Staubli 机器人逆运动学通解

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列举 RX60、RX160L、TX90 机器人 DH 参数(基本涵盖了 Staubli 六轴机器人所有 DH 类型):

注:此处已简化 GetDefaultDH()函数获取的 DH 参数 i=1,2,3,4,5,6

机器人型号	i	RZ(度)θ	X(mm) a	Z(mm) d	RX(度)α
Staubli RX60	1	θ1	0	0	-90
	2	θ2-90°	<mark>290</mark>	0	0
	3	θ3+90°	0	<mark>49</mark>	90
	4	θ4	0	<mark>310</mark>	-90
	5	θ5	0	0	90
	6	θ6	0	<mark>65</mark>	0

机器人型号	i	RZ(度)θ	X(mm) a	Z(mm) d	RX(度)α
RX160L	1	θ1	<mark>150</mark>	0	-90
	2	θ2-90°	<mark>825</mark>	0	0
	3	θ3+90°	0	0	90
	4	θ4	0	<mark>925</mark>	-90
	5	θ5	0	0	90
	6	θ6	0	<mark>110</mark>	0

机器人型号	i	RZ(度)θ	X(mm) a	Z(mm) d	RX(度)α
Staubli TX90	1	θ1	<mark>50</mark>	0	-90
	2	θ2-90°	<mark>425</mark>	0	0
	3	θ3+90°	0	<mark>50</mark>	90
	4	θ4	0	<mark>425</mark>	-90
	5	θ5	0	0	90
	6	θ6	0	<mark>100</mark>	0

写出 DH 参数通式:

机器人型号	i	RZ(度)θ	X(mm) a	Z(mm) d	RX(度)α
Staubli 机器人	1	θ1	<mark>a1</mark>	0	-90
	2	θ2-90°	<mark>a2</mark>	0	0
	3	θ3+90°	0	<mark>d3</mark>	90
	4	θ4	0	<mark>d4</mark>	-90
	5	θ5	0	<mark>0</mark>	90
	6	θ6	0	<mark>d6</mark>	0

把关节轴处的坐标系写成矩阵:

把关节轴处的坐标系写成矩阵:
$$trsf_1 = Rz(\theta_1) \cdot Dx(a_1) \cdot Dz(a_1') \cdot Rx(\alpha_1) = \begin{bmatrix} c1 & 0 & -s1 & a1 \cdot c1 \\ s1 & 0 & c1 & a1 \cdot s1 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$trsf_2 = Rz(\theta_2) \cdot Dx(a_2) \cdot Dz(a_2') \cdot Rx(\alpha_2) = \begin{bmatrix} s2 & c2 & 0 & a2 \cdot s2 \\ -c2 & s2 & 0 & -a2 \cdot c2 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$trsf_3 = Rz(\theta_3) \cdot Dx(a_3) \cdot Dz(a_3') \cdot Rx(\alpha_3) = \begin{bmatrix} -s3 & 0 & c3 & 0 \\ c3 & 0 & s3 & 0 \\ 0 & 1 & 0 & a3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$trsf_4 = Rz(\theta_4) \cdot Dx(a_4) \cdot Dz(a_4) \cdot Rx(\alpha_4) = \begin{bmatrix} c4 & 0 & -s4 & 0 \\ s4 & 0 & c4 & 0 \\ 0 & -1 & 0 & a4 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$trsf_5 = Rz(\theta_5) \cdot Dx(a_5) \cdot Dz(a_5') \cdot Rx(\alpha_5) = \begin{bmatrix} c5 & 0 & s5 & 0 \\ s4 & 0 & -c5 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$trsf_6 = Rz(\theta_6) \cdot Dx(a_6) \cdot Dz(a_6') \cdot Rx(\alpha_6) = \begin{bmatrix} c6 & -s6 & 0 & 0 \\ s6 & c6 & 0 & 0 \\ 0 & 0 & 1 & d6 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$E \Pi P_1 = \{x_1, y_1, z_1, rx_1, ry_1, rz_1\} \quad \text{代表 flange } \ \mathbb{H} \text{ $\mathbb{R}} \text{ $\mathbb{H}} \text{ $\mathbb$$

已知 $P_1 = \{x_1, y_1, z_1, rx_1, ry_1, rz_1\}$ 代表 flange 记录的一点

 $P_2 = \{x_2, y_2, z_2, rx_2, ry_2, rz_2\}$ 代表 flange 根部的一点与 P_1 在工具坐标系 Z 方向相差 d6所以 $P_2 = appro(P_1, \{0,0,-d6,0,0,0\})$ 从 P_2 计算逆解会相对容易 如果用矩阵表达 P.与 P.关系:

$$[P_2] = [P_1] \cdot \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & -d6 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

注: P_2 与 P_3 都为4x4矩阵,由 $\{x,y,z,rx,ry,rz\}$ 六个参数转化而来

$$\mathbf{H} \theta_1 : trsf_1^{-1} \cdot trsfP_2 = trsf_2 \cdot trsf_3 \cdot trsf_4 \cdot trsf_5 \cdot trsf_6$$

两边矩阵元素 (3,4) 相等得到 : $c1p_v - s1p_v$

三角恒等变换:

$$\Rightarrow p_{\nu} = A \sin \phi$$

$$\Leftrightarrow p_x = A\cos\phi$$

$$A = \sqrt{p_x^2 + p_y^2}$$

$$\phi = a \tan 2(p_v, p_x)$$

$$As\phi c1 - Ac\phi s1 = d3$$

$$s(\phi - \theta_1) = \frac{d^3}{4}$$

$$c(\phi - \theta_1) = \pm \sqrt{1 - \left(\frac{d^3}{A}\right)^2}$$

$$\phi - \theta_1 = a \tan 2(\frac{d3}{A}, \pm \sqrt{1 - \left(\frac{d3}{A}\right)^2})$$

$$\theta_1 = a \tan 2(p_y, p_x) - a \tan 2(\frac{d3}{A}, \pm \sqrt{1 - \left(\frac{d3}{A}\right)^2})$$

 $\mathbf{H}\,\theta_2\ :\ \mathit{trsf}_2^{-1}\cdot\mathit{trsf}_1^{-1}\cdot\mathit{trsf}P_2=\mathit{trsf}_3\cdot\mathit{trsf}_4\cdot\mathit{trsf}_5\cdot\mathit{trsf}_6$

$$trsf_{2}^{-1} \cdot trsf_{1}^{-1} \cdot trsfP_{2} = \begin{bmatrix} \dots & \dots & \dots & p_{z}c2 + p_{x}c1s2 + p_{y}s1c2 - a1s2 - a2 \\ \dots & \dots & \dots & -p_{z}s2 + p_{x}c1c2 + p_{y}s1c2 - a1c2 \\ \dots & \dots & \dots & \dots \\ \dots & \dots & \dots & \dots \end{bmatrix}$$

$$trsf_3 \cdot trsf_4 \cdot trsf_5 \cdot trsf_6 = \begin{bmatrix} \dots & \dots & \dots & c3 \cdot d4 \\ \dots & \dots & \dots & s3 \cdot d4 \\ \dots & \dots & \dots & \dots \\ \dots & \dots & \dots & \dots \end{bmatrix}$$

两边矩阵元素(1,4)和(2,4)分别相等

(1)
$$\rightarrow \int p_z c^2 + p_x c ls^2 + p_y s ls^2 - a ls^2 - a^2 = c^3 d^4$$

(2) $\rightarrow \int -p_z s^2 + p_x c lc^2 + p_y s lc^2 - a lc^2 = s^3 d^4$

$$(2) \rightarrow \int -p_{z}s^{2} + p_{y}c^{2}c^{2} + p_{y}s^{2}c^{2} - a^{2}c^{2} = s^{3}d^{4}$$

$$(1) \cdot s2 \to \int p_z s2c2 + p_x c1(s2)^2 + p_y s1(s2)^2 - a1(s2)^2 - a2s2 = s2c3d4$$

$$(2) \cdot c2 \to \begin{cases} -p_z s2c2 + p_x c1(c2)^2 + p_y s1(c2)^2 - a1(c2)^2 = c2s3d4 \\ (1) \cdot s2 + (2) \cdot c2 \end{cases}$$

$$p_x c1 + p_y s1 - a_1 = d4s23 + a2s2$$

$$\Leftrightarrow B = p_{x}c1 + p_{y}s1 - a_{1}$$

所以
$$B = d4s23 + a2s2$$

$$s23 = \frac{B - a2s2}{d4}$$

$$(1) \cdot c2 \to \int p_z (c2)^2 + p_x c_1 c_2 s_2 + p_y s_1 c_2 s_2 - a_1 c_2 s_2 - a_2 c_2 = c_2 c_3 d_4$$

$$(2) \cdot s2 \to \begin{cases} -p_z (s2)^2 + p_x c_1 c_2 s_2 + p_y s_1 c_2 s_2 - a_1 c_2 s_2 = s_2 s_3 d_4 \\ (1) \cdot c_2 - (2) \cdot s_2 \end{cases}$$

$$p_z - a_2 c_2 = d_4 c_2 s_3$$

$$c23 = \frac{p_z - a2c2}{d4}$$

$$(s23)^{2} + (c23)^{2} = 1$$

$$(\frac{B - a2s2}{d4})^{2} + (\frac{P_{z} - a2c2}{d4})^{2} = 1$$

$$B^{2} + 2B(a2)(s2) + (a2)^{2}(s2)^{2} + p_{z}^{2} - 2p_{z}a2c2 + (a2)^{2}(c2)^{2} = (d4)^{2}$$

$$B(s2) + p_{z}(c2) = \frac{B^{2} + p_{z}^{2} + (a2)^{2} - (d4)^{2}}{2(a2)}$$

三角恒等变换:

$$B = C\sin\phi$$

$$p_z = C\cos\phi$$

$$C = \sqrt{B^2 + p_z^2}$$

$$\phi = a\tan 2(B, p_z)$$

$$Cs\phi s2 + Cc\phi c2 = \frac{B^2 + p_z^2 + (a2)^2 - (d4)^2}{2(a2)}$$

$$c(\phi - \theta_2) = \frac{B^2 + p_z^2 + (a2)^2 - (d4)^2}{2(a2)C} = D$$

$$s(\phi - \theta_2) = \pm\sqrt{1 - D^2}$$

$$\phi - \theta_2 = a\tan 2(\pm\sqrt{1 - D^2}, D)$$

$$\theta_2 = a\tan 2(B, p_z) - a\tan 2(\pm\sqrt{1 - D^2}, D)$$

$$解\theta$$
;:

$$\theta_2 + \theta_3 = a \tan 2(s23, c23)$$

$$\theta_3 = a \tan 2(s23, c23) - \theta_2$$

$$\theta_3 = a \tan 2(\frac{B - a2s2}{d4}, \frac{p_z - a2c2}{d4}) - \theta_2$$

 $\mathbf{H}\theta_5$: $trsf_3^{-1} \cdot trsf_2^{-1} \cdot trsf_1^{-1} \cdot trsfP_2 = trsf_4 \cdot trsf_5 \cdot trsf_6$

$$trsf_{3}^{-1} \cdot trsf_{2}^{-1} \cdot trsf_{1}^{-1} \cdot trsfP_{2} = \begin{bmatrix} ... & ..$$

$$trsf_{4} \cdot trsf_{5} \cdot trsf_{6} = \begin{bmatrix} ... & ... & s5 \cdot c4 & ... \\ ... & ... & s5 \cdot s4 & ... \\ -s5 \cdot c6 & s5 \cdot s6 & c5 & ... \\ ... & ... & ... & ... \end{bmatrix}$$

$$\Leftrightarrow E = -r33 \cdot s23 + r13 \cdot c1 \cdot c23 + r23 \cdot s1 \cdot c23$$

$$\diamondsuit F = r23 \cdot c1 - r13 \cdot s1$$

$$G = r11 \cdot c1 \cdot s23 + r31 \cdot c23 + r21 \cdot s1 \cdot s23$$

$$\Rightarrow H = r12 \cdot c1 \cdot s23 + r32 \cdot c23 + r22 \cdot s1 \cdot s23$$

$$c5 = I$$

$$s5 = \pm \sqrt{1 - I^2}$$

$$\theta_5 = a \tan 2(s5, c5)$$

$$\theta_5 = a \tan 2(\pm \sqrt{1 - I^2}, I)$$

解 θ_4 :

$$\begin{cases} s5 \cdot c4 = E \\ s5 \cdot s4 = F \end{cases}$$

$$s4 = \frac{F}{s5}$$

$$c4 = \frac{E}{s5}$$

$$\theta_4 = a \tan 2(s4, c4)$$

$$\theta_4 = a \tan 2(\frac{F}{s5}, \frac{E}{s5})$$

解
$$\theta_6$$
:

$$\begin{cases} s5 \cdot s6 = H \\ -s5 \cdot c6 = G \end{cases}$$

$$s6 = \frac{H}{s5}$$

$$c6 = -\frac{G}{s5}$$

$$\theta_6 = a \tan 2(s6, c6)$$

$$\theta_6 = a \tan 2(\frac{H}{s5}, \frac{G}{s5})$$

心得:

一个工具坐标系{x,y,z,rx,ry,rz},理论上有8种手臂的姿态可以到达,还需要肩部、肘部、腕部来定义。Shoulder(Lefty、Righty) Elbow(Positive、Negative) Wrist(Positive、Negative)。

问题:

在算逆解的时候,8 种手臂形态对应的关节值已经求出且验证,但存在一些问题。 比如 4 轴运动范围为-270°—270°,逆解的时候 matlab 算出的关节值是 120°, Val3 算出 的是-240°。虽然手臂形态是一样的。