



COLLEGE OF ENGINEERING  
SCHOOL OF AEROSPACE ENGINEERING

AE6210: ADVANCED DYNAMICS I

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## Homework 3

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# I Instructions

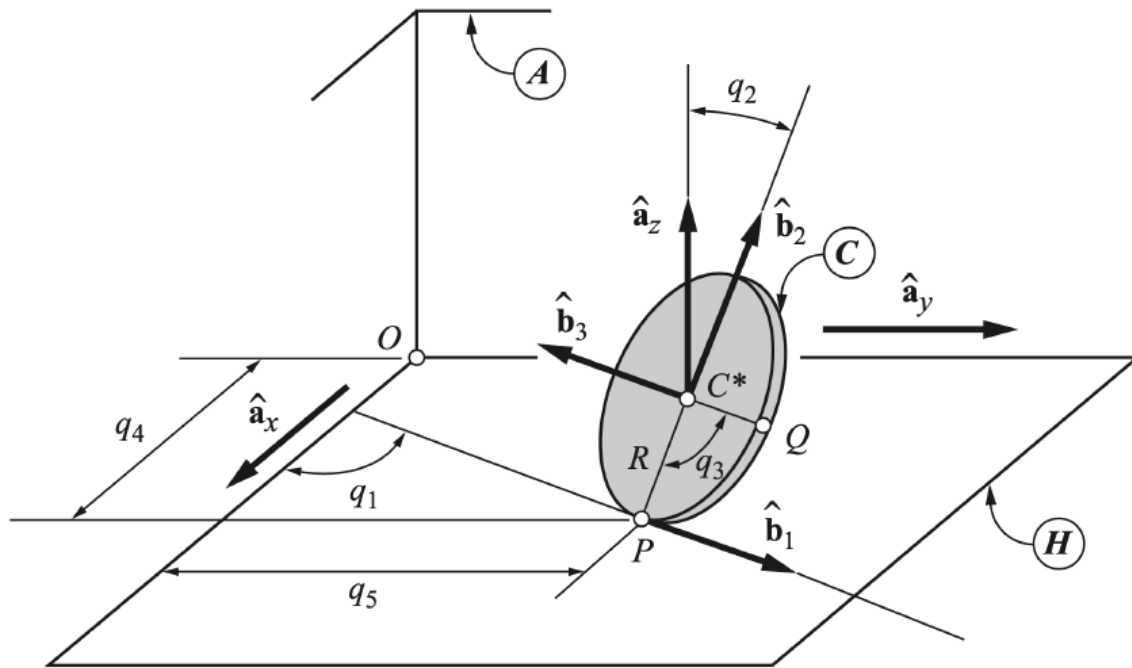


Figure 1: Kane's Problem 2.7 diagram

The figure above shows a circular disk  $C$  of radius  $R$  in contact with a horizontal plane  $H$  that is fixed in a reference frame  $A$  rigidly attached to the Earth. Mutually perpendicular unit vectors  $\hat{a}_x$ ,  $\hat{a}_y$ , and  $\hat{a}_z = \hat{a}_x \times \hat{a}_y$  are fixed in  $A$ , and  $\hat{b}_1$ ,  $\hat{b}_2$ ,  $\hat{b}_3$  form a dextral set of orthogonal unit vectors, with  $\hat{b}_1$  parallel to the tangent to the periphery of  $C$  at the point of contact between  $H$  and  $C$  (denoted by  $\hat{C}$ ),  $\hat{b}_2$  parallel to the line connecting this contact point ( $\hat{C}$ ) to  $C^*$ , the center of  $C$ , and  $\hat{b}_3$  normal to the plane of  $C$ .

The orientation of  $C$  in  $A$  can be described in terms of three angles  $q_1$ ,  $q_2$ ,  $q_3$ , where  $Q$  is a point fixed on the periphery of  $C$ . The two quantities  $q_4$  and  $q_5$  characterize the position in  $A$  of the point  $P$  (which represents a point on the path made by the disk on the  $H$ ).

## II Problem One

The angular velocity of  $C$  in  $A$  can be expressed as:

$${}^A\vec{\omega}^C = u_1\hat{b}_1 + u_2\hat{b}_2 + u_3\hat{b}_3. \quad (\text{II.1})$$

Determine  $u_1$ ,  $u_2$ , and  $u_3$ , which we can also choose as the generalized velocities for the problem. The expression for  $u_i$ 's should be written in terms of the generalized coordinates and their time derivatives.

**Solution:**

Let a unit vector with no specific frame be expressed as

$$\hat{X} = (1, 0, 0)^T, \quad \hat{Y} = (0, 1, 0)^T, \quad \hat{Z} = (0, 0, 1)^T,$$

and for clarity and my preference, let  $(\hat{a}_x, \hat{a}_y, \hat{a}_z) = (\hat{a}_1, \hat{a}_2, \hat{a}_3)$  and define new coordinate frames:  $c$ -frame and  $h$ -frame. The new frames are observed in Figure 2.

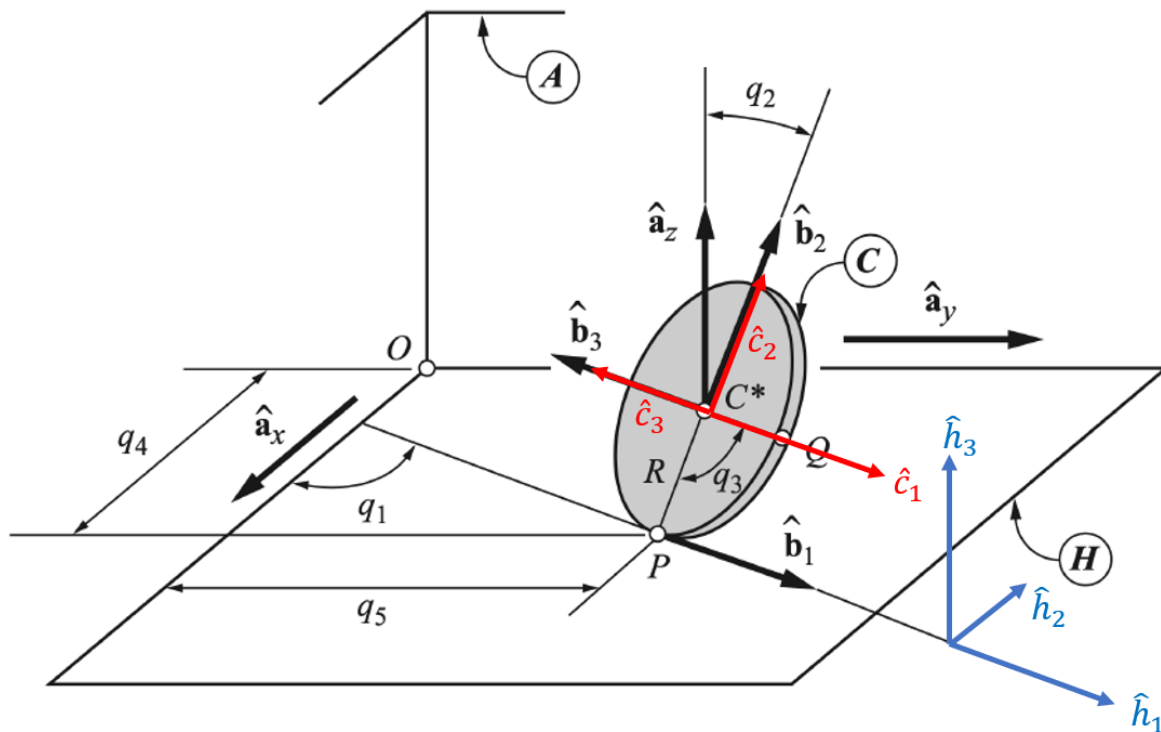


Figure 2: Problem diagram with extra coordinate frames.

To make the transitions between different frames easy, we will define the relations between each frames with rotations. If  $S(\cdot)$  indicates the skew-symmetric matrix operation and  $\otimes$  is the outer

product (tensor product) then we have

$$\begin{aligned}\hat{h} &= L(q_1, \hat{Z}) \hat{a} = R_a^h \hat{a} \\ \hat{h} &= \left[ (I - \hat{Z} \otimes \hat{Z}) \cos(q_1) - S(\hat{Z}) \sin(q_1) + \hat{Z} \otimes \hat{Z} \right] \hat{a} \\ \begin{bmatrix} \hat{h}_1 \\ \hat{h}_2 \\ \hat{h}_3 \end{bmatrix} &= \begin{bmatrix} \cos(q_1) & \sin(q_1) & 0 \\ -\sin(q_1) & \cos(q_1) & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \hat{a}_1 \\ \hat{a}_2 \\ \hat{a}_3 \end{bmatrix}.\end{aligned}\tag{II.2}$$

Similarly,

$$\begin{aligned}\hat{b} &= L\left(\frac{\pi}{2} - q_2, \hat{X}\right) \hat{h} = R_h^b \hat{h} \\ \hat{b} &= \left[ (I - \hat{X} \otimes \hat{X}) \cos\left(\frac{\pi}{2} - q_1\right) - S(\hat{X}) \sin\left(\frac{\pi}{2} - q_2\right) + \hat{X} \otimes \hat{X} \right] \hat{h} \\ \begin{bmatrix} \hat{b}_1 \\ \hat{b}_2 \\ \hat{b}_3 \end{bmatrix} &= \begin{bmatrix} 1 & 0 & 0 \\ 0 & \sin(q_2) & \cos(q_2) \\ 0 & -\cos(q_2) & \sin(q_2) \end{bmatrix} \begin{bmatrix} \hat{h}_1 \\ \hat{h}_2 \\ \hat{h}_3 \end{bmatrix}.\end{aligned}\tag{II.3}$$

And finally,

$$\begin{aligned}\hat{c} &= L\left(q_3 - \frac{\pi}{2}, \hat{Z}\right) \hat{b} = R_b^c \hat{b} \\ \hat{c} &= \left[ (I - \hat{Z} \otimes \hat{Z}) \cos\left(q_3 - \frac{\pi}{2}\right) - S(\hat{Z}) \sin\left(q_3 - \frac{\pi}{2}\right) + \hat{Z} \otimes \hat{Z} \right] \hat{b} \\ \begin{bmatrix} \hat{c}_1 \\ \hat{c}_2 \\ \hat{c}_3 \end{bmatrix} &= \begin{bmatrix} \sin(q_3) & -\cos(q_3) & 0 \\ \cos(q_3) & \sin(q_3) & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \hat{b}_1 \\ \hat{b}_2 \\ \hat{b}_3 \end{bmatrix}.\end{aligned}\tag{II.4}$$

Now that we have that defined we can find  ${}^A\vec{\omega}^C$  using the additive property of angular velocities. It becomes

$${}^A\omega^C = {}^a\omega^h + {}^h\omega^b + {}^b\omega^c$$

From the definition of angular velocity we have

$$-S({}^a\omega^h) = \dot{R}_a^h \left(R_a^h\right)^T = \dot{R}_a^h R_h^a\tag{II.5}$$

$$-\begin{bmatrix} 0 & -{}^a\omega_3^h & {}^a\omega_2^h \\ {}^a\omega_3^h & 0 & -{}^a\omega_1^h \\ -{}^a\omega_2^h & {}^a\omega_1^h & 0 \end{bmatrix} = \begin{bmatrix} -\dot{q}_1 \sin(q_1) & \dot{q}_1 \cos(q_1) & 0 \\ -\dot{q}_1 \cos(q_1) & -\dot{q}_1 \sin(q_1) & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} \cos(q_1) & -\sin(q_1) & 0 \\ \sin(q_1) & \cos(q_1) & 0 \\ 0 & 0 & 1 \end{bmatrix}\tag{II.6}$$

$$\therefore {}^a\omega^h = \dot{q}_1 \hat{a}_3.\tag{II.7}$$

Similarly we can compute,

$${}^h\omega^b = -\dot{q}_2 \hat{h}_1 = -\dot{q}_2 \hat{b}_1\tag{II.8}$$

$${}^b\omega^c = \dot{q}_3 \hat{b}_3.\tag{II.9}$$

Thus, from (II.7)-(II.9) we have

$${}^A\omega^C = \dot{q}_1 \hat{a}_3 - \dot{q}_2 \hat{b}_1 + \dot{q}_3 \hat{b}_3.\tag{II.10}$$

From the transformations (II.2) and (II.3), we can convert  $\hat{a}_3$  as follows

$$\hat{a}_3 = \left( \left( R_h^b R_a^h \right)^{-1} \hat{b} \right) \cdot \hat{Z} = \left( R_h^a R_b^h \hat{b} \right) \cdot \hat{Z}$$

$$\hat{a}_3 = \cos(q_2) \hat{b}_2 + \sin(q_2) \hat{b}_3.$$

The generalized velocities are

$$u_1 = -\dot{q}_2$$

$$u_2 = \dot{q}_1 \cos(q_2)$$

$$u_3 = \dot{q}_1 \sin(q_2) + \dot{q}_3.$$

Hence,

$${}^A\vec{\omega}^C = -\dot{q}_2 \hat{b}_1 + \dot{q}_1 \cos(q_2) \hat{b}_2 + (\dot{q}_1 \sin(q_2) + \dot{q}_3) \hat{b}_3. \quad (\text{II.11})$$

### III Problem Two

Similarly determine  ${}^A\vec{\omega}^B$  as represented in the  $B$  reference frame. You will need this to determine many of the quantities asked below. Try to write the angular velocity in terms of the generalized coordinates and generalized velocities only.

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**Solution:**

Similar to Problem One, we compute angular velocity as

$$\begin{aligned} {}^A\omega^B &= {}^a\omega^h + {}^h\omega^b \\ &= \dot{q}_1 \hat{a}_3 - \dot{q}_2 \hat{b}_1 \end{aligned}$$

Hence,

$$\begin{aligned} {}^A\vec{\omega}^B &= -\dot{q}_2 \hat{b}_1 + \dot{q}_1 \cos(q_2) \hat{b}_2 + \dot{q}_1 \sin(q_2) \hat{b}_3 \\ &= -\dot{q}_2 \hat{b}_1 + \dot{q}_1 \cos(q_2) \hat{b}_2 + \dot{q}_1 \cos(q_2) \tan(q_2) \hat{b}_3 \end{aligned}$$

and

$${}^A\vec{\omega}^B = u_1 \hat{b}_1 + u_2 \hat{b}_2 + u_2 \tan(q_2) \hat{b}_3.$$

(III.1)

## IV Problem Three

The angular acceleration of  $C$  in terms of  $A$  can be expressed as

$${}^A\vec{\alpha}^C = \alpha_1 \hat{b}_1 + \alpha_2 \hat{b}_2 + \alpha_3 \hat{b}_3. \quad (\text{IV.1})$$

Determine  $\alpha_1$ ,  $\alpha_2$ , and  $\alpha_3$  in terms of the generalized coordinates, generalized velocities, and the time derivatives of generalized velocities.

### Solution:

The acceleration is the derivative of the angular velocity, and therefore, from (II.11) and (III.1) we can compute this as follows.

$${}^A\vec{\alpha}^C = \frac{b}{dt} {}^A\vec{\omega}^C + {}^A\vec{\omega}^B \times {}^A\vec{\omega}^C.$$

Hence,

$${}^A\vec{\alpha}^C = (\dot{u}_1 + u_2(u_3 - u_2 \tan(q_2))) \hat{b}_1 + (\dot{u}_2 - u_1(u_3 - u_2 \tan(q_2))) \hat{b}_2 + \dot{u}_3 \hat{b}_3, \quad (\text{IV.2})$$



## V Problem Four

Define  $u_4 = \dot{q}_4$  and  $u_5 = \dot{q}_5$ , two more generalized velocities. The velocity of  $C^*$  in  $A$  can be expressed as:

$${}^A\vec{v}^{C^*} = v_1\hat{b}_1 + v_2\hat{b}_2 + v_3\hat{b}_3. \quad (\text{V.1})$$

Determine  $v_1$ ,  $v_2$ , and  $v_3$  in terms of the generalized coordinates ( $q_i$ 's) and generalized velocities ( $u_i$ 's) only.

### Solution:

The position of point  $C^*$  with respect to the origin is

$$\begin{aligned} \vec{r}_{OC^*} &= \vec{r}_{OP} + \vec{r}_{PC^*} \\ &= q_4\hat{a}_1 + q_5\hat{a}_2 + R\hat{b}_2. \end{aligned} \quad (\text{V.2})$$

Then the velocity is

$$\begin{aligned} {}^a\vec{v}_{OC^*} &= \frac{d\vec{r}_{OC^*}}{dt} \\ &= \frac{d}{dt}(q_4\hat{a}_1 + q_5\hat{a}_2) + {}^A\vec{\omega}^B \times (R\hat{b}_2) \\ &= \dot{q}_4\hat{a}_1 + \dot{q}_5\hat{a}_2 + (u_1\hat{b}_1 + u_2\hat{b}_2 + u_2\tan(q_2)\hat{b}_3) \times (R\hat{b}_2) \\ &= u_4\hat{a}_1 + u_5\hat{a}_2 + (u_1\hat{b}_1 + u_2\hat{b}_2 + u_2\tan(q_2)\hat{b}_3) \times (R\hat{b}_2) \\ &= u_4\hat{a}_1 + u_5\hat{a}_2 - Ru_2\tan(q_2)\hat{b}_1 + Ru_1\hat{b}_3. \end{aligned} \quad (\text{V.3})$$

Since,

$$\begin{aligned} \hat{a}_1 &= \left( (R_h^b R_a^h)^{-1} \hat{b} \right) \cdot \hat{X} = (R_h^a R_b^h \hat{b}) \cdot \hat{X} \\ &= \cos(q_1)\hat{b}_1 - \sin(q_1)\sin(q_2)\hat{b}_2 + \sin(q_1)\cos(q_2)\hat{b}_3, \end{aligned}$$

and

$$\begin{aligned} \hat{a}_2 &= \left( (R_h^b R_a^h)^{-1} \hat{b} \right) \cdot \hat{Y} = (R_h^a R_b^h \hat{b}) \cdot \hat{Y} \\ &= \sin(q_1)\hat{b}_1 + \cos(q_1)\sin(q_2)\hat{b}_2 - \cos(q_1)\cos(q_2)\hat{b}_3. \end{aligned}$$

Plug in these results to (V.3) and we can compute the results

$$\begin{aligned} v_1 &= -Ru_2\tan(q_2) + u_4\cos(q_1) + u_5\sin(q_1) \\ v_2 &= -u_4\cos(q_1)\sin(q_1) + u_5\cos(q_1)\sin(q_2) \\ v_3 &= Ru_1 + u_4\sin(q_1)\cos(q_2) - u_5\cos(q_1)\cos(q_2) \end{aligned}$$

## VI Problem Five

The acceleration of  $C^*$  in  $A$  can be expressed as:

$${}^A\vec{a}^{C^*} = a_1\hat{b}_1 + a_2\hat{b}_2 + a_3\hat{b}_3. \quad (\text{VI.1})$$

Determine  $a_1$ ,  $a_2$ , and  $a_3$  in terms of the generalized coordinates ( $q_i$ 's), generalized velocities ( $\dot{u}_i$ 's), and the time derivatives of generalized velocities ( $\dot{u}_i$ 's).

### Solution:

This is simply the derivative of the answer in Problem V in the  $b$ -frame which is

$${}^A\vec{a}^{C^*} = \frac{{}^b d}{{}^b dt} {}^A\vec{v}^{C^*} + {}^A\vec{\omega}^B \times {}^A\vec{v}^{C^*},$$

which reduces to

$$\begin{aligned} a_1 &= -R\dot{u}_2 \tan(q_2) + \dot{u}_4 \cos(q_1) + \dot{u}_5 \sin(q_1) + Ru_1 u_2 (1 + \sec^2(q_2)) \\ a_2 &= -\dot{u}_4 \sin(q_1) \sin(q_2) + \dot{u}_5 \cos(q_1) \sin(q_2) - Ru_1^2 - Ru_2^2 \tan^2(q_2) \\ a_3 &= R\dot{u}_1 + \dot{u}_4 \sin(q_1) \cos(q_2) - \dot{u}_5 \cos(q_1) \cos(q_2) + Ru_2^2 \tan(q_2) \end{aligned}$$

## VII Problem Six

At any time, there exists precisely one point on the disk  $C$  that is in contact with the plane  $H$ . Calling this point  $\hat{C}$ , determine the velocity of this point  ${}^A\vec{v}^{\hat{C}}$  as represented in the  $A$  reference frame.

### Solution:

For this problem, we use the two-point formula since points  $C^*$  and  $\hat{C}$  are on the same rigid body. Therefore, in the  $b$ -frame the velocity is expressed as

$$\begin{aligned} {}^A\vec{v}^{\hat{C}} &= {}^A\vec{v}^{C^*} + {}^A\vec{\omega}^C \times \vec{r}_{C^*\hat{C}} \\ &= {}^A\vec{v}^{C^*} + {}^A\vec{\omega}^C \times R(-\hat{b}_2) \\ &= \begin{bmatrix} u_4 \cos(q_1) + Ru_3 + u_5 \sin(q_1) - Ru_2 \tan(q_2) \\ \sin(q_2) (u_5 \cos(q_1) - u_4 \sin(q_1)) \\ -\cos(q_2) (u_5 \cos(q_1) - u_4 \sin(q_1)) \end{bmatrix}. \end{aligned}$$

To express this in the  $a$ -frame we plug the above result into (II.2) and (II.3) as a sequence of rotations

$$\begin{bmatrix} \hat{a}_1 \\ \hat{a}_2 \\ \hat{a}_3 \end{bmatrix} = \begin{bmatrix} \cos(q_1) & \sin(q_1) & 0 \\ -\sin(q_1) & \cos(q_1) & 0 \\ 0 & 0 & 1 \end{bmatrix}^T \begin{bmatrix} 1 & 0 & 0 \\ 0 & \sin(q_2) & \cos(q_2) \\ 0 & -\cos(q_2) & \sin(q_2) \end{bmatrix}^T \begin{bmatrix} \hat{b}_1 \\ \hat{b}_2 \\ \hat{b}_3 \end{bmatrix}.$$

Thus, we obtain

$$\begin{aligned} {}^A\vec{v}^{\hat{C}} &= (u_4 + u_3 R \cos(q_1) - u_2 R \cos(q_1) \tan(q_2)) \hat{a}_1 \\ &\quad + (u_5 + u_3 R \sin(q_1) - u_2 R \sin(q_1) \tan(q_2)) \hat{a}_2. \end{aligned}$$