

Name	Team Number
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## AAE 251: Introduction to Aerospace Design

### Assignment 6—The Rocket Equation, Rocket Thrust and Staging

**Due Tuesday March 5, 10:00 am on Blackboard**

**No 24hr extensions**

#### Instructions

*Write or type your answers into the appropriate boxes. **Make sure you submit a single PDF on Blackboard.***

*Make sure you keep a record of submission receipts or the confirmation emails after each submission as a proof that your submission was accepted.*

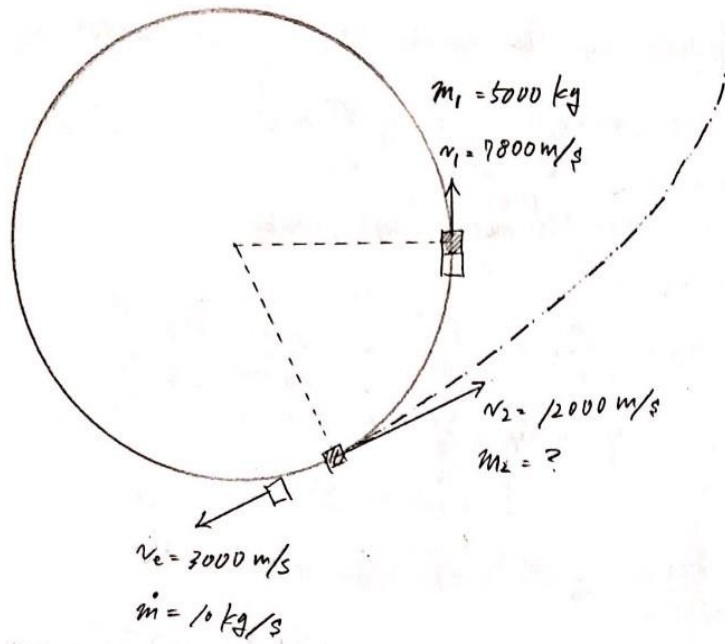
***There is no 24hr extension on this homework. Any submission after March 5, 10:00 am will not be accepted.***

	<b>Score</b>	<b>Max</b>
<b>Question 1</b>		<b>8</b>
<b>Question 2</b>		<b>9</b>
<b>Question 3</b>		<b>10</b>
<b>Question 4</b>		<b>10</b>
<b>Question 5</b>		<b>13</b>
<b>Question 6</b>		<b>25</b>
<b>TOTAL</b>		<b>75</b>

### **Question 1**

A spacecraft weighing  $5,000\text{ kg}$  is travelling in an orbit around Earth at a velocity of  $7,800\text{ m/s}$ . Its engine places it on an escape trajectory by accelerating it to a velocity of  $12,000\text{ m/s}$ . The engine expels mass at a rate of  $10\text{ kg/s}$  at an effective exhaust velocity of  $3,000\text{ m/s}$ . What is the duration of the burn?

Answer 1:



total change in momentum  $\equiv \Delta p = m_1 v_1 - m_2 v_2$

$$F_{\text{thrust}} = \frac{dm_{\text{re}}}{dt} = m_{\text{ve}}$$

and  $(F_{\text{thrust}}) \Delta t = \Delta p \iff \Delta t = \frac{\Delta p}{F_{\text{thrust}}} = \frac{m_1 v_1 - m_2 v_2}{F_{\text{thrust}}} \dots \textcircled{D}$

since we still do not know  $m_2$

$$\therefore dv = -v_e \frac{dm}{m} \quad \rightarrow \quad v_2 - v_1 = -v_e \ln \frac{m_2}{m_1}$$

$$\int_{v_1}^{v_2} dv = -v_e \int_{m_1}^{m_2} \frac{dm}{m} \quad m_2 = m_1 \exp\left(-\frac{v_2 - v_1}{v_e}\right) \dots \dots \textcircled{2}$$

$$\therefore \textcircled{2} \Rightarrow m_2 = (5000 \text{ kg}) \cdot \exp\left(-\frac{1000 \text{ m/s} - 7000 \text{ m/s}}{30000 \text{ m/s}}\right) \approx 944.378 \text{ kg}$$

∴ ① ② ③

$$A \dot{x} = \frac{(5000 \text{ kg})(7800 \text{ m/s}) - (944,378 \text{ kg})(12000 \text{ m/s})}{(10 \text{ kg/s})(3000 \text{ m/s})} \approx 922,25 \text{ s}$$

## **Question 2**

A single-stage rocket is used to launch a satellite weighing  $1000\text{ kg}$  into a circular orbit at an altitude of  $200\text{ km}$ . The specific impulse of the rocket is  $20,000\text{ m/s}$ . The structural mass of the rocket is 20% of the initial mass. Calculate the mass of propellant needed for this mission.

$$GM = 3.986 \times 10^5 \text{ km}^3/\text{s}^2; \quad R_e = 6378 \text{ km}$$

Answer 2:

this is mass-based so  $v_e$  has unit  $m/s$   $v_e = 20000 m/s$

$$GM = \mu = 3.986 \times 10^5 \text{ km}^3/s^2 = 3.986 \times 10^{14} \text{ m}^3/s^2$$

$$R_e = 6378 \text{ km} = 6.378 \times 10^6 \text{ m}$$

$$R = 200 \text{ km}, \text{ satellite mass} = m = 1000 \text{ kg}$$

initial velocity  $v_i = 0$

$$\text{Final velocity } v_f = \sqrt{\frac{\mu}{r}} = \sqrt{\frac{\mu}{R+R_e}} = \sqrt{\frac{3.986 \times 10^{14} \text{ m}^3/s^2}{2.00 \times 10^5 + 6.378 \times 10^6}}$$

$$\approx 7784.34 \text{ m/s}$$

now using

$$dv = -v_e \frac{dm}{m}$$

$$v_f - v_i = -v_e \ln \frac{m_i}{m_f}$$

$$f_{\text{inert}} = \frac{0.2 m_i}{m_i - m_{\text{pay}}}$$

thus

$$m_{\text{pay}} = 1000 \text{ kg}$$

$$m_{\text{inert}} = 0.2 m_i$$

$$m_i = m_{\text{prop}} + m_{\text{pay}} + m_{\text{inert}} = m_{\text{prop}} + m_{\text{pay}} + 0.2 m_i$$

$$m_{\text{prop}} = 0.8 m_i - m_{\text{pay}} \quad \dots \textcircled{D}$$

$$m_f = m_{\text{pay}} + m_{\text{inert}} = m_{\text{pay}} + 0.2 m_i$$

$$v_f - v_i = -v_e \ln \frac{m_i}{m_f} \quad \rightarrow \quad 0.67759 m_i = m_{\text{pay}} + 0.2 m_i$$

$$m_i = 2093.85 \text{ kg}$$

$$m_f = m_i \exp\left(-\frac{v_f}{v_e}\right)$$

$$m_f \approx 0.67759 m_i$$

$$m_{\text{pay}} = \textcircled{D} = 675.08$$

$$\boxed{675.08 \text{ kg}}$$

### **Question 3**

The ARIANE 5 launch vehicle has two P230 solid propellant boosters and a main Vulcain engine that are ignited at lift-off. The two components of the launch vehicle have the following characteristics:

Effective exhaust velocities:  $c_{Vulcain} = 3285 \text{ m/s}$ ;  $c_{P230} = 2355 \text{ m/s}$

Mass flows:  $\dot{m}_{Vulcain} = 255 \text{ kg/s}$ ;  $\dot{m}_{P230} = 1835 \text{ kg/s}$

Calculate the average effective exhaust velocity and average specific impulse for the launch vehicle.

Answer 3:

$$\begin{aligned} \text{mean}(C_{eff}) &= \frac{C_{utrain} \dot{m}_{utrain} + 2 C_{p230} \dot{m}_{p230}}{\dot{m}_{utrain} + 2 \dot{m}_{p230}} \\ &= \frac{(3285 \text{ m/s})(255 \text{ kg/s}) + 2(2355 \text{ m/s})(1835 \text{ kg/s})}{255 \text{ kg/s} + 2(1835 \text{ kg/s})} \\ &\approx \boxed{2415.42 \text{ m/s}} \end{aligned}$$

$$\text{mean}(I_{sp}) = \frac{\text{mean}(C_{eff})}{g_0} = \frac{2415.42 \text{ m/s}}{9.81 \text{ m/s}^2} \approx \boxed{246.32 \text{ s}}$$



#### Question 4

The mass of the payload of a spacecraft is 1000 kg, and the inert mass fraction is 0.10. If the velocity change,  $\Delta V$  and the exit velocity of the propellant are 4860 m/s and 4267 m/s respectively,

- a) What is the mass of the propellant on board the spacecraft?
- b) What is the inert mass of the spacecraft?
- c) What is the initial mass of the spacecraft?

Answer 4:

$$m_{\text{pay}} = 1000 \text{ kg}$$

$$f_{\text{inert}} = \beta = 0.10$$

$$\Delta V = 4860 \text{ m/s}$$

$$v_e = 4267 \text{ m/s}$$

(a) using the formula

$$m_{\text{prop}} = \frac{m_{\text{pay}} (e^{\frac{\Delta V}{v_e}} - 1)(1 - \beta)}{1 - \beta e^{\frac{\Delta V}{v_e}}} = \frac{(1000 \text{ kg}) (e^{\frac{4860}{4267}} - 1)(1 - 0.10)}{1 - (0.10)e^{\frac{4860}{4267}}} \\ \approx 2779.35 \text{ kg}$$

$$(b) \quad \beta = \frac{m_{\text{inert}}}{m_{\text{inert}} + m_{\text{prop}}} \Leftrightarrow m_{\text{inert}} = \frac{\beta}{1 - \beta} m_{\text{prop}} = \frac{0.10}{0.90} (2779.35 \text{ kg}) \\ \approx 308.82 \text{ kg}$$

(c)

$$m_i = m_{\text{pay}} + m_{\text{inert}} + m_{\text{prop}} \\ = 1000 \text{ kg} + 308.82 \text{ kg} + 2779.35 \text{ kg} \\ = 4088.17 \text{ kg}$$

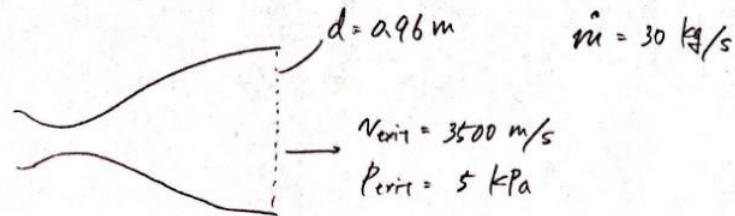
### **Question 5**

A rocket's engine has an exit diameter of  $0.96\text{ m}$ . It is ejecting mass at a rate of  $30\text{ kg/s}$  with an exit velocity of  $3,500\text{ m/s}$ . The pressure at the exit of the nozzle is  $5\text{ kPa}$ . Calculate:

- a) The thrust of the engine in vacuum
- b) Final mass of the rocket if the initial mass was  $1000\text{ kg}$  and the burn duration was  $25\text{ s}$ .
- c) Specific impulse
- d) Effective exhaust velocity

Answer 5:

Q5.



(a) at vacuum  $P_{atm} = 0$

so  $A = \frac{\pi}{4} d^2 = \frac{\pi}{4} (0.96 \text{ m})^2 \approx 0.7238 \text{ m}^2$

and

$$F_{\text{thrust}} = \dot{m} [V_{\text{exit}} + (P_{\text{exit}} - P_{\text{atm}}) A]$$

$$= (30 \text{ kg/s}) [3500 \text{ m/s}] + (5 \times 10^3 \text{ Pa}) (0.7238 \text{ m}^2)$$

$$= \boxed{108619 \text{ N}}$$

(b)

$$\frac{dm}{dt} = \dot{m}$$

$$\int_1^2 dm = \int_0^{25} \dot{m} dt$$

$$m_f - m_i = -\dot{m} \Delta t$$

$$m_f = -\dot{m} \Delta t + m_i$$

$$= -(30 \text{ kg/s})(25 \text{ s}) + 1000 \text{ kg} = \boxed{250 \text{ kg}}$$

(c) specific impulse  $\equiv I_{sp} = \frac{F_{\text{thrust}}}{\dot{m} g_0}$

$$= \frac{108619 \text{ N}}{(30 \text{ kg/s})(9.81 \text{ m/s}^2)} \approx \boxed{369.08 \text{ s}}$$

(d)

$$C = v_e = \frac{F_{\text{thrust}}}{\dot{m}} = \boxed{3620.13 \text{ m/s}}$$

## **Question 6**

The shape of NACA airfoils is described through their numerical identifier. We can input the parameters from the identifier into equations to precisely generate the cross-section of the airfoil. The four-digit series, in particular, defines the profile through three parameters. The first digit describes maximum camber as a percentage of the chord. The second digit provides the distance of the maximum camber from the airfoil leading edges in tens of percentages of the chord. The last two digits give us the maximum thickness of the airfoil as a percentage of the chord.

For example, the NACA 2215 airfoil has a maximum camber of 2%, located at 0.2 chords (20%) from the leading edge of the airfoil, with a maximum thickness of 15% of the chord. Since we can use equations to describe the shape of the airfoil, we can automate the process of drawing different airfoils!

Write a MATLAB script that takes a NACA 4-digit series code and the chord length as inputs and plots the shape of the airfoil. On your plot, include the chord and mean camber line. Plot three different airfoils to show that your algorithm works with various inputs. Include a symmetric airfoil, a cambered airfoil, and a third airfoil of your choice.

If you need inspiration when choosing NACA airfoils to plot, you can find airfoil designations for a variety of aircraft on "*The Incomplete Guide to Airfoil Usage*" at <https://m-selig.ae.illinois.edu/ads/aircraft.html>. On this website, you will notice that the Supermarine Spitfire has a different airfoil for the root and the tip of the wing. The Air Tractor, on the other hand, maintains the same airfoil from root to tip. Why do you think that is?

For this question, you will be graded on your MATLAB code, plot, and discussion on the last prompt. Make sure your code is well commented and describes the variables and equations you have used to generate the plots. Make it easy for a third person to read and understand.

# Airfoil Plotter

- This program will plot the airfoil of a NACA 4-digit series aircraft.

## Theory

First of all, the nomenclature of the 4-digit is the following

1. First digit: The **maximum camber** as percentage of chord
2. Second Digit: **Distance of the maximum camber** from the airfoil leading edge in tens of percents of chord
3. Last two digits: The **maximum thickness** of airfoil as percentage of chord

Then, the equations we will use to calculate the airfoil shape are shown below.

The equation for the airfoil is expressed as a pair of parametric equations for  $X$  and  $Y$  using the parameter  $\theta$  for  $\theta = [0, 2\pi]$ . The equations are

$$X(\theta) = 0.5 + 0.5 \frac{|\cos(\theta)|^B}{\cos(\theta)} \quad \dots (1)$$

$$Y(\theta) = \frac{T}{2} \frac{|\sin(\theta)|^B}{\sin(\theta)} (1 - X^P) + C \sin(X^E \pi) + R \sin(X 2\pi) \quad \dots (2)$$

where

1. B: Describes the **Base shape coefficient**. This parameter determines mainly the shape of the leading edge. When B is closer to 2 the base shape of the airfoil becomes more elliptical, whereas when it is more closer to 1 the shape becomes more rectangular.
2. T: Describes **thickness** as a fraction/percentage of the chord
3. P: Describes the **Taper Exponent**. The more P is closer to 1 the thickness tends to decrease more linearly when approaching 0, whereas the more P is a higher value the thickness decreases more suddenly
4. E: Describes the **Camber Exponent**. This defines the position of the maximum camber point on the chord. Where  $E = 1$  indicates the camber point to be at the middle of the airfoil, that is 50% camber point. Smaller value of E shifts the camber point more toward the leading edge
5. R: Describes the **Reflex Parameter**. When this value is a positive value the trailing edge becomes reflexed, whereas when it is negative one emulates flaps

Next, the Equation to plot the mean chord line will be simply horizontal line connecting  $x = [0, 1] \dots (3)$ .

Finally, the equation for the mean camber line will be

$$C_m(\theta) = C \sin(X^E \pi) + R \sin(X 2\pi) \quad \dots (4)$$

Now the equations from (1) to (4) is the theory of this function.

## Function

```
function airfoil_plotter_func(fourDigitCode, B_coeff, Taper_coeff, reflex_para)
```

## >>INPUT

1. fourDigitCode: The NACA 4-digit code
2. B\_coeff: Base shape coefficient
3. Taper\_coeff: Taper exponent
4. reflex\_para: Reflex parameter

## >>OUTPUT

1. none (only plot)

## >>SETUP

```
% Take out the parameters from the 4-digit code
% Hold the code
place_holder = fourDigitCode;
% Maximum camber
C_max = floor(fourDigitCode / 1000);
% Take the modulus of the four digit code for further manipulation
fourDigitCode = mod(fourDigitCode, 1000);
% Position of maximum camber
C_exp = floor(fourDigitCode / 100);
% Repeat modulus operation
fourDigitCode = mod(fourDigitCode, 100);
% Maximum thickness
Th_max = fourDigitCode;

% Default settings for the input parameters
% base shape coefficient
if B_coeff == 0
    B_coeff = 2;
end
% Taper coefficient
if Taper_coeff == 0
    Taper_coeff = 1;
end
% Reflex parameter
if reflex_para == 0
    reflex_para = 0;
end

% Assign simpler variables to make the subsequent calculations easier
% while fixing the parameters from percent to decimal
C = C_max / 100;
B = B_coeff;
P = Taper_coeff;
E = C_exp / 10;
T = Th_max / 100;
R = reflex_para;
```

## >>CALCULATIONS

```
% The main function will be a for loop to retrieve all the points for the plots
% The stepsize/increment for each iteration will of the loop will be
stepsize = 2 * pi / 1000;

% Before the loop we must preallocate the vector including all the x- and y-values
% and point for mean camber line
X_theta = zeros(1000, 1);
Y_theta = zeros(1000, 1);
Cm_theta = zeros(1000,1);

% The loop
% Initialize index counter
n = 1;

for theta = 0:stepsize:2*pi
    % Calculating the x-value
    X = 0.5 + 0.5 * (abs(cos(theta)))^B / cos(theta);
    % Calculating the y-value
    Y = T * (abs(sin(theta)))^B * (1-X^P) / 2 / sin(theta) + C * sin(X^E * pi)...
        + R * sin(X * 2 * pi);
    % Calculating point for mean camber line
    Cm = C * sin(X^E * pi) + R * sin(X * 2 * pi);

    % Appending these values into the vector
    X_theta(n) = X;
    Y_theta(n) = Y;
    Cm_theta(n) = Cm;

    % Increment counter
    n = n + 1;
end
% The chord line will be
X_chord = [0,1];
Y_chord = [0,0];
```

## >>PLOTING

```
figure(1)
plot(X_theta, Y_theta, "-b", 'Linewidth', 2.5)
title(['The Airfoil Geometry of NACA' num2str(place_holder)])
xlabel('0 to 1 from Leading Edge to Trailing Edge')
ylabel('Vertical Direction')
grid on
grid minor
ylim([-0.2, 0.2])
box on
hold on
```

```
plot(X_theta, Cm_theta, "-r", 'Linewidth', 1.5)
plot(X_chord, Y_chord, "--g")
hold off
```

#### **Terminate Function**

```
end
```



## >>Execution

- Plotting 3 types of airfoils

### #1. NACA 0015

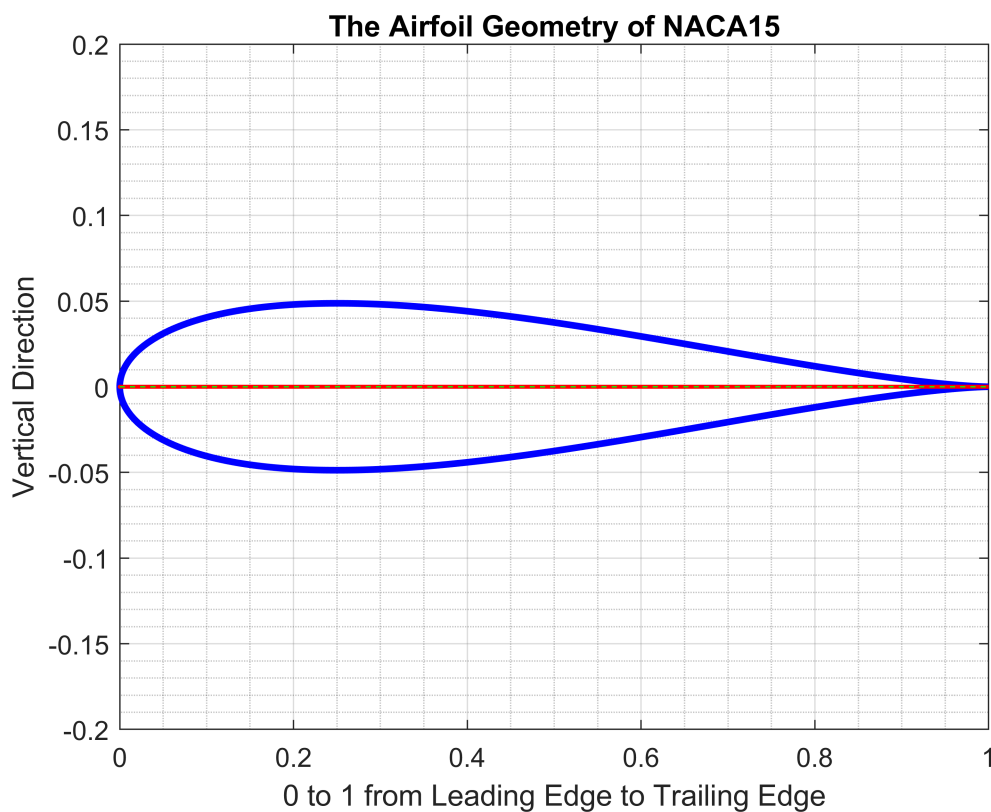
With

base shape coefficient = B = default (0)

taper exponent = P = default (0)

reflex parameter = R = default (0)

```
airfoil_plotter_func(0015,0,0,0);
```



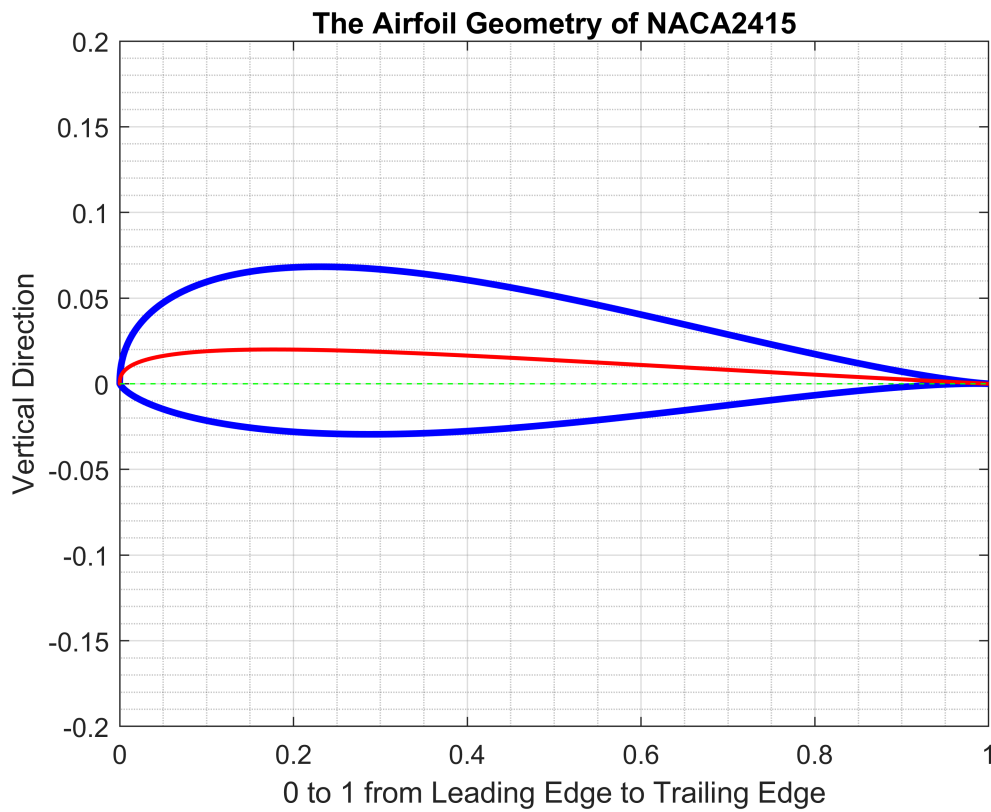
### #2. NACA 2415

base shape coefficient = B = default (0)

taper exponent = P = default (0)

reflex parameter = R = default (0)

```
airfoil_plotter_func(2415,0,0,0);
```



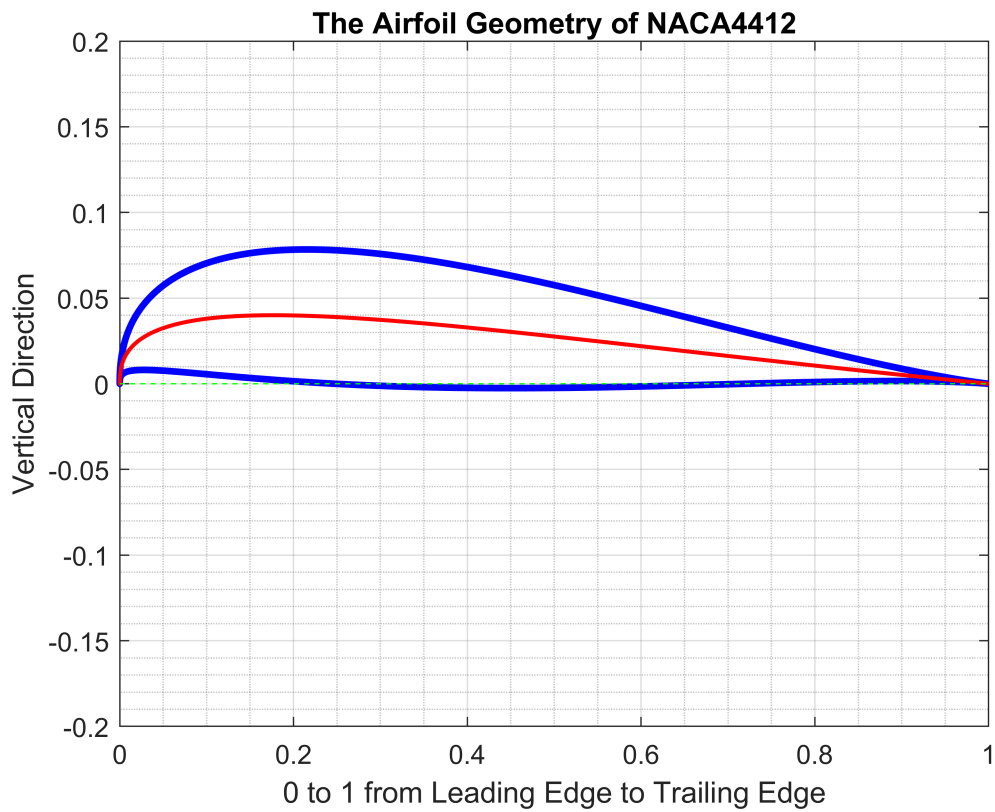
### #3. NACA 4412

base shape coefficient = B = default (0)

taper exponent = P = default (0)

reflex parameter = R = default (0)

```
airfoil_plotter_func(4412,0,0,0);
```



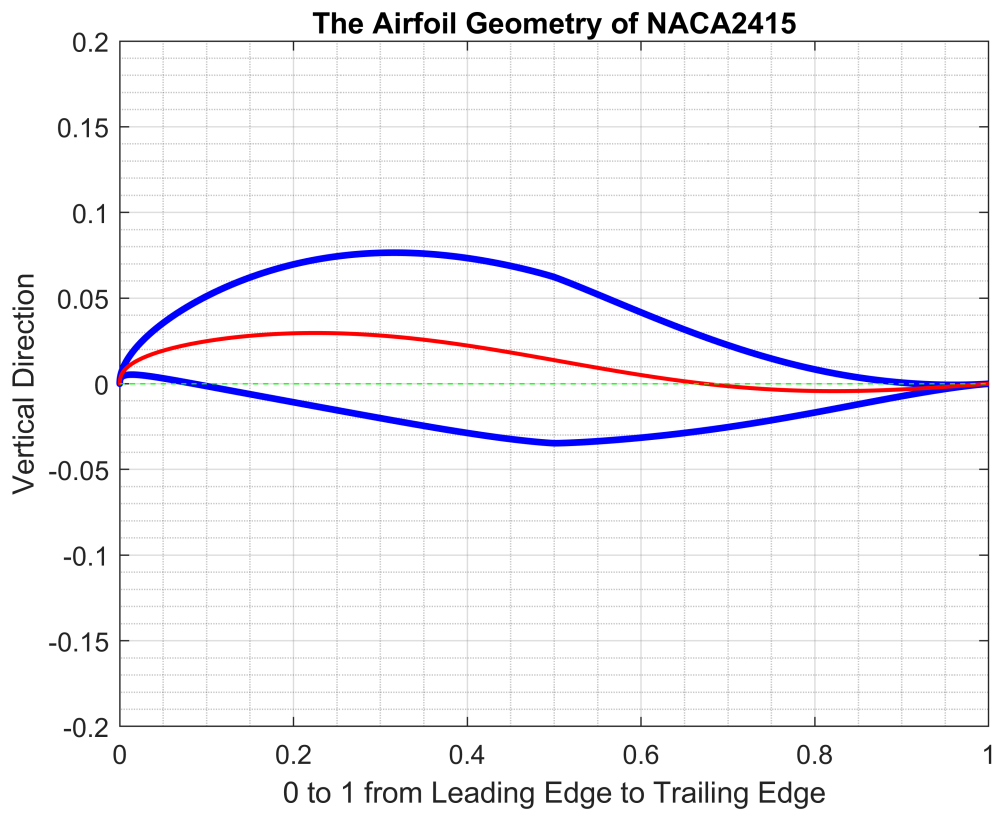
#### #4. NACA 2415 (NOT DEFAULT SETTINGS)

base shape coefficient =  $B = 2.5$

taper exponent =  $P = \text{default } 1.8$

reflex parameter =  $R = \text{default } 0.02$

```
airfoil_plotter_func(2415,2.5,1.5,0.01);
```



## Analysis:

The Supermarine Spitfire has a unique wing configuration of having the root and tip of the wings be different airfoils. At the time of its design this was a new approach, and this was done to reduce the induced drag and improve performance. This is because the airfoil at the tip managed to make the lift coefficient smaller. Spitfire's main requirements were to gain victory in dogfights, and therefore, higher maneuverability was expected. In contrast, the Air Tractor is active in high production agriculture required to maintain a stable flight in low altitudes with slow speed. Due to its main usage of disseminating chemicals to grow vast fields of crops, it is rather ideal to maintain the same airfoil from root to tip to have a constant lift and drag.

## REFERENCES

Ziemkiewicz, David. "*Simple Analytic Equation for Airfoil Shape Description.*" December 2016, [https://www.researchgate.net/publication/312222678\\_Simple\\_analytic\\_equation\\_for\\_airfoil\\_shape\\_description](https://www.researchgate.net/publication/312222678_Simple_analytic_equation_for_airfoil_shape_description). Accessed on 1 March 2019.