

Space Station OS

AOCS System: Orbital Motion, Attitude Dynamics & Controller

Design, Simulation, and Performance

Presented by: Sanket Sharma

Date: March 10, 2025

Overview

Agenda:

- Project Background & Objectives
- Orbital Motion Dynamics
- AOCS System Overview
- Simulation Setup & Results
- Challenges & Future Work



Project Background & Objectives

Our focus is on developing an Attitude and Orbit Control System (AOCS) that ensures both precise orientation and stable orbital dynamics.

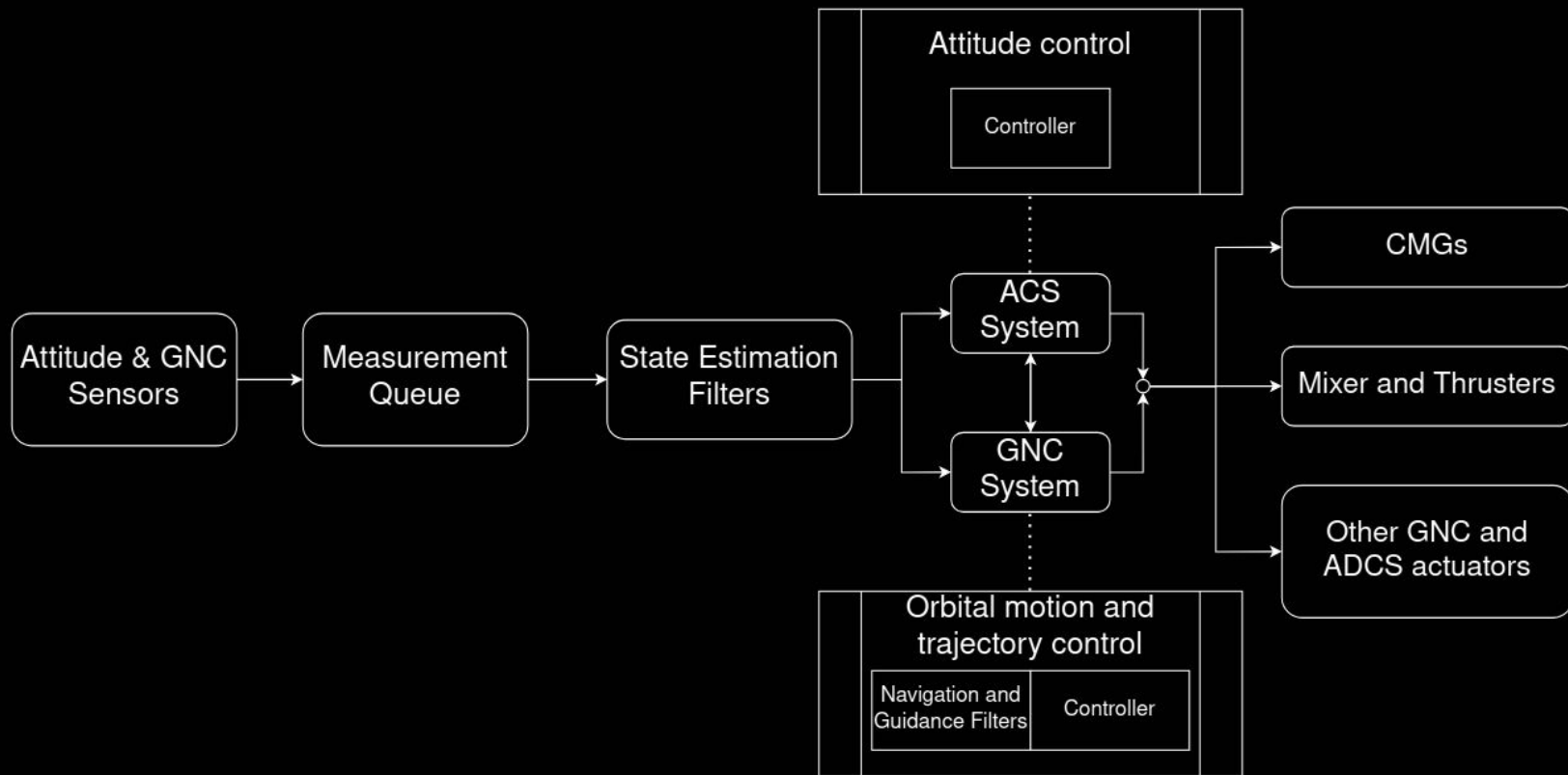
Key Objectives:

- Design system model and control architecture
- Optimize energy consumption through efficient control algorithms
- Achieve high-precision attitude and orbital control under varying conditions

Milestones:

- Successful integration of physics and AOCS subsystem components
- Completion of simulation validations
- Integration phase

Architecture



Orbital and Attitude Dynamics

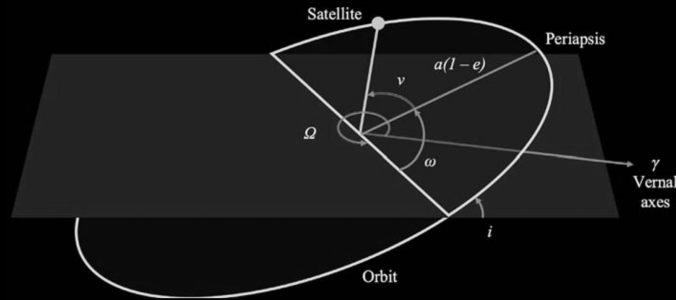
Orbital and attitude model dynamics are written to help with simulation of the AOCS system and help designing the optimal controller & state estimation algorithms.

Key Components:

- Non-linear 1st order differential equations for attitude dynamics and orbital dynamics
 - Kepler's Law, two-body problem and Euler-Newton law
 - 6 states orbital dynamics and 10 states attitude dynamics
 - Perturbation Forces and Torques considered for the currently dynamics:
 - Atmospheric Drag
 - Microgravity
 - Gravity Gradient
 - CMG's dynamics
- The diagram illustrates a satellite in an elliptical orbit around Earth. Key parameters shown include:

 - Satellite**: The object in orbit.
 - Periapsis**: The point of closest approach to Earth.
 - $a(1-e)$** : The distance from Earth's center to the periapsis.
 - v** : The true anomaly, the angle between the periapsis direction and the satellite's current position.
 - ω** : The argument of periapsis, the angle between the line of nodes and the periapsis direction.
 - Ω** : The right ascension of the ascending node, the angle between the reference direction and the line of nodes.
 - γ** : The inclination, the angle between the orbital plane and the reference plane.
 To the right of the diagram, two state vectors are defined:

 - $\mathbf{x} = \begin{bmatrix} x \\ y \\ z \\ v_x \\ v_y \\ v_z \end{bmatrix}$** : The position and velocity vector in the reference frame.
 - $\mathbf{x} = \begin{bmatrix} p \\ q \\ r \\ \phi \\ \theta \\ \psi \\ \delta_1 \end{bmatrix}$** : The attitude vector, representing orientation parameters.



$$\mathbf{x} = \begin{bmatrix} x \\ y \\ z \\ v_x \\ v_y \\ v_z \end{bmatrix}$$

$$\mathbf{x} = \begin{bmatrix} p \\ q \\ r \\ \phi \\ \theta \\ \psi \\ \delta_1 \\ \delta_2 \\ \delta_3 \\ \delta_4 \end{bmatrix}$$

AOCS System Overview

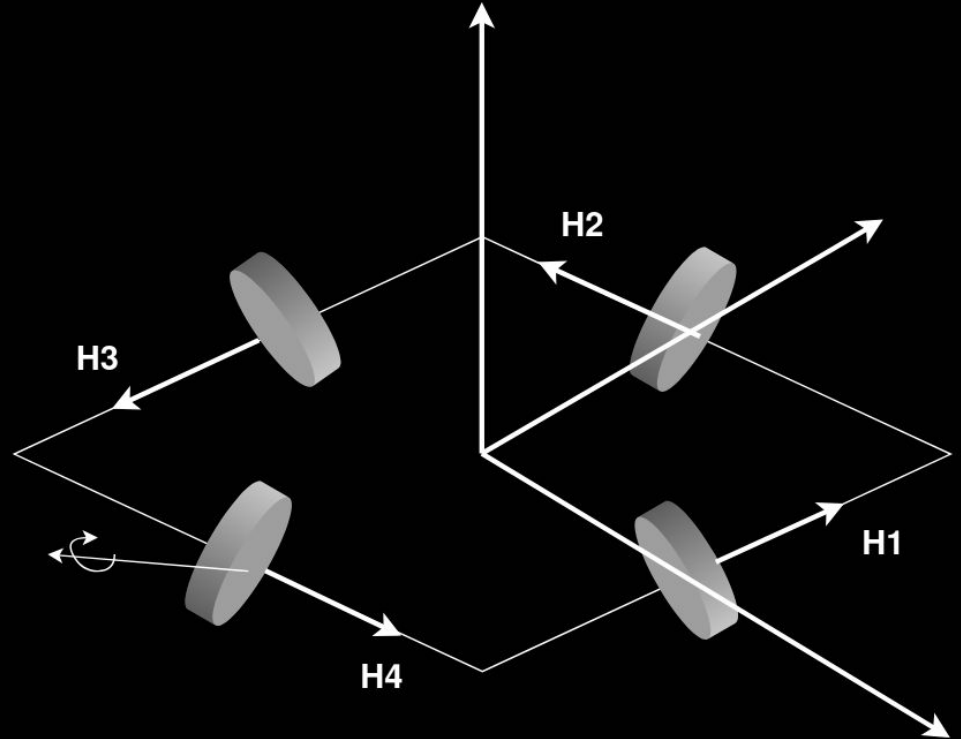
The Attitude and Orbit Control System (AOCS) is the core system that maintains the space station's correct orientation and trajectory in orbit.

Key Components:

- Attitude Control Actuators: Single Gimbaled CMGs, Thrusters & Engines
- Orbital Control Actuators: Thrusters & Engines
- Attitude Control System: PD Controller, NMPC Optimal Control*
- Orbital Control System: PID Controller with actuator mapping & H^∞ controller(in-progress)*

Single Gimbaled CMGs

- This design employs four single gimbaled CMGs arranged in a pyramid formation, with each CMG positioned on one edge of the pyramid.
- This configuration ensures effective distribution of control torques across all three axes, allowing controllability of the attitude.
- The pyramid model is great for minimizing singularities and improves responsiveness.



Simulation setup - Initial Conditions

State Variables

$$\begin{aligned} p_0 &= 0.0, & q_0 &= 0.001, & r_0 &= 0.0 \\ \phi_0 &= 0.0, & \theta_0 &= 0.0, & \psi_0 &= 0.0 \\ \delta_s &= \mathbf{0}_{4 \times 1} & & & & \text{(Zero vector of size 4)} \end{aligned}$$

Spacecraft and Environmental Parameters

$$\begin{aligned} I_{xx} &= 10.0, & I_{yy} &= 12.0, & I_{zz} &= 9.0 \\ I_{xy} &= 0.0, & I_{xz} &= 0.0, & I_{yz} &= 0.0 \\ \mu &= 3.986 \times 10^{14} \text{ m}^3/\text{s}^2 & & & \text{(Gravitational parameter)} \\ r_{\text{orbit}} &= 7.0 \times 10^6 \text{ m} & & & \text{(Orbit radius)} \\ \mathbf{T}_{\text{cmg}} &= \begin{bmatrix} 1 \\ 1 \\ 0 \end{bmatrix} & & & \text{(CMG torque)} \end{aligned}$$

Initial Position and Velocity

$$\begin{aligned} x_0 &= 0.0, & y_0 &= 0.0, & z_0 &= 7.0 \times 10^6 \text{ m} \\ v_{\text{circ}} &= \sqrt{\frac{\mu}{r_{\text{orbit}}}} & & & \text{(Circular orbit speed)} \\ v_{\text{elip}} &= \sqrt{\mu \left(\frac{2}{r_{\text{orbit}}} - \frac{1}{7.5 \times 10^6} \right)} & & & \text{(Elliptical orbit speed)} \\ v_{x_0} &= v_{\text{circ}} \cos(0.3), & v_{y_0} &= v_{\text{circ}} \sin(0.3), & v_{z_0} &= 0.0 \end{aligned}$$

Atmospheric and Spacecraft Properties

$$\begin{aligned} C_d &= 2.2 & & & \text{(Drag coefficient)} \\ A &= 4 \text{ m}^2 & & & \text{(Cross-sectional area)} \\ m &= 500 \text{ kg} & & & \text{(Mass of spacecraft)} \\ P &= 1.57 \times 10^{-5} & & & \text{(Atmospheric pressure)} \\ T_{\text{atm}} &= 2000 \text{ K} & & & \text{(Atmospheric temperature)} \end{aligned}$$

Thermospheric Parameters

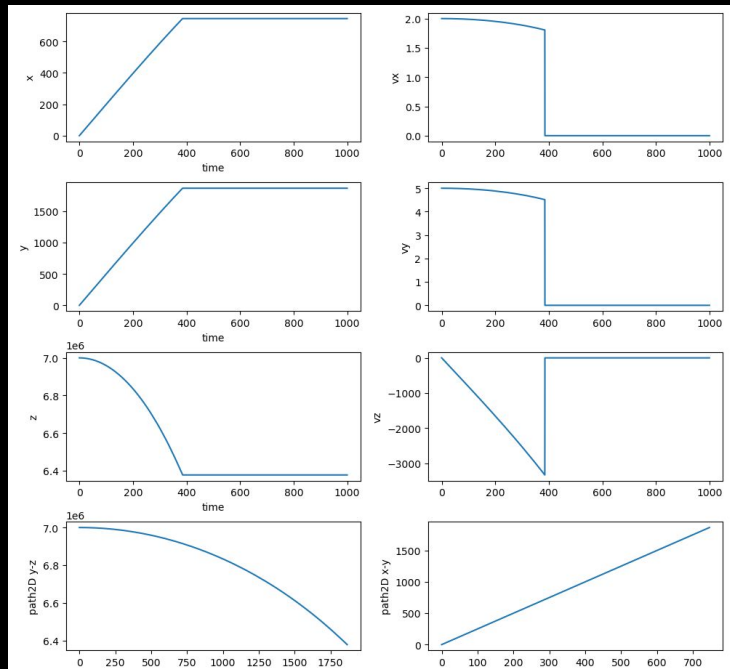
$$\begin{aligned} m_{\text{mol}} &= 2.66 \times 10^{-26} \text{ kg} & & & \text{(Molecular mass)} \\ k_B &= 1.380649 \times 10^{-23} \text{ J/K} & & & \text{(Boltzmann constant)} \\ \rho_{\text{therm}} &= 4 \times 10^{-10} \text{ kg/m}^3 & & & \text{(Density)} \\ h_0 &= 400 \text{ km}, & H &= 70 \text{ km} & \text{(Scale height)} \end{aligned}$$

Integration Settings

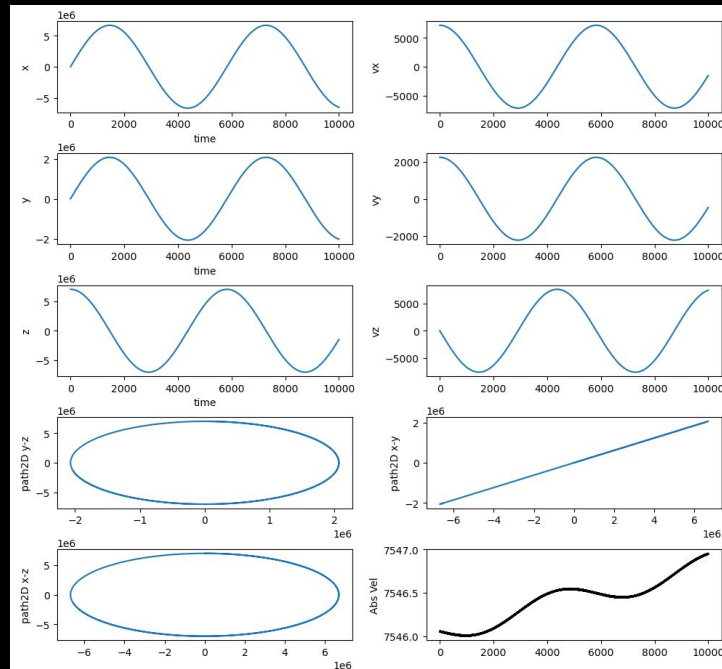
$$\begin{aligned} \Delta t &= 0.1 \text{ s} & & & \text{(Time step)} \\ N_{\text{steps}} &= 100000 & & & \text{(Number of integration steps)} \end{aligned}$$

Simulation results - 1

Orbital dynamics



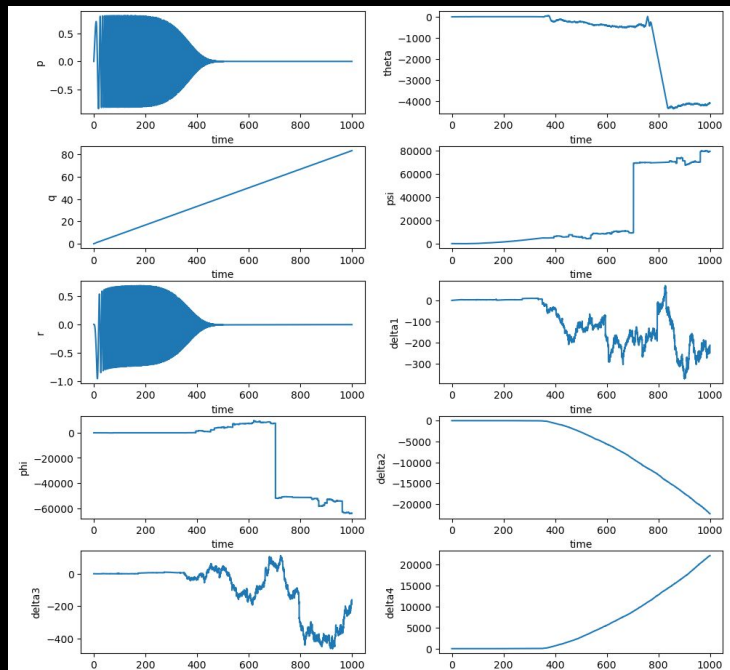
Negligible tangential
velocity, free fall



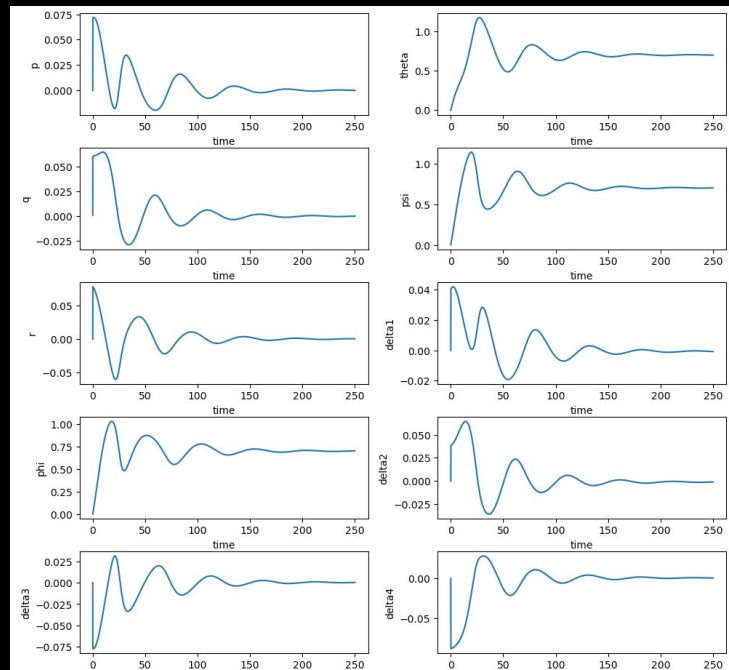
Balanced initial orbital
velocity, elliptical orbit

Simulation results - 2

Attitude dynamics and PD controller



No controller, static
initial conditions



PD controller,
untuned

Considerations and TODOs

Considerations:

Attitude System:

- Modeled with a static inertial frame and constant atmospheric conditions (fixed pressure and density).
- Torques and dynamics are referenced to both the body frame and LVLH frame.

Orbital System:

- Modeled using a static inertial Earth frame with a constant atmospheric model.
- Forces and dynamics are expressed in the inertial frame with outputs in Cartesian coordinates.

Future Enhancements (TODO):

Perturbations:

- Incorporate additional effects such as aerodynamic/magnetic torques, solar radiation pressure, and Gaussian noise.

Simulation & Visualization:

- Shift to ROS2 for real-time, live visualization as the solver processes the equations.

Model Complexity:

- Consider more complex body shapes and inertia parameters; include rotational inertial frames for both systems.

Controller Improvements:

- Add an NMPC controller for attitude adjustments using CMGs (and later thrusters).
- Implement a controller for orbital altitude regulation once thrusters/engines are integrated.
- Merge attitude dynamics with orbital models for comprehensive control.

Control System Tuning:

- Use root-locus and bode-plot analyses to design compensators and fine-tune PID controller performance.

Thank You