

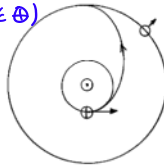
K1

Passage through "Local" Gravity Fields

To examine interplanetary transfers completely, it would be necessary to consider all gravitational influences at all times. However, that is an inconvenient approach and can be solved only numerically. But, it is possible to obtain a pretty good approximation to the $\Delta \vec{v}$ requirements by considering the transfer in three phases, each of which involves only a two-body problem, for which there are a large number of analysis techniques.

For an example, consider that you are planning an Earth-to-Mars mission. Assume that the planets are in circular orbits about the Sun and move in the same plane. To determine the $\Delta \vec{v}$, examine the mission as 3 two-body problems:

- I. Short time near departure planet ($\% \oplus$)
- II. Long time under solar influence ($\% \odot$)
- III. Short time near arrival planet ($\% \Mars$)



Denoted the "patched conic" approach.

Approximate but yields a good guess of the requirements. Consider each phase separately.

Two-Body Problem #1 (near \oplus)

Assume that the vehicle is originally in a circular "parking" orbit around the Earth. Motion is influenced solely by the \oplus , totally neglecting the Sun since, at that close range, the Earth is certainly dominant. The vehicle will transfer "instantaneously" from the influence of the \oplus to the influence of the \odot . To escape the \oplus , the spacecraft must be on a parabolic or hyperbolic orbit with respect

Observations:

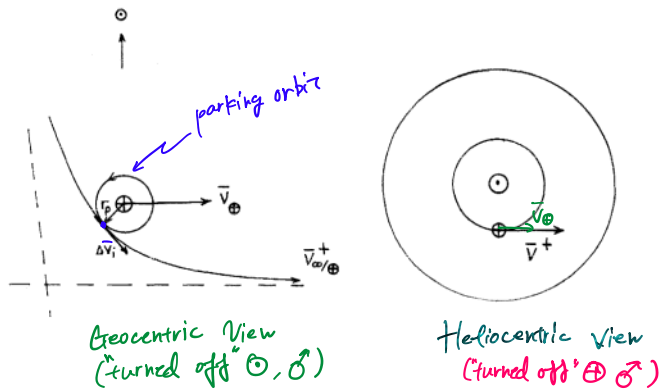
(1) $\Delta \vec{v} = \vec{v}_2 - \vec{v}_1 \rightarrow$ vector eqn

(2) E eccentric anomaly
how is it measured?

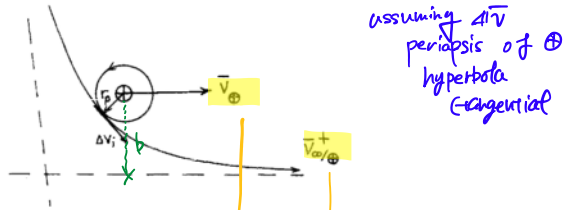
(3) Diagrams larger

(4) \hat{b} unit vector ck how defined?!

to the Earth. Once "escaped", the vehicle must be moving on the correct transfer orbit about the \odot to enable arrival at σ . Consider two views of the situation.



- Circular parking at \oplus (could be any orbit actually)
- No effect of \odot
- Transfer "instantaneously" from influence of \oplus to influence of \odot
- To escape \oplus , must depart on parabola or hyperbola
- Once escaped, possess exactly correct velocity for transfer orbit about \odot
- For trip to σ , s/c velocity wrt \odot must be $>$ velocity of Earth wrt \odot (gain energy) \longrightarrow



Geocentric: maneuver $\Delta \vec{v}_i$ (tangential) so spacecraft jumps from circular \oplus orbit to hyperbolic orbit to escape \oplus . After escape, velocity is $\vec{v}_{\infty/\oplus}^+$. Note that this is a **vector** quantity. To determine s/c velocity with respect to \odot , relate vectors

$$\vec{v}^+ = \vec{v}_{\infty/\oplus}^+ + \vec{v}_{\oplus}$$

heliocentric velocity of \oplus wrt \odot

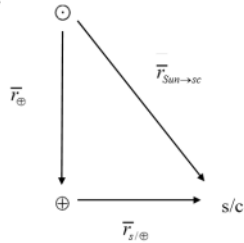
heliocentric velocity of s/c on ellipse wrt

excess velocity at \oplus escape

v_{∞} velocity along the hyperbola

← relative "shift"

NOTE:



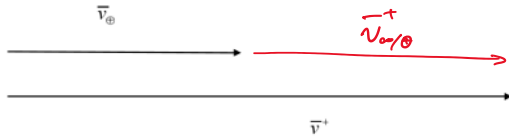
$$\begin{aligned} \vec{r}_s &= \vec{r}_{s/\oplus} + \vec{r}_{\oplus} \\ \vec{v}_s &= \vec{v}_{s/\oplus} + \vec{v}_{\oplus} \\ &\quad \underbrace{\frac{d\vec{r}_{s/\oplus}}{dt}} \\ \vec{v}^+ &= \vec{v}_{\infty/\oplus}^+ + \vec{v}_{\oplus} \end{aligned}$$

VECTOR Equation

a tangential
departure
for Hohmann transfer

requires vector diagram

$$\vec{v}^+ = \vec{v}_{\oplus} + \underbrace{\vec{v}_{\infty/\oplus}^+}_{\text{required change in velocity}}$$



Assuming knowledge of the required \vec{v}^+ to transfer to $\vec{\sigma}$, solve for the $\vec{v}_{\infty/\oplus}^+$ vector required to escape

Use excess velocity to compute the exact vector $\Delta \vec{v}_i$ to jump from the parking orbit to the required hyperbola.



Jump at hyperbolic perigee most effective

At perigee, velocity on hyperbola: $v_c + \Delta v_i$

required change
in velocitycircular velocity
in PO (parking orbit)energy \mathcal{E} on
hyperbolic
orbit

$$\mathcal{E} = \frac{v_{\infty}^2}{2} = \frac{(v_c + \Delta v_i)^2}{2} - \frac{\mu_{\oplus}}{r_p}$$

tangential
maneuver

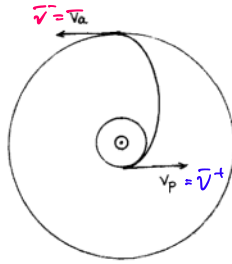
$$\Delta v_i = \sqrt{v_{\infty}^2 + \frac{2\mu_{\oplus}}{r_p}} - v_c$$

magnitude of Δv_i to
depart \oplus orbit

Δv_i : initial burn required to place s/c on heliocentric ellipse with correct \vec{v}^+

Two-Body Problem #2 (influence of \odot)

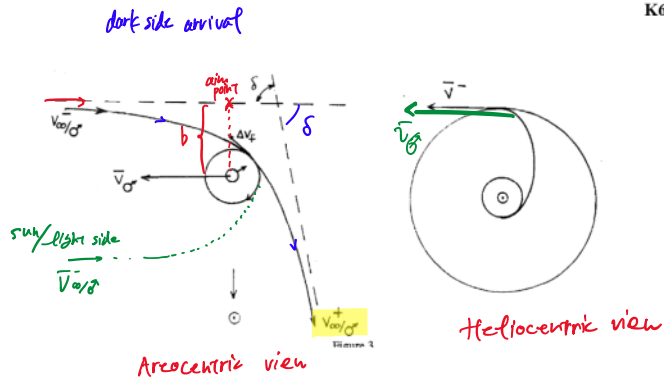
- assume: leaving and approaching massless planets
- $v^+ = v_p$ i.e., perihelion on Hohmann transfer ellipse
- easily compute velocity wrt \odot at σ arrival, i.e., the apohelion velocity on Hohmann transfer ellipse
- $v_a = v^-$ i.e., heliocentric velocity for σ approach



Note: departure from \oplus phased correctly s.t. Mars is in proper position when s/c rendezvous

Two-Body Problem #3 (near σ)

- Assume that the goal is capture into a circular orbit about σ at a given radius r_f ; also consider the circular orbit must be defined in a particular direction
- Since s/c at apohelion on transfer ellipse, s/c will be moving
- s/c will enter Martian vicinity on hyperbola and – at appropriate time – add Δv_f to slow s/c for capture
- final velocity



Use heliocentric velocity to determine the velocity on the hyperbola:

Vector Diagram *Arrival*

$$\vec{v}_{\infty/\phi} = \vec{v}^- - \vec{v}_{\phi}$$

$$\vec{v}^- = \vec{v}_{\phi} + \vec{v}_{\infty/\phi}$$

CAPTURE

Solve the vector equation for $\vec{v}_{\infty/\phi}$ and determine Δv_f $\vec{v}_c = \vec{v}_{pl} - A$

$$\frac{V_{\infty/\phi}^2}{2} = \frac{(V_c + \Delta v_f)^2}{2} - \frac{\mu_g}{r_f}$$

Total: $\Delta v_{total} = \Delta v_i + \Delta v_f$

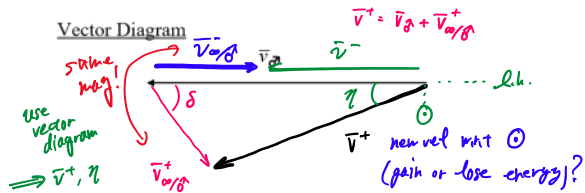
SWINGBY

Rather than capture into σ orbit, assume pass by of planet at a closest approach of r_f

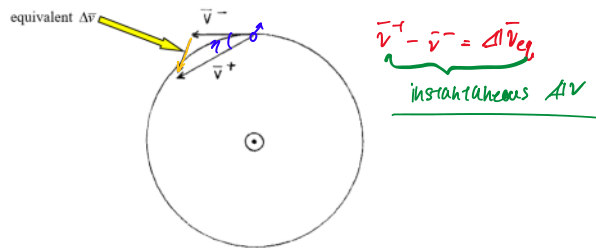
→ same approach hyperbola, but continues past planet on outbound leg of hyperbola

Below: passes on the "dark" side i.e., "behind" Mars

Use vector relationships to determine impact of passage on spacecraft heliocentric velocity



passage through the local gravity field of Mars instantaneously changes the **magnitude** and **direction** of the spacecraft heliocentric velocity



Consider the following:

Does the spacecraft gain or lose energy via the Mars passage?

“light” side of the planet?

How can the departure from Earth be timed such that Mars is in the assigned position at the proper time?

$$\left. \begin{aligned} \zeta^- &= \frac{v_-^2}{2} - \frac{\mu_0}{r^-} \\ \zeta^+ &= \frac{v_+^2}{2} - \frac{\mu_0}{r^+} \end{aligned} \right\} r^- = r^+ \text{ in heliocentric view}$$

Example:

$$v_{\oplus} = 24.13 \text{ km/s}$$



$$\mathcal{E} = \frac{v_{\infty}^2}{2} - \frac{\mu_{\odot}}{r_{\odot}} = -\frac{\mu}{2a} \Rightarrow v_a = 21.48 \text{ km/s}$$

Hohmann
on
apoptosis

$$v_{\infty/\sigma} = 2.65 \text{ km/s}$$

$$r_f = R_{\oplus} + 1500 \text{ km} \quad (4.91 \times 10^3 \text{ km})$$

$$\delta = 67.36^\circ$$



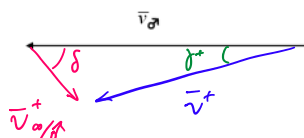
$$\mathcal{E} = \frac{v_{\infty}^2}{2} = \frac{\mu_{\oplus}}{2|a|} \Rightarrow |a| = 6.1132 \times 10^3 \text{ km}$$

$$e = \frac{r_p}{|a|} + 1$$

$$\sin \frac{\delta}{2} = \frac{1}{e}$$

r_p on hyperbola

hyperbota



l.h.

cosine law

$$v^+ = 23.2 \text{ km/s}$$

$\theta^* = -1.05^\circ \rightarrow$ below l.h.

$\vec{v}^+ \cos \gamma$
 \vec{v}^+
 \odot
 $v^+ = 23.2 \text{ km/s}$
 $\gamma^+ = -1.65^\circ \rightarrow \text{below d.h.}$
 $\sin \text{ law}$

K10

Alternatively:

$$r_f = R_{\oplus} + 200 \text{ km} \quad (3.61 \times 10^3 \text{ km})$$

$$\left. \begin{aligned} \delta &= 77.9^\circ \\ v^+ &= 23.7 \text{ km/s} \\ \gamma^+ &= -6.3^\circ \end{aligned} \right\} \text{ gain energy}$$

- Of course, a sunside passage will yield same v^+ but now γ^+ positive \rightarrow changes orbit relative to Sun
But $v^+ > v^- \rightarrow$ gain energy (from Δv)
- Project Galileo: at one time, plans included a flyby of \odot on way to Jupiter
Hohmann to \odot — 8.5 months
actual ToF ~ 3 months
pass distance r_p on hyp $\sim 275 \text{ km}$ altitude
- Patched-conic method for calculating trajectories (or Δv estimates) yields pretty accurate thrust requirements (surprisingly) \rightarrow pretty accurate nominal trajectories [some error in transfer time because only time along actual Hohmann is incorporated]
- Greatest difficulty in practice is implementation \leftarrow hyperbola
Hyperbolic excess speed, v_∞ , is extremely sensitive to small errors in injection velocity

Example: \oplus departure

$\vec{v}_c + \Delta \vec{v} = \vec{v}_p$ \leftarrow Velocity required at periapsis of hyperbola
 \uparrow
 added thrust

from energy \mathcal{E} : *energy on hyperbola for \oplus departure* **K11**
 $v_x^2 = v_p^2 - \frac{2\mu}{r_p}$ first-order difference eqn for small errors in v_p

$$2 v_\infty \delta v_\infty = 2 v_p \delta v_p$$

$$\frac{\delta v_\infty}{v_\infty} = \left(\frac{v_p}{v_\infty}\right)^2 \frac{\delta v_p}{v_p}$$

Hohmann to Mars \rightarrow $v_p \cong 11.5 \text{ km/s}$ $v_\infty = 3 \text{ km/s}$

1% error in v_p

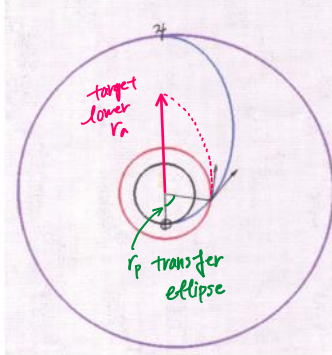
\Rightarrow 15% error in v_∞

assume perfect implementation

Example: Swingby when Arrival not Tangential

Assume Hohmann transfer to Jupiter and intercept Mars
How will Mars swingby affect orbit?

Assume Mars and Jupiter orbits are circular and coplanar



→ smaller r_a
 ΔV lower
 than necessary
 at \oplus
 ↓
 more
 efficient with
 fly-by
 ↓
 complications:
 - shift in line-of-apsides
 - 2 phase angle
 - navigations
 - untangential arrival

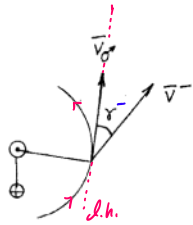
Determine conditions as Mars arrival

$$a = \frac{1}{2}(r_{\oplus} + r_{Jup}) = 3.1 \text{ AU}$$

$$r_{\oplus} = r_p = a(1-e) \Rightarrow e = .677 \quad (p = 1.68 \text{ AU})$$

radius $r_{\theta} = \frac{a(1-e^2)}{1+e \cos \theta} \Rightarrow \theta^* = 81.3^\circ$

Assume: Mars is in circular orbit : v_g circular vel along l.h.



$$\bar{v}_g = 24.187 \text{ km/s}$$

$$\frac{(v^-)^2}{2} - \frac{\mu_{\odot}}{r_g} = -\frac{\mu_{\odot}}{2a_t} \quad \text{for transfer path}$$

$$\rightarrow v^- = 29.7 \text{ km/s}$$

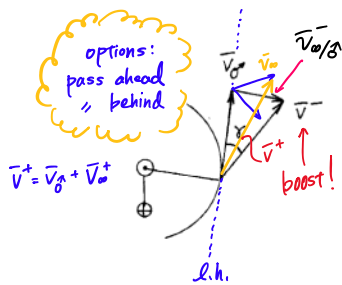
variety of ways to determine δ^-

$$\frac{v_p^2}{2} - \frac{\mu_{\odot}}{r_p} = -\frac{\mu_{\odot}}{2a} \rightarrow v_p = 38.66 \text{ km/s}$$

$$\delta = \pm 31.3^\circ$$

$$h = \sqrt{\mu_{\odot} p} = r_g v^- \cos \gamma \rightarrow \gamma = 31.3^\circ \quad (\text{why } +?)$$

ascending on transfer orbit
 $0^\circ < \delta^* < 180^\circ$



known known

$$\bar{v}^- = \bar{v}_g + \bar{v}_{x/g}$$

$$\bar{v}_{x/g} = \bar{v}^- - \bar{v}_g$$

Solve for $v_{x/g}$ from cosine law

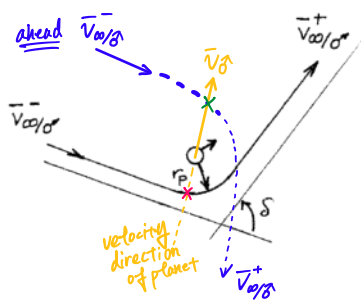
$$v_{x/g}^2 = v_g^2 + (v^-)^2 - 2v_g v^- \cos \gamma$$

$$\bar{v}_{x/g} = 15.476 \text{ km/s}$$

That is fast!

get a "boost" to outer solar system
by Mars encounter
which way to pass to increase or decrease energy?

Mars is moving
away in
this instance



“leading” or “trailing”

“ahead” or “behind”

GAIN energy?

Pass behind

$$r_f = R_{\oplus} + 300 \text{ km}$$

altitude

$$r_{\text{pass}} = r_p \text{ of hyp.}$$

choose a close pass of \vec{O}

Hyperbolic orbit wrt ♂

$$\rightarrow |\bar{v}_{\alpha/\delta}| = |\bar{v}_{\alpha/\delta}^+|$$

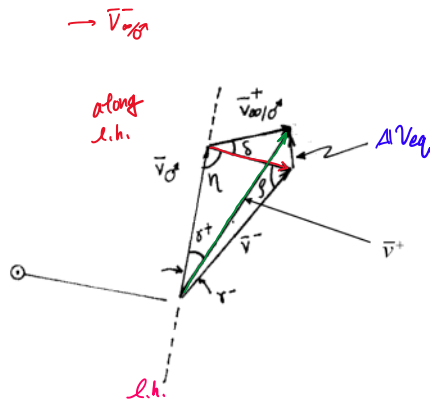
known

$$\mathcal{E} = \frac{v_{\infty}^2}{2} = \frac{\mu_{\odot}}{2|a|} \longrightarrow |a| = 179.536 \text{ km}$$

$$e = \frac{r_p}{|a|} + 1 = 21.55$$

$$\sin \frac{\delta}{2} = \frac{1}{e} \longrightarrow \delta = 5.3^\circ \text{ passing a small planet very fast}$$

↑
what impact



$$\frac{v^-}{\sin \eta} = \frac{v_{x/\sigma}}{\sin \gamma^-} \quad \eta = 85.57^\circ \text{ or } 94.43^\circ \text{ how to check?}$$

$$\frac{v_{\sigma}}{\sin \zeta_p} = \frac{v_{x/\sigma}}{\sin \gamma^-} \quad \zeta_p = 54.3^\circ \text{ or } 125.7^\circ$$

$$(v^-)^2 = \left(v_{x/\sigma} \right)^2 + v_{\sigma}^2 - 2v_{x/\sigma}v_{\sigma}\cos \eta \rightarrow \cos \eta \text{ negative}$$

Need to add to this term

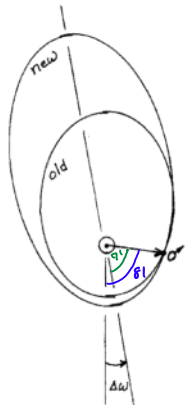
$$(v^+)^2 = v_{\sigma}^2 + \left(v_{x/\sigma} \right)^2 - 2v_{\sigma}v_{x/\sigma}\cos(\eta + \delta) \quad \boxed{v^- = 29.7 \text{ km/s}} \quad \boxed{v^+ = 30.84 \text{ km/s}}$$

Increased velocity \rightarrow higher energy orbit (pass ahead, drop vel?)

$$\frac{v_{x/\sigma}}{\sin \gamma^+} = \frac{v^+}{\sin(\eta + \delta)} \rightarrow \boxed{\gamma^+ = 29.63^\circ}$$

change $v \sim 1 \text{ km/s}$

$$\tan \theta^* = \frac{\left(\frac{rv^2}{\mu}\right) \sin \gamma \cos \gamma}{\left(\frac{rv^2}{\mu}\right) \cos^2 \gamma - 1} \rightarrow \theta^* = \theta^{*-} = 81.3^\circ \text{ or } 252^\circ \quad (\gamma > 0)$$



$\Delta \omega = 9.4^\circ$
perihelion advances

	before encounter	after encounter
r	1.52 AU	1.52 AU
v	29.7 km/s	30.84 km/s
γ	31.3°	29.63°
e	.677	.7348
θ^*	81.3°	71.9°
a	3.07 AU	4.02 AU
r_p	1 AU	1.066 AU
r_a	5.2 AU	6.97 AU ☆☆