

# **Supercritical Extraction**

A process model and a sensitivity analysis

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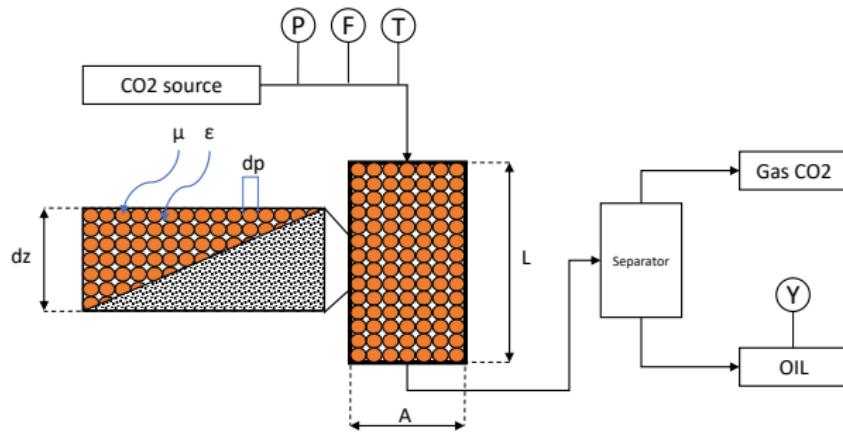
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## **Supercritical extraction - process description**

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**Figure 1:** Schematic representation of SFE process

## **Model description**

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# Model of the extractor

control variables, state variables, variables and parameters

(1) Fluid phase mass balance

$$\frac{\partial \textcolor{blue}{c}(t, z)}{\partial t} = -\frac{1}{\epsilon \textcolor{green}{A}} \frac{\textcolor{red}{F}(t)}{\rho(\textcolor{blue}{T}(t, z)\textcolor{red}{P}(t))} \frac{\partial \textcolor{blue}{c}(t, z)}{\partial z} + \textcolor{brown}{D}_e^M (\textcolor{blue}{T}(t, z)\textcolor{red}{P}(t)) \frac{\partial^2 \textcolor{blue}{c}(t, z)}{\partial z^2} + \frac{1 - \epsilon}{\epsilon} \textcolor{blue}{r}_e(t, z)$$

(2) Solid phase mass balance

$$\frac{\partial \textcolor{blue}{q}(t, z)}{\partial t} = \textcolor{blue}{r}_e(t, z)$$

(3) Heat balance

$$\frac{\partial \textcolor{blue}{T}(t, z)}{\partial t} = -\frac{\textcolor{red}{F}(t)}{\textcolor{green}{A}} \frac{\textcolor{brown}{C}_p(\textcolor{blue}{T}(t, z)\textcolor{red}{P}(t))}{[(1 - \epsilon)\rho(\textcolor{blue}{T}(t, z)\textcolor{red}{P}(t))\textcolor{brown}{C}_p(\textcolor{blue}{T}(t, z)\textcolor{red}{P}(t)) + \epsilon \rho_s \textcolor{brown}{C}_{ps}]} \frac{\partial \textcolor{blue}{T}(t, z)}{\partial z} + \textcolor{brown}{D}_e^T (\textcolor{blue}{T}(t, z)\textcolor{red}{P}(t)) \frac{\partial^2 \textcolor{blue}{T}(t, z)}{\partial z^2}$$

Extraction kinetic

$$\textcolor{blue}{r}_e(t, z) = -\frac{\textcolor{brown}{D}_i(\textcolor{blue}{T}(t, z))}{\mu l^2} \left( \textcolor{blue}{q}(t, z) - \textcolor{blue}{c}(t, z) \frac{\rho_s}{k_m(\textcolor{blue}{T}(t, z))\rho(\textcolor{blue}{T}(t, z)\textcolor{red}{P}(t))} \right)$$

Output function

$$\textcolor{blue}{y}(t) = \textcolor{blue}{g}(x(t)) = \frac{\sum_{i=1}^{N_z} \left( \frac{1}{N_z} (\textcolor{green}{m}_0 - \textcolor{blue}{m}_i(t, z)) \right)}{m_0} = \frac{\sum_{i=1}^{N_z} \left( \frac{\textcolor{green}{V}}{N_z} (\textcolor{green}{q}_0 - \textcolor{blue}{q}_i(t, z)) \right)}{q_0 V}$$

## SFE - assumptions

- One-dimensional model
- Plug flow
- No pressure drop
- Negligible external diffusion
- Single component
- Pseudo-homogeneous thermal properties
- Uniformly distribution of the particles

# Model dependencies

(1) Density - Peng-Robinson

$$P(t) = \frac{RT}{V_m - b} - \frac{a\alpha}{V_m^2 + 2bV_m - b^2}$$

(2) Solid phase mass balance

$$C_p(\textcolor{blue}{T}(t, z)P(t)) = C_{pideal} + Cv_{corr} + T \left( \frac{\partial P}{\partial T} \right)_V \left( \frac{\partial V}{\partial T} \right)_P - R$$

(3) Axial diffusion of the mass

$$D_e^M(\textcolor{blue}{T}(t, z)P(t)) = \frac{u(\textcolor{blue}{T}(t, z)P(t))d_p}{\epsilon P_e}$$

(4) Axial diffusion of the heat

$$D_e^T \left[ \frac{m^2}{s} \right] (\textcolor{blue}{T}(t, z)P(t)) = \frac{k^T(\textcolor{blue}{T}(t, z)P(t))}{\rho(\textcolor{blue}{T}(t, z)P(t))C_p(\textcolor{blue}{T}(t, z)P(t))}$$

(5) Internal diffusion

$$\textcolor{brown}{D}_i(\textcolor{blue}{T}(t, z)) \left[ \frac{m^2}{s} \right] = D_{i0} \exp \left( \frac{-EA_{D_i}}{R\textcolor{blue}{T}(t, z)} \right)$$

(6) Partition coefficient

$$k_m(\textcolor{blue}{T}(t, z)) [-] = k_{m0} \exp \left( \frac{-EA_{k_m}}{R\textcolor{blue}{T}(t, z)} \right)$$

## SFE - state-space model

$$\begin{bmatrix} \frac{\partial c(t, z)}{\partial t} \\ \frac{\partial q(t, z)}{\partial t} \\ \frac{\partial T(t, z)}{\partial t} \end{bmatrix} = \begin{bmatrix} \phi_1(c(t, z), q(t, z), T(t, z); \theta) \\ \phi_2(c(t, z), q(t, z), T(t, z); \theta) \\ \phi_3(c(t, z), q(t, z), T(t, z); \theta) \end{bmatrix} = \phi(t, z; \theta) = \frac{\partial \chi(t, z)}{\partial t}$$

where  $\theta$  is a set of parameters present in the model,  $\phi$  is a set of functions which correspond to state equations of the model and  $\chi$  is the state space model.

## SFE - discretization

$$\frac{dx(t)}{dt} = \begin{bmatrix} \frac{dc_1(t)}{dt} \\ \vdots \\ \frac{dc_{N_z}(t)}{dt} \\ \frac{dq_1(t)}{dt} \\ \vdots \\ \frac{dq_{N_z}(t)}{dt} \\ \frac{dT_1(t)}{dt} \\ \vdots \\ \frac{dT_{N_z}(t)}{dt} \end{bmatrix} = \begin{bmatrix} F_1(c(t), q(t), T(t); p) \\ \vdots \\ F_{N_z}(c(t), q(t), T(t); p) \\ F_{N_z+1}(c(t), q(t), T(t); p) \\ \vdots \\ F_{2N_z}(c(t), q(t), T(t); p) \\ F_{2N_z+1}(c(t), q(t), T(t); p) \\ \vdots \\ F_{3N_z}(c(t), q(t), T(t); p) \end{bmatrix} = F(t; p)$$

where  $x \in \mathbb{R}^{N_x=3N_z}$  and  $p \in \mathbb{R}^{N_p=N_\theta+N_u}$

## Sensitivity Analysis

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Local derivative-based methods involve taking the partial derivative of the output with respect to an input parameter. In sensitivity analysis the original system of equations is solved simultaneously with  $\frac{\partial \mathbf{F}(x(t); p)}{\partial p}$ , where  $p$  is a vector of all the parameters and the control variables.

# Sensitivity Analysis

$$Z = \frac{\partial \mathbf{x}(t, p)}{\partial p}$$

$$\dot{Z} = \frac{\partial Z(t, p)}{\partial t} = \frac{\partial}{\partial t} \left( \frac{\partial \mathbf{x}(t, p)}{\partial p} \right) = \frac{\partial}{\partial p} \left( \frac{\partial \mathbf{x}(t, p)}{\partial t} \right) = \frac{\partial F(x(t); p)}{\partial p}$$

$$\begin{aligned}\frac{dF(x(t); p)}{dp} &= \frac{\partial F(x(t); p)}{\partial x(t)} \frac{\partial x(t)}{\partial p} + \frac{\partial F(x(t); p)}{\partial p} \\ &= J_x(x(t); p) S(x(t); p) + J_p(x(t); p)\end{aligned}$$

$$\frac{dF(x(t); p)}{dp} = J_x S + J_p$$

$(N_x \times N_p)$        $(N_x \times N_x)$        $(N_x \times N_p)$        $(N_x \times N_p)$

# Sensitivity Analysis

$$\frac{dF(x(t); p)}{dp} = \left( \begin{array}{cccc} \frac{\partial F_1(x(t); p)}{\partial x_1(t)} & \frac{\partial F_1(x(t); p)}{\partial x_2(t)} & \dots & \frac{\partial F_1(x(t); p)}{\partial x_{N_X}(t)} \\ \frac{\partial F_2(x(t); p)}{\partial x_1(t)} & \frac{\partial F_2(x(t); p)}{\partial x_2(t)} & \dots & \frac{\partial F_2(x(t); p)}{\partial x_{N_X}(t)} \\ \vdots & \vdots & \ddots & \vdots \\ \frac{\partial F_{N_X}(x(t); p)}{\partial x_1(t)} & \frac{\partial F_{N_X}(x(t); p)}{\partial x_2(t)} & \dots & \frac{\partial F_{N_X}(x(t); p)}{\partial x_{N_X}(t)} \end{array} \right) \left( \begin{array}{cccc} \frac{dx_1(t)}{dp_1} & \frac{dx_1(t)}{dp_2} & \dots & \frac{dx_1(t)}{dp_{N_p}} \\ \frac{dx_2(t)}{dp_1} & \frac{dx_2(t)}{dp_2} & \dots & \frac{dx_2(t)}{dp_{N_p}} \\ \vdots & \vdots & \ddots & \vdots \\ \frac{dx_{N_X}(t)}{dp_1} & \frac{dx_{N_X}(t)}{dp_2} & \dots & \frac{dx_{N_X}(t)}{dp_{N_p}} \end{array} \right) +$$

$$+ \left( \begin{array}{cccc} \frac{\partial F_1(x(t); p)}{\partial p_1} & \frac{\partial F_1(x(t); p)}{\partial p_2} & \dots & \frac{\partial F_1(x(t); p)}{\partial p_{N_p}} \\ \frac{\partial F_2(x(t); p)}{\partial p_1} & \frac{\partial F_2(x(t); p)}{\partial p_2} & \dots & \frac{\partial F_2(x(t); p)}{\partial p_{N_p}} \\ \vdots & \vdots & \ddots & \vdots \\ \frac{\partial F_{N_X}(x(t); p)}{\partial p_1} & \frac{\partial F_{N_X}(x(t); p)}{\partial p_2} & \dots & \frac{\partial F_{N_X}(x(t); p)}{\partial p_{N_p}} \end{array} \right)$$

## Sensitivity Analysis

The  $F(x(t); p)$  is augmented with sensitivity equations and denoted as  $\mathbf{F}(x(t); p)$ . The size of  $\mathbf{F}(x(t); p)$  is equal to  $N_s = N_x(N_p + 1)$ .

$$\mathbf{F}(x(t); p) = \begin{bmatrix} F(x(t); p) \\ J_x(x(t); p)S(x(t); p) + J_p(x(t); p) \end{bmatrix}$$

The initial conditions are described as

$$\mathbf{F}(x(t_0); p) = \left[ x(t_0), \quad \frac{dx(t_0)}{dp_1}, \quad \dots, \quad \frac{dx(t_0)}{dp_{N_p}} \right]^T$$

# Sensitivity Analysis

$$y(t) = g(x(t)) = \frac{\sum_{i=1}^{N_z} \left( \frac{1}{N_z} (m_0 - m_i(t, z)) \right)}{m_0} = \frac{\sum_{i=1}^{N_z} \left( \frac{V}{N_z} (q_0 - q_i(t, z)) \right)}{q_0 V}$$

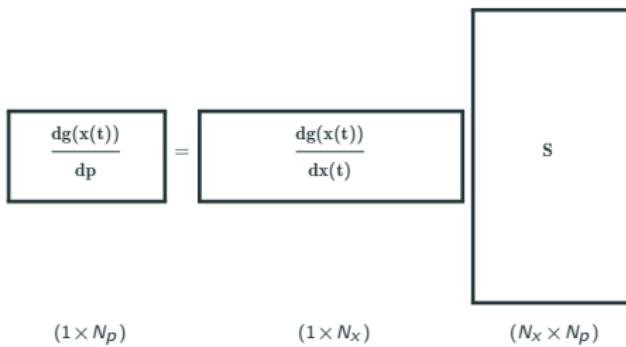
By taking a total derivative of  $y(t)$  with respect to  $p$ , the new sensitivity equation can found.

$$\begin{aligned} \frac{dy(t)}{dp} &= \frac{dg(x(t))}{dp} = \frac{\partial g(x(t))}{\partial x(t)} \frac{\partial x(t)}{\partial p} + \frac{\partial g(x(t))}{\partial p} \\ \frac{\partial g(x(t))}{\partial p} &= \frac{\partial g(x(t))}{\partial x(t)} \frac{\partial x(t)}{\partial p} + 0 = \frac{\partial g(x(t))}{\partial x(t)} S(x(t); p) = \\ &\quad \left( \begin{array}{cccc} \frac{\partial g_1(x(t))}{\partial x_1} & \frac{\partial g_1(x(t))}{\partial x_2} & \dots & \frac{\partial g_1(x(t))}{\partial x_{N_x}} \\ \frac{\partial g_2(x(t))}{\partial x_1} & \frac{\partial g_2(x(t))}{\partial x_2} & \dots & \frac{\partial g_2(x(t))}{\partial x_{N_x}} \\ \vdots & \vdots & \ddots & \vdots \\ \frac{\partial g_{N_g}(x(t))}{\partial x_1} & \frac{\partial g_{N_g}(x(t))}{\partial x_2} & \dots & \frac{\partial g_{N_g}(x(t))}{\partial x_{N_x}} \end{array} \right) \left( \begin{array}{cccc} s_{(1,1)} & s_{(1,2)} & \dots & s_{(1,N_p)} \\ s_{(2,1)} & s_{(2,2)} & \dots & s_{(2,N_p)} \\ \vdots & \vdots & \ddots & \vdots \\ s_{(N_x,1)} & s_{(N_x,2)} & \dots & s_{(N_x,N_p)} \end{array} \right) \end{aligned}$$

# Sensitivity Analysis

Because the output function returns only one value, the equation becomes

$$\begin{aligned} & \left( \frac{\partial y(x(t))}{\partial p_1}, \frac{\partial y(x(t))}{\partial p_2}, \dots, \frac{\partial y(x(t))}{\partial p_{N_p}} \right) = \\ &= \left( \frac{\partial g(x(t))}{\partial x_1}, \frac{\partial g(x(t))}{\partial x_2}, \dots, \frac{\partial g(x(t))}{\partial x_{N_x}} \right) \begin{pmatrix} s_{(1,1)} & s_{(1,2)} & \cdots & s_{(1,N_p)} \\ s_{(2,1)} & s_{(2,2)} & \cdots & s_{(2,N_p)} \\ \vdots & \vdots & \ddots & \vdots \\ s_{(N_x,1)} & s_{(N_x,2)} & \cdots & s_{(N_x,N_p)} \end{pmatrix} \end{aligned}$$



## Results

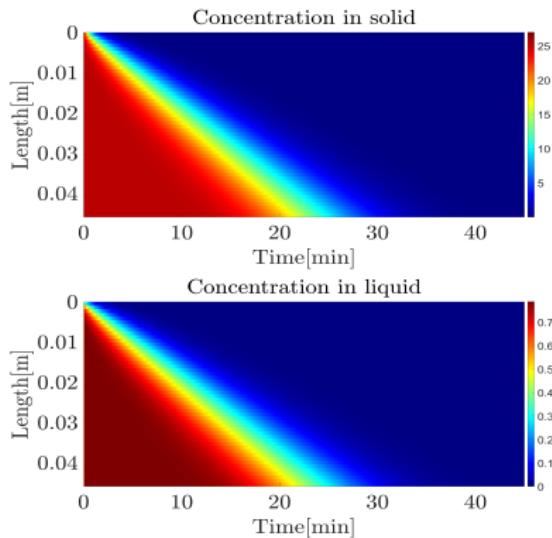
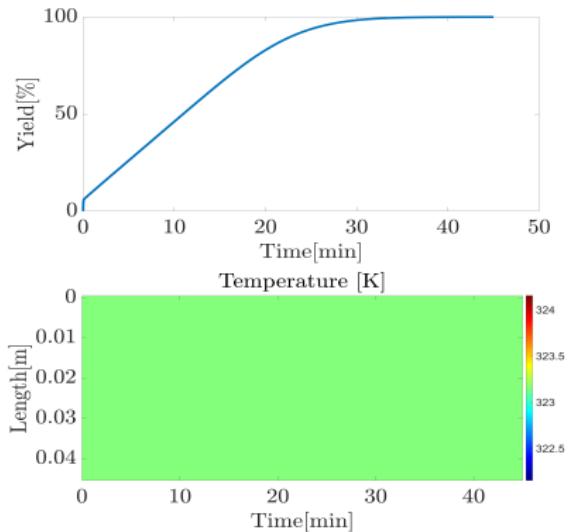
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# Results of the simulation

Product: CARQUEJA essential oil

Ref	$F[kg/hr]$	$T_{Inlet}[C]$	$T_{extractor}[C]$	$P[bar]$	$c[kg/m^3]$	$q[kg/m^3]$
Vargas	0.035	50	50	90	0	27

Table 1: Initial conditions

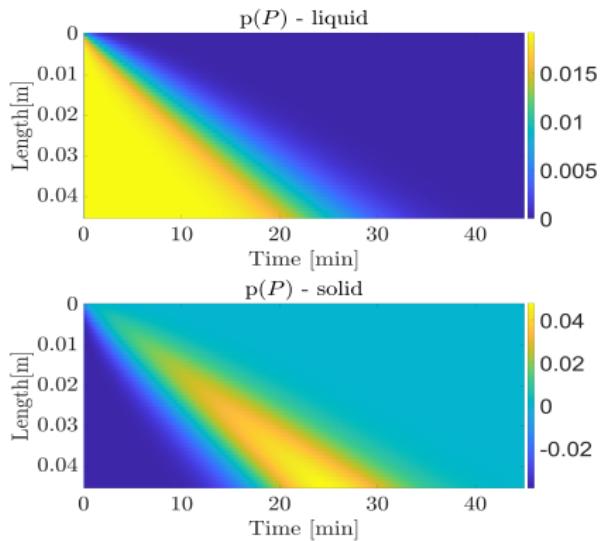
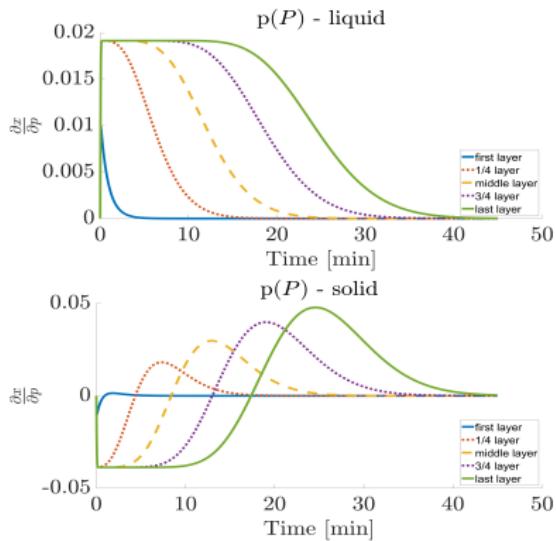


# Sensitivity Analysis - Pressure

$$\frac{\partial \textcolor{blue}{c}(t, z)}{\partial t} = -\frac{F(t)}{\epsilon A \rho(T(t, z) \textcolor{red}{P}(t))} \frac{\partial c(t, z)}{\partial z} + D_e^M(T(t, z) \textcolor{red}{P}(t)) \frac{\partial^2 c(t, z)}{\partial z^2} + \frac{1 - \epsilon}{\epsilon} \frac{D_i(T(t, z))}{\mu l^2} \left( q(t, z) - \frac{c(t, z) \rho_s}{k_m(T(t, z)) \rho(T(t, z) \textcolor{red}{P}(t))} \right)$$

$$\frac{\partial \textcolor{violet}{q}(t, z)}{\partial t} = -\frac{D_i(T(t, z))}{\mu l^2} \left( q(t, z) - c(t, z) \frac{\rho_s}{k_m(T(t, z)) \rho(T(t, z) \textcolor{red}{P}(t))} \right)$$

$$\frac{\partial \textcolor{blue}{T}(t, z)}{\partial t} = -\frac{F(t)}{A} \frac{C_p(T(t, z) \textcolor{red}{P}(t))}{[(1 - \epsilon) \rho(T(t, z) \textcolor{red}{P}(t)) C_p(T(t, z) \textcolor{red}{P}(t)) + \epsilon \rho_s C_{ps}]} \frac{\partial T(t, z)}{\partial z} + D_e^T(T(t, z) \textcolor{red}{P}(t)) \frac{\partial^2 T(t, z)}{\partial z^2}$$

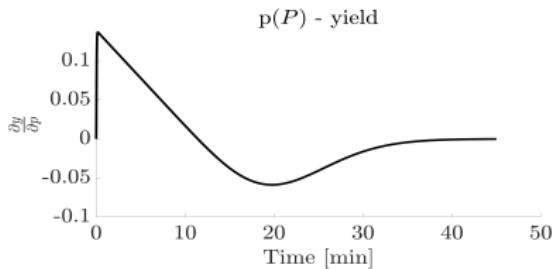
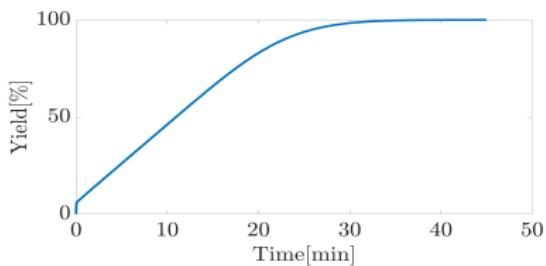


## Sensitivity Analysis - Pressure

$$\frac{\partial \textcolor{blue}{c}(t, z)}{\partial t} = -\frac{F(t)}{\epsilon A \rho(T(t, z) \textcolor{red}{P}(t))} \frac{\partial c(t, z)}{\partial z} + D_e^M(T(t, z) \textcolor{red}{P}(t)) \frac{\partial^2 c(t, z)}{\partial z^2} + \frac{1 - \epsilon}{\epsilon} \frac{D_i(T(t, z))}{\mu l^2} \left( q(t, z) - \frac{c(t, z) \rho_s}{k_m(T(t, z)) \rho(T(t, z) \textcolor{red}{P}(t))} \right)$$

$$\frac{\partial \textcolor{blue}{q}(t, z)}{\partial t} = -\frac{D_i(T(t, z))}{\mu l^2} \left( q(t, z) - c(t, z) \frac{\rho_s}{k_m(T(t, z)) \rho(T(t, z) \textcolor{red}{P}(t))} \right)$$

$$\frac{\partial \textcolor{blue}{T}(t, z)}{\partial t} = -\frac{F(t)}{A} \frac{C_p(T(t, z) \textcolor{red}{P}(t))}{[(1 - \epsilon) \rho(T(t, z) \textcolor{red}{P}(t)) C_p(T(t, z) \textcolor{red}{P}(t)) + \epsilon \rho_s C_{ps}]} \frac{\partial T(t, z)}{\partial z} + D_e^T(T(t, z) \textcolor{red}{P}(t)) \frac{\partial^2 T(t, z)}{\partial z^2}$$

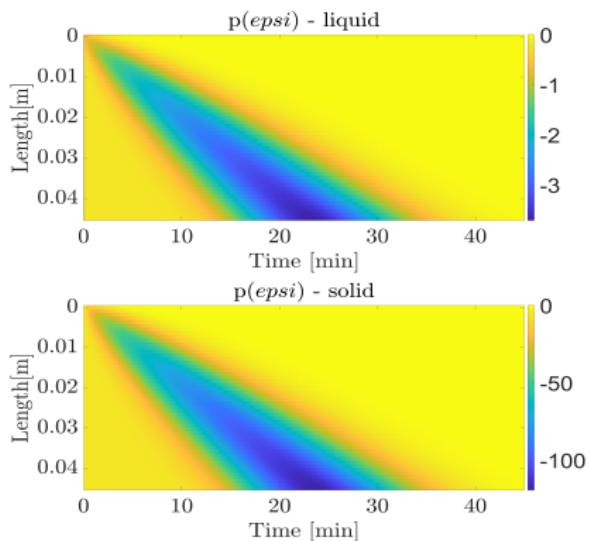
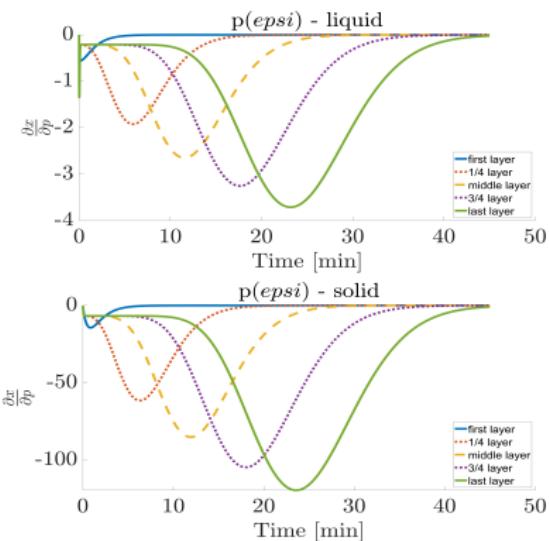


# Sensitivity Analysis - Void Fraction

$$\frac{\partial \mathbf{c}(t, z)}{\partial t} = -\frac{F(t)}{\epsilon A \rho(T(t, z)P(t))} \frac{\partial c(t, z)}{\partial z} + D_e^M(T(t, z)P(t)) \frac{\partial^2 c(t, z)}{\partial z^2} + \frac{1 - \epsilon}{\epsilon} \frac{D_i(T(t, z))}{\mu l^2} \left( q(t, z) - \frac{c(t, z)\rho_s}{k_m(T(t, z))\rho(T(t, z)P(t))} \right)$$

$$\frac{\partial \mathbf{q}(t, z)}{\partial t} = -\frac{D_i(T(t, z))}{\mu l^2} \left( q(t, z) - c(t, z) \frac{\rho_s}{k_m(T(t, z))\rho(T(t, z)P(t))} \right)$$

$$\frac{\partial \mathbf{T}(t, z)}{\partial t} = -\frac{F(t)}{A} \frac{C_p(T(t, z)P(t))}{[(1 - \epsilon)\rho(T(t, z)P(t))C_p(T(t, z)P(t)) + \epsilon\rho_s C_{ps}]} \frac{\partial T(t, z)}{\partial z} + D_e^T(T(t, z)P(t)) \frac{\partial^2 T(t, z)}{\partial z^2}$$

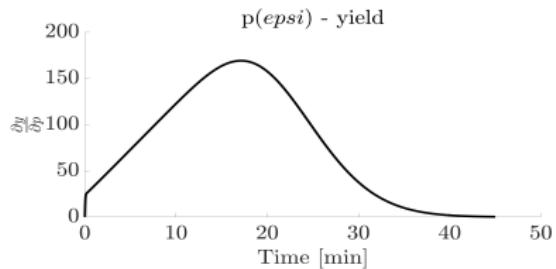
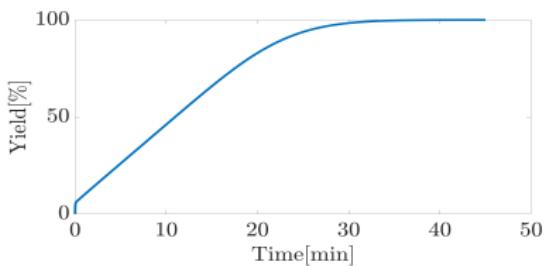


# Sensitivity Analysis - Void Fraction

$$\frac{\partial \textcolor{blue}{c}(t, z)}{\partial t} = -\frac{F(t)}{\epsilon A \rho(T(t, z)P(t))} \frac{\partial c(t, z)}{\partial z} + D_e^M(T(t, z)P(t)) \frac{\partial^2 c(t, z)}{\partial z^2} + \frac{1 - \epsilon}{\epsilon} \frac{D_i(T(t, z))}{\mu l^2} \left( q(t, z) - \frac{c(t, z)\rho_s}{k_m(T(t, z))\rho(T(t, z)P(t))} \right)$$

$$\frac{\partial \textcolor{blue}{q}(t, z)}{\partial t} = -\frac{D_i(T(t, z))}{\mu l^2} \left( q(t, z) - c(t, z) \frac{\rho_s}{k_m(T(t, z))\rho(T(t, z)P(t))} \right)$$

$$\frac{\partial \textcolor{blue}{T}(t, z)}{\partial t} = -\frac{F(t)}{A} \frac{C_p(T(t, z)P(t))}{[(1 - \epsilon)\rho(T(t, z)P(t))C_p(T(t, z)P(t)) + \epsilon\rho_s C_{ps}]} \frac{\partial T(t, z)}{\partial z} + D_e^T(T(t, z)P(t)) \frac{\partial^2 T(t, z)}{\partial z^2}$$

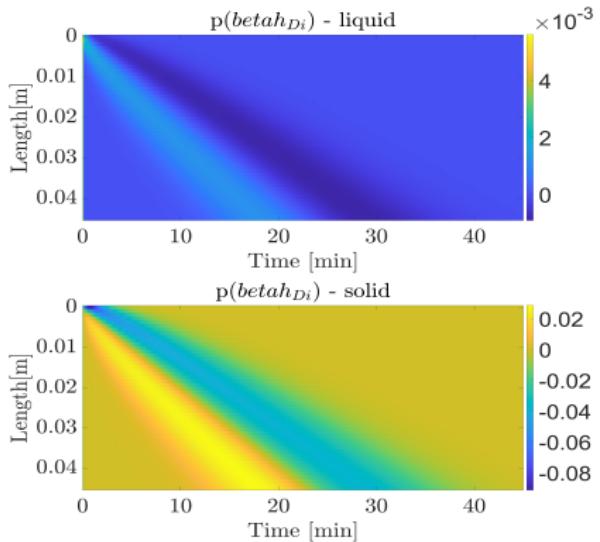
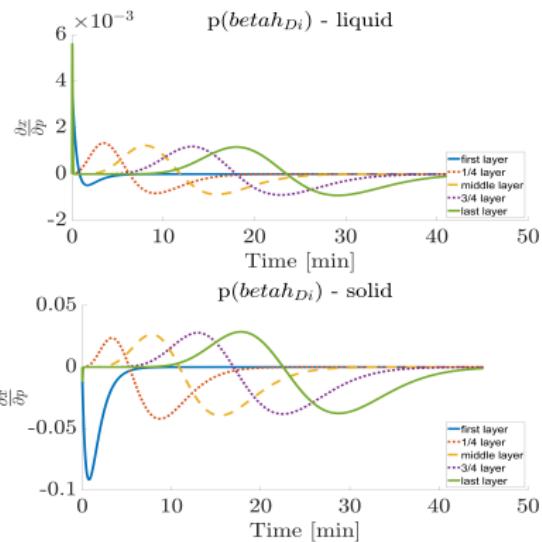


# Sensitivity Analysis - Internal Diffusion

$$\frac{\partial \textcolor{blue}{c}(t, z)}{\partial t} = -\frac{F(t)}{\epsilon A \rho(T(t, z)P(t))} \frac{\partial c(t, z)}{\partial z} + D_e^M(T(t, z)P(t)) \frac{\partial^2 c(t, z)}{\partial z^2} + \frac{1 - \epsilon}{\epsilon} \frac{\textcolor{brown}{D}_i(\textcolor{blue}{T}(t, z))}{\mu l^2} \left( q(t, z) - \frac{c(t, z)\rho_s}{k_m(T(t, z))\rho(T(t, z)P(t))} \right)$$

$$\frac{\partial \textcolor{brown}{q}(t, z)}{\partial t} = -\frac{\textcolor{brown}{D}_i(\textcolor{blue}{T}(t, z))}{\mu l^2} \left( q(t, z) - \frac{c(t, z)\rho_s}{k_m(T(t, z))\rho(T(t, z)P(t))} \right)$$

$$\frac{\partial \textcolor{blue}{T}(t, z)}{\partial t} = -\frac{F(t)}{A} \frac{C_p(T(t, z)P(t))}{[(1 - \epsilon)\rho(T(t, z)P(t))C_p(T(t, z)P(t)) + \epsilon\rho_s C_{ps}]} \frac{\partial T(t, z)}{\partial z} + D_e^T(T(t, z)P(t)) \frac{\partial^2 T(t, z)}{\partial z^2}$$

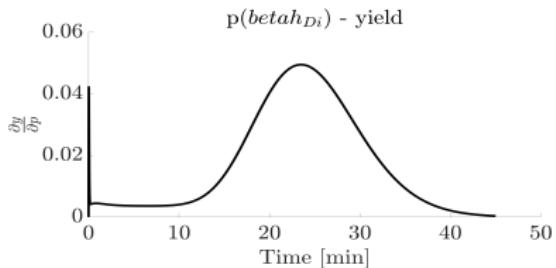
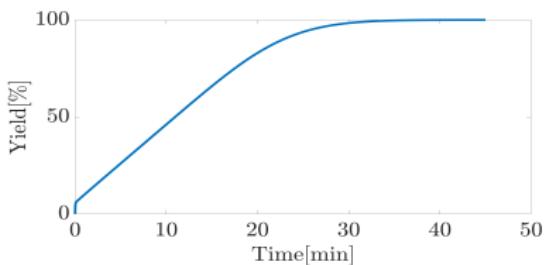


# Sensitivity Analysis - Internal Diffusion

$$\frac{\partial \textcolor{blue}{c}(t, z)}{\partial t} = -\frac{F(t)}{\epsilon A \rho(T(t, z)P(t))} \frac{\partial c(t, z)}{\partial z} + D_e^M(T(t, z)P(t)) \frac{\partial^2 c(t, z)}{\partial z^2} + \frac{1 - \epsilon}{\epsilon} \frac{\textcolor{brown}{D}_i(\textcolor{blue}{T}(t, z))}{\mu l^2} \left( q(t, z) - \frac{c(t, z)\rho_s}{k_m(T(t, z))\rho(T(t, z)P(t))} \right)$$

$$\frac{\partial \textcolor{brown}{q}(t, z)}{\partial t} = -\frac{\textcolor{brown}{D}_i(\textcolor{blue}{T}(t, z))}{\mu l^2} \left( q(t, z) - \frac{c(t, z)\rho_s}{k_m(T(t, z))\rho(T(t, z)P(t))} \right)$$

$$\frac{\partial \textcolor{blue}{T}(t, z)}{\partial t} = -\frac{F(t)}{A} \frac{C_p(T(t, z)P(t))}{[(1 - \epsilon)\rho(T(t, z)P(t))C_p(T(t, z)P(t)) + \epsilon\rho_s C_{ps}]} \frac{\partial T(t, z)}{\partial z} + D_e^T(T(t, z)P(t)) \frac{\partial^2 T(t, z)}{\partial z^2}$$



## What's next?

- Paper related to the sensitivity analysis
- Control of the extraction process
- NovelBaltic
- Laboratory work