# **AEEM 3062**

# **HOMEWORK #6**

### 2022-2023 SPRING

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### **Problem 1**

A pipe of length 2L is formed by joining two tubes of different materials but with the same length L and with the same inner diameter, d, and outer diameter, D, as shown in Fig. 1. Tube BC is made of a material of Young's modulus,  $E_1$ , and thermal expansion coefficient,  $\alpha_1$ ,; the corresponding constants for tube CD are  $E_2$  and  $\alpha_2$ . The pipe is clamped at both ends and tube BC is subject to a temperature increase,  $\Delta T$ , that is uniform along a cross section but varies along the tube axis according to

$$\Delta T(x) = T_1 + T_2 \sin \frac{\pi x}{L}$$

where  $T_1$  and  $T_2$  are constants.

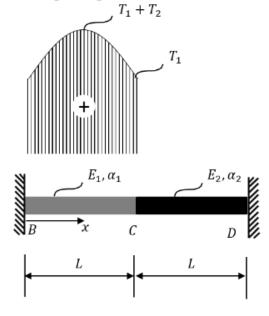
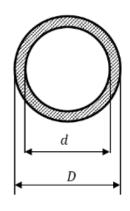


Figure 1

#### **CROSS SECTION**



Write the system of equations that is needed to find the expressions of the functions describing how the normal force N and the axial displacement u vary along the length of the bar. Write the system of equations in matrix form [30 pts]

For section B-C, the body force is 0:

$$n(x) = 0$$

Then the normal force is given by:

$$\frac{\partial N}{\partial x} + n(x) = 0$$

$$\frac{\partial N}{\partial x} = 0$$

Then this is integrated to get N:

$$N(x)_{B o C}=c_1$$

For a thermal expansions case, the displacement is given by:

$$rac{du}{dx} = rac{N(x)}{A(x)E(x)} + lpha \Delta T$$

$$rac{du}{dx} = rac{N(x)}{A(x)E(x)} + lpha_1(T_1 + T_2\sinrac{\pi x}{L})$$

Then this can be integrated to get:

$$u(x)_{B
ightarrow C}=rac{c_1x}{A_1E_1}+lpha_1T_1x-rac{lpha_1T_2L}{\pi} \cosrac{\pi x}{L}+c_2$$

Then we can do the same for section C-D, except  $\Delta T=0$ , so the thermal expansion terms disappear.

The body forces are also gone in this section, so:

$$N(x)_{C \to D} = c_3$$

The displacement will end up the same except for expansion:

$$\frac{du}{dx} = \frac{N(x)}{A(x)E(x)} + \alpha 0$$

$$u(x)_{C o D}=rac{c_3x}{A_2E_2}+c_4$$

Then we can set the boundary conditions. For a clamped end, the displacement is 0:

$$u(0) = u(2L) = 0$$

$$rac{c_1 0}{A_1 E_1} + lpha_1 T_1 0 - rac{lpha_1 T_2 L}{\pi} \cos rac{\pi 0}{L} + c_2 = 0$$

$$c_2=rac{lpha_1 T_2 L}{\pi}$$

$$\frac{c_3 2L}{A_2 E_2} + c_4 = 0$$

Since the pipes are connected, their displacement must be equal at the location where they meet:

$$u(L)_{B o C}=u(L)_{C o D}$$

$$rac{c_1 L}{A_1 E_1} + lpha_1 T_1 L - rac{lpha_1 T_2 L}{\pi} ext{cos} \, rac{\pi L}{L} + c_2 = rac{c_3 L}{A_2 E_2} + c_4$$

$$rac{c_1 L}{A_1 E_1} + lpha_1 (T_1 L + rac{T_2 L}{\pi}) + c_2 = rac{c_3 L}{A_2 E_2} + c_4$$

The normal forces also must be the same at that location:

$$N(L)_{B
ightarrow C}=N(L)_{C
ightarrow D}=c_1=c_3$$

Then rearrange to have all of the constants on one side:

$$rac{c_1 L}{A_1 E_1} + c_2 - rac{c_3 L}{A_2 E_2} - c_4 = -lpha_1 (T_1 L + rac{T_2 L}{\pi})$$

$$c_1 - c_3 = 0$$

Then the equations can be combined to create an Ax=b matrix system:

$$\begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & 0 & \frac{2L}{A_2E_2} & 1 \\ \frac{L}{A_1E_1} & 1 & -\frac{L}{A_2E_2} & -1 \\ 1 & 0 & -1 & 0 \end{bmatrix} \begin{bmatrix} c_1 \\ c_2 \\ c_3 \\ c_4 \end{bmatrix} = \begin{bmatrix} \frac{\alpha_1T_2L}{\pi} \\ 0 \\ -\alpha_1(T_1L + \frac{T_2L}{\pi}) \\ 0 \end{bmatrix}$$

#### Part B

Solve the system of equations assuming that: L = 600 mm, D = 25 mm, d = 22 mm,  $E_1 = 68.9 \text{ GPa}$ ,  $\alpha_1 = 25.5 \times 10^{-6} / ^{\circ}\text{C}$ ,  $E_2 = 207 \text{ GPa}$ ,  $\alpha_1 = 9.0 \times 10^{-6} / ^{\circ}\text{C}$ ,  $T_1 = 200 ^{\circ}\text{C}$ , and  $T_2 = 50 ^{\circ}\text{C}$ . Provide the expressions of the functions describing how the displacement u and normal force N vary along the length of the bar with the appropriate units [10 pts]

L = 0.6m, D = 0.025m, d = 0.022m, 
$$E_1 = 6.89E10$$
Pa $lpha_1 = 25.5E - 6/^{\circ}C, E_2 = 2.07E11$ Pa,  $T_1 = 200^{\circ}\mathrm{C}, T_2 = 50^{\circ}\mathrm{C}$  $A_1 = A_2 = \pi(0.025/2)^2 - \pi(0.022/2)^2 = 1.107E - 4m^2$ 

We can plug the given values into the matrix and solve for the constants using Matlab:

$$egin{bmatrix} 0 & 1 & 0 & 0 \ 0 & 0 & 5.237E - 8 & 1 \ 7.8666E - 8 & 1 & -2.6184E - 8 & -1 \ 1 & 0 & -1 & 0 \ \end{bmatrix} egin{bmatrix} c_1 \ c_2 \ c_3 \ c_4 \ \end{bmatrix} = egin{bmatrix} 2.435E - 4 \ 0 \ -0.0033 \ 0 \ \end{bmatrix}$$

$$c_1 = -33795.25 \text{N}$$
  $c_2 = 0.0002435 \text{m}$   $c_3 = -33795.25 \text{N}$   $c_4 = 0.00176 \text{m}$ 

Then we can substitute in the constants and given values to get the equations for normal force and displacement along the bar:

$$N(x)_{B o C} = -33795.25 ext{ Newtons}$$

$$N(x)_{C o D} = -33795.25 ext{ Newtons}$$

$$u(x)_{B
ightarrow C}=rac{c_1x}{A_1E_1}+lpha_1T_1x-rac{lpha_1T_2L}{\pi} \cosrac{\pi x}{L}+c_2$$

$$u(x)_{B \to C} = -0.00443x + 0.0051x - (2.435E - 4)\cos 5.236x + 0.0002435$$

$$u(x)_{B
ightarrow C} = (6.7E-4)x - (2.435E-4)\cos{(5.236x)} + 0.0002435 ext{ meters}$$

$$u(x)_{C o D}=rac{c_3x}{A_2E_2}+c_4$$

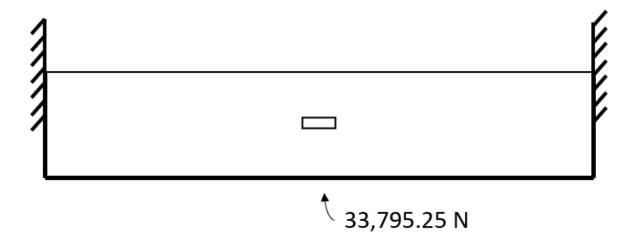
$$u(x)_{C o D} = -0.001475 x + 0.00176 ext{ meters}$$

### Part C

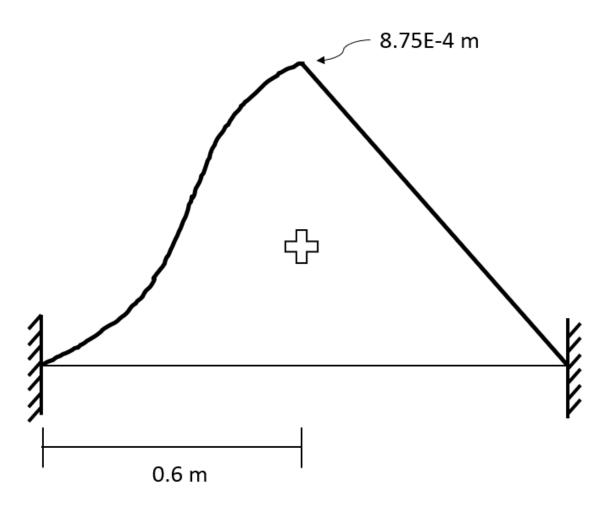
Plot the axial force, displacement, and reaction diagrams (no explanation needed) [15 pts]

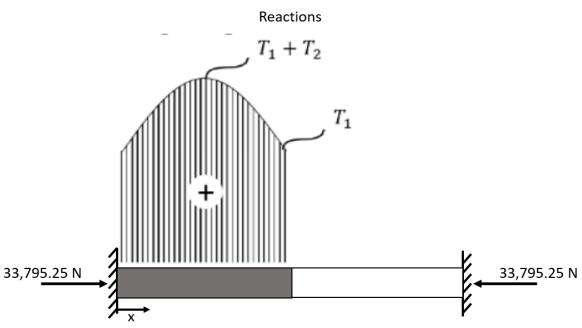


# **Axial Force**



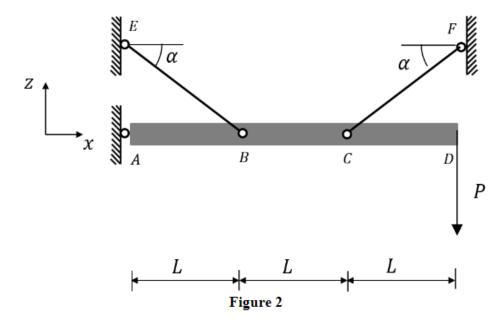
# Displacement





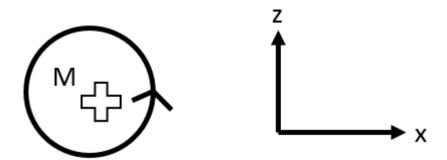
Problem 2

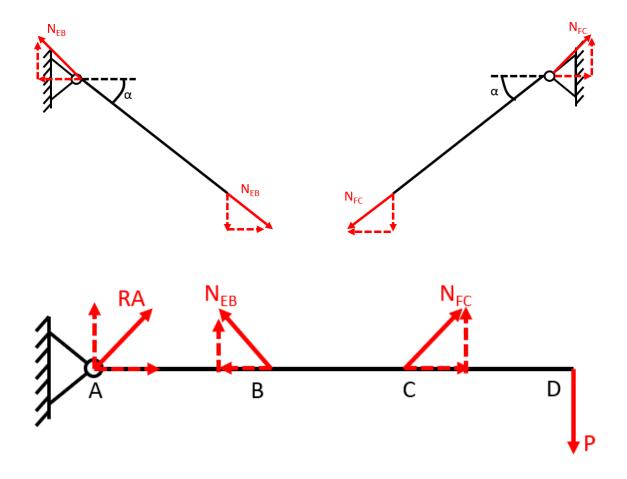
A rigid bar AD of length, 3L, is pinned at end A and is loaded by force P at the other end, D. Moreover, it is supported by two rods, EB, and, FC, which are pinned to the bar at distance L/3 from ends A and D, respectively. The rods are also pinned at the other ends E and F and form the angle  $\alpha$  relative to the horizontal axis as shown in Fig. 2. The rods have cross-sectional area,  $\Sigma$ , and Young's modulus, E.



#### Part A

Sketch the free body diagram for each rod and for the bar (no need for explanation)[10 pts]





### Part B

Express the normal force in each rod as a function of the displacement of pins B and C. [10 pts]

As given in the notes, the displacement of the rods can be given by:

$$\delta = rac{Nc}{EA}$$

Both rods have length (c) given by:

$$\cos \alpha = \frac{L}{c}, \quad c = \frac{L}{\cos \alpha}$$

As well as area  $\Sigma$  and young's modulus E given in the problem. Therefore:

$$\delta_B = rac{N_{EB}L}{E\Sigma\coslpha}, \quad \delta_C = rac{N_{FC}L}{E\Sigma\coslpha}$$

Then this can be rearranged to get the normal force in terms of displacement:

$$oxed{N_{EB} = rac{\delta_B E \Sigma \cos lpha}{L}, \quad N_{FC} = rac{\delta_C E \Sigma \cos lpha}{L}}$$

#### Part C

Find the normal forces in the rods and the reactions in A [20 pts]

Considering the angle of the bar to be  $\theta$ , the displacements are given by:

$$\delta_B = L\theta, \quad \delta_C = 2L\theta$$

Then we can find the ratio of displacement of B to displacement of C:

$$\frac{\delta_B}{\delta_C} = \frac{L\theta}{2L\theta} = \frac{1}{2}$$

This ratio is the same as the ratio of normal forces:

$$rac{\delta_B}{\delta_C} = rac{1}{2} = rac{N_{EB}}{N_{FC}}, \quad N_{FC} = 2N_{EB}$$

We also know that the sum of the moments about pin A must be equal to 0:

$$M_A = 0 = -3LP + 2LN_{FCz} + LN_{EBz}$$

Then this can be solved by substituting in  $N_{FC}=2N_{EB}$ :

$$3LP = 2L(2N_{EBz}) + LN_{EBz} \ 5LN_{EBz} = 3LP \ N_{EBz} = rac{3}{5}P$$

Which means  $N_{FCz}$  is:

$$N_{FCz}=2N_{EBz}=2(rac{3}{5})P$$
  $N_{FCz}=rac{6}{5}P$ 

Then we can use trig to get  $N_{EB}$  and  $N_{FC}$ :

$$egin{align} N_{EBz} &= N_{EB} \sin lpha, & N_{EB} &= rac{3P}{5 \sin lpha} \ N_{FCz} &= N_{FC} \sin lpha, & N_{FC} &= rac{6P}{5 \sin lpha} \ N_{FC} &= rac{4P}{5 \sin lpha} \ N_{FC} &= rac{4P}{5$$

Then to find the reactions at A we can sum the forces in the x and z directions:

$$\Sigma F_x = 0 = R_{Ax} - N_{EBx} + N_{FCx} = R_{Ax} - rac{3P}{5\sinlpha}\coslpha + rac{6P}{5\sinlpha}\coslpha$$

$$R_{Ax} = -rac{3}{5}P\cotlpha$$

$$\Sigma F_z = 0 = R_{Az} + N_{EBz} + N_{FCz} - P = R_{Az} + rac{3P}{5} + rac{6P}{5} - P$$

$$oxed{R_{Az}=-rac{4}{5}P}$$

#### Part D

### Determine the displacement of point D where the force is applied [5 pts]

The displacement of the bar at D depends on its rotation (which we previously defined as  $\theta$ ). This gives its displacement as:

$$\delta_D = 3L\theta$$

Then we can solve for  $\theta$  from the displacement for point B:

$$\delta_B = L heta, \quad heta = rac{\delta_B}{L}$$

Then by substituting in  $\delta_B$  and  $N_{EB}$  we can solve for  $\theta$ :

$$heta = rac{rac{N_{EB}L}{E\Sigma\coslpha}}{L} = rac{N_{EB}}{E\Sigma\coslpha} = rac{rac{3P}{5\sinlpha}}{E\Sigma\coslpha} = rac{3P}{5E\Sigma\sinlpha\coslpha}$$

Then substituting  $\theta$  back in gives the value for  $\delta_D$ :

$$\delta_D = rac{9PL}{5E\Sigma\sinlpha\coslpha}$$