_l + \mathbf{w}.$$

## Algoritmo di Katzenelson

$$\mathbf{T}_l \mathbf{x}_l = \mathbf{w}_l + \mathbf{w}.$$

alla k-esima iterazione:

Jacobiano:

$$\mathbf{f}^k = \mathbf{T}_l^k \mathbf{x}^k - \mathbf{w}_l^k - \mathbf{w}$$

 $\mathbf{M}^k = \mathbf{T}^k$ 

Newton-Raphson:

$$\mathbf{T}_l^k \Delta \mathbf{x}^k = -\mathbf{f}^k$$

$$\hat{\mathbf{x}}^{k+1} = \mathbf{x}^k + \Delta \mathbf{x}^k$$

Se nessun elemento cambia regione,  $\hat{\mathbf{X}}^{k+1}$  è la soluzione.

Altrimenti:

$$\mathbf{x}^{k+1} = \mathbf{x}^k + t^k \Delta \mathbf{x}^k$$

## Algoritmo di Katzenelson

$$\mathbf{x}^{k+1} = \mathbf{x}^k + t^k \Delta \mathbf{x}^k$$

Katzenelson: si sceglie  $t^k$  in modo che il punto di lavoro di un solo elemento vada a finire sul confine della regione attuale.

$$t_i^k = \frac{x_{li} - x_i^k}{\Delta x_i},$$
 se  $\Delta x_i > 0$   $t_i^k = \frac{x_i^k - x_{(l-1)i}}{\Delta x_i},$  se  $\Delta x_i < 0$ 

$$t^k = \min_i (t_i^k)$$

## Algoritmo di Katzenelson

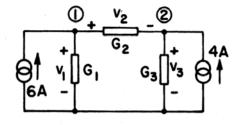
sul confine, due equazioni, per due regioni contigue, sono valide:

$$\mathbf{f}^{k+1} = \mathbf{T}_{l}^{k+1} \mathbf{x}^{k+1} - \mathbf{w}_{l}^{k+1} - \mathbf{w}$$

$$= \mathbf{T}_{l}^{k} \mathbf{x}^{k+1} - \mathbf{w}_{l}^{k} - \mathbf{w}.$$
cioè:
$$\mathbf{f}^{k+1} = (\mathbf{T}_{l}^{k} \mathbf{x}^{k} - \mathbf{w}_{l}^{k} - \mathbf{w}) + t^{k} \mathbf{T}_{l}^{k} \Delta \mathbf{x}^{k}$$

$$= \mathbf{f}^{k} - t^{k} \mathbf{f}^{k}$$

$$= (1 - t^{k}) \mathbf{f}^{k}$$

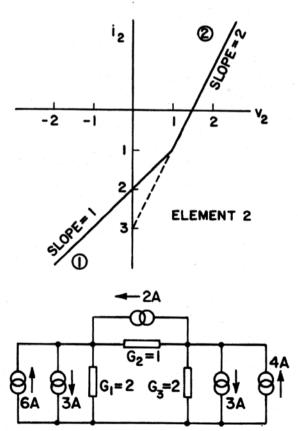


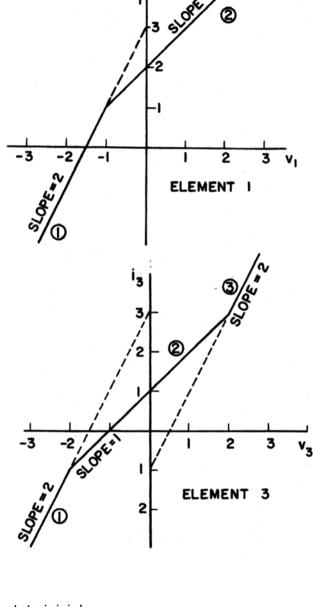
tensioni di nodo iniziali:

$$v_{n1} = -3$$
  $v_{n2} = -3$ 

tensioni di ramo:

$$v_1 = v_3 = -3$$
  $v_2 = 0$ 





stato iniziale

$$\mathbf{f}^0 = \mathbf{T}_l^0 \mathbf{x}^0 - \mathbf{w}_l^0 - \mathbf{w}.$$

$$\mathbf{f}^0 = \begin{bmatrix} 3 & -1 \\ -1 & 3 \end{bmatrix} \begin{bmatrix} -3 \\ -3 \end{bmatrix} - \begin{bmatrix} -1 \\ -5 \end{bmatrix} - \begin{bmatrix} 6 \\ 4 \end{bmatrix} = \begin{bmatrix} -11 \\ -5 \end{bmatrix}$$

$$\mathbf{T}_{I}^{k}\Delta\mathbf{x}^{k}=-\mathbf{f}^{k}.$$

$$\begin{bmatrix} 3 & -1 \\ -1 & 3 \end{bmatrix} \begin{bmatrix} \Delta v_{n1}^0 \\ \Delta v_{n2}^0 \end{bmatrix} = \begin{bmatrix} 11 \\ 5 \end{bmatrix} \longrightarrow \begin{bmatrix} \Delta v_{n1}^0 \\ \Delta v_{n2}^0 \end{bmatrix} = \begin{bmatrix} \frac{19}{4} \\ \frac{13}{4} \end{bmatrix}$$

$$\begin{bmatrix} \hat{v}_{n1}^1 \\ \hat{v}_{n2}^1 \end{bmatrix} = \begin{bmatrix} -3 \\ -3 \end{bmatrix} + \begin{bmatrix} \frac{19}{4} \\ \frac{13}{4} \end{bmatrix} = \begin{bmatrix} \frac{7}{4} \\ \frac{1}{4} \end{bmatrix}$$

$$\begin{bmatrix} \hat{v}_1^1 \\ \hat{v}_2^1 \\ \hat{v}_2^1 \end{bmatrix} = \begin{bmatrix} \frac{7}{4} \\ \frac{6}{4} \\ \frac{1}{4} \end{bmatrix}$$
 tutti gli elementi cambiano regione

$$t_1^0 = \frac{-1 - (-3)}{\frac{19}{4}} = \frac{8}{19}$$

$$t_2^0 = \frac{1 - 0}{\frac{6}{4}} = \frac{4}{6} \qquad \qquad b^0 = \min_i (t_i^0) = \frac{4}{13}$$

$$t_3^0 = \frac{-2 - (-3)}{\frac{13}{2}} = \frac{4}{13}$$

tensioni di nodo:

$$\begin{bmatrix} v_{n1}^{1} \\ v_{n2}^{1} \end{bmatrix} = \begin{bmatrix} -3 \\ -3 \end{bmatrix} + \frac{4}{13} \begin{bmatrix} \frac{19}{4} \\ \frac{13}{4} \end{bmatrix} = \begin{bmatrix} -\frac{20}{13} \\ -\frac{26}{13} \end{bmatrix} \qquad \begin{bmatrix} v_{1}^{1} \\ v_{2}^{1} \\ v_{3}^{1} \end{bmatrix} = \begin{bmatrix} -\frac{20}{13} \\ \frac{6}{13} \\ -\frac{26}{13} \end{bmatrix}$$

$$\mathbf{f}^{1} = (1 - \frac{4}{13}) \begin{bmatrix} -11 \\ -5 \end{bmatrix} = \begin{bmatrix} -\frac{99}{13} \\ -\frac{45}{13} \end{bmatrix}$$

tensioni sui componenti:

fine della 1° iterazione

siamo in una nuova regione, con:  $G_1 = 2$   $G_2 = 1$   $G_3 = 1$ 



Nuova iterazione.