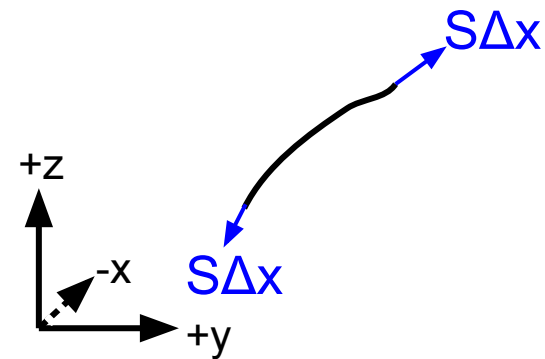


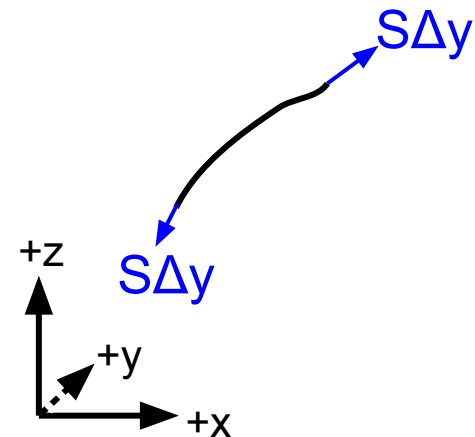
Predicting Drum Vibrations Using the Polar Wave Equation

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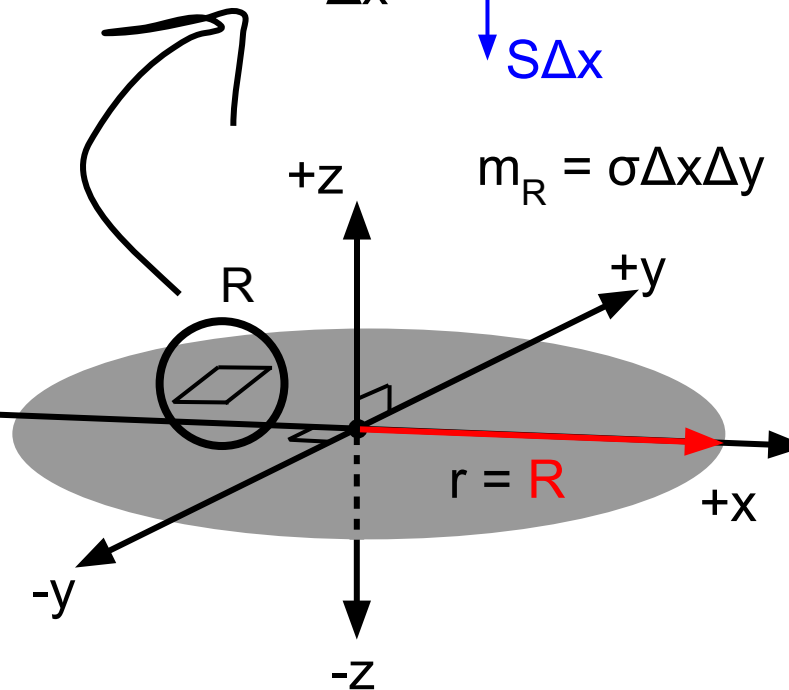
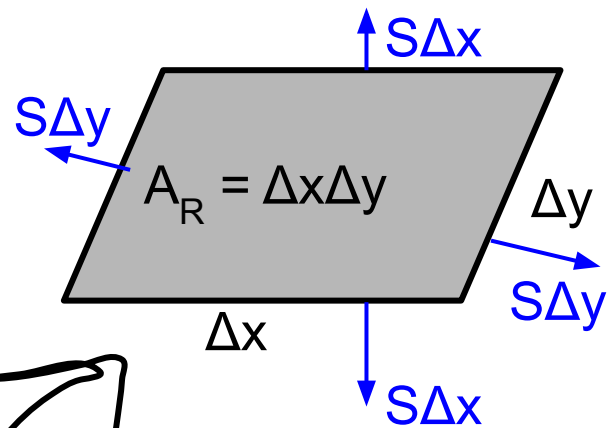
Deriving the (2 + 1)D Wave Equation



$$\begin{aligned}
 F_y &= S\Delta x \left(\frac{\partial z}{\partial y}(y + \Delta y) - \frac{\partial z}{\partial y}(y) \right) \\
 &= S\Delta x \Delta y \left(\frac{\frac{\partial z}{\partial y}(y + \Delta y) - \frac{\partial z}{\partial y}(y)}{\Delta y} \right) \\
 &= S\Delta x \Delta y \frac{\partial^2 z}{\partial x^2}
 \end{aligned}$$



$$\begin{aligned}
 F_x &= S\Delta y \left(\frac{\partial z}{\partial x}(x + \Delta x) - \frac{\partial z}{\partial x}(x) \right) \\
 &= S\Delta y \Delta x \left(\frac{\frac{\partial z}{\partial x}(x + \Delta x) - \frac{\partial z}{\partial x}(x)}{\Delta x} \right) \\
 &= S\Delta y \Delta x \frac{\partial^2 z}{\partial x^2}
 \end{aligned}$$



Deriving the (2 + 1)D Wave Equation

$$ma = F_{net}$$

$$(\sigma \Delta x \Delta y) \frac{\partial^2 z}{\partial t^2} = F_x + F_y$$

$$(\sigma \Delta x \Delta y) \frac{\partial^2 z}{\partial t^2} = S \Delta y \Delta x \left(\frac{\partial^2 z}{\partial x^2} + \frac{\partial^2 z}{\partial y^2} \right)$$

$$\frac{\partial^2 z}{\partial t^2} = \frac{S}{\sigma} \left(\frac{\partial^2 z}{\partial x^2} + \frac{\partial^2 z}{\partial y^2} \right)$$

$$\frac{\partial^2 z}{\partial t^2} = c^2 \nabla^2 z(x, y, t), c = \sqrt{\frac{S}{\sigma}}$$

Assumptions:

- Density is constant across the drum head
- Only forces acting on rectangular patches are tension forces, and tension is constant
- Points in membrane only move in transverse direction up and down, and not parallel to the xy-plane

Physical Representation

- Telegraph Equation
- Can be used to account for friction and other damping forces on the drum
- Does not change spatial solution, only time

$$\frac{\partial^2 z}{\partial t^2} = c^2 \nabla^2 z - \alpha \frac{\partial z}{\partial t}, \quad \alpha > 0$$

Solutions

Undamped

$$z_{m,n}(r, \theta, t) = J_m \left(\sqrt{\lambda_{m,n}} r \right) \cdot \begin{cases} \cos \left(\sqrt{\mu_m} \theta \right) \\ \sin \left(\sqrt{\mu_m} \theta \right) \end{cases} \cdot \begin{cases} \cos \left(c \sqrt{\lambda_{mn}} t \right) \\ \sin \left(c \sqrt{\lambda_{mn}} t \right) \end{cases}$$

$$z_{m,n}(r, \theta, t) = J_m \left(\sqrt{\lambda_{m,n}} r \right) \cdot \begin{cases} \cos \left(\sqrt{\mu_m} \theta \right) \\ \sin \left(\sqrt{\mu_m} \theta \right) \end{cases} \cdot \begin{cases} e^{\frac{-\alpha + \sqrt{\alpha^2 - 4\lambda c^2}}{2} t} \\ e^{\frac{-\alpha - \sqrt{\alpha^2 - 4\lambda c^2}}{2} t} \end{cases}$$

for $\alpha > 2c\sqrt{\lambda}$

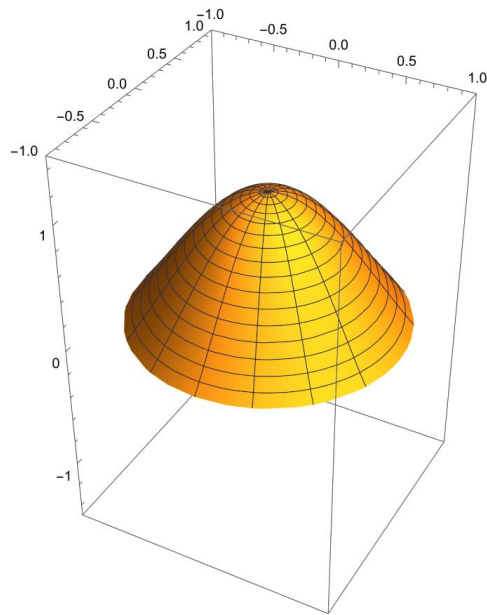
Damped

$$z_{m,n}(r, \theta, t) = J_m \left(\sqrt{\lambda_{m,n}} r \right) \cdot \begin{cases} \cos \left(\sqrt{\mu_m} \theta \right) \\ \sin \left(\sqrt{\mu_m} \theta \right) \end{cases} \cdot \begin{cases} e^{-\alpha t/2} \\ t e^{-\alpha t/2} \end{cases}$$

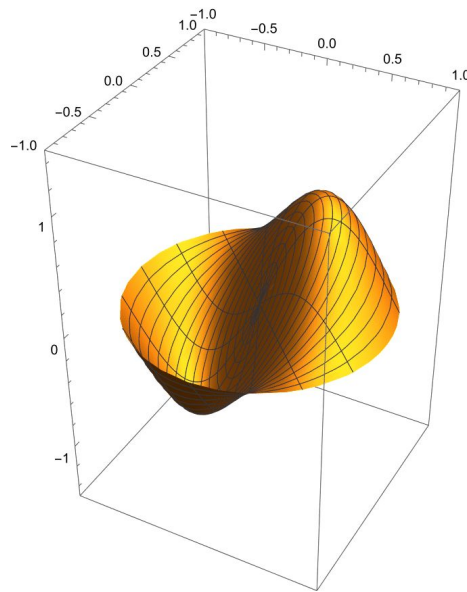
for $\alpha = 2c\sqrt{\lambda}$

$$z_{m,n}(r, \theta, t) = J_m \left(\sqrt{\lambda_{m,n}} r \right) \cdot \begin{cases} \cos \left(\sqrt{\mu_m} \theta \right) \\ \sin \left(\sqrt{\mu_m} \theta \right) \end{cases} \cdot \begin{cases} e^{-\alpha t/2} \cos(\alpha^2 - 4\lambda c^2)t \\ e^{-\alpha t/2} \sin(\alpha^2 - 4\lambda c^2)t \end{cases}$$

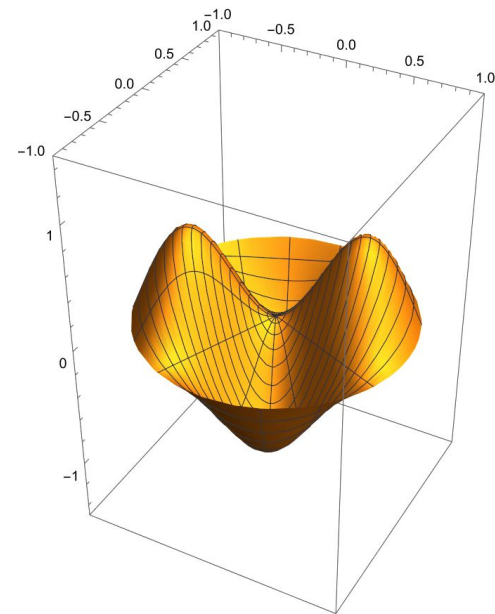
Undamped Modes



Mode (0, 1)

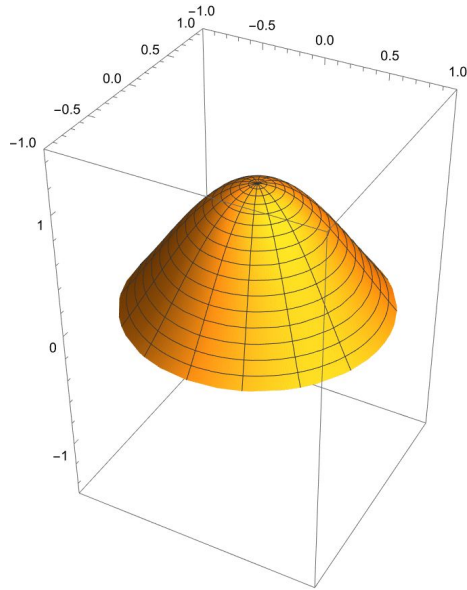


Mode (1, 1)

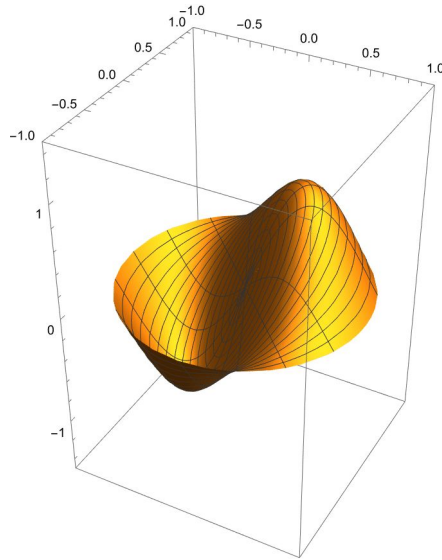


Mode (2, 1)

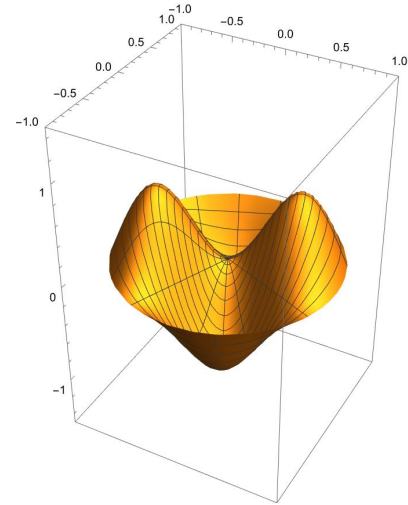
Damped Modes



Mode (0, 1)

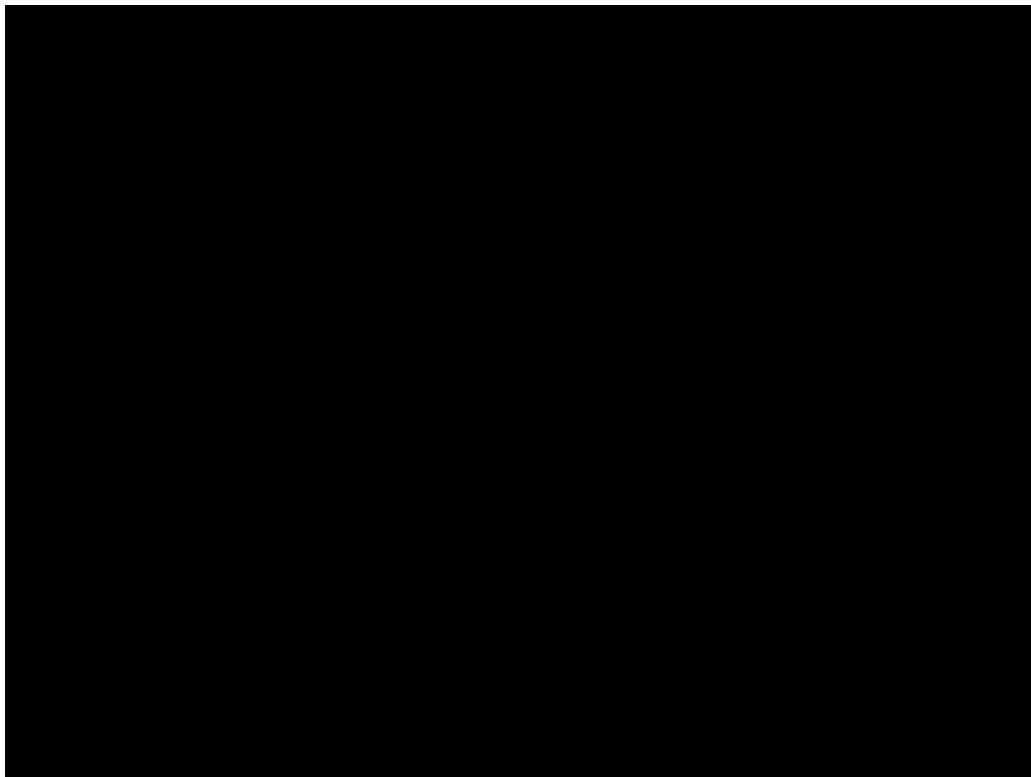


Mode (1, 1)



Mode (2, 1)

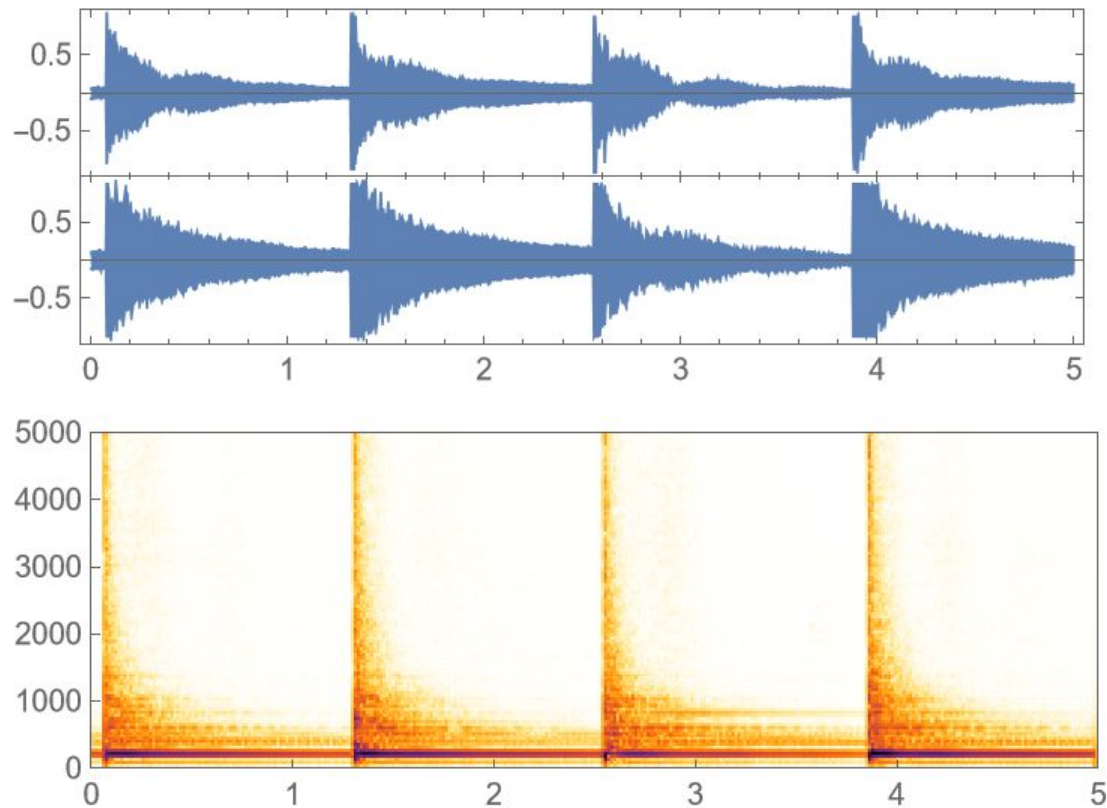
Comparison to Real World



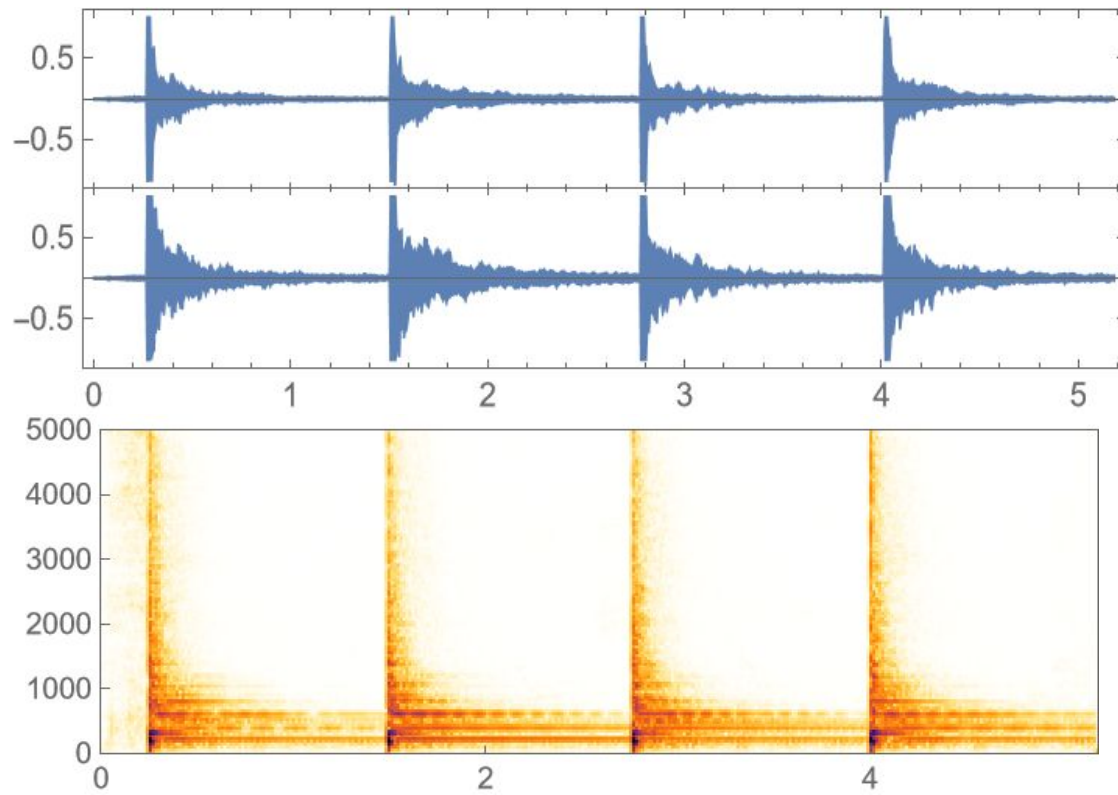
Experimental results

- Used 6 inch radius floor tom
- Polyethylene Terephthalate drum head with density around 1.38 g/cm^3
- Tensioned with roughly 16 N/cm of force

Spectrogram and Waveform - Center hit



Spectrogram and Waveform - Off-center hit



Conclusion

- Striking the drum in the center results in lower frequencies being more pronounced
- When struck off center, frequencies are more varied, resulting in a fuller sound
- The frequency of individual drum modes is not dependent on where or how hard the drum is struck
 - Location and velocity of the drum strike still result in a different sound
 - This is due to changes in amplitude and a difference of overlapping frequencies
- The tension and material of the drum head determine the resulting frequency

Further goals

- Construct a more accurate model for initial conditions, primarily for strikes that are off center on the drum head
- Take measurements for assumed constants in experimental tests
 - Measure drum tension rather than just use an assumed average