

Slade Brooks

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AEEM6042 Module 2 Assignment

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Problem 1

Part A

Solve for T_2 with isentropic relations assuming $\gamma = 1.4$.

$$\begin{aligned}\frac{T_2}{T_1} &= \left(\frac{P_2}{P_1}\right)^{\frac{\gamma-1}{\gamma}} \\ T_2 &= T_1 \left(\frac{P_2}{P_1}\right)^{\frac{\gamma-1}{\gamma}} \\ T_2 &= 1400\text{K} \left(\frac{1}{8}\right)^{\frac{1.4-1}{1.4}} \\ \boxed{T_2 = 772.86\text{K}}\end{aligned}$$

Part B

Solve mass flow rate for area, using ideal gas assumption to get density.

$$\begin{aligned}\rho_1 &= \frac{P_1}{RT_1} \\ \rho_1 &= \frac{810600\text{Pa}}{287\text{J/kgK} * 1400\text{K}} \\ \rho_1 &= 2.017\text{kg/m}^3 \\ V_1 &= M_1 \sqrt{\gamma RT_1} \\ V_1 &= 0.3 \sqrt{1.4 * 287\text{J/kgK} * 1400\text{K}} \\ V_1 &= 225\text{m/s}\end{aligned}$$

$$\dot{m} = \rho_1 V_1 A_1$$

$$A_1 = \frac{\dot{m}}{\rho_1 V_1}$$

$$A_1 = \frac{100 \text{ kg/s}}{2.017 \text{ kg/m}^3 \cdot 225 \text{ m/s}}$$

$$A_1 = 0.22 \text{ m}^2$$

Part C

First check if the nozzle is choked. P_0 is constant since the nozzle is isentropic.

$$\frac{P_0}{P} = \left(1 + \frac{\gamma - 1}{2} M^2\right)^{\frac{\gamma}{\gamma - 1}}$$

$$P_0 = P_1 \left(1 + \frac{\gamma - 1}{2} M_1^2\right)^{\frac{\gamma}{\gamma - 1}}$$

$$P_0 = (810600 \text{ Pa}) \left(1 + \frac{1.4 - 1}{2} 0.3^2\right)^{\frac{1.4}{1.4 - 1}}$$

$$P_0 = 862827.2 \text{ Pa}$$

$$\frac{P_0}{P} = \frac{862827.2}{101325} = 8.52$$

The pressure ratio is higher than the critical pressure ratio so the nozzle is choked. First find M_2 from the isentropic relations since we know total temperature is constant because it's isentropic.

$$T_{01} = T_1 \left(1 + \frac{\gamma - 1}{2} M_1^2\right)$$

$$T_{01} = 1450.4 \text{ K}$$

$$M_2 = \sqrt{\left(\frac{T_{01}}{T_2} - 1\right) \frac{2}{\gamma - 1}}$$

$$M_2 = 2.1$$

Then find the area ratio to the throat from inlet, and use the throat area with M_2 to find the exit area.

$$\frac{A_1}{A^*} = \frac{1}{M_1} \left[\frac{2}{\gamma + 1} \left(1 + \frac{\gamma - 1}{2} M_1^2 \right) \right]^{\frac{\gamma + 1}{2(\gamma - 1)}}$$

$$A^* = A_1 / \frac{1}{M_1} \left[\frac{2}{\gamma + 1} \left(1 + \frac{\gamma - 1}{2} M_1^2 \right) \right]^{\frac{\gamma + 1}{2(\gamma - 1)}}$$

$$A^* = 0.108 \text{m}^2$$

$$A_2 = A^* \frac{1}{M_2} \left[\frac{2}{\gamma + 1} \left(1 + \frac{\gamma - 1}{2} M_2^2 \right) \right]^{\frac{\gamma + 1}{2(\gamma - 1)}}$$

$$A_2 = 0.1984 \text{m}^2$$

Problem 2

Part A

Solve for total pressure and temperature with isentropic relations, then solve MFP for mass flow rate.

$$P_0 = P_1 \left(1 + \frac{\gamma - 1}{2} M_1^2 \right)^{\frac{\gamma}{\gamma - 1}}$$

$$P_0 = 4 \text{psia} \left(1 + \frac{1.4 - 1}{2} 2.5^2 \right)^{\frac{1.4}{1.4 - 1}}$$

$$P_0 = 68.3 \text{psia}$$

$$T_0 = T_1 \left(1 + \frac{\gamma - 1}{2} M_1^2 \right)$$

$$T_0 = (-55 + 459.67 \text{R}) \left(1 + \frac{1.4 - 1}{2} 2.5^2 \right)$$

$$T_0 = 910.5 \text{R}$$

$$MFP = \sqrt{\frac{\gamma g_c}{R}} M_1 \left(1 + \frac{\gamma - 1}{2} M_1^2 \right)^{-\frac{\gamma + 1}{2(\gamma - 1)}}$$

$$MFP = \sqrt{\frac{1.4(32.174 \text{lbm-ft/lbf-s}^2)}{53.34 \text{ft-lbf/lbm-R}}} \cdot 2.5 \left(1 + \frac{1.4 - 1}{2} 2.5^2 \right)^{-\frac{1.4 + 1}{2(1.4 - 1)}}$$

$$MFP = 0.202$$

$$\dot{m} = \frac{A_1 P_0}{\sqrt{T_0}} MFP$$

$$\dot{m} = \frac{1.5\text{ft}^2 68.3\text{psia} \frac{144\text{si}}{\text{sf}}}{\sqrt{910.5\text{R}}} (.202)$$

$$\boxed{\dot{m} = 98.76\text{lbm/s}}$$

Part B

Use isentropic relations to get the pressure and temperature at the exit.

$$P_2 = P_0 / \left(1 + \frac{\gamma - 1}{2} M_2^2 \right)^{\frac{\gamma}{\gamma - 1}}$$

$$\boxed{P_2 = 66.4 \text{ psia}}$$

$$T_2 = T_0 / \left(1 + \frac{\gamma - 1}{2} M_2^2 \right)$$

$$\boxed{T_2 = 903.3^\circ\text{R}}$$

Part C

Use MFP with the exit conditions to get the exit area.

$$MFP = \sqrt{\frac{\gamma g_c}{R}} M_2 \left(1 + \frac{\gamma - 1}{2} M_2^2 \right)^{-\frac{\gamma + 1}{2(\gamma - 1)}}$$

$$MFP = \sqrt{\frac{1.4(32.174\text{lbm-ft/lbf-s}^2)}{53.34\text{ft-lbf/lbm-R}}} \cdot 0.2 \left(1 + \frac{1.4 - 1}{2} 0.2^2 \right)^{-\frac{1.4 + 1}{2(1.4 - 1)}}$$

$$MFP = 0.179$$

$$A_2 = \frac{\dot{m} \sqrt{T_0}}{MFP \cdot P_0}$$

$$A_2 = \frac{98.76\text{lbm/s} \sqrt{910.5\text{R}}}{0.179 \cdot 68.3\text{psia} \frac{144\text{si}}{\text{sf}}}$$

$$\boxed{A_2 = 1.693\text{ft}^2}$$

Problem 3

Part A

Simply use isentropic relations to solve for upstream totals.

$$T_{01} = T_1 \left(1 + \frac{\gamma - 1}{2} M_1^2 \right)$$

$$T_{01} = 260 \left(1 + \frac{1.4 - 1}{2} 3^2 \right)$$

$$\boxed{T_{01} = 728\text{K}}$$

$$P_{01} = P_1 \left(1 + \frac{\gamma - 1}{2} M_1^2 \right)^{\frac{\gamma}{\gamma - 1}}$$

$$P_{01} = 20 \left(1 + \frac{1.4 - 1}{2} 3^2 \right)^{\frac{1.4}{1.4 - 1}}$$

$$\boxed{P_{01} = 734.65\text{kPa}}$$

Part B

Since the shock is adiabatic across, $T_{02} = T_{01}$.

$$\boxed{T_{02} = 728\text{K}}$$

Solve for M_2 with shock relation then use P_2 from part C and M_2 to solve isentropic relation for P_{02} .

$$M_2 = \sqrt{\frac{1 + \frac{\gamma - 1}{2} M_1^2}{\gamma M_1^2 - \frac{\gamma - 1}{2}}}$$

$$M_2 = \sqrt{\frac{1 + \frac{1.4 - 1}{2} 3^2}{1.4 \cdot 3^2 - \frac{1.4 - 1}{2}}}$$

$$M_2 = 0.4752$$

$$P_{02} = P_2 \left(1 + \frac{\gamma - 1}{2} M_2^2 \right)^{\frac{\gamma}{\gamma - 1}}$$

$$P_{02} = 206.67 \left(1 + \frac{0.4}{2} 0.4752^2 \right)^{\frac{1.4}{0.4}}$$

$$\boxed{P_{02} = 241.22\text{kPa}}$$

Part C

Solve for static conditions using shock relation equations.

$$T_2 = T_1 \left[1 + \frac{2\gamma}{\gamma+1} (M_1^2 - 1) \right] \left[\frac{2 + (\gamma - 1)M_1^2}{(\gamma + 1)M_1^2} \right]$$

$$T_2 = 260 \left[1 + \frac{2 \cdot 1.4}{2.4} (3^2 - 1) \right] \left[\frac{2 + (0.4)3^2}{(2.4)3^2} \right]$$

$$T_2 = 696.54\text{K}$$

$$P_2 = P_1 \left(1 + \frac{2\gamma}{\gamma+1} (M_1^2 - 1) \right)$$

$$P_2 = 20 \left(1 + \frac{2.8}{2.4} (3^2 - 1) \right)$$

$$P_2 = 206.67\text{kPa}$$

Problem 4

Part A

Input mach number and specific heat ratio to gastab to get:

ratio of specific heats Cp/Cv	1.40
Mach number M	0.30000
total temperature ratio Tt/Tt*	0.34686
static temperature ratio T/T*	0.40887
static pressure ratio P/P*	2.1314
total pressure ratio Pt/Pt*	1.1985
velocity ratio V/V*	0.19183

First find T_{02} from q.

$$q = c_p(T_{02} - T_{01})$$

$$T_{02} = q/c_p + T_{01}$$

$$T_{02} = \frac{500\text{kJ/kg}}{1.004\text{kJ/kg-K}} + 500\text{K}$$

$$T_{02} = 998\text{K}$$

Now use the gastab results and the ratios to determine T_{02}/T_0 , then use gastab again to find the Mach number and total pressure ratio.

$$\begin{aligned}\frac{T_{02}}{T_{01}} &= \left(\frac{T_{02}}{T_0^*} \right) \left(\frac{T_0^*}{T_{01}} \right) \\ \frac{T_{02}}{T_0^*} &= \frac{T_{02}}{T_{01}} \frac{T_0^*}{T_{01}} \\ \frac{T_{02}}{T_0^*} &= \frac{998}{500} (0.34686) \\ \frac{T_{02}}{T_0^*} &= 0.692\end{aligned}$$

Get the subsonic gastab results because it started subsonic:

ratio of specific heats C_p/C_v	1.40
Mach number M	0.50044
total temperature ratio T_t/T_t^*	0.69200
static temperature ratio T/T^*	0.79079
static pressure ratio P/P^*	1.7770
total pressure ratio P_t/P_t^*	1.1139
velocity ratio V/V^*	0.44502

$$M_2 = 0.5$$

Get P_0^* from the first results:

$$\begin{aligned}\frac{P_{01}}{P_0^*} &= 1.1985 \\ P_0^* &= 500.63 \text{ kPa}\end{aligned}$$

Then get P_{02} from the new gastab results:

$$\frac{P_{02}}{P_0^*} = 1.1139$$
$$P_{02} = 500.63(1.1139)$$

$P_{02} = 557.65\text{kPa}$

Part B

Same process with different values:

ratio of specific heats Cp/Cv	1.325
Mach number M	0.30000
total temperature ratio Tt/Tt*	0.33896
static temperature ratio T/T*	0.38836
static pressure ratio P/P*	2.0773
total pressure ratio Pt/Pt*	1.1929
velocity ratio V/V*	0.18696

$$T_{02} = \frac{500\text{kJ/kg}}{1.171\text{kJ/kg-K}} + 500\text{K}$$

$T_{02} = 927\text{K}$

$$\frac{T_{02}}{T_0^*} = \frac{927}{500}(0.33896)$$
$$\frac{T_{02}}{T_0^*} = 0.628$$

ratio of specific heats C_p/C_v	1.33
Mach number M	0.46447
total temperature ratio T_t/T_t^*	0.62800
static temperature ratio T/T^*	0.70532
static pressure ratio P/P^*	1.8081
total pressure ratio P_t/P_t^*	1.1263
velocity ratio V/V^*	0.39008

$$M_2 = 0.46447$$

$$\frac{P_{01}}{P_0^*} = 1.1929$$

$$P_0^* = 502.976 \text{ kPa}$$

$$\frac{P_{02}}{P_0^*} = 1.1263$$

$$P_{02} = 502.976(1.1263)$$

$$P_{02} = 566.5 \text{ kPa}$$

Problem 5

First we need the hydraulic diameter, which is just one side length for a square.

$$D = 1 \text{ ft}$$

Plug mach number into gastab to get results:

ratio of specific heats C_p/C_v	1.40
Mach number M	0.60000
static temperature ratio T/T^*	1.1194
static pressure ratio P/P^*	1.7634
total pressure ratio P_t/P_t^*	1.1882
velocity ratio V/V^*	0.63480
impulse function ratio I/I^*	1.1050
friction factor $4fL_{max}/D$	0.49080

Get the * static temp and pressure from the gastab ratios as well as the total pressure ratio.

$$P^* = 10/1.7634 = 5.67 \text{ psia}$$

$$T^* = 500/1.1194 = 446.67^\circ\text{R}$$

$$P_0/P_0^* = 1.1882$$

First calculate the regular $4c_f L/D$.

$$\frac{4c_f L}{D} = \frac{4(0.004)(8)}{1} = 0.128$$

Now get the $4c_f L_2^*/D$ by solving:

$$\frac{4c_f L_2^*}{D} = 0.49080 - 0.128 = 0.3628$$

Then plug that friction factor back into gastab to get the subsonic (because started subsonic) Mach number.

ratio of specific heats C_p/C_v	1.40
Mach number M	0.63684
static temperature ratio T/T^*	1.1100
static pressure ratio P/P^*	1.6543
total pressure ratio P_0/P_0^*	1.1483
velocity ratio V/V^*	0.67090
impulse function ratio I/I^*	1.0807
friction factor $4fL_{max}/D$	0.36280

$$M_2 = 0.63684$$

Get the pressure and temperature based on the new gastab ratios.

$$P_2 = 5.67 \cdot 1.6543$$

$$P_2 = 9.38 \text{ psia}$$

$$T_2 = 446.67 \cdot 1.11$$

$$T_2 = 495.8^\circ\text{R}$$

$$P_{02}/P_{01} = 1.1483/1.1882$$

$$\frac{P_{02}}{P_{01}} = 0.9664$$