Control over CAN and Flexray

Embedded Control Systems

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Contents

Introduction

Chapter 1

Part 1

1.1 Introduction

1.2 Response Time analysis

1.2.1 Response time analysis per processing unit

Table 1.1: By running the Matlab script ResponsetimeAnylsis_FPP.m with the different parameters given for PU1 and PU2 these response times are obtained for each of the tasks. These files are then delivered as PU1.m PU2.m

PU1	T_1	T_2	T_3	T_4 (T_s)
Matlab (ms)	0.1	2.1	4.1	7.2

PU2	T_5	T_6	T_7	T_8
Matlab (ms)	6	3	9	5

1.2.2 Response time analysis for the CAN bus messages

Table 1.2: Response times for the CAN bus messages

CAN	m_2	m_1	m_3	m_8
Matlab (ms)	2	3	4	4

1.3 System Model Derivation and Control Parameter Design

The objectives for the controller is to properly control the given system with a set of design parameters. These parameters, shown in Table

There are namely a number of steps taken until all parameters can be considered to satisfy the performance constraints of the controller. These basic steps can be seen in the following list.

1. Step 1: Derive the system model. Determine the A, B and C matrices in relation to all constants by hand calculations. We are already provided with the matrices in assignment description, hence no need to derive.Insert this into Matlab.

2. Step 2: Derive the values for sampling period and sensor-to-actuator delay based on our system design.

3. Step 3: Choosing desired poles according to the given requirements. Verfiying the controllability of the system for the choosen values. Computing the controller Feed-Forward and Feed-Back gains F and K. Inserting these calculations into MATLAB. More about this step can be found in Section

4. Step4: Design K and F values, compute current input activation(u) and outputs(x) from equations, insert these calculations to MATLAB and simulate the system.

5. Step5: Apply multi-objective genetic algorithm on the above system, with pole positions as parameters, and settling-time and maximum input voltage as our objectives. Obtain pareto optimal points satisfying design constraints.

Table 1.3: Constants and design parameters referenced to in calculations

Symbol	Description	Value	Unit
θ	Rotor position	-	rad
i_m	Motor current	-	A
J	Inertia	$3.2284 \cdot 10^{-6}$	Kgm^2
b	Friction coefficient	$3.5077 \cdot 10^{-6}$	Nms/rad
R	Armature Resistance	4	Ohm
L	Inductance of Motor Winding	$2.75 \cdot 10^{-6}$	H
K_m	Motor constant	0.0274	Nm/A
K	Feed-BackGain	-	-
F	Feed-Forward Gain	-	-

1.3.1 Controller Structure

The system can be described with the second order differential equation shown in Equation 1.1 as given in the assignment description. Equation 1.2 and Equation 1.3 describe the statespace representation of our system. From these equations the Feedback- and Feedforward gain can be determined in relations to the constants in the system.

$$\boldsymbol{x} = \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} = \begin{bmatrix} \theta \\ \dot{\theta} \\ i \end{bmatrix} = \begin{bmatrix} \theta \\ \omega \\ i \end{bmatrix} \quad \text{and} \quad \dot{\boldsymbol{x}} = \begin{bmatrix} \dot{\theta} \\ \ddot{\theta} \\ \dot{i} \end{bmatrix} \tag{1.1}$$

$$\dot{\boldsymbol{x}} = \mathbf{A}\boldsymbol{x} + \mathbf{B}u \text{ and } y = \mathbf{C}\boldsymbol{x} \qquad \text{where} \quad \text{input: } u = V \quad \text{, output: } y = i \tag{1.2}$$

$$\dot{\boldsymbol{x}} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & \frac{-b}{J} & \frac{K_m}{J} \\ 0 & \frac{-K_m}{L} & \frac{-R}{L} \end{bmatrix} \begin{bmatrix} \theta \\ \omega \\ i \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ \frac{1}{L} \end{bmatrix} V \quad \text{and} \quad y = \begin{bmatrix} 1 & 0 & 0 \end{bmatrix} \begin{bmatrix} \theta \\ \omega \\ i \end{bmatrix} \tag{1.3}$$

1.3.2 Controller Design

In this subsection we discuss the method for designing the controller design parameters FeedbackGain-K and FeedForwardGain-F. In this problem we have the scenario where $D_c < h$. Since our controller operates in discrete sample time, we start with converting our continuous system as described in equation 1.4 into discrete domain. Therefore on applying ZOH sampling with period h_c and constant sensor-actuator Delay D_c we achieve the equation 1.5 for discrete sample time system. From 1.5 we can notice that the next output not only depends on current input but also on previous input. Hence, we simplify the system and get it into standard form representing equation 1.6 by invoking equation1.7. After applying above simplification input

$u[k]$ can be represented in terms of controller gains using equation1.8. and matrices Φ ,C are converted to corresponding augmented matrices Φ_{aug},C_{aug}, whereas Γ_1,Γ_2 are converted to single augmented matrix Γ_{aug}.

$$\dot{x} = Ax + Bu \quad \text{and} \quad y = Cx \tag{1.4}$$

$$x[k+1] = \phi x[k] + \Gamma_1(D_c)u[k-1] + \Gamma_0(D_c)u[k] \quad \text{and} \quad y[k] = Cx[k] \tag{1.5}$$

$$x[k+1] = \phi z[k] + \Gamma_{aug}u[k] \quad \text{and} \quad y[k] + C_{aug}z[k] \tag{1.6}$$

$$z[k] = \begin{bmatrix} x[k] \\ u[k-1] \end{bmatrix} \tag{1.7}$$

$$u[k] = Kz[k] + Fr \tag{1.8}$$

$$K = -[\ 0\ 0\ \cdots\ 1\ ]\gamma_{aug}^{-1}H(\phi_{aug}) \tag{1.9}$$

$$F = \frac{1}{C_{aug}(I - \phi_{aug} - \Gamma_{aug}K)^{-1}\Gamma_{aug}} \tag{1.10}$$

Before deriving the controller gains it is important to verify if the system is controllable under given configuration. This can be verified by calculating $det(\gamma_{aug})$. If the determinent is not equal to 0, then system is controllable. After verifying the controllability of the system K can be derived by applying Ackermanns formula described in equation 1.9 and F can be derived from equation 1.10 . However, one can notice the matrix $H(\Phi_{aug})$ depends on the desired poles which in turn depends on the design requirements. The desired poles alter the frequency spectrum of the transfer function of the system and play a significant role in controlling the behavariour of output parameters of the system. Therefore various design requirements such as Overshooot, settling time, boundary ranges of the parameters in the system depends on the desired poles and thus in turn influence controller gains K and F. Following design, work flow has been developed in MATLAB to derive pareto optimal points(pole locations) satisfying design constraints using multi-objective genetic algorithm and one of the optimal point is selected for simluation.

1.4 System model

1.5 Design decision

1.6 Results

Firstly: Response time analysis
Secondly: Control system input and output

Chapter 2

Part 2

2.1 Introduction

Analyzing and confirming broad analysis done on paper and in Matlab allows us to confirm the hypothesis made about the behavior of the CAN bus and its specific tasks. This analyses is in this case done in Inchron, which allows us to explore the real-time behavior of this embedded system in full detail. Some exploration on how the system should work has already been done in Part 1 by feeding the settings of the embedded system to the tool. The settings included is the hierarchy of the Processing Units (PUs) and their tasks which each have different periods, execution time and priority. The tree view, Figure 2.1, shows the details of the hierarchy from the Inchron's perspective.

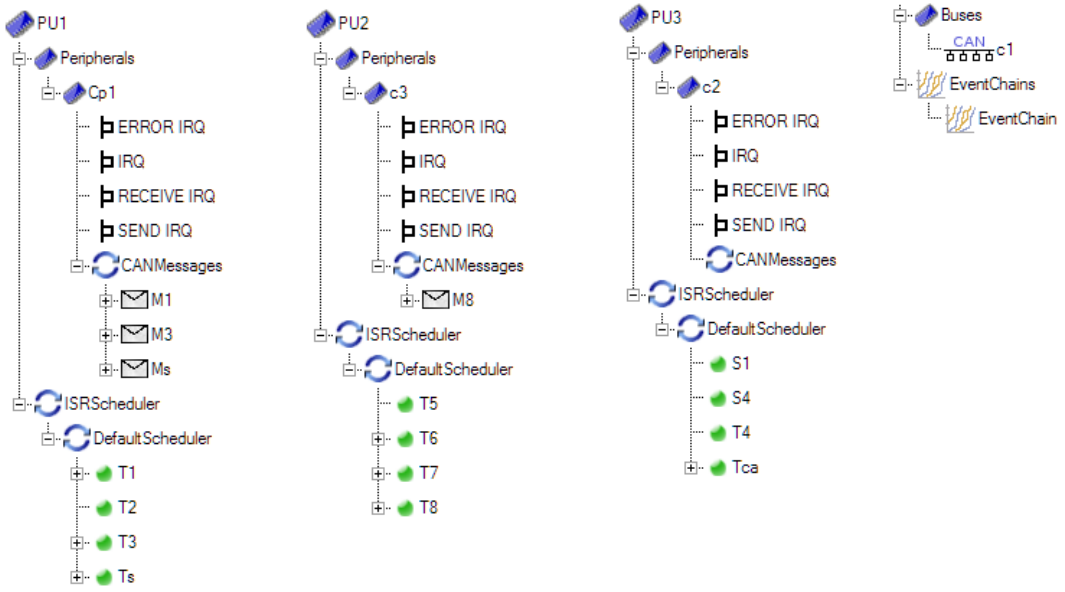

Figure 2.1: This shows the coarse grain hierarchy of the system ported into Inchron for verification and simulation of the real time components of our embedded system.

2.2 Response Time analysis

2.2.1 Response time analysis per processing unit

For this analysis all details have to be imported to Inchron as stated earlier. Now paying special attention to the messages which transfer the packets between controllers which make a full system.

When validating and simulating the model with the settings mentioned in Part 1 and Figure 2.1 and 2.4 we can observer the

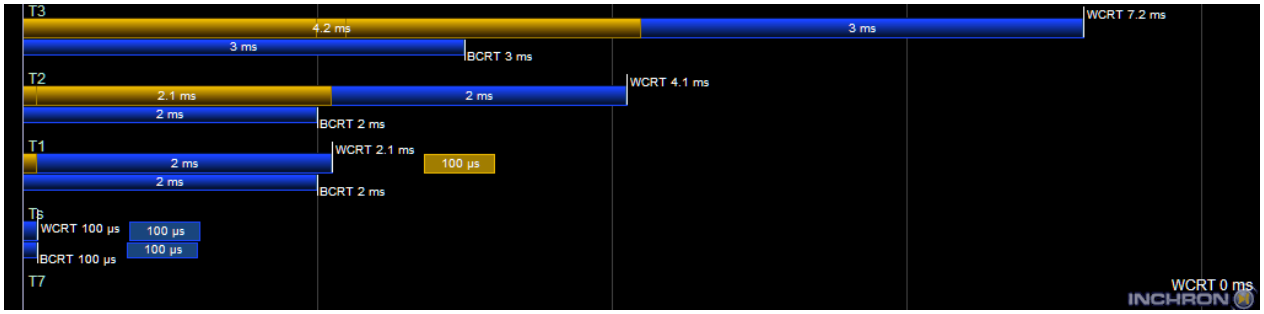

Figure 2.2:

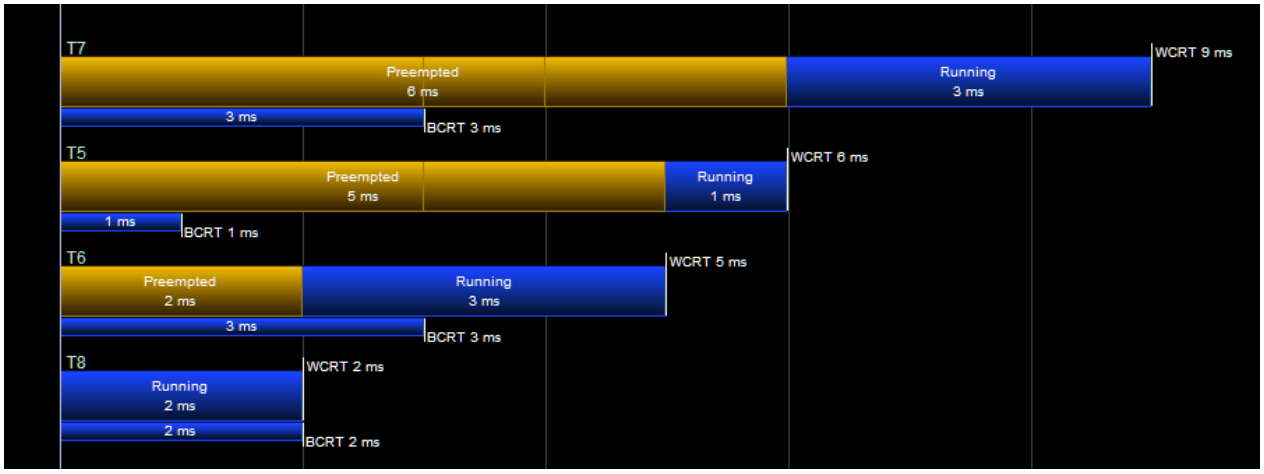

Figure 2.3:

Table 2.1: By running the Matlab script ResponsetimeAnylsis_FPP.m with the different parameters given for PU1 and PU2 these response times are obtained. These files are then delivered as PU1.m PU2.m

PU1	T_1	T_2	T_3	T_4 (T_s)
Matlab (ms)	0.1	2.1	4.1	7.2
Inchron (ms)	0.1	2.1	4.1	7.2

PU2	T_5	T_6	T_7	T_8
Matlab (ms)	6	3	9	5
Inchron (ms)	6	3	9	5

2.2.2 Response time analysis for the CAN bus messages

PU1 amd PU2 are the only units within the system that are sending messages, shown for clarity in Figure 2.4, but PU3 contains the computing and actuating task which will receive the m_s message and mark the end of the sensor to actuator delay.

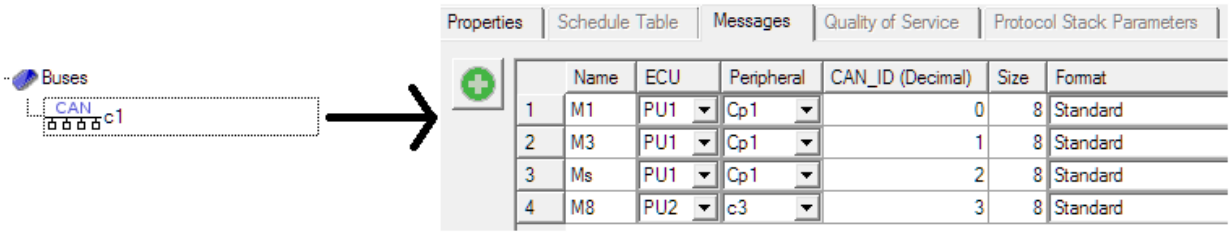

Figure 2.4: To

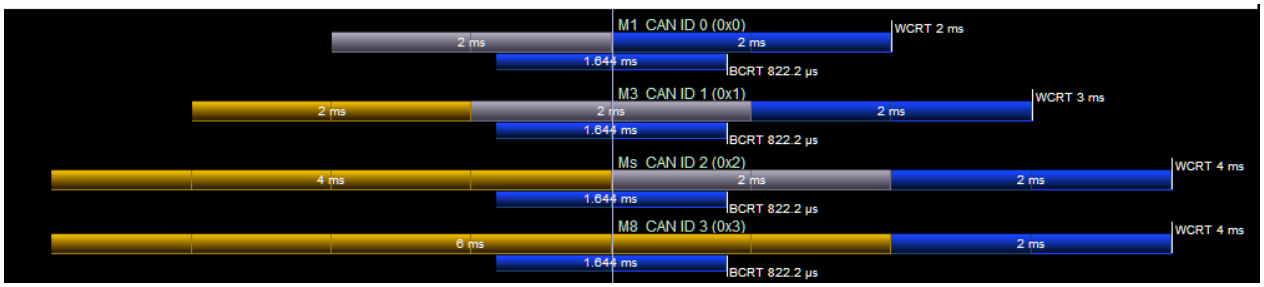

Figure 2.5: To

Table 2.2: Add caption

CAN	m_2	m_1	m_3	m_8
Matlab ms	2	3	4	4
Inchron	2	3	4	4

2.3 Optimisation for sensor-to-actuator delay

2.4 System model

2.5 Design decision

2.6 Results

Firstly: Response time analysis
Secondly: Plots from chronVIEW (before and after optimization)
Last: Control system input and output

2.7 Conclusions

Chapter 3

Part 3

3.1 Introduction

3.2 Answer all the questions

3.2.1 Theoretical analysis versus actual implementation

3.3 Design decision

3.4 Results

Firstly: Solution to the design problem. (Include the parameters you have chosen)
Secondly: from chronVIEW for your design

3.5 Conclusions

3.6 Results

3.7 Conclusion