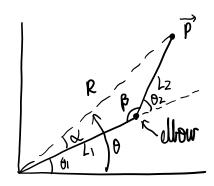
Fourord Kinematics



$$\theta = \theta_1 + \alpha$$

$$\beta = \pi - \theta_2$$

$$R^2 = L_1^2 + L_2^2 - 2L_1L_2 \cos \beta$$

$$\frac{R}{\sin \beta} = \frac{L_2}{\sin \alpha}$$

$$\Rightarrow \cos \beta = \frac{R^2 - L_1^2 - L_2^2}{-2L_1L_2}$$

$$\lim_{X \to \infty} X = \frac{L_2 \lim \beta}{R}$$

$$X = \lim_{X \to \infty} \left(\frac{L_2 \lim \beta}{R} \right)$$

 $\beta = 665 \left(\frac{R^2 - L_1^2 - L_2^2}{-21112} \right)$

ellow =
$$(L_1 \otimes \theta_1, L_1 \otimes \theta_1)$$

 $P = \text{ellow} + (L_2 \otimes (\theta_1 + \theta_2), L_2 \sin(\theta_1 + \theta_2))$
 $\text{end} = (R_1 \otimes \theta_1)$

for a standard dress board

Poolet parties

= 533.4 mm

21"= 533.4 mm

= 533.4 mm

Rmon = 596.359 mm (sognished)

mane = 596.359

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For my fusion model I had started with dimensions -
            L_1 = 153 \text{ mm} L_2 = 148 \text{ mm}
  from the model, when \theta_1 = 78.7^{\circ} and \theta_2 = 104.6^{\circ}
                                                         → R= 184 mm
       on calculating & and B,
                     \beta = 60^{-1} \left( \frac{184^2 - 153^2 - 148^2}{-2(153)(148)} \right) = 60^{-1} (0.2530) = 75.35^{\circ}
                      \alpha = \sin^{-1}\left(\frac{(148)(0.9675)}{184}\right) = \sin^{-1}(0.7782) = 51.10^{\circ}
       from the model, X = 50.97^{\circ} \beta = 75.384^{\circ}
            \theta = \theta_1 + \infty
            \theta = 78.7^{\circ} + 51.10^{\circ}
             \theta = 129.8^{\circ}
   end = (R,\theta) = (184, (29.8°)
       \overrightarrow{p} = \left( \underbrace{L_{1} \otimes \theta_{1} + L_{2} \otimes (\theta_{1} + \theta_{2})}_{\text{1}}, \underbrace{L_{1} \times \hat{\mu} \theta_{1} + L_{2} \times \hat{\mu} (\theta_{1} + \theta_{2})}_{\text{1}} \right)
\overrightarrow{p} = \left( \underbrace{153 \otimes (78.7^{\circ}) + |\mu_{8} \otimes (163.3^{\circ})}_{\text{1}}, \underbrace{153 \times \hat{\mu} (78.7^{\circ}) + |\mu_{8} \times \hat{\mu} (163.3^{\circ})}_{\text{1}} \right)
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 $\overrightarrow{p} = (-117.775, 141.515)$