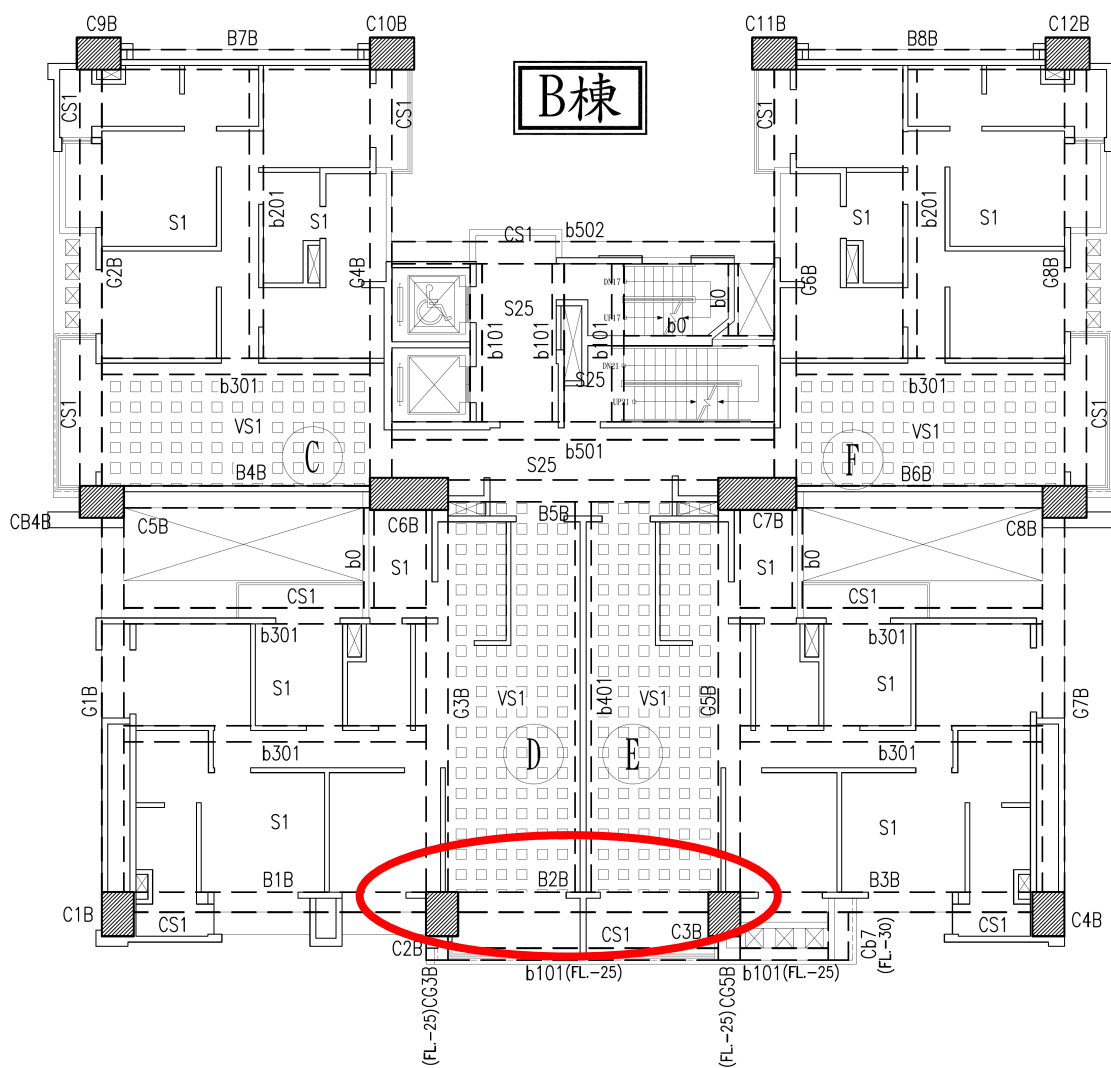


四、結構桿件設計說明

4-1 鋼筋混凝土梁韌性設計

鋼筋混凝土梁之韌性設計(附篇 B、C)
以 15FL (BAY NO.18), 梁編號 B2B 為例



(一) 已知條件

$F_y =$	4200	kg/cm ²	$F_c' =$	245	kg/cm ²
$F_{vy} =$	4200	kg/cm ²	$L_n =$	7.1	m
$B =$	50	cm	$H =$	75	cm
$d' =$	7	cm	$d =$	68	cm



(二) 基本設計資料

$m =$	20.17	$\rho_b =$	0.025
$F_s' =$	4200	kg/cm ²	
$AS_{max} =$	63.75	cm ² -----	$(0.025 \times B \times d, (f_c' + 100) / 4 f_y \times B \times d)$
$AS_{min} =$	11.33	cm ² -----	$(14 / f_y \times B \times d, 0.8 \sqrt{f_c' / f_y} \times B \times d)$
$V_{n_{max}} =$	141.03	T -----	$(2.65 \sqrt{f_c'} \times B \times d)$



(三) 樑分析後所得之應力

FORCE	Mi (T-m)	Vi (T)	Mj (T-m)	Vj (T)
DL	-21.23	-16.02	-21.06	15.96
LL	-3.54	-2.63	-3.56	2.63
AEQ	42.76	13.57	-42.72	13.57
BEQ	47.88	15.19	-47.84	15.19
DYN	49.54	15.72	49.51	15.72



(四) 計算樑設計彎矩Mu

載重組合：		$1.4 \times MD + 1.7 \times ML$ $0.75(1.4 \times MD + 1.7 \times ML) \pm 1.00 \times ME_h \pm 0.30 \times ME_v$ $0.75(1.4 \times MD + 1.7 \times ML) \pm 0.30 \times ME_h \pm 1.00 \times ME_v$ $0.9 \times MD \pm 1.00 \times ME_h \pm 0.30 \times ME_v$ $0.9 \times MD \pm 0.30 \times ME_h \pm 1.00 \times ME_v$			
		NOTE：ME={AEQ；BEQ；DYN}取大值			
		<div style="display: flex; justify-content: space-between;"> i 端 j 端 </div>			
-Mu =	-79.80	T-M (36)	-Mu =	-79.61	T-M (37)
+Mu =	33.88	T-M (47)	+Mu =	34.00	T-M (46)

(五) 計算樑AS

i 端			j 端		
AST=	34.59	cm ² > Asmin OK	AST=	34.5	cm ² > Asmin OK
ASB=	13.74	cm ² > Asmin OK	ASB=	13.79	cm ² > Asmin OK



(六) 樑主筋配筋(AST ≥ ASB/2 ; ASB ≥ AST/2)

i 端			j 端		
TOP :	5 -#8		TOP :	5 -#8	
	2 -#8			2 -#8	
AST=	35.49	cm ² < Asmax OK	AST=	35.49	cm ² < Asmax OK
BOT :	0 -#8		BOT :	0 -#8	
	4 -#8			4 -#8	
ASB=	20.28	cm ² < Asmax OK	ASB=	20.28	cm ² < Asmax OK



(七) 樑剪力筋設計

設計應力組合：	1.4×VD+1.7×VL
	0.75(1.4×VD+1.7×VL)±1.00×Veh
	0.75(1.4×VD+1.7×VL)±0.30×VEh±1.00×Vev
	0.9×VD±1.00×VEh±0.30×VEv
	0.9×VD±0.30×VEh±1.00×VEv
NOTE：	VE={AEQ；BEQ；DYN}取大值
	VPi=(MTi+MBj) / Ln
	VPj=(MBi+MTj) / Ln
	Vei=0.75(1.4×VDi+1.7×VLi)+VPi
	Vej=0.75(1.4×VDj+1.7×VLj)+VPj



(八) 計算樑彎矩強度Mpr (Fs=1.25Fy φ=1.0)

i 端			j 端		
以AST=	35.49	cm ² 為張力筋	以AST=	35.49	cm ² 為張力筋
ASB=	20.28	cm ² 為壓力筋	ASB=	20.28	cm ² 為壓力筋
得MTi=	-114.95	T-M	得MTj=	-114.95	T-M
以AST=	35.49	cm ² 為壓力筋	以AST=	35.49	cm ² 為壓力筋
ASB=	20.28	cm ² 為張力筋	ASB=	20.28	cm ² 為張力筋
得MBi=	67.50	T-M	得MBj=	67.50	T-M



(九) 計算樑設計剪力 V_u

i 端	j 端
$V_{pi} = (MT_i + MB_j) / L_n$	$V_{pj} = (MT_j + MB_i) / L_n$
$= 25.7 \quad T$	$= 25.7 \quad T$
$V_{vi} = 0.75(1.4 \cdot V_{Di} + 1.7 V_{Li})$	$V_{vj} = 0.75(1.4 \cdot V_{Dj} + 1.7 V_{Lj})$
$= 20.17 \quad T$	$= 20.11 \quad T$
$V_{ei} = V_{pi} + V_{vi}$	$V_{ej} = V_{pj} + V_{vj}$
$= 45.87 \quad T$	$= 45.81 \quad T$



(十) 計算剪力鋼筋量及配筋

i 端	j 端
$V_n = 45.87 \div 0.85$	$V_n = 45.81 \div 0.85$
$53.96 \quad t < V_{max} \quad ok$	$53.89 \quad t < V_{max} \quad ok$
$V_c = 0 \quad (V_{pi} > 0.5 V_{ei})$	$V_c = 0 \quad (V_{pj} > 0.5 V_{ej})$
$AV/S = (V_n - V_c) \div (f_y \times d)$	$AV/S = (V_n - V_c) \div (f_y \times d)$
$= 0.189 \quad cm^2/cm$	$= 0.189 \quad cm^2/cm$
STIR : 1-#4@12	STIR : 1-#4@12
$A_{vt}/S = 0.212 \quad cm^2/cm$	$A_{vt}/S = 0.212 \quad cm^2/cm$



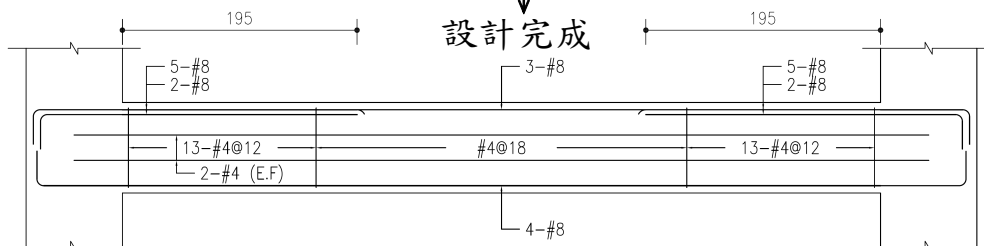
(十一) 樑(中央)分析後所得之應力及設計彎矩、剪力

FORCE	Mc (T-m)	Vc (T)			
DL	18.59	-9.26		$-M_u = 0.00$	T-M (0)
LL	3.24	1.68		$+M_u = 31.53$	T-M (1)
			→		
AEQ	0.02	13.57		$V_u = 25.25$	T (44)
BEQ	0.02	15.19			
DYN	0.02	15.72			



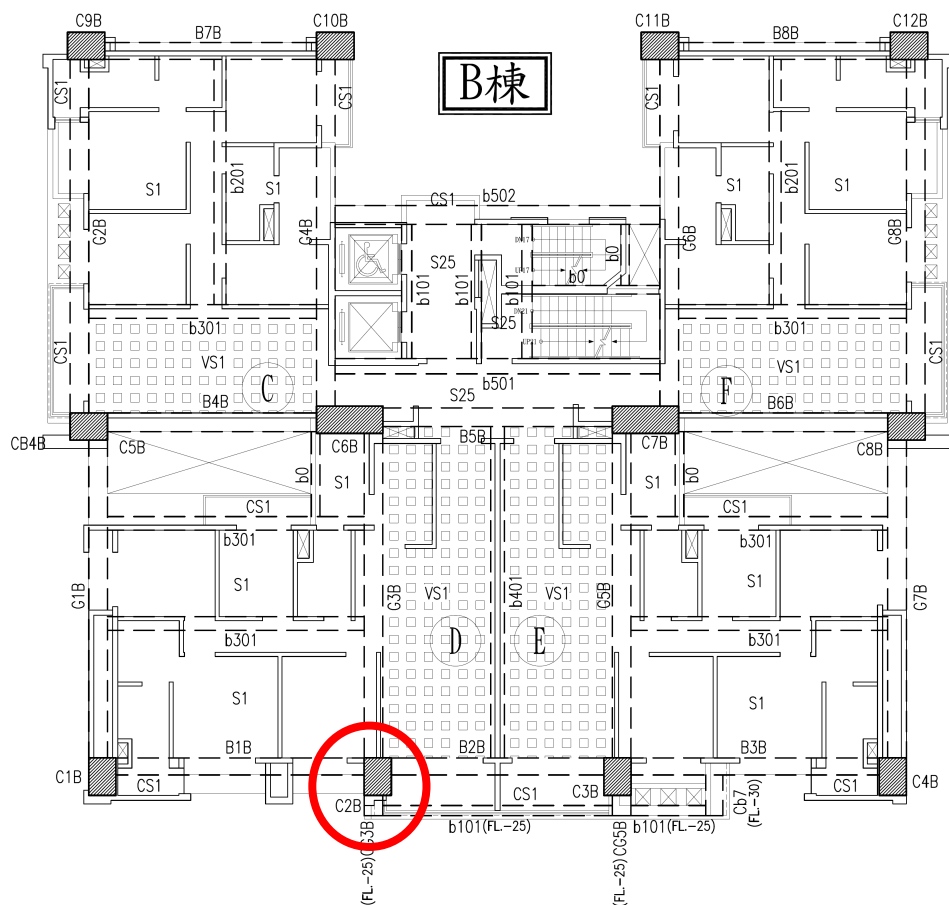
(十二) 計算樑(中央)斷面鋼筋量及配筋

AS計算	配筋
$AST = 0 \quad cm^2$	$AST = 15.21 \quad cm^2 \quad (3\text{-}\#8)$
$ASB = 12.75 \quad cm^2$	$ASB = 20.28 \quad cm^2 \quad (4\text{-}\#8)$
	→
$AV/S = (V_u / \phi - V_c) \div (f_y \times d)$	STIR : 1-#4@18
$= 0.104 \quad cm^2/cm$	$A_{vt}/S = 0.141 \quad cm^2/cm$



4-2 鋼筋混凝土柱韌性設計

鋼筋混凝土柱之韌性設計(附篇 B、C)
以 5FL (COL. NO.15),柱編號 C2B 為例 (CHECK X 向)



(一) 已知條件

$F_c' =$	245	kg/cm ²	$F_y =$	4200	kg/cm ²
$D_{maj} =$	80	cm	$D_{min} =$	110	cm
$H_n =$	230	cm	$F_{vy} =$	4200	kg/cm ²



(二) 柱彈性分析所得之應力

COLUMN FORCES AT LEVEL 6F			IN FRAME SPACE FRAME					
COL ID	OUTPUT ID	OUTPUT POINT	(T-m) MAJOR MOMENT	(T) MAJOR SHEAR	(T-m) MINOR MOMENT	(T) MINOR SHEAR	(T) AXIAL FORCE	(T-m) TORSIONAL MOMENT
15	CASE 1	TOP	9.98	-8.80	23.06	-19.97	-682.69	0.06
		BOTTOM	-10.27		-22.95			
15	CASE 2	TOP	1.94	-1.73	3.84	-3.30	-106.83	0.01
		BOTTOM	-2.03		-3.77			
15	CASE 3	TOP	-78.10	69.34	3.69	-2.44	64.51	-3.61
		BOTTOM	81.39		-1.94			
15	CASE 4	TOP	-93.73	82.68	5.97	-5.00	65.32	0.85
		BOTTOM	96.43		-5.55			
15	CASE 5	TOP	91.42	80.06	13.74	12.28	52.59	3.80
		BOTTOM	93.89		15.82			



(三) 柱主筋彈性設計結果

由第1組載重組合控制

	$P_u(T)$	$M_{umaj}(T-m)$	$V_{umaj}(T)$	$M_{umin}(T-m)$	$V_{umin}(T)$	$T_u(T-m)$
TOP	-1101.05	43.21	-14.67	53.11	-32.45	0.1
BOTTOM		43.21		53.11		

$A_{s, req} =$ 33.5 cm²



(四) 求樑彎矩強度和 ΣM_{bn} $L_n=7.30m$ $L_{s1}=3.75m$ $t_s=18cm$ 考慮T型梁(僅一側翼板) $=\min(L_n/12, 6 \times t_s, (L_{s1})/2)=\min(60.83, 108, 187.5)=60.83cm$ 版配筋#3@15($f_y=2800$)T型梁內版筋總量 $=1 \times 60.83/15 \times 0.71=2.88cm^2$

[柱頂]

B1B(50x80)

(6F bay 17)

B= 50 cm

D= 80 cm

AST= 6- #10 + 2.88cm²

ASB= 6- #10

[Mbpc_clock = Mpj_bottom - Vp_cntclock * col_wide * 0.01 = 191.42 (t-m)]

[Mbpc_cntclock = Mpj_top - Vp_clock * col_wide * 0.01 = -187.27 (t-m)]

[Mbnc_clock = Mnj_bottom - Vn_cntclock * col_wide * 0.01 = 154.38 (t-m)]

[Mbnc_cntclock = Mnj_top - Vn_clock * col_wide * 0.01 = -150.93 (t-m)]

B2B(50x80)

(6F bay 18)

B= 50 cm

D= 80 cm

AST= 8- #10

ASB= 6- #10

[Mbpc_clock = Mpi_top + Vp_cntclock * col_wide * 0.01 = -249.29 (t-m)]

[Mbpc_cntclock = Mpi_bottom + Vp_clock * col_wide * 0.01 = 196.44 (t-m)]

[Mbnc_clock = Mni_top + Vn_cntclock * col_wide * 0.01 = -201.92 (t-m)]

[Mbnc_cntclock = Mni_bottom + Vn_clock * col_wide * 0.01 = 158.11 (t-m)]

[柱底]

B1B(50x80)

(5F bay 17)

B= 50 cm

D= 80 cm

AST= 6- #10 + 2.88cm²

ASB= 6- #10

[Mbpc_clock = Mpj_bottom - Vp_cntclock * col_wide * 0.01 = 191.42 (t-m)]

[Mbpc_cntclock = Mpj_top - Vp_clock * col_wide * 0.01 = -187.27 (t-m)]

[Mbnc_clock = Mnj_bottom - Vn_cntclock * col_wide * 0.01 = 154.38 (t-m)]

[Mbnc_cntclock = Mnj_top - Vn_clock * col_wide * 0.01 = -150.93 (t-m)]

B2B(50x80)

(5F bay 18)

B= 50 cm

D= 80 cm

AST= 8- #10

ASB= 6- #10

[Mbpc_clock = Mpi_top + Vp_cntclock * col_wide * 0.01 = -249.29 (t-m)]

[Mbpc_cntclock = Mpi_bottom + Vp_clock * col_wide * 0.01 = 196.44 (t-m)]

[Mbnc_clock = Mni_top + Vn_cntclock * col_wide * 0.01 = -201.92 (t-m)]

[Mbnc_cntclock = Mni_bottom + Vn_clock * col_wide * 0.01 = 158.11 (t-m)]



(五) 強柱弱樑設計分配彎矩

5F上半層柱分配彎矩

[R_top = Mc / fabs(Mc_up - Mc) = 0.56]

[Mcu_top_clock = R_top * 1.2 Σ (ϕ b x Mbn_sum_clock) = -203.24 (t-m)][Mcu_top_cntclock = R_top * 1.2 Σ (ϕ b x Mbn_sum_cntclock) = -179.59 (t-m)]

Mcu_top_clock(face) = fabs(Mcu_top_clock) - fabs(Vcu_clock) * D * 0.01 = 109.58

Mcu_top_cntclock(face) = fabs(Mcu_top_cntclock) - fabs(Vcu_cntclock) * D * 0.01 = 96.83

[Mcu = 109.58]

5F下半層柱分配彎矩

[R_bottom = Mc / fabs(Mc - Mc_down) = 0.44]

[Mcu_bottom_clock = R_bottom * 1.2 Σ (ϕ b x Mbn_sum_clock) = 159.69 (t-m)][Mcu_bottom_cntclock = R_bottom * 1.2 Σ (ϕ b x Mbn_sum_cntclock) = 141.11 (t-m)]

Mcu_bottom_clock(face) = fabs(Mcu_bottom_clock) = 159.69

Mcu_bottom_cntclock(face) = fabs(Mcu_bottom_cntclock) = 141.11

[Mcu = 159.69]



(六) 柱主筋配筋

彈性分析鋼筋設計 (第1組載重組合控制)					
$P_u =$	-1101.05	T	$M_{u_{maj}} =$	43.21	T-M
$M_{u_{min}} =$	53.11	T-M	$A_s =$	33.5	cm ²
強柱弱樑分析鋼筋設計 (柱底控制)					
$P_u =$	-1101.05	T	$M_{u_{maj}} =$	159.4	T-M
$M_{u_{min}} =$	0	T-M	$A_s =$	139.6	cm ²
			$A_s(req) =$	139.6	cm ²
主筋: 30- #8			$A_s(pro) =$	152.1	cm ²

(七) 求柱設計剪力(梁 M_{pr} : $F_s=1.25F_y$ $\phi=1.0$, 韌性分析剪力)

柱頂分配彎矩	
$[R_{top}=M_c / f_{abs}(M_{c_up}-M_c)=$	0.56

$[M_{cp_top_clock} = R_{top} * f_{abs}(M_{bp_sum_clock})$	= -233.09(t-m)]
$[M_{cp_top_cntclock}=R_{top} * f_{abs}(M_{bp_sum_cntclock})$	= -206.48(t-m)]
柱底分配彎矩	
$[R_{bottom}=M_c / f_{abs}(M_c-M_{c_down})=$	0.44

$[M_{cp_bottom_clock} = R_{bottom} * f_{abs}(M_{bp_sum_clock})$	= 183.14(t-m)]
$[M_{cp_bottom_cntclock}=R_{bottom} * f_{abs}(M_{bp_sum_cntclock})$	= 162.23(t-m)]

$V_p=(M_{top}-M_{bot})/H$	
$[H=$	3.1 m]
$[V_{cp_clock} = f_{abs}((M_{cp_top_clock} - M_{cp_bottom_clock})/H)=$	134.27]
$[V_{cp_cntclock}=f_{abs}((M_{cp_top_cntclock}-M_{cp_bottom_cntclock})/H)=$	118.94]
$[V_{cu_clock} = f_{abs}((M_{cu_top_clock} - M_{cu_bottom_clock})/H)=$	117.08]
$[V_{cu_cntclock}=f_{abs}((M_{cu_top_cntclock}-M_{cu_bottom_cntclock})/H)=$	103.45]

[V_p = 134.27]	



(八) 計算柱橫向鋼筋

柱圍束區箍筋量之公式：

$$A_{sh}/S = 0.30 \times h_c \times (A_g/A_c - 1) \times (f_c' / f_y) \text{----- eq.(1)}$$

$$A_{sh}/S = 0.09 \times h_c \times (f_c' / f_y) \text{----- eq.(2)}$$

柱中央區剪力筋之公式：

$$A_v/S = (V_{max}/\phi - V_c) / (f_y x d) \text{----- eq.(3)}$$

(major)

(IF $P_u < 0.05 A_g f_c'$, $V_c = 0$)

$$V_u(\max) = 134.27 \quad T$$

$$h_c = 100.73 \text{ cm}$$

$$A_g = 8800 \text{ cm}^2$$

$$A_c = 7344 \text{ cm}^2$$

$$A_{sh}/S = 0.529 \text{ cm}^2/\text{cm} \quad (\text{圍束區}) < \text{--- 由 eq.(2) 控制}$$

$$A_{vh}/S = 0.210 \text{ cm}^2/\text{cm} \quad (\text{中央區})$$

(minor)

$$A_{sh}/S = 0.371 \text{ cm}^2/\text{cm} \quad (\text{圍束區}) < \text{--- 由 eq.(2) 控制}$$

$$A_{vh}/S = 0.079 \text{ cm}^2/\text{cm} \quad (\text{中央區})$$



(九) 柱圍束區及中央區之箍筋量配置

(major)

$$\text{圍束區：(Hoop：1-}\#4\text{+Ties：4-}\#4\text{) @ 10} \quad A_{sh}/S = 0.762 \text{ cm}^2/\text{cm}$$

$$\text{中央區：(Hoop：1-}\#4\text{+Ties：4-}\#4\text{) @ 15} \quad A_{vh}/S = 0.508 \text{ cm}^2/\text{cm}$$

(minor)

$$\text{圍束區：(Hoop：1-}\#4\text{+Ties：2-}\#4\text{) @ 10} \quad A_{sh}/S = 0.508 \text{ cm}^2/\text{cm}$$

$$\text{中央區：(Hoop：1-}\#4\text{+Ties：2-}\#4\text{) @ 15} \quad A_{vh}/S = 0.339 \text{ cm}^2/\text{cm}$$



柱設計及配筋完成

C2B (COL. LINE :15)

FL:5F	(80.0)x(110.0)	$F_c' = 245$	$F_y = 4200$	$F_{yh} = 4200$	
As(1) = 139.6	< A>			o 30-#8 [152.1]	
1.6%	[15]			X- 7(0)	
				Y-10(0)	
Maj .Av/S= 0.529				Hoop: 1-#4	
0.210	< B> [15]			Ties: 4-#4 @ 10 - 15	
Min .Av/S= 0.371				2-#4	
0.079	< B> [15]				

