P1: A BP Wednesday, January 8, 2020 10:57 PM A1 Mathematical Background In the mathematical formulation and solution of problems in mechanics, we encounter numerous useful mathematical quantities. Some are already familiar concepts. For example, many of your courses have discussed physical phenomena through the use of *vector methods*. This is a particularly useful approach because, in the application of physical laws, the results must be independent of coordinate system. Also, vector notation provides a compact method of expressing complicated results. You have previously developed proficiency with many definitions and vector operations. It will be useful in this course to expand your prior development of vector approaches and introduce new quantities and notation as well. We will consider topics of specific use in the analysis of the dynamics of spacecraft. Some review is initially included for notational clarity; then, alternative algebraic definitions of vectors and other associated quantities are discussed. Gibbsian Vectors The three-dimensional vector analysis we use today is essentially in the form developed around 1880-1882 by Josiah Willard Gibbs (1839-1903). Much of the current vector notation originated with an English electrical engineer, Oliver viside (1850-1925), dating from about 1893. Gibbs and Heaviside actually utilized modified versions of an approach by William Rowan Hamilton (1805-1865) that utilized four-element entities (quaternions) for operations in three-dimensional space. Gibbs argued that three-element quantities (vectors) were more efficient and could be extended to higher dimensions. The Gibbsian vector approach was very controversial at the time, but was eventually accepted and put into general practice by physicists and engineers. A2 **Vector Definitions** Gibbsian vectors are usually defined in terms of 3-D Euclidian geometry: Vectors are directed line segments that add commutatively $(\overline{u} + \overline{v} = \overline{v} + \overline{u})$ and associatively $\lceil \overline{u} + (\overline{v} + \overline{w}) = (\overline{u} + \overline{v}) + \overline{w} \rceil$ according to the parallelogram rule Operational Rules: (i) dot product $\overline{u} \cdot \overline{v} = |\overline{u}| |\overline{v}| \cos(\overline{u}, \overline{v})$ commutative 14.V = V.U ên Lu, v $\overline{u} \times \overline{v} = |\overline{u}| |\overline{v}| \sin(\overline{u} |\overline{v}|) \hat{e}$ (ii) cross product =

commutative IL. V = V · W

êr Lu, v (ii) cross product $\overline{u} \times \overline{v} = |\overline{u}| |\overline{v}| \sin(\overline{u}, \overline{v}) \hat{e}_n$

anticommutative JUXIV = -UXIV

Useful Identities

- (i) $\overline{u} \times \overline{v} \cdot \overline{w} = \overline{u} \cdot \overline{v} \times \overline{w}$
- (ii) $\overline{u} \times (\overline{v} \times \overline{w}) = (\overline{u} \cdot \overline{w}) \overline{v} (\overline{u} \cdot \overline{v}) \overline{w}$

convenient to use a destral orthonormal triad

Notation and Operations

$$\overline{v} = v_1 \hat{e}_1 + v_2 \hat{e}_2 + v_3 \hat{e}_3$$

$$Component - form$$

$$\hat{v}_1, v_2, v_3 \Longrightarrow scalar components$$

$$measure numbers$$

subscript form
$$\bar{v} = \sum_{j=1}^{3} v_{j} \hat{e}_{j} = v_{j} \hat{e}_{j} \implies \text{summation convention}$$

Kronecker delta (represents the result of a dot product)

$$\delta_{ij} = \begin{cases} 1 & i = j \\ 0 & i \neq j \end{cases} \quad \hat{\ell}_{i} \cdot \hat{\ell}_{j} = \vec{\xi}_{i},$$

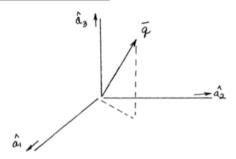
Permutation symbol (represents the result of a cross product)

$$\varepsilon_{\alpha\beta\gamma} = \begin{cases} 1 & \alpha\beta\gamma \text{ cyclic} \\ 0 & \text{represted index} \\ -1 & \alpha\beta\gamma \text{ anticyclic} \end{cases} \hat{\ell}_{\mathbf{v}} \times \hat{\ell}_{\mathbf{p}} = \hat{\ell}_{\alpha\beta\gamma} \hat{\ell}_{\mathbf{y}}$$

A4

Coordinate Transformations

relationships between sets of unit vectors

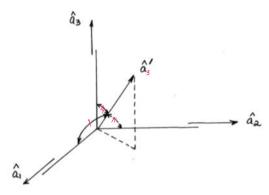


$$\overline{q}=q_1\hat{a}_1+q_2\hat{a}_2+q_3\hat{a}_3$$

$$\begin{array}{c} \therefore \ q_1 = \overline{q} \bullet \hat{a}_1 \\ q_2 = \overline{q} \bullet \hat{a}_2 \\ q_3 = \overline{q} \bullet \hat{a}_3 \end{array} \qquad \begin{array}{c} \dot{\lambda} \colon \text{ not repeated} \\ \\ f_{\hat{\lambda}} = - f_{\hat{\lambda}} \circ \hat{a}_{\hat{\nu}} \\ \\ \text{represents 3 differents} \end{array}$$

$$\overline{q} = (\overline{q} \cdot \hat{a}_1)\hat{a}_1 + (\overline{q} \cdot \hat{a}_2)\hat{a}_2 + (\overline{q} \cdot \hat{a}_3)\hat{a}_3$$

A5



$$\begin{split} \hat{a}_1' &= \left(\hat{a}_1' \bullet \hat{a}_1\right) \hat{a}_1 + \left(\hat{a}_1' \bullet \hat{a}_2\right) \hat{a}_2 + \left(\hat{a}_1' \bullet \hat{a}_3\right) \hat{a}_3 \\ \hat{a}_2' &= \left(\hat{a}_2' \bullet \hat{a}_1\right) \hat{a}_1 + \left(\hat{a}_2' \bullet \hat{a}_2\right) \hat{a}_2 + \left(\hat{a}_2' \bullet \hat{a}_3\right) \hat{a}_3 \\ \hat{a}_3' &= \left(\hat{a}_3' \bullet \hat{a}_1\right) \hat{a}_1 + \left(\hat{a}_3' \bullet \hat{a}_2\right) \hat{a}_2 + \left(\hat{a}_3' \bullet \hat{a}_3\right) \hat{a}_3 \end{split}$$

$$\hat{a}_2' = (\hat{a}_2' \cdot \hat{a}_1)\hat{a}_1 + (\hat{a}_2' \cdot \hat{a}_2)\hat{a}_2 + (\hat{a}_2' \cdot \hat{a}_3)\hat{a}_3$$

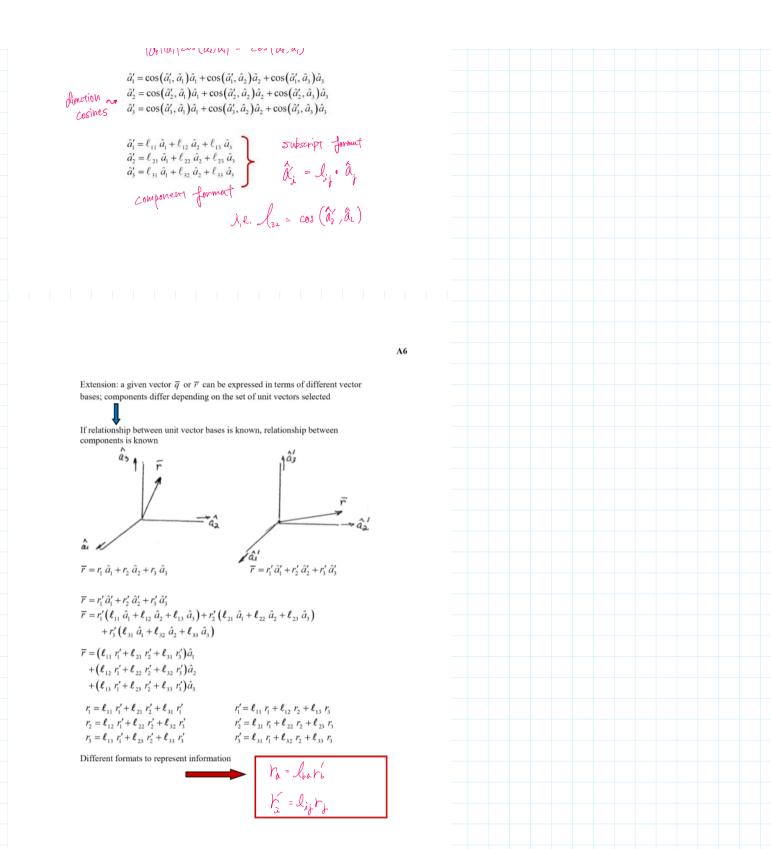
$$\hat{a}_3' = (\hat{a}_3' \cdot \hat{a}_1)\hat{a}_1 + (\hat{a}_3' \cdot \hat{a}_2)\hat{a}_2 + (\hat{a}_3' \cdot \hat{a}_3)\hat{a}_3$$

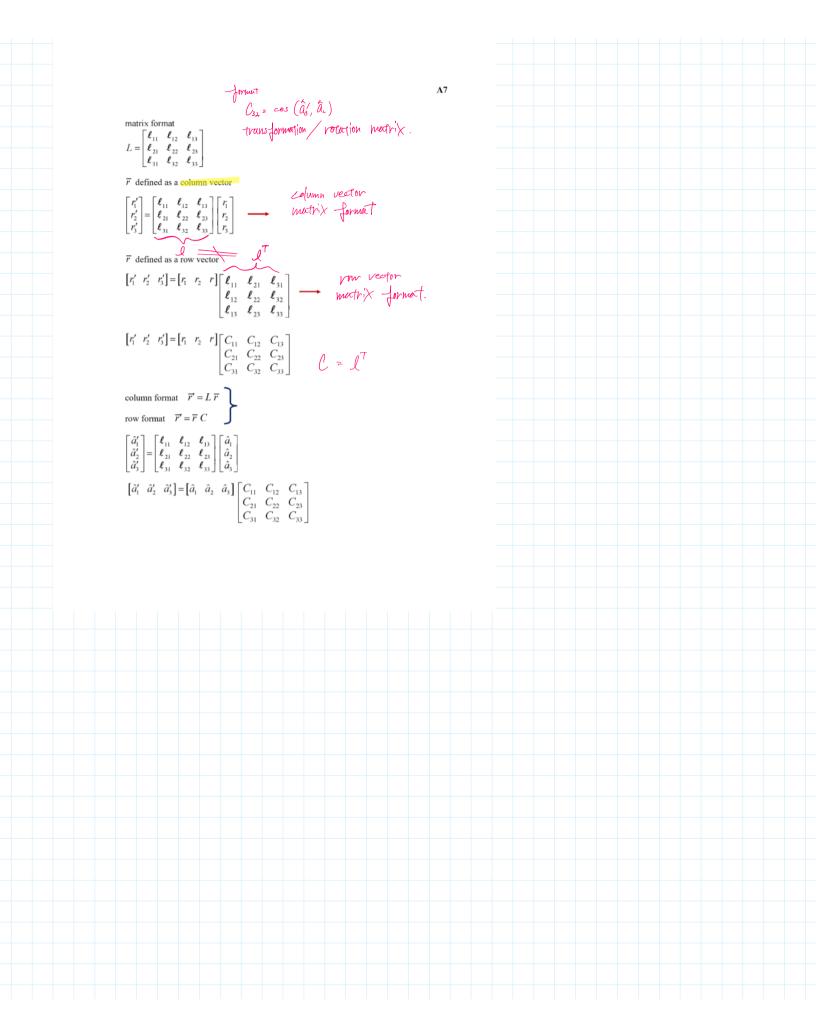
$$|\hat{\partial}_{\xi}'||\hat{\alpha}_{t}|\cos(\hat{\alpha}_{\xi},\hat{\alpha}_{t}) = \cos(\hat{\alpha}_{\xi}',\hat{\alpha}_{t})$$

 $\hat{a}_1' = \cos(\hat{a}_1', \hat{a}_1)\hat{a}_1 + \cos(\hat{a}_1', \hat{a}_2)\hat{a}_2 + \cos(\hat{a}_1', \hat{a}_3)\hat{a}_3$

 $\hat{a}'_{1} = \cos(\hat{a}'_{1}, \hat{a}_{1})\hat{a}_{1} + \cos(\hat{a}'_{1}, \hat{a}_{1})\hat{a}_{2} + \cos(\hat{a}'_{1}, \hat{a}_{1})\hat{a}_{3}$

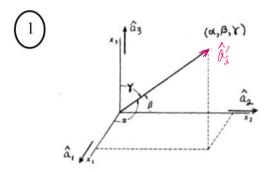
n. See





Properties of Rotation Matrices

Properties of L (or C) _____ ℓ_y (or C_y) ____ are based on twotrigonometric results:



$$\hat{a}'_{1} = (\hat{a}'_{1} \cdot \hat{a}_{1})\hat{a}_{1} + (\hat{a}'_{1} \cdot \hat{a}_{2})\hat{a}_{2} + (\hat{a}'_{1} \cdot \hat{a}_{3})\hat{a}_{3}$$

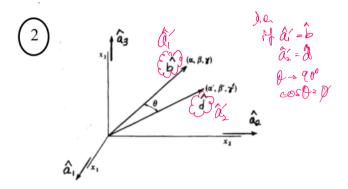
$$\hat{a}'_{1} = \cos(\hat{a}'_{1}, \hat{a}_{1})\hat{a}_{1} + \cos(\hat{a}'_{1}, \hat{a}_{2})\hat{a}_{2} + \cos(\hat{a}'_{1}, \hat{a}_{3})\hat{a}_{3}$$

$$\hat{a}'_{1} = \cos\alpha\,\hat{a}_{1} + \cos\beta\,\hat{a}_{2} + \cos\gamma\,\hat{a}_{3}$$
white the following the angle of the second of



$$\begin{array}{ll} \cos\left(\hat{a}_{1}^{\prime},\hat{a}_{1}\right) & \cos\left(\hat{a}_{1}^{\prime},\hat{a}_{2}\right) & \cos\left(\hat{a}_{1}^{\prime},\hat{a}_{3}\right) \\ \cos\alpha = \ell_{11} & \cos\beta = \ell_{12} & \cos\gamma = \ell_{13} \end{array}$$

$$\begin{array}{ccc} \therefore & \boldsymbol{\ell}_{11}^2 + \boldsymbol{\ell}_{12}^2 + \boldsymbol{\ell}_{13}^2 = 1 \\ & \boldsymbol{\ell}_{21}^2 + \boldsymbol{\ell}_{22}^2 + \boldsymbol{\ell}_{23}^2 = 1 \\ & \boldsymbol{\ell}_{31}^2 + \boldsymbol{\ell}_{32}^2 + \boldsymbol{\ell}_{33}^2 = 1 \end{array}$$



$$\begin{split} \hat{b} &= \cos\alpha \ \hat{a}_1 + \cos\beta \ \hat{a}_2 + \cos\gamma \ \hat{a}_3 \\ \hat{d} &= \cos\alpha' \ \hat{a}_1 + \cos\beta' \ \hat{a}_2 + \cos\gamma' \ \hat{a}_3 \\ \hat{b} \cdot \hat{d} &= \left| \hat{b} \right| \left| \hat{d} \right| \cos\theta \ = \ \cos\theta \end{split}$$

assume \(\preceq \) unit vectors

Let
$$\hat{b} = \hat{a}'_1$$
 $\hat{d} = \hat{a}'_2$ $\theta = 90^\circ$

Also then
$$\cos \alpha = \int_{\mathbb{N}} \cos \alpha' = \int_{\mathbb{N}} \cos \alpha' = \int_{\mathbb{N}} \cos \beta' = \int_{\mathbb{N}} \cos \gamma' = \int_{\mathbb{N}} \cos \gamma$$

$$\cos 90^{\circ} = 0 = \ell_{11}\ell_{21} + \ell_{12}\ell_{22} + \ell_{13}\ell_{23}$$
$$0 = \ell_{21}\ell_{31} + \ell_{22}\ell_{32} + \ell_{23}\ell_{33}$$
$$0 = \ell_{11}\ell_{31} + \ell_{12}\ell_{32} + \ell_{13}\ell_{33}$$

Note: relationships based on the assumption that unit vectors are mutually perpendicular

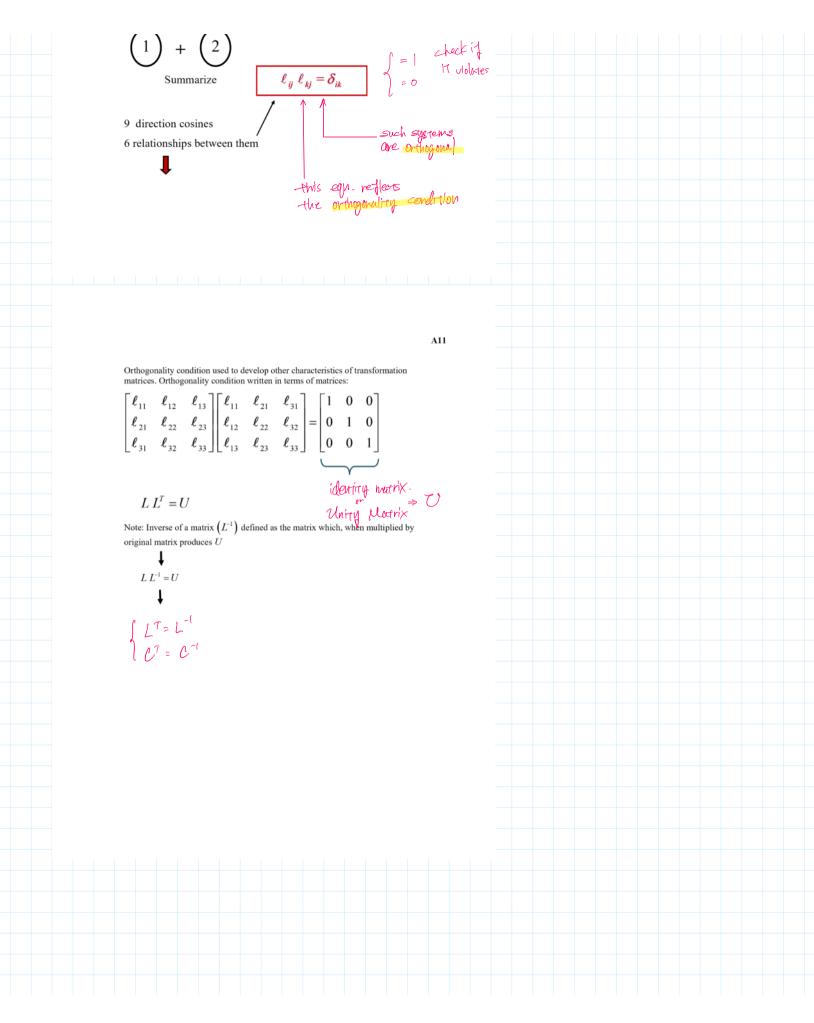


 $\ell = \ell = \delta$

 $\int = 1$

check if

A10



Example: Set of moments and products of inertia

$$I = \begin{bmatrix} I_{11} & I_{12} & I_{13} \\ I_{21} & I_{22} & I_{23} \\ I_{31} & I_{32} & I_{33} \end{bmatrix}$$

We already know that any inertia matrix is associated with

(i) phylicular point

(ii) particular vector tasks **

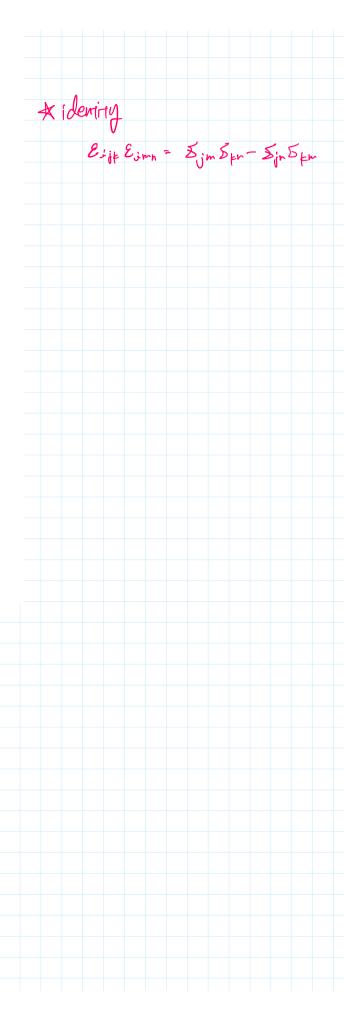
We already know that any inertia matrix can be transformed to another vector basis the probability to the first inertia matrix can be transformed to another vector basis

through the use of the similarity transformation

Define: matrix I associated with vector basis \hat{u} matrix I' associated with vector basis \hat{u}'

$$\begin{bmatrix} \hat{u}'_1 \\ \hat{u}'_2 \\ \hat{u}'_3 \end{bmatrix} = \begin{bmatrix} \ell_{11} & \ell_{12} & \ell_{13} \\ \ell_{21} & \ell_{22} & \ell_{23} \\ \ell_{31} & \ell_{32} & \ell_{33} \end{bmatrix} \begin{bmatrix} \hat{u}_1 \\ \hat{u}_2 \\ \hat{u}_3 \end{bmatrix}$$

$$\begin{bmatrix} \hat{u}_1' \\ \hat{u}_2' \\ \hat{u}_3' \end{bmatrix} = L \begin{bmatrix} \hat{u}_1 \\ \hat{u}_2 \\ \hat{u}_3 \end{bmatrix}$$
 In 340 we used the notation: $L \Leftrightarrow \begin{bmatrix} \ell \end{bmatrix}$ $\hat{u}' \cdot \hat{u}$



$$\lceil \hat{u}' \rceil = L \lceil \hat{u} \rceil$$

Transform a vector

Transform a matrix

$$\begin{bmatrix} \mathbf{I} \end{bmatrix} = \begin{bmatrix} \mathbf{J} \end{bmatrix} \begin{bmatrix} \mathbf{I} \end{bmatrix} \begin{bmatrix} \mathbf{J} \end{bmatrix} \begin{bmatrix} \mathbf{J} \end{bmatrix}$$
 trensformation
$$\mathbf{V} \quad \hat{\mathbf{V}} \cdot \hat{\mathbf{V}} \quad \hat{\mathbf{V}}$$

$$\mathbf{T} = \mathbf{L} \mathbf{T} \mathbf{L}^{\mathsf{T}} \quad \text{or} \quad \mathbf{T} = \mathbf{C}^{\mathsf{T}} \mathbf{C}$$

$$\begin{bmatrix} I_{11}' & I_{12}' & I_{13}' \\ I_{21}' & I_{22}' & I_{23}' \\ I_{31}' & I_{32}' & I_{33}' \end{bmatrix} = \begin{bmatrix} \ell_{11} & \ell_{12} & \ell_{13} \\ \ell_{21} & \ell_{22} & \ell_{23} \\ \ell_{31} & \ell_{32} & \ell_{33} \end{bmatrix} \begin{bmatrix} I_{11} & I_{12} & I_{13} \\ I_{21} & I_{22} & I_{23} \\ I_{31} & I_{32} & I_{33} \end{bmatrix} \begin{bmatrix} \ell_{11} & \ell_{21} & \ell_{31} \\ \ell_{12} & \ell_{22} & \ell_{32} \\ \ell_{13} & \ell_{23} & \ell_{33} \end{bmatrix}$$

Represents 9 equations (one for each I'_{ii})

A15

We would like to have more flexibility

element

Vectors: matrix format $\begin{bmatrix} t_1 & t_2 & t_3 \end{bmatrix}$ $\begin{bmatrix} v_1 \\ v_2 \\ v_3 \end{bmatrix}$

component format $\overline{v} = v_1 \hat{e}_1 + v_2 \hat{e}_2 + v_3 \hat{e}_3$

component format ???

component format – corresponding to vector component format; use <u>dvadic</u> representation to carry vector basis explicitly



component format - corresponding to vector component format; use dvadic

representation to carry vector basis explicitly
$$\vec{T} = \prod_{11} \hat{\mathbf{e}}_{1} \hat{\mathbf{e}}_{1} + \prod_{12} \hat{\mathbf{e}}_{1} \hat{\mathbf{e}}_{1} + \prod_{13} \hat{\mathbf{e}}_{2} \hat{\mathbf{e}}_{3} + \prod_{14} \hat{\mathbf{e}}_{2} \hat{\mathbf{e}}_{4} \\
+ \prod_{12} \hat{\mathbf{e}}_{2} \hat{\mathbf{e}}_{2} + \prod_{13} \hat{\mathbf{e}}_{2} \hat{\mathbf{e}}_{3} + \prod_{15} \hat{\mathbf{e}}_{3} \hat{\mathbf{e}}_{1} + \prod_{15} \hat{\mathbf{e}}_{3} \hat{\mathbf{e}}_{4} + \prod_{15} \hat{\mathbf{e}}_{4} \hat{\mathbf{e}}_{4} + \prod_{15}$$

9 elements - 9 terms in expressions (each term is scalar + dyad)

A16

dyad - two vectors sitting together; no intervening operation like dot/cross

NOT commutative
$$\overline{u} \, \overline{v} \neq \overline{v} \, \overline{u} \quad \bigvee = V_1 \, \hat{v}_{\lambda}$$
Summation convention $\left\{ \int_{\mathcal{F}_{\lambda}} \hat{h}_{\lambda} \, \hat{h}_{\lambda} \right\}$

Use of dyadics extends to any quantity that we have traditionally represented as a matrix. One advantage of dyadic format is that dyads and dyadics operate on vectors using the operational rules similar to those for vectors

Example: Angular Momentum

$$\overline{H} = H_1 \, \hat{e}_1 + H_2 \, \hat{e}_2 + H_3 \, \hat{e}_3$$

To evaluate \bar{H} typically uses matrix format

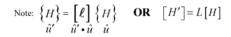
$$\left\{ \boldsymbol{H} \right\} = \begin{bmatrix} \boldsymbol{I} \end{bmatrix} \left\{ \boldsymbol{\omega} \right\} \qquad \mathbf{OR} \qquad \begin{bmatrix} \boldsymbol{H} \end{bmatrix} = \boldsymbol{I} \begin{bmatrix} \boldsymbol{\omega} \end{bmatrix}$$

$$\begin{bmatrix} H_1 \\ H_2 \\ H_3 \end{bmatrix} = \begin{bmatrix} I_{11} & I_{12} & I_{13} \\ I_{21} & I_{22} & I_{23} \\ I_{31} & I_{32} & I_{33} \end{bmatrix} \begin{bmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \end{bmatrix}$$

$$\begin{bmatrix} H \text{ vector} \\ \text{for basis} \\ \hat{V} \end{bmatrix} \text{ and velo of rigid body must inertial frame; basis } \hat{V}$$

MN = (2, h, + v2h, + v3h3) (V, h, + V2h, + V3h8) = U, V, h, h. + U, V, h, h, + U, V, h, h, = 422 6, 6,





Utilizing inertia dyadic

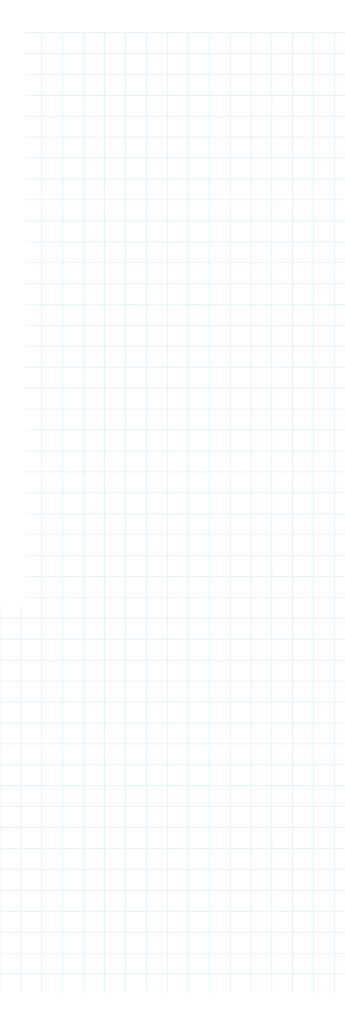
 $\overline{H} = \overline{\overline{I}} \bullet \overline{\varpi} \qquad \text{dot product between a dyadic and a vector is a vector}$ Note: in general

$$\begin{split} \overline{u} \bullet \overline{v} &= \left(u_1 \hat{e}_1 + u_2 \hat{e}_2 + u_3 \hat{e}_3 \right) \bullet \left(v_1 \hat{e}_1 + v_2 \hat{e}_2 + v_3 \hat{e}_3 \right) \\ &= u_1 v_1 \left(\hat{e}_1 \bullet \hat{e}_1 \right) + u_1 v_2 \left(\hat{e}_1 \bullet \hat{e}_2 \right) + u_1 v_3 \left(\hat{e}_1 \bullet \hat{e}_3 \right) \\ &+ u_2 v_1 \left(\hat{e}_2 \bullet \hat{e}_1 \right) + u_2 v_2 \left(\hat{e}_2 \bullet \hat{e}_2 \right) + u_2 v_3 \left(\hat{e}_2 \bullet \hat{e}_3 \right) \\ &+ u_3 v_1 \left(\hat{e}_3 \bullet \hat{e}_1 \right) + u_3 v_2 \left(\hat{e}_3 \bullet \hat{e}_2 \right) + u_3 v_3 \left(\hat{e}_3 \bullet \hat{e}_3 \right) \end{split}$$

 $\overline{u} \bullet \overline{v} =$

$$\begin{split} \overline{\overline{I}} \bullet \overline{\omega} &= \begin{pmatrix} I_{11} \hat{e}_1 \hat{e}_1 + I_{12} \hat{e}_1 \hat{e}_2 + I_{13} \hat{e}_1 \hat{e}_3 + I_{21} \hat{e}_2 \hat{e}_1 + I_{22} \hat{e}_2 \hat{e}_2 + I_{23} \hat{e}_2 \hat{e}_3 \\ &+ I_{31} \hat{e}_3 \hat{e}_1 + I_{32} \hat{e}_3 \hat{e}_2 + I_{33} \hat{e}_3 \hat{e}_3 \end{pmatrix} \bullet \begin{pmatrix} \omega_1 \hat{e}_1 + \omega_2 \hat{e}_2 + \omega_3 \hat{e}_3 \end{pmatrix} \\ &= I_{11} \omega_1 \hat{e}_1 \begin{pmatrix} \hat{e}_1 \bullet \hat{e}_1 \end{pmatrix} + I_{11} \omega_2 \hat{e}_1 \begin{pmatrix} \hat{e}_1 \bullet \hat{e}_2 \end{pmatrix} + I_{11} \omega_3 \hat{e}_1 \begin{pmatrix} \hat{e}_1 \bullet \hat{e}_3 \end{pmatrix} + \\ &I_{12} \omega_1 \hat{e}_1 \begin{pmatrix} \hat{e}_2 \bullet \hat{e}_1 \end{pmatrix} + I_{12} \omega_2 \hat{e}_1 \begin{pmatrix} \hat{e}_2 \bullet \hat{e}_2 \end{pmatrix} + I_{12} \omega_3 \hat{e}_1 \begin{pmatrix} \hat{e}_2 \bullet \hat{e}_3 \end{pmatrix} + \\ &I_{13} \omega_1 \hat{e}_1 \begin{pmatrix} \hat{e}_3 \bullet \hat{e}_1 \end{pmatrix} + I_{13} \omega_2 \hat{e}_1 \begin{pmatrix} \hat{e}_3 \bullet \hat{e}_2 \end{pmatrix} + I_{13} \omega_3 \hat{e}_1 \begin{pmatrix} \hat{e}_3 \bullet \hat{e}_3 \end{pmatrix} + \dots \end{split}$$

 $\overline{\overline{I}} \bullet \overline{\omega} =$



A18

$$\begin{split} \overline{\overline{I}} \bullet \overline{\omega} &= \begin{pmatrix} I_{11}\omega_1 + I_{12}\omega_2 + I_{13}\omega_3 \end{pmatrix} \hat{e}_1 \\ &+ \begin{pmatrix} I_{21}\omega_1 + I_{22}\omega_2 + I_{23}\omega_3 \end{pmatrix} \hat{e}_2 \\ &+ \begin{pmatrix} I_{31}\omega_1 + I_{32}\omega_2 + I_{33}\omega_3 \end{pmatrix} \hat{e}_3 \end{split}$$

Let
$$I = \begin{bmatrix} 200 & 150 & 0 \\ 150 & 300 & 0 \\ 0 & 0 & 500 \end{bmatrix}$$
 kg-m²

$$\overline{\omega} = 3\hat{a}_2 + 2\hat{a}_3 \text{ rad/s}$$

$$\overline{I} \bullet \overline{\varpi} = (200\hat{a}_1\hat{a}_1 + 150\hat{a}_1\hat{a}_2 + 150\hat{a}_2\hat{a}_1 + 300\hat{a}_2\hat{a}_2 + 500\hat{a}_3\hat{a}_3) \bullet (3\hat{e}_2 + 2\hat{e}_3) \quad \text{kg-m}^2/\text{s}$$

$$= 200\hat{a}_1\hat{a}_1 \bullet (3\hat{a}_2 + 2\hat{a}_3)$$

$$150\hat{a}_1\hat{a}_2 \bullet (3\hat{a}_2 + 2\hat{a}_3)$$

$$150\hat{a}_2\hat{a}_1 \bullet (3\hat{a}_2 + 2\hat{a}_3)$$

$$300\hat{a}_2\hat{a}_2 \bullet (3\hat{a}_2 + 2\hat{a}_3)$$

$$500\hat{a}_3\hat{a}_3 \bullet (3\hat{a}_2 + 2\hat{a}_3)$$

$$500\hat{a}_3\hat{a}_3 \bullet (3\hat{a}_2 + 2\hat{a}_3)$$

$$\overline{H} = \text{kg-m}^2/\text{s}$$

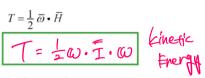
Example: Rotational Kinetic Energy

Scalar
$$T = \frac{1}{2} \left\{ \omega \right\}^T \begin{bmatrix} I \\ \hat{a} \end{bmatrix} \left\{ \omega \right\} = \frac{1}{2} \left\{ \omega \right\}^T \left\{ H \right\}$$



$$=\frac{1}{2} \left\{ \begin{matrix} \omega_1 & \omega_2 & \omega_3 \end{matrix} \right\} \begin{bmatrix} I_{11} & I_{12} & I_{13} \\ I_{21} & I_{22} & I_{23} \\ I_{31} & I_{32} & I_{33} \end{bmatrix} \begin{bmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \end{bmatrix}$$

$$T = \frac{1}{2} \, \overline{\omega} \cdot \overline{H}$$



Previous example

$$T = \frac{1}{2} (3\hat{e}_2 + 2\hat{e}_3) \cdot (200\hat{a}_1\hat{a}_1 + 150\hat{a}_1\hat{a}_2 + 150\hat{a}_2\hat{a}_1 + 300\hat{a}_2\hat{a}_2 + 500\hat{a}_3\hat{a}_3) \cdot (3\hat{e}_2 + 2\hat{e}_3)$$

$$2T = (3\hat{e}_2 + 2\hat{e}_3) \cdot 200\hat{a}_1\hat{a}_1 \cdot (3\hat{e}_2 + 2\hat{e}_3)$$

$$+ (3\hat{e}_2 + 2\hat{e}_3) \cdot 150\hat{a}_1\hat{a}_2 \cdot (3\hat{e}_2 + 2\hat{e}_3)$$

$$+ (3\hat{e}_2 + 2\hat{e}_3) \cdot 150\hat{a}_2\hat{a}_1 \cdot (3\hat{e}_2 + 2\hat{e}_3)$$

$$+ (3\hat{e}_2 + 2\hat{e}_3) \cdot 300\hat{a}_2\hat{a}_2 \cdot (3\hat{e}_2 + 2\hat{e}_3)$$

$$+ (3\hat{e}_2 + 2\hat{e}_3) \cdot 500\hat{a}_3\hat{a}_3 \cdot (3\hat{e}_2 + 2\hat{e}_3)$$

$$+ (3\hat{e}_2 + 2\hat{e}_3) \cdot 500\hat{a}_3\hat{a}_3 \cdot (3\hat{e}_2 + 2\hat{e}_3)$$

$$+ (3\hat{e}_2 + 2\hat{e}_3) \cdot 500\hat{a}_3\hat{a}_3 \cdot (3\hat{e}_2 + 2\hat{e}_3)$$

$$+ (3\hat{e}_2 + 2\hat{e}_3) \cdot 500\hat{a}_3\hat{a}_3 \cdot (3\hat{e}_2 + 2\hat{e}_3)$$

$$T = 2350 \text{ kg-m}^2/\text{s}^2$$

