

$$A = \begin{bmatrix} 0 & 1 & 0 \\ 49.05 & -200 & 0 \\ 0 & 0 & 0 \end{bmatrix} \quad B = \begin{bmatrix} 0 \\ -3.5 \\ 8 \end{bmatrix} \quad \gamma = \begin{bmatrix} \theta_1 \\ \theta_2 \\ \theta_3 \end{bmatrix}$$

a). Co: $n=3$

$$\begin{bmatrix} 0 & AB & A^2B \end{bmatrix} = \begin{bmatrix} 0 & -3.5 & 700 \\ -3.5 & 700 & -140171.675 \\ 8 & 0 & 0 \end{bmatrix}$$

$$\det(A) = 1806.9 \neq 0 \rightarrow \text{Rang} = 3 = n$$

\therefore SI es controlable.

$$T_{es} \leq 2.5 \text{ seg}$$

$$M_p \leq 5\%$$

Sist. de 3er orden \rightarrow Se usa el de 2^{do}: $\bar{s}, \bar{c} = \sigma_d \pm \omega_d j$

$$\sigma_d = \frac{\xi}{T_n} \quad \omega_d = \frac{\pi \omega_n}{\ln(M_p)}$$

$$\sigma_d = -2 \quad \omega_d = 2.0973$$

$$s_1 = -2 + 2.0973j$$

$$s_2 = -2 - 2.0973j$$

$$s_3 = -10$$

$$\alpha(s) = (s + 2 - 2.0973j)(s + 2 + 2.0973j)(s + 10)$$

$$s^2 + 2s + 2.0973j^2 + 2s + 4 + 4.1946j - 2.0973s - 9.1946j + 9.3974$$

$$(s^2 + 4s + 8.3974)(s + 10) = s^3 + 4s^2 + 8.3974s + 10s^2 + 40s + 83.974$$

$$\alpha(s) = s^3 + 14s^2 + 48.3974s + 83.974$$

$$\phi(A) = A^3 + 14A^2 + 48.3974A + 83.974I$$

$$K = [0 \ 0 \ 1] C_o^{-1} \phi(A)$$

$$K = [-125.67 \ 52.654 \ -0.214]$$

b). $y = Cx$

$$C_1 = [1 \ 0 \ 0] \vee [0 \ 1 \ 0] \vee [0 \ 0 \ 1]$$

$$\phi: \begin{bmatrix} C \\ CA \\ CA^2 \end{bmatrix}$$

$$C_1: \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 49.05 & -200 & 0 \end{bmatrix} \quad \det(C_1) = 0 \quad \therefore \text{No}$$

$$C_2: \begin{bmatrix} 0 & 1 & 0 \\ 49.05 & -200 & 0 \\ -9810 & 40018.950 & 0 \end{bmatrix} \quad \det(C_2) = 0$$

2.

$$\ddot{h} = g - \frac{k}{m} \left(\frac{I}{h} \right)^2$$

$$0 = g - \frac{k}{m h^2} \cdot I^2 \quad -\ddot{h} = P(\ddot{h}, h, I)$$

$$k = 0.001$$

$$g = 9.81$$

$$m = 0.2$$

$$\bar{h} = 0.01 \text{ m}$$

$$x_1 = h - \bar{h}$$

$$u = I - \bar{I}$$

$$P = P(\bar{h}, \sqrt{\bar{I}}, \bar{I}) + \frac{\partial P}{\partial \bar{h}} \Delta h + \frac{\partial P}{\partial \bar{I}} \Delta I + \frac{\partial P}{\partial \bar{I}} \Delta I$$

$$\bar{h} = 0.01 \rightarrow \bar{I} = 0$$

$$0 = g - \frac{k}{m} \left(\frac{\bar{I}}{0.01} \right)^2 \Rightarrow \sqrt{\frac{g m}{k}} (0.01)^2 = \bar{I} = 0.442945 \text{ A}$$

$$0 = -\Delta \ddot{h} + \frac{-k}{m} \left(\frac{\bar{I}}{\bar{h}} \right)^2 \Delta h + \left(\frac{-2k}{m \bar{h}^3} \bar{I} \right) \Delta I$$

$$0 = -\Delta \ddot{h} + 1961.6 \frac{\Delta h}{x_1} - 44.29 \frac{\Delta I}{u}$$

a). Sea $x_2 = \Delta \dot{h} = \dot{x}_1$

$$\dot{x}_2 = \Delta \ddot{h}$$

$$\dot{x}_2 = +1961.6 x_1 - 44.29 u$$

b). E.B.

$$\dot{x}_1 = x_2$$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ +1961.6 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ -44.29 \end{bmatrix} u$$

$$y = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \end{bmatrix} u$$

$$\begin{aligned} T_{el} &= 1 \text{ s} \Rightarrow \sigma_d = \frac{4}{1} = 4 & S_{1,z} &= -4 \pm 2.729j \\ M_F &= 1 \text{ l} & \omega_d &= 2.729 & S_y &= -20 \end{aligned}$$

$$((s+4)-2.729j)(s+4)+2.729j)$$

$$(s+4)^2 - (2.729j)^2 = s^2 + 8s + 16 + 7.447 = s^2 + 8s + 23.45 \rightarrow \alpha(s) = (s^2 + 8s + 23.45)(s+20)$$

$$s^3 + 8s^2 + 23.45s + 20s^2 + 160s + 464$$

$$\alpha(s) = s^3 + 28s^2 + 183.45s + 469$$

Considere $m=0.2\text{Kg}$, $g=9.81\text{m/s}^2$, $k=0.001$. Se desea controlar la posición de la bola.

- a) Linealizar el modelo dinámico alrededor de un punto de equilibrio $\bar{h} = 0.01 \text{ m}$.
Para ello deberá calcular \bar{I} . Considerar $x_1 = h - \bar{h} = l - \bar{l}$. (2 puntos)
- b) Diseñar un servosistema agregando integrador para controlar x_1 con las especificaciones de diseño $T_{es} = 1$; $M_p = 1\%$. (4 puntos)
- c) Diseñar un observador de estado. (2 puntos)
- d) Graficar el diagrama de simulación del servosistema con observador con la planta lineal. (2 puntos)
- e) Graficar el diagrama de simulación del servosistema con la planta no lineal. Considerar un bloque de elevación y un bloque de elevación al cuadrado. (2 puntos)

Servosistema agregando integrador:

$$\begin{bmatrix} \dot{x}(t) \\ \dot{z}(t) \end{bmatrix} = \underbrace{\begin{bmatrix} A & 0 \\ -C & 0 \end{bmatrix}}_{A_N} \begin{bmatrix} x(t) \\ z(t) \end{bmatrix} + \underbrace{\begin{bmatrix} B \\ 0 \end{bmatrix}}_{B_N} u(t) + \underbrace{\begin{bmatrix} 0 \\ 1 \end{bmatrix}}_{B_r} r(t) \quad y = C_N x + D$$

$$AN = \begin{bmatrix} 0 & 1 & 0 \\ 146.6 & 0 & 0 \\ -1 & 0 & 0 \end{bmatrix} \quad DN = \begin{bmatrix} 0 \\ -44.24 \\ 0 \end{bmatrix} \quad B_r = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$

Usando Ackermann:

$$C_0 = \begin{bmatrix} B_N & A_N^T B_N & A_N^T B_N \\ -44.24 & 0 & -86879.264 \\ 0 & 0 & 44.24 \end{bmatrix}$$

$$\det(C_0) = -86379.44559 \neq 0 \rightarrow S1 \text{ es controlable}$$

$$\alpha(s) = s^3 + 28s^2 + 183.45s + 469$$

$$\chi(A_N) = A^3 + 28A^2 + 183.45A + 469I$$

$$\hat{K} = [0 \ 0 \ 1] C_0^{-1} \phi(A_{00}) = \underbrace{[-48.43 \ -0.6322]}_K \underbrace{[10.389]}_{K_x}$$

c). Überwachungs:

$$\theta = \begin{bmatrix} c \\ ca \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \rightarrow \det(\theta) = 1 \neq 0 \therefore \text{si es}$$

$$S_{1,2} = -4 \pm 2.729j$$

$$S_5 = -20$$

$$S_4 = 2S_1 = -8 + 5.458j$$

$$S_5 = 2S_2 = -8 - 5.458j$$

$$\Rightarrow \omega_e(s) = ((s+8) - 5.458j)((s+8) + 5.458j)$$

$$(s+8)^2 - (5.458j)^2 = s^2 + 16$$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ +1941.6 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ -99.29 \end{bmatrix} u$$

$$y = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \end{bmatrix} u$$

$$\alpha_e(A) = A^2 + 16A + 93.79I$$

Ackermann:

$$L = \alpha_c(A) \cdot 0.6^{-1} \begin{bmatrix} 0 \\ 1 \end{bmatrix} = \begin{bmatrix} 16 \\ 2055.91 \end{bmatrix}$$

$$A \times C \subseteq B \times D$$

$$-kx$$

$$\dot{x} = Ax + Bu$$



