

P2: J

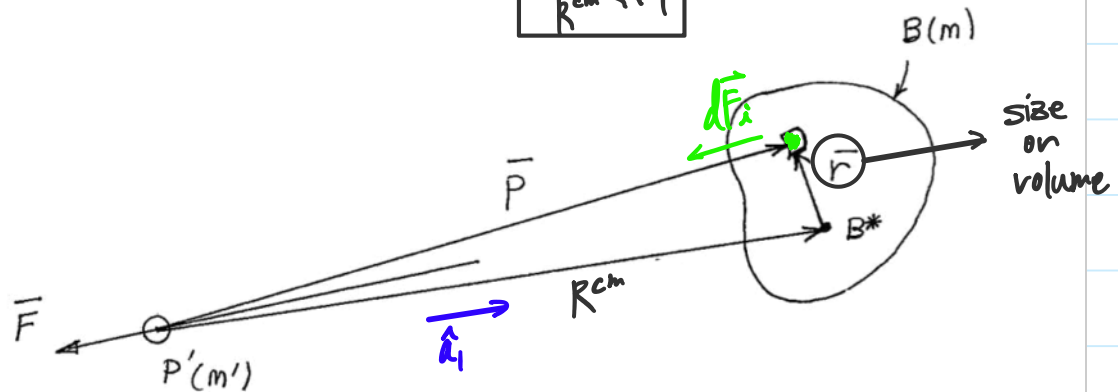
2020年2月21日 金曜日 午後1:11

Gravity Expansion

reasonable assumption

$$\frac{r}{R_{cm}} \ll 1$$

if true \rightarrow can approx



For $|\vec{r}| \ll |\vec{R}|$ useful form for general expression for \vec{F}

$$\vec{F} = -Gm' \int \vec{p} (\vec{p} \cdot \vec{p})^{-\frac{3}{2}} \nu d\tau \quad \text{exact gravity force}$$

$$\vec{p} = \vec{R} + \vec{r}$$

$$\vec{F} = -Gm' \int (\vec{R} + \vec{r}) \left[(\vec{R} + \vec{r}) \cdot (\vec{R} + \vec{r}) \right]^{-\frac{3}{2}} \nu d\tau$$

$$(\vec{R}^2 + 2\vec{R} \cdot \vec{r} + r^2)^{-\frac{3}{2}}$$

$$\vec{F} = -Gm' \int \vec{R} \left(\frac{\vec{R}}{R} + \frac{\vec{r}}{R} \right) \frac{1}{R^3} \left(\frac{R^2}{R^2} + \frac{2\vec{R} \cdot \vec{r}}{R^2} + \frac{r^2}{R^2} \right)^{-\frac{3}{2}} \nu d\tau$$

Define $\frac{\vec{R}}{R} = \hat{a}_1$ $\frac{\vec{r}}{R} = \vec{q}$ (small magnitude)

$$\bar{F} = -\frac{Gm'}{R^2} \int (\hat{a}_1 + \bar{q}) \underbrace{\left(1 + 2\hat{a}_1 \bullet \bar{q} + q^2\right)^{-\frac{3}{2}}}_{\text{use binomial expansion}} v d\tau$$

R not necessarily constant but not involved in integration

use binomial expansion

$$(1+x)^m = 1 + mx + \frac{m(m-1)}{2!}x^2 + \frac{m(m-1)(m-2)}{3!}x^3 + \dots$$

✓ brackets

$$\bar{F} = -\frac{Gm'}{R^2} \int (\hat{a}_1 + \bar{q}) \left[1 - \frac{3}{2}(2\hat{a}_1 \bullet \bar{q} + q^2) + q^2 + \frac{15}{8}((4\hat{a}_1 \bullet \bar{q})^2 + 4\hat{a}_1 \bullet \bar{q} q^2 + q^4) + \dots \right] v d\tau$$

Neglect terms of order q^3 and higher \longrightarrow keep terms to second order!

$$\bar{F} = -\frac{Gm'}{R^2} \int \left\{ \hat{a}_1 \left[1 - \frac{3}{2}(2\hat{a}_1 \bullet \bar{q} + q^2) + \frac{15}{2}(\hat{a}_1 \bullet \bar{q})^2 + \dots \right] + \bar{q} \left[1 - 3\hat{a}_1 \bullet \bar{q} + \dots \right] \right\} v d\tau$$

Observe:

Term (1) $\int \bar{q} v d\tau \Rightarrow \text{zero}$

def. of CM from basepoint

$$\bar{q} = \frac{\bar{r}}{R} \Rightarrow \frac{1}{R} \int \bar{r} v d\tau = \text{zero}$$

from CM

$$\hat{a}_1 = \frac{\bar{r}}{R}$$

Term ② $\int \hat{a}_1 \hat{a}_1 \cdot \bar{q} \, v \, d\tau$

\hat{a}_1 not involved in integration

$$\hat{a}_1 \cdot \hat{a}_1 \cdot \int \bar{q} \, v \, d\tau = 0$$

Term ③ $\int \hat{a}_1 \, v \, d\tau$

\hat{a}_1 not involved in integrate

$$\hat{a}_1 \int v \, d\tau = \hat{a}_1 \int dm = M \hat{a}_1$$

total mass



Substitute back $\bar{q} = \frac{\bar{r}}{R}$

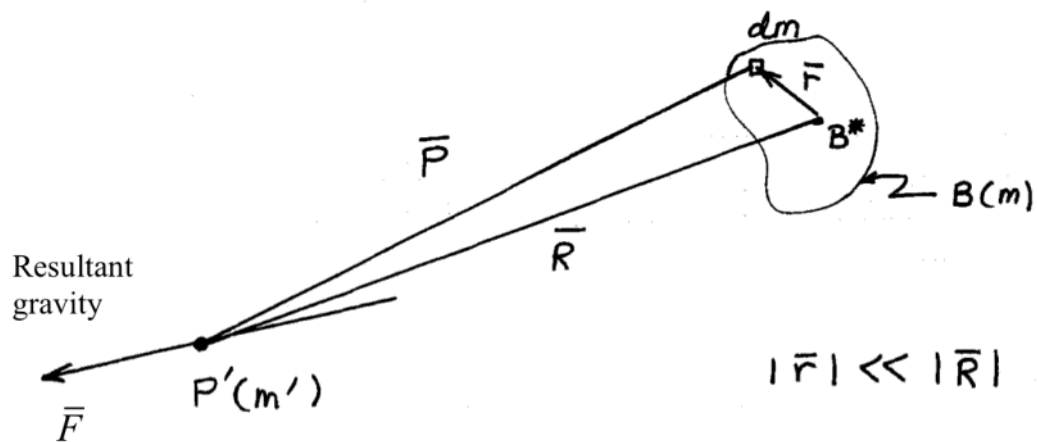
$$\bar{F} = -\frac{G m' \textcircled{m}}{R^2} \hat{a}_1 + \frac{3}{2} \frac{G m'}{R^2} \left[\hat{a}_1 \int \left(\frac{r}{R} \right)^2 v d\tau - 5 \hat{a}_1 \int \underbrace{\left(\hat{a}_1 \cdot \frac{\bar{r}}{R} \right)^2}_{\text{inertia moment}} v d\tau + 2 \int \frac{\bar{r}}{R} \hat{a}_1 \cdot \frac{\bar{r}}{R} v d\tau \right] + \dots$$

Note: $\left(\hat{a}_1 \cdot \frac{\bar{r}}{R} \right)^2 = \left(\hat{a}_1 \cdot \frac{\bar{r}}{R} \right) \left(\hat{a}_1 \cdot \frac{\bar{r}}{R} \right) = \frac{\hat{a}_1 \cdot \bar{r} \bar{r} \cdot \hat{a}_1}{R^2}$

inertia moment is an important piece of gravity force

$$\bar{F} = -\frac{G m' m}{R^2} \hat{a}_1 + \frac{3}{2} \frac{G m'}{R^4} \left[\hat{a}_1 \int \textcircled{r^2} v d\tau - 5 \hat{a}_1 \hat{a}_1 \cdot \int \textcircled{\bar{r} \bar{r}} v d\tau \cdot \hat{a}_1 + 2 \int \textcircled{\bar{r} \bar{r}} v d\tau \cdot \hat{a}_1 \right] + \dots$$

related to inertia integrals



$$\vec{F} = -\frac{Gm'm}{R^2} \hat{a}_1 + \frac{3}{2} \frac{Gm'}{R^4} \left[\hat{a}_1 \int r^2 \nu d\tau - 5 \hat{a}_1 \hat{a}_1 \cdot \int \vec{r} \vec{r} \nu d\tau \cdot \hat{a}_1 + 2 \int \vec{r} \vec{r} \nu d\tau \cdot \hat{a}_1 \right] + \dots$$

Can relate integrals to inertia properties of B

$$\bar{I}_{B^*}^{ij} = \int \nu (\hat{u}_i \hat{r}^2 - \vec{r} \vec{r}) d\tau$$

\uparrow
 $\hat{u}_1 \hat{h}_1 + \hat{u}_2 \hat{h}_2 + \hat{u}_3 \hat{h}_3$

Observations:

1. Note: $tr(\bar{\bar{I}}) = I_{11} + I_{22} + I_{33}$

For any vector basis \hat{n}_i

$$tr(\bar{\bar{I}}) = \hat{n}_1 \bullet \bar{\bar{I}} \bullet \hat{n}_1 + \hat{n}_2 \bullet \bar{\bar{I}} \bullet \hat{n}_2 + \hat{n}_3 \bullet \bar{\bar{I}} \bullet \hat{n}_3$$

$$\begin{aligned} tr(\bar{\bar{I}}) &= \hat{n}_1 \bullet \int \nu (\bar{\bar{U}} r^2 - \bar{r} \bar{r}) d\tau \bullet \hat{n}_1 \\ &\quad + \hat{n}_2 \bullet \int \nu (\bar{\bar{U}} r^2 - \bar{r} \bar{r}) d\tau \bullet \hat{n}_2 \\ &\quad + \hat{n}_3 \bullet \int \nu (\bar{\bar{U}} r^2 - \bar{r} \bar{r}) d\tau \bullet \hat{n}_3 \end{aligned}$$

$$\begin{aligned} tr(\bar{\bar{I}}) &= \int \left[\hat{n}_1 \bullet \bar{\bar{U}} r^2 \bullet \hat{n}_1 + \hat{n}_2 \bullet \bar{\bar{U}} r^2 \bullet \hat{n}_2 + \hat{n}_3 \bullet \bar{\bar{U}} r^2 \bullet \hat{n}_3 \right. \\ &\quad \left. - (\hat{n}_1 \bullet \bar{r} \bar{r} \bullet \hat{n}_1 + \hat{n}_2 \bullet \bar{r} \bar{r} \bullet \hat{n}_2 + \hat{n}_3 \bullet \bar{r} \bar{r} \bullet \hat{n}_3) \right] \nu d\tau \end{aligned}$$

↖ $\hat{n}_1 \hat{n}_1 + \hat{n}_2 \hat{n}_2 + \hat{n}_3 \hat{n}_3$

But $\hat{n}_i \bullet \bar{\bar{U}} r^2 \bullet \hat{n}_i = 3r^2$

$$tr(\bar{\bar{I}}) = \int 3r^2 - (r_1^2 + r_2^2 + r_3^2) \nu d\tau$$

$$\Rightarrow \boxed{tr(\bar{\bar{I}}) = \int 2r^2 \nu d\tau}$$

$$\Rightarrow \boxed{\int r^2 \nu d\tau = \frac{tr(\bar{\bar{I}})}{2}}$$

$$2. \quad \bar{\bar{I}} = \int [\bar{\bar{U}} r^2 - \bar{r} \bar{r}] v d\tau$$

$$\bar{\bar{I}} = \bar{\bar{U}} \int r^2 v d\tau - \underbrace{\int \bar{r} \bar{r} v d\tau}_{\text{other integral in } \bar{F}}$$

OR

$$\int \bar{r} \bar{r} v d\tau = \bar{\bar{U}} \boxed{\int r^2 v d\tau} - \bar{\bar{I}}$$

$$\boxed{\int \bar{r} \bar{r} v d\tau = \frac{\bar{\bar{U}} + \bar{\bar{I}}}{2} - \bar{\bar{I}}}$$

Now return to gravity force!

$$\bar{F} = -\frac{Gm'm}{R^2}\hat{a}_1 + \frac{3}{2}\frac{Gm'}{R^4}\left[\hat{a}_1\int r^2 v d\tau - 5\hat{a}_1\hat{a}_1 \bullet \int \bar{r}\bar{r} v d\tau \bullet \hat{a}_1 + 2\int \bar{r}\bar{r} v d\tau \bullet \hat{a}_1\right] + \dots$$

Substitute for integrals

$$\bar{F} = -\frac{Gm'm}{R^2}\hat{a}_1 + \frac{3}{2}\frac{Gm'}{R^4}\left[\hat{a}_1\frac{tr(\bar{I})}{2} - 5\hat{a}_1\hat{a}_1 \bullet \left(\frac{\bar{U} tr(\bar{I})}{2} - \bar{I}\right) \bullet \hat{a}_1 + 2\left(\frac{\bar{U} tr(\bar{I})}{2} - \bar{I}\right) \bullet \hat{a}_1\right] + \dots$$

$$\bar{F} = -\frac{Gm'm}{R^2}\hat{a}_1 + \frac{3}{2}\frac{Gm'}{R^4}\left[\hat{a}_1\frac{tr(\bar{I})}{2} - 5\hat{a}_1 \bullet \left(\frac{tr(\bar{I})}{2}\right) + 5\hat{a}_1\hat{a}_1 \bullet \bar{I} \bullet \hat{a}_1 + \left(tr(\bar{I})\hat{a}_1 - 2\bar{I} \bullet \hat{a}_1\right)\right] + \dots$$

$$\bar{F} = -\frac{Gm'm}{R^2}\hat{a}_1 - \frac{3}{2}\frac{Gm'}{R^4}\left[tr(\bar{I}) - 5\hat{a}_1 \bullet \bar{I} \bullet \hat{a}_1\right]\hat{a}_1 - \frac{3}{2}\frac{Gm'}{R^4}\bar{I} \bullet \hat{a}_1 + \dots$$

can write in form

$$\bar{F} = -\frac{G m' m}{R^2} \left(\hat{a}_1 + \sum_{i=2}^{\infty} \bar{f}^{(i)} \right)$$

where $\bar{f}^{(i)}$ are a collection of terms of degree i in $\frac{r}{R}$

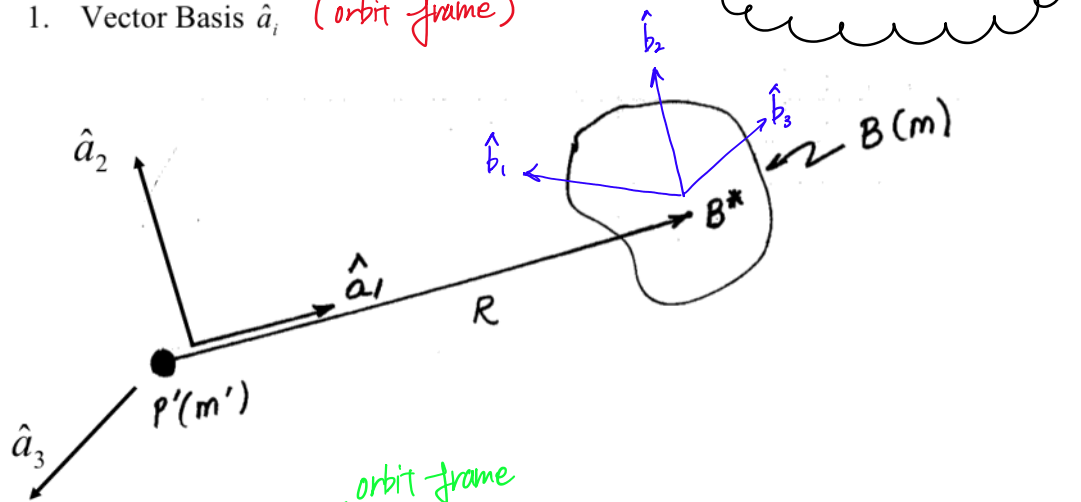
$$\bar{f}^{(2)} = \frac{1}{m R^2} \left\{ \frac{3}{2} \left[\text{tr}(\bar{I}) - 5 \hat{a}_1 \cdot \bar{I} \cdot \hat{a}_1 \right] \hat{a}_1 + 3 \bar{I} \cdot \hat{a}_1 \right\}$$

Useful approximations:

1. Particle term
2. 2nd order effects

To clarify the significance of $\bar{f}^{(2)}$, write it out in component format in different vector bases

1. Vector Basis \hat{a}_i (orbit frame)



Let $I_{ij} = \hat{a}_{\hat{i}} \cdot \bar{\bar{I}} \cdot \hat{a}_{\hat{j}} \quad (j, k = 1, 2, 3)$

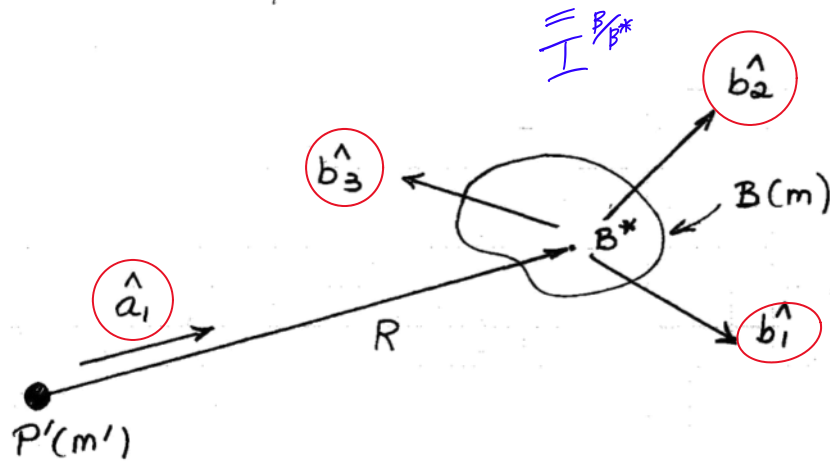
$$\bar{f}^{(2)} = \frac{1}{mR^2} \left\{ \frac{3}{2} \left[\text{tr}(\bar{\bar{I}}) - 5 \hat{a}_1 \cdot \bar{\bar{I}} \cdot \hat{a}_1 \right] \hat{a}_1 + 3 \bar{\bar{I}} \cdot \hat{a}_1 \right\}$$

$$\bar{f}^{(2)} = \frac{1}{mR^2} \left\{ \frac{3}{2} [I_{11} + I_{22} + I_{33} - 5I_{11}] \hat{a}_1 + 3(I_{11}\hat{a}_1 + I_{21}\hat{a}_2 + I_{31}\hat{a}_3) \right\}$$

$$\bar{f}^{(2)} = \frac{3}{mR^2} \left\{ \frac{1}{2} [I_{22} - I_{33} - 2I_{11}] \hat{a}_1 + I_{21} \hat{a}_2 + I_{31} \hat{a}_3 \right\}$$

- 1) \hat{a}_i (orbit frame) is used for evaluation
- 2) I are all time dep. \rightarrow rates of change for \dot{I} ?

2. Vector Basis \hat{b}_i Body-fixed



Let \hat{b}_i be parallel to central principal axes

$$I_j = \hat{b}_j \cdot \bar{\bar{I}}^{B/B^*} \cdot \hat{b}_j$$

→ introduce kinematic variables into dynamic model

$$C_{ij} = \hat{a}_i \cdot \hat{b}_j \quad \longrightarrow \quad {}^A C^B \begin{array}{c|ccc} & \hat{b}_1 & \hat{b}_2 & \hat{b}_3 \\ \hline \hat{a}_1 & C_{11} & C_{12} & C_{13} \\ \hat{a}_2 & C_{21} & C_{22} & C_{23} \\ \hat{a}_3 & C_{31} & C_{32} & C_{33} \end{array}$$

orientation must be incorporated in the gravity expression

→ changes gravity torque

$$\bar{f}^{(2)} = \frac{1}{mR^2} \left\{ \frac{3}{2} \left[\text{tr}(\bar{\bar{I}}) - 5 \hat{a}_1 \cdot \bar{\bar{I}} \cdot \hat{a}_1 \right] \hat{a}_1 + 3 \bar{\bar{I}} \cdot \hat{a}_1 \right\}$$

→ I_i are constant! b/c in \hat{b}_i

$\text{tr}(\bar{\mathbf{I}}) = I_1 + I_2 + I_3$ (invariance) always the same

$$\hat{a}_1 \bullet \bar{\mathbf{I}} \bullet \hat{a}_1 = \hat{a}_1 \bullet \left[\hat{b}_1 I_1 \hat{b}_1 + \hat{b}_2 I_2 \hat{b}_2 + \hat{b}_3 I_3 \hat{b}_3 \right] \bullet \hat{a}_1$$

$$= I_1 C_{11}^2 + I_2 C_{12}^2 + I_3 C_{13}^2$$

$$\bar{f}^{(2)} = \frac{1}{mR^2} \left\{ \frac{3}{2} \left[I_1 + I_2 + I_3 - 5(I_1 C_{11}^2 + I_2 C_{12}^2 + I_3 C_{13}^2) \right] \hat{a}_1 + \right.$$

$$\left. + 3(I_1 C_{11} \hat{b}_1 + I_2 C_{12} \hat{b}_2 + I_3 C_{13} \hat{b}_3) \right\}$$

$C_{11} \hat{a}_1 + C_{21} \hat{a}_2 + C_{31} \hat{a}_3$

$C_{12} \hat{a}_1 + C_{22} \hat{a}_2 + C_{32} \hat{a}_3$

$C_{13} \hat{a}_1 + C_{23} \hat{a}_2 + C_{33} \hat{a}_3$

$$\bar{f}^{(2)} = \frac{3}{mR^2} \left\{ \frac{1}{2} \left[I_1 (1 - 3C_{11}^2) + I_2 (1 - 3C_{12}^2) + I_3 (1 - 3C_{13}^2) \right] \hat{a}_1 + \right.$$

$$+ [I_1 C_{21} C_{11} + I_2 C_{22} C_{12} + I_3 C_{23} C_{13}] \hat{a}_2$$

$$\left. + [I_1 C_{31} C_{11} + I_2 C_{32} C_{12} + I_3 C_{33} C_{13}] \hat{a}_3 \right\}$$

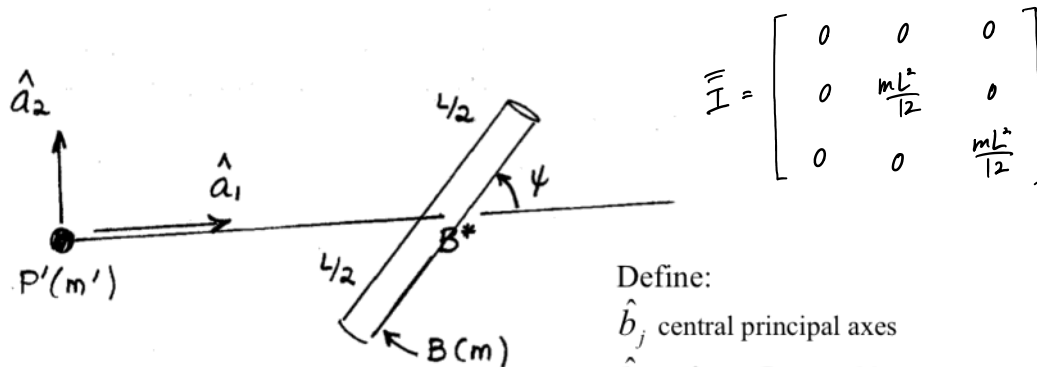
Note: I's here are CONSTANT

- 1) Inertia elements are in terms of \hat{b}_i
- 2) Inertia elements are constant

Example

body w/ same
inertia characteristic

Return to "rod" satellite but consider a more general orientation
(restricted to 2D)



$$\bar{I} = \begin{bmatrix} 0 & 0 & 0 \\ 0 & \frac{mL^2}{12} & 0 \\ 0 & 0 & \frac{mL^2}{12} \end{bmatrix}$$

Define:

\hat{b}_j central principal axes

$\hat{b}_j = \hat{a}_j \quad @ \psi = 0^\circ$

$$\bar{I}^{B/B^*} = \frac{mL^2}{12} (\hat{b}_2 \hat{b}_2 + \hat{b}_3 \hat{b}_3)$$

${}^A C^B$	\hat{b}_1	\hat{b}_2	\hat{b}_3
\hat{a}_1	c_ψ	$-s_\psi$	0
\hat{a}_2	s_ψ	c_ψ	0
\hat{a}_3	0	0	1

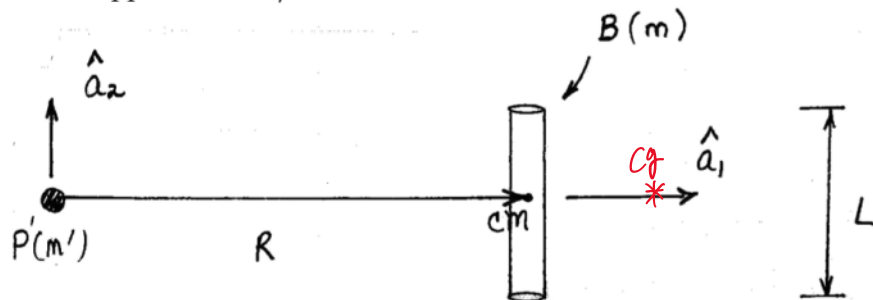
$$\begin{aligned} \bar{f}^{(2)} = \frac{3}{mR^2} \left\{ \frac{1}{2} \left[0 + \frac{mL^2}{12} (1 - 3s_\psi^2) + \frac{mL^2}{12} (1 - 0) \right] \hat{a}_1 \right. \\ \left. + \left[0 + \frac{mL^2}{12} c_\psi (-s_\psi) + 0 \right] \hat{a}_2 + 0 \hat{a}_3 \right\} \end{aligned}$$

$$\bar{F} = -\frac{Gm'm}{R^2} \left\{ \hat{a}_1 + \overbrace{\frac{L^2}{8R^2} (2 - 3s_\psi^2) \hat{a}_1 - \frac{L^2}{8R^2} s_{2\psi} \hat{a}_2}^{\bar{f}^{(2)}}$$

particle @
center of mass

add effect due to rod shape.
positive or negative depending
on attitude.

What happens when $\psi = 90^\circ$?



$\psi = 90^\circ$

$$\bar{F} = -\frac{Gm'm}{R^2} \left\{ \hat{a}_1 + \frac{L^2}{8R^2} (-1) \hat{a}_1 \right\}$$

$$\bar{F} = -\frac{Gm'm}{R^2} \left(1 - \frac{L^2}{8R^2} \right) \hat{a}_1$$

$cm \neq cg$: force is less than
if all the mass is @ cm

Recall cg location

$$R^{cg} = \left[\frac{Gm'm}{|\bar{F}|} \right]^{\frac{1}{2}} \longrightarrow |\bar{F}| = \frac{Gm'm}{R^2} \left(\frac{8R^2 - L^2}{8R^2} \right)$$

$$R^{cg} = \left[\frac{8R^4}{(8R^2 - L^2)} \right]^{\frac{1}{2}}$$

If $L > R$ assumptions associated with approximation violated

$$R = 4L \text{ (assumption)}$$

$$R^{cg} = \left(\frac{128}{127} \right)^{\frac{1}{2}} R$$

Note: $\psi = 0^\circ \longrightarrow$ orientation stable

