

Pordan sinclair

Question One:

The dynamics of a hard disk drive serve system are given by $y = \frac{K_P}{S^2} \sum_{i=1}^{\infty} \frac{b_{ii} s_i + b_{0i}}{s^2 + 25_{ii} \omega_i s_i + \omega_i^2} U$

Where ωi, i = 1,..., 6, are the resonant frequencies which are large, i.e., ωi = 11.2π×10³ rad/s, ωz = 15.5π×10³ rad/s, ω3 = 16.6π×10³ rad/s, ωμ = 18π×10³ rad/s, ω = 23.8π×10³ rad/s. The unknown constants by are of the order 10°, boi are of the order of 10°, and Kp is of the order 10°. The damping coefficients bi are of the order of 10°.

a. Derive a low order model for the servo system.

\[\frac{\alpha}{\omega} \cong \infty \frac{\alpha^2}{\omega_i^2} \cong \infty \frac{\alpha}{\omega_i^2} \cong \infty \frac{\alpha}{\omega_i^2} \lefta \infty \frac{\omega}{\omega_i^2} \lefta \infty \frac{\omega}{\omega_i^2} \lefta \infty \frac{\omega}{\omega_i^2} \lefta \infty \frac{\omega}{\omega} \lefta \infty \lefta \infty \frac{\omega}{\omega} \lefta \infty \infty \frac{\omega}{\omega} \lefta \infty \infty \frac{\omega}{\omega} \lefta \infty \infty \infty \frac{\omega}{\omega} \lefta \infty \infty \frac{\omega}{\omega} \lefta \infty \infty \inft

The system has 7 poles from the integrator, 1/57, and 7 from the damped component.

To reduce the number of poles and, in turn, the complexity of the system, each term is divided by the highest order frequencies, w:7, and compared with the others. The negliquible terms can then be ignored.

$$y = \frac{K_{0}}{S^{2}} \left\{ \frac{b_{1}}{\sum_{i=1}^{2} \frac{b_{1}}{\omega_{i}^{2}}} + \frac{b_{0}}{\sum_{i=1}^{2} \frac{b_{0}}{\omega_{i}^{2}}} \right\}$$

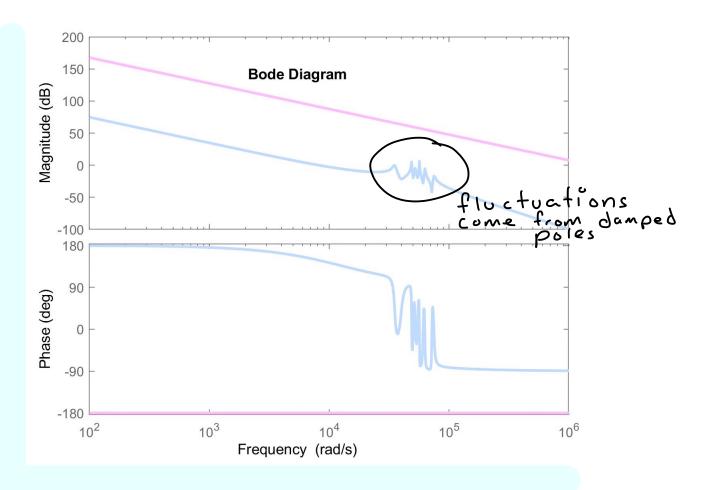
$$= \frac{S^{2}}{\sum_{i=1}^{2} \frac{b_{1}}{\omega_{i}^{2}}} + \frac{b_{0}}{\sum_{i=1}^{2} \frac{b_{0}}{\omega_{i}^{2}}} + \frac{b_{0}}{\sum_{i=1}^{2} \frac{b_{0}}{\omega_{i}$$

the bit terms are on the order of 104, as are the witerms. The boiterms have an order of 10?
Thus, the low order model is:

yred = Ke (bo1 + bo2 + ... + bo6) U



b. Obtain a Bode plot for the full-order and reduced-order models.



C. Use the reduced-order model in (a) to obtain a parametric model for the unknown parameters. Design a robust adaptive law to estimate the unknown parameters online.

the unknown parameters online.

reduced order models

yred =
$$\frac{K_{P}}{S^{2}} \left(\frac{D_{01}}{D_{1}^{2}} + \frac{D_{02}}{D_{2}^{2}} + \dots + \frac{D_{06}}{D_{06}^{2}} \right) U$$

original models

y = $\frac{K_{P}}{S^{2}} \sum_{i=1}^{6} \frac{D_{ii}S_{i}}{S^{2}+25_{i}D_{i}S_{i}} U$
 $\Delta(s) = \left(\sum_{i=1}^{6} \frac{D_{1i}S_{i}}{S^{2}+25_{i}D_{i}S_{i}} \right) - 1$
 $\Rightarrow y = \frac{K_{P}}{S^{2}} \left(\frac{D_{01}}{D_{1}^{2}} + \frac{D_{02}}{D_{2}^{2}} + \dots + \frac{D_{06}}{D_{06}^{2}} \right) \left(\left(+ \Delta m(s) \right) U \right) U$
 $y = \frac{K_{P}}{S^{2}} \left(\frac{D_{01}}{D_{1}^{2}} + \frac{D_{02}}{D_{2}^{2}} + \dots + \frac{D_{06}}{D_{06}^{2}} \right) \left(\left(+ \Delta m(s) \right) U \right) U$
 $filtering with $\frac{1}{(s+\lambda)^{2}}$
 $\frac{S^{2}}{(s+\lambda)^{2}} = K_{P} \left(\frac{D_{01}}{D_{01}} + \frac{D_{02}}{D_{2}^{2}} + \dots + \frac{D_{06}}{D_{06}^{2}} \right) \left(\frac{1}{(s+\lambda)^{2}} \right) \left(\left(+ \Delta m(s) \right) U \right) U$

Constant$

$$\frac{S^{2}}{(S+\lambda)^{2}}y = \frac{b_{01} + b_{02} + b_{02}}{(\omega_{1}^{2} + \omega_{2}^{2})} \frac{1}{(\omega_{1}^{2} + \omega_{2}^{2} + \omega_{2}^$$

$$Z = \frac{S^2}{(s+\lambda)^2} Y (\omega_1 + \omega_2 + ... + \omega_6)$$

$$Q^* = \begin{bmatrix} V_p \text{ bot } & V_p \text{ bot } \\ \frac{1}{(s+\lambda)^2} \end{bmatrix}$$

$$M = 1 + \Delta_M(s) = \frac{6}{S^2 + 2 \lambda_1^2} \frac{D_{11} S}{S^2 + 2 \lambda_1^2}$$

Since the reduced order spm, Z=0*4, doesn't include all unknown parameters, the adaptive law will need to be robustified. I plan to implement a gradient adaptive law with instaneous cost, a o-modification, and a dynamic normalization term.

$$\hat{\Theta} = \Gamma \mathcal{E} \Phi - O_{S} \Gamma \hat{\Theta}$$
where $\mathcal{E} = \frac{Z - \hat{\Theta}^{T} \Phi}{M^{Z}}$ and $M^{Z}(t) = 1 + \bigcap_{s=1}^{Z}(t) + \bigcap_{s=1}^{Z}(t)$

Additionally, using a switching modification to will vary according to o of \(\frac{\sqrt{\frac{1}{2}\cdot \frac{1}{2}\cdot where Mo>O is a constant such that \(\Sto_{0}^{2} \) = Mo^{2}

and 6. > 0 is a design constant.

Question Two: The linearized dynamics of a throttle angle O to vehicle speed V subsystem are given by the third order systems bp.p. 0+d (Sta)(S+P)(S+P2) where p, p > 20, 12 a > 0, and d is a load disturbance. a. Obtain a parametric model for the parameters of the dominant part of the Sys tem the poles at p. and p. decay much faster than at a. Thus, the part of the system containing p. andper represents the neglected dynamics— $\Delta(s) = \frac{1}{(s+p_1)(s+p_2)}$ that the dominant, or nominal, part of the system This means given by: รีร 4 = 6 U Thus, a spm can be found for this reduced systems 4 (s+a) = bu y i ay = bu

-> y = bu-ay

Filtering with 1/ s+2 $\frac{s}{s+2} = b = \frac{1}{s+7} \quad -\alpha = \frac{1}{s+7} \quad \varphi$ Z= 0 0 -> spm b. Design a robost adaptive law for estimating these parameters online. Including the unknown dynamics ->
y = b[1 + \D(s)] U + d -> 4 -- ay + bu+ b Δ(s) u filtering with 1: $\frac{s}{s+7} + \frac{1}{s+7} + \frac{1}$ $M = b \frac{1}{s+2} \left(\frac{\rho_1 \rho_2}{(s+\rho_1)(s+\rho_2)} - 1 \right) u(t) + d$ $\phi = \int_{-\frac{1}{S+7}} \dot{q}(t) \frac{1}{S+2}$ Z = 0 4 0 + 4

Since the system contains unknown dynamics, it will need to be robustified to prevent destabilization from those dynamics. I plan to use an \mathcal{E} - modification with a dynamic normalization term. $\hat{\theta} = \Gamma \mathcal{E} \hat{\phi} - 6 \Gamma \hat{\theta}$ where $\mathcal{E} = \frac{Z - \hat{\Theta}^T \hat{\phi}}{M^2}$

L> $M^2 = 1 + n_s^2(+) + n_d(+) = 1 + \phi^T \phi + n_d(+)$ n_d is a dynamic normalization term such that $n_d = -\delta_0 \cdot n_d + \upsilon^2(+), \, n_d(\upsilon) = \upsilon$

where $\delta o > 0$ is chosen so that $\Delta_i(s)$ has no poles to the right of $-\frac{\delta o}{2}$.

-> â = 8, 8 \$, -08, â(+)

6= 82 E Az - 682 6(+)

where $\mathcal{E} = \frac{Z(+) - \hat{\alpha}(+) \phi_1(+) - \hat{b}(+) \phi_2(+)}{1 + \phi_1^2 + \phi_2^2 + \Lambda_3(+)}$ and $O = |\mathcal{E}M| V_0$ Ly $V_0 > 0$ is a design constant.