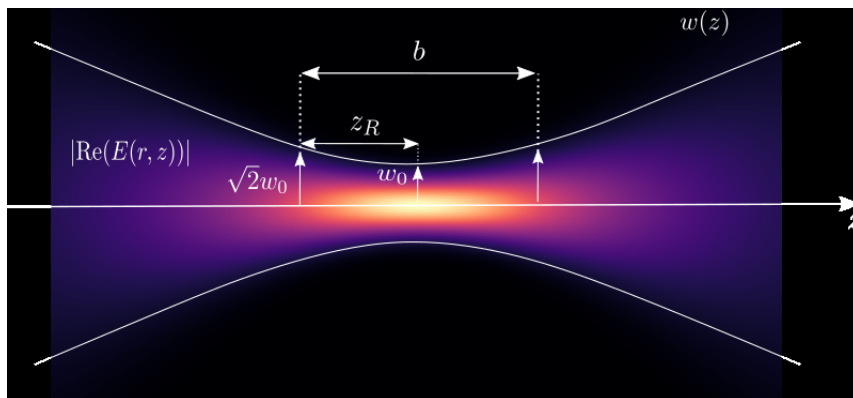

Homework Problem 2



Chiari EVEN
M1 Compuphys 2023

Supervisor : John DUDLEY

March 31, 2023

Contents

1	Plano-Convex Laser Cavity Stability Condition	3
1.1	Question 1:	3
1.2	Question 2:	3
1.3	Question 3 and 4:	4
1.4	Question 5:	5
2	Classical Electron Oscillator Model	6
2.1	Question 1:	6
2.2	Question 2:	7
2.3	Question 3:	8
2.4	Question 4:	8

1 Plano-Convex Laser Cavity Stability Condition

1.1 Question 1:

We consider the following system :

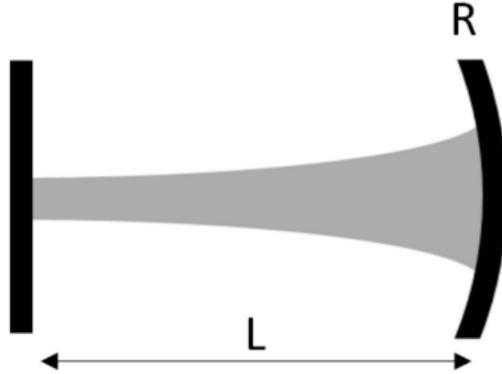


Figure 1: Picture of a Laser cavity consisting of a plane and a concave mirror

We want determine the location of the beam waist in this cavity, we have to show that is given by :

$$w_0^2 = \frac{\lambda}{\pi} \sqrt{L(R-L)} \quad (1)$$

We know that the radius of curvature of a Gaussian beams is given by the formula :

$$R(z) = z \left(1 + \left(\frac{z_r}{z} \right)^2 \right) \quad (2)$$

With $z_r = \frac{\pi w_0^2}{\lambda}$. When the Beam is in $z = L$ the radius of curvature of it is equal to R :

$$R(L) = L \left(1 + \left(\frac{z_r}{L} \right)^2 \right) \quad (3)$$

$$R = L \frac{z_r^2}{L} \quad (4)$$

$$L(R-L) = z_r^2 \quad (5)$$

$$\sqrt{L(R-L)} = \frac{\pi w_0^2}{\lambda} \quad (6)$$

$$w_0^2 = \frac{\lambda}{\pi} \sqrt{L(R-L)} \quad (7)$$

$$(8)$$

1.2 Question 2:

Now we want to verify the stability condition of the previous cavity, we know the stability condition for a Gaussian Beam is $q_s = \frac{Aq_s+B}{Cq_s+D}$ we can find A, B, C, D is our optical system under matrix forms, we start from the concave mirror and we propagate our system until we go back to it :

$$\begin{aligned} \begin{pmatrix} A & B \\ C & D \end{pmatrix} &= \begin{pmatrix} 1 & 0 \\ -2/R & 1 \end{pmatrix} \begin{pmatrix} 1 & L \\ 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & L \\ 0 & 1 \end{pmatrix} \\ \begin{pmatrix} A & B \\ C & D \end{pmatrix} &= \begin{pmatrix} 1 & 0 \\ -2/R & 1 \end{pmatrix} \begin{pmatrix} 1 & 2L \\ 0 & 1 \end{pmatrix} \\ \begin{pmatrix} A & B \\ C & D \end{pmatrix} &= \begin{pmatrix} 1 & 2L \\ -2/R & -4L/R + 1 \end{pmatrix} \end{aligned}$$

We can easily see that the determinant of it is equal to 1. Now we can transform our stability condition to find an inequality :

$$q_s = \frac{Aq_s + B}{Cq_s + D} \quad (9)$$

$$Cq_s^2 + q_s D = Aq_s + D \quad (10)$$

$$C + \frac{D}{q_s} = \frac{A}{q_s} + \frac{B}{q_s^2} \quad (11)$$

$$\frac{B}{q_s^2} + \frac{A - D}{q_s} - C = 0 \quad (12)$$

$$(13)$$

We have a second degree equation with $x = \frac{1}{q_s}$ so we can solve it :

$$\frac{1}{q_s} = \frac{(D - A) \pm \sqrt{(A - D)^2 + 4BC}}{2B} \quad (14)$$

$$\frac{1}{q_s} = \frac{(D - A) \pm \sqrt{A^2 - 2AD + D^2 + 4AD - 4}}{2B} \quad (15)$$

$$\frac{1}{q_s} = \frac{(D - A) \pm \sqrt{(A + D)^2 - 4}}{2B} \quad (16)$$

$$(17)$$

We can easily do the comparison with :

$$\frac{1}{q_s} = \frac{1}{R} - i \frac{\lambda}{\pi w^2} \quad (18)$$

We have to get a complex number on the right of the equation so :

$$(A + D)^2 = 4 \quad (19)$$

$$\frac{A + D}{2} < 1 \text{ and } \frac{A + D}{2} > -1 \quad (20)$$

$$-1 < \frac{A + D}{2} < 1 \quad (21)$$

$$0 < \frac{A + D}{2} + 1 < 2 \quad (22)$$

$$0 < \frac{A + D + 2}{4} < 1 \quad (23)$$

$$0 < \frac{1 - 4L/R + 1 + 2}{4} < 1 \quad (24)$$

$$0 < 1 - L/R < 1 \quad (25)$$

$$-1 < -L/R < 0 \quad (26)$$

$$-R < -L < 0 \quad (27)$$

$$R > L > 0 \quad (28)$$

$$(29)$$

1.3 Question 3 and 4:

Now we can plot the evolution of w_0 over the stability range of L :

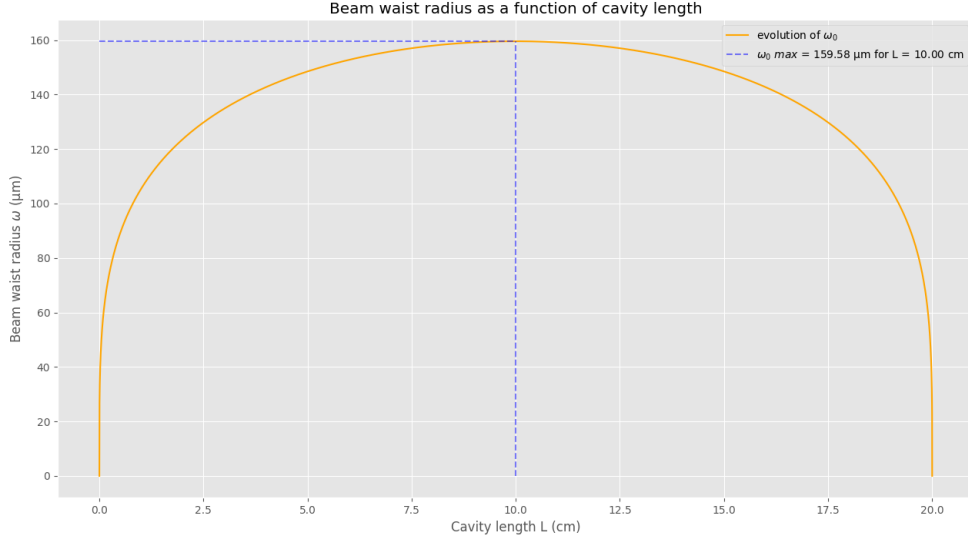
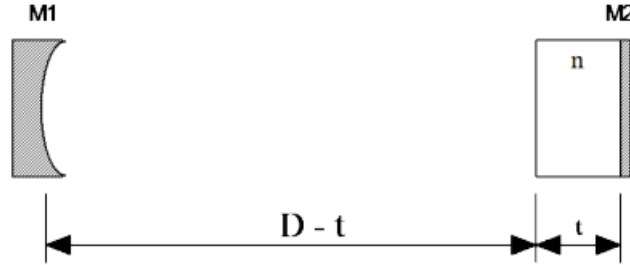


Figure 2: Graph of the evolution of the waist size over the stability range of L

We can see the evolution start with a waist equal to 0 and pass through a maximum at $L = R/2$ and finally collapse to 0 when L goes closer to R. At the maximum the waist size is equal to $w_0 = 24.56 \text{ nm}$ at $L = R/2$.

1.4 Question 5:

Now we want study the stability condition for :



We write our matrix system :

$$\begin{aligned}
 \begin{pmatrix} A & B \\ C & D \end{pmatrix} &= \begin{pmatrix} 1 & 0 \\ -2/R & 1 \end{pmatrix} \begin{pmatrix} 1 & (D-t) \\ 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & t/n \\ 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & t/n \\ 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & (D-t) \\ 0 & 1 \end{pmatrix} \\
 \begin{pmatrix} A & B \\ C & D \end{pmatrix} &= \begin{pmatrix} 1 & (D-t) \\ -2/R & -\frac{2(D-t)}{R} + 1 \end{pmatrix} \begin{pmatrix} 1 & 2t/n \\ 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & (D-t) \\ 0 & 1 \end{pmatrix} \\
 \begin{pmatrix} A & B \\ C & D \end{pmatrix} &= \begin{pmatrix} 1 & 2t/n + (D-t) \\ -2/R & -\frac{4t}{Rn} - \frac{2(D-t)}{R} + 1 \end{pmatrix} \begin{pmatrix} 1 & (D-t) \\ 0 & 1 \end{pmatrix} \\
 \begin{pmatrix} A & B \\ C & D \end{pmatrix} &= \begin{pmatrix} 1 & 2t/n + 2(D-t) \\ -2/R & -\frac{4t}{Rn} - \frac{4(D-t)}{R} + 1 \end{pmatrix}
 \end{aligned}$$

We can easily see that $AD - BC = 1$, now we can show the stability condition :

$$\begin{aligned}
0 &< \frac{A+D+2}{4} < 1 \\
0 &< \frac{1 - \frac{4t}{Rn} - \frac{4(D-t)}{R} + 1 + 2}{4} < 1 \\
0 &< \frac{-\frac{4t}{Rn} - \frac{4(D-t)}{R} + 4}{4} < 1 \\
0 &< -\frac{t}{Rn} - \frac{(D-t)}{R} + 1 < 1 \\
-1 &< -\frac{t}{Rn} - \frac{(D-t)}{R} < 0 \\
R &> \frac{t}{n} + (D-t) > 0 \\
R - \frac{t}{n} &> (D-t) > 0 \\
(D-t) &< R - \frac{t}{n}
\end{aligned}$$

2 Classical Electron Oscillator Model

2.1 Question 1:

In the classical electron oscillator model of an atomic transition, the polarization is defined like $P(\omega) = \epsilon_0 \chi(\omega) E(\omega)$ where $\chi(\omega)$ is the atomic susceptibility defined like :

$$\chi(\omega) = -i \left(\frac{Ne^2}{m\omega_0 \sigma \epsilon_0} \right) \frac{1}{1 + i2 \frac{(\omega - \omega_0)}{\sigma}} \quad (30)$$

We can write it like $\chi(\omega) = \chi'(\omega) - i\chi''(\omega)$:

$$\begin{aligned}
\chi(\omega) &= \left(\frac{Ne^2}{m\omega_0 \sigma \epsilon_0} \right) \frac{-i}{1 + i2 \frac{(\omega - \omega_0)}{\sigma}} = \left(\frac{Ne^2}{m\omega_0 \sigma \epsilon_0} \right) \frac{-i \left(1 - i2 \frac{(\omega - \omega_0)}{\sigma} \right)}{\left(1 + i2 \frac{(\omega - \omega_0)}{\sigma} \right) \left(1 - i2 \frac{(\omega - \omega_0)}{\sigma} \right)} \\
&= \left(\frac{Ne^2}{m\omega_0 \sigma \epsilon_0} \right) \frac{-i - 2 \frac{(\omega - \omega_0)}{\sigma}}{1 - i2 \frac{\omega - \omega_0}{\sigma} + i2 \frac{\omega - \omega_0}{\sigma} + 4 \frac{(\omega - \omega_0)^2}{\sigma^2}} = \left(\frac{Ne^2}{m\omega_0 \sigma \epsilon_0} \right) \frac{-i - 2 \frac{(\omega - \omega_0)}{\sigma}}{1 + 4 \frac{(\omega - \omega_0)^2}{\sigma^2}} \\
&= \left(\frac{Ne^2}{m\omega_0 \sigma \epsilon_0} \right) \frac{-i\sigma^2 - 2 \frac{(\omega - \omega_0)}{\sigma} \sigma^2}{\sigma^2 + 4 (\omega - \omega_0)^2} = \left(\frac{Ne^2}{m\omega_0 \epsilon_0} \right) \frac{-i\sigma - 2 (\omega - \omega_0)}{\sigma^2 + 4 (\omega - \omega_0)^2} \\
&= \left(\frac{Ne^2}{m\omega_0 \epsilon_0} \right) \frac{-i\sigma - 2 (\omega - \omega_0)}{\sigma^2 + 4 (\omega - \omega_0)^2}
\end{aligned}$$

We know $\nu = \omega/2\pi$, so $\nu_0 = \omega_0/2\pi$ and $\Delta\nu = \sigma/2\pi$

$$\begin{aligned}
&= \left(\frac{Ne^2}{m\nu_0 2\pi\epsilon_0} \right) \frac{-i\Delta\nu 2\pi - 2(\nu 2\pi - \nu_0 2\pi)}{(\Delta\nu 2\pi)^2 + 4(\nu 2\pi - \nu_0 2\pi)^2} \\
&= \left(\frac{Ne^2}{m\nu_0 \epsilon_0} \right) \frac{1}{32\pi^3} \frac{-i\Delta\nu 2\pi + 4\pi(\nu_0 - \nu)}{(\Delta\nu/2)^2 + (\nu - \nu_0)^2} \\
&= \left(\frac{Ne^2}{m\nu_0 \epsilon_0} \right) \frac{1}{32\pi^3} \frac{-i\Delta\nu 2\pi + 4\pi(\nu_0 - \nu)}{(\Delta\nu/2)^2 + (\nu - \nu_0)^2} \\
\chi'(v) &= \left(\frac{Ne^2}{m\nu_0 \epsilon_0} \right) \frac{1}{32\pi^3} \frac{4\pi(\nu_0 - \nu)}{(\Delta\nu/2)^2 + (\nu - \nu_0)^2} = \left(\frac{Ne^2}{m\nu_0 8\pi^2 \epsilon_0} \right) \frac{(\nu_0 - \nu)}{(\Delta\nu/2)^2 + (\nu - \nu_0)^2} \\
\chi''(v) &= \left(\frac{Ne^2}{m\nu_0 \epsilon_0} \right) \frac{1}{32\pi^3} \frac{\Delta\nu 2\pi}{(\Delta\nu/2)^2 + (\nu - \nu_0)^2} = \left(\frac{Ne^2}{m\nu_0 16\pi^2 \epsilon_0} \right) \frac{\Delta\nu}{(\Delta\nu/2)^2 + (\nu - \nu_0)^2}
\end{aligned}$$

We can see that we can rewrite $\chi(\nu)$ like $\chi'(\nu) - i\chi''(\nu)$

2.2 Question 2:

Now we want to show that $\Delta\nu$ is the FWHM, first we will evaluate $\chi''(\nu_0)/2$ to have the half maximum, and we will show that we can reach this value in $\nu_0 + \Delta\nu/2$ and $\nu_0 - \Delta\nu/2$:

$$\begin{aligned}
\chi''(\nu_0)/2 &= \left(\frac{Ne^2}{m\nu_0 16\pi^2 \epsilon_0} \right) \frac{\Delta\nu}{2((\Delta\nu/2)^2 + (\nu_0 - \nu_0)^2)} \\
\chi''(\nu_0)/2 &= \left(\frac{Ne^2}{m\nu_0 16\pi^2 \epsilon_0} \right) \frac{\Delta\nu}{2\Delta\nu^2/4} \\
\chi''(\nu_0)/2 &= \left(\frac{Ne^2}{m\nu_0 16\pi^2 \epsilon_0} \right) \frac{2}{\Delta\nu}
\end{aligned}$$

We can evaluate $\chi''(\nu_0 + \Delta\nu/2)$:

$$\begin{aligned}
\chi''(\nu_0 + \Delta\nu/2) &= \left(\frac{Ne^2}{m\nu_0 16\pi^2 \epsilon_0} \right) \frac{\Delta\nu}{(\Delta\nu/2)^2 + (\nu_0 + \Delta\nu/2 - \nu_0)^2} \\
\chi''(\nu_0 + \Delta\nu/2) &= \left(\frac{Ne^2}{m\nu_0 16\pi^2 \epsilon_0} \right) \frac{\Delta\nu}{(\Delta\nu/2)^2 + (\Delta\nu/2)^2} \\
\chi''(\nu_0 + \Delta\nu/2) &= \left(\frac{Ne^2}{m\nu_0 16\pi^2 \epsilon_0} \right) \frac{\Delta\nu}{2\Delta\nu^2/4} \\
\chi''(\nu_0 + \Delta\nu/2) &= \left(\frac{Ne^2}{m\nu_0 16\pi^2 \epsilon_0} \right) \frac{2}{\Delta\nu}
\end{aligned}$$

We can evaluate $\chi''(\nu_0 - \Delta\nu/2)$:

$$\begin{aligned}
\chi''(\nu_0 - \Delta\nu/2) &= \left(\frac{Ne^2}{m\nu_0 16\pi^2 \varepsilon_0} \right) \frac{\Delta\nu}{(\Delta\nu/2)^2 + (\nu_0 - \Delta\nu/2 - \nu_0)^2} \\
\chi''(\nu_0 - \Delta\nu/2) &= \left(\frac{Ne^2}{m\nu_0 16\pi^2 \varepsilon_0} \right) \frac{\Delta\nu}{(\Delta\nu/2)^2 + (-\Delta\nu/2)^2} \\
\chi''(\nu_0 - \Delta\nu/2) &= \left(\frac{Ne^2}{m\nu_0 16\pi^2 \varepsilon_0} \right) \frac{\Delta\nu}{2\Delta\nu^2/4} \\
\chi''(\nu_0 - \Delta\nu/2) &= \left(\frac{Ne^2}{m\nu_0 16\pi^2 \varepsilon_0} \right) \frac{2}{\Delta\nu}
\end{aligned}$$

We can see $\chi''(\nu_0)/2 = \chi''(\nu_0 + \Delta\nu/2) = \chi''(\nu_0 - \Delta\nu/2)$
We have show that $\Delta\nu$ is the FWHM.

2.3 Question 3:

We can study the effect of susceptibility on an incident plan wave because this modify the expression of the wave vector :

$$\vec{E} = \vec{E}_0 e^{i(\omega t - k z)} \text{ with } k' = k \left(1 + \frac{\chi'(\omega)}{2n^2} \right) - ik \frac{\chi''(\omega)}{2n^2} \quad (31)$$

We can replace k by k' :

$$\vec{E} = \vec{E}_0 e^{i(\omega - k' z)} \quad (32)$$

$$= \vec{E}_0 e^{i \left(\omega t - z \left(k \left(1 + \frac{\chi'(\omega)}{2n^2} \right) - ik \frac{\chi''(\omega)}{2n^2} \right) \right)} \quad (33)$$

$$= \vec{E}_0 e^{i\omega t} e^{-izk \left(1 + \frac{\chi'(\omega)}{2n^2} \right)} e^{-zk \frac{\chi''(\omega)}{2n^2}} \quad (34)$$

$$(35)$$

we can see this leads to an additional phase delay (dispersion) that depends on $\chi'(\omega)$ and an absorption term that depends on $\chi''(\omega)$

2.4 Question 4:

Now we have a fours levels system like :

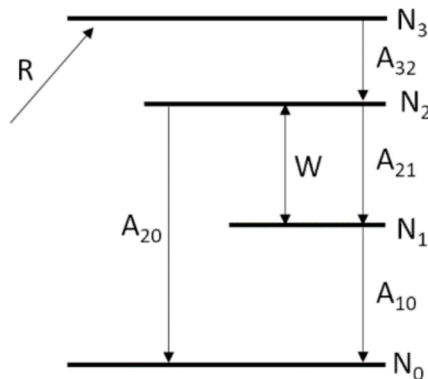


Figure 3: Picture of a fourth system laser

The rate equation for N_1, N_2 are :

$$\frac{dN_2}{dt} = R - W(N_2 - N_1) - N_2(A_{21} + A_{20}) \quad (36)$$

$$\frac{dN_1}{dt} = W(N_2 - N_1) + N_2 A_{21} - N_1 A_{10} \quad (37)$$

We want know the steady state inversion $N_2 - N_1$, we are in steady state so $\frac{dN_i}{dt} = 0$:

$$0 = R - W(N_2 - N_1) - N_2(A_{21} + A_{20}) \implies R = W(N_2 - N_1) + N_2(A_{21} + A_{20}) \quad (38)$$

$$0 = W(N_2 - N_1) + N_2 A_{21} - N_1 A_{10} \quad (39)$$

We can put that under matrix form :

$$\begin{pmatrix} -W & W + A_{21} + A_{20} \\ -W - A_{10} & W + A_{21} \end{pmatrix} \begin{pmatrix} N_1 \\ N_2 \end{pmatrix} = \begin{pmatrix} R \\ 0 \end{pmatrix}$$

We can easily solve that by Cramer's rule :

for N_1 :

$$\begin{aligned} N_1 &= \frac{\begin{vmatrix} R & W + A_{21} + A_{20} \\ 0 & W + A_{21} \end{vmatrix}}{\begin{vmatrix} -W & W + A_{21} + A_{20} \\ -W - A_{10} & W + A_{21} \end{vmatrix}} \\ N_1 &= \frac{R(W + A_{21})}{-W(W + A_{21}) - [(-W - A_{10})(W + A_{21} + A_{20})]} \\ N_1 &= \frac{R(W + A_{21})}{-W^2 - W A_{21} - [-W^2 - W A_{21} - W A_{20} - W A_{10} - A_{10}(A_{21} + A_{20})]} \\ N_1 &= \frac{R(W + A_{21})}{-W^2 - W A_{21} + W^2 + W A_{21} + W A_{20} + W A_{10} + A_{10}(A_{21} + A_{20})} \\ N_1 &= \frac{R(W + A_{21})}{W A_{20} + W A_{10} + A_{10}(A_{21} + A_{20})} \end{aligned}$$

for N_2 :

$$\begin{aligned} N_2 &= \frac{\begin{vmatrix} -W & R \\ -W - A_{10} & 0 \end{vmatrix}}{\begin{vmatrix} -W & W + A_{21} + A_{20} \\ -W - A_{10} & W + A_{21} \end{vmatrix}} \\ N_2 &= \frac{R(W + A_{10})}{W A_{20} + W A_{10} + A_{10}(A_{21} + A_{20})} \end{aligned}$$

Now We can express $N_2 - N_1$:

$$\begin{aligned}
N_2 - N_1 &= \frac{R(W + A_{10})}{WA_{20} + WA_{10} + A_{10}(A_{21} + A_{20})} - \frac{R(W + A_{21})}{WA_{20} + WA_{10} + A_{10}(A_{21} + A_{20})} \\
N_2 - N_1 &= \frac{R(W + A_{10}) - R(W + A_{21})}{WA_{20} + WA_{10} + A_{10}(A_{21} + A_{20})} \\
N_2 - N_1 &= \frac{RW + RA_{10} - RW - RA_{21}}{A_{10}(A_{21} + A_{20}) \left(1 + \frac{WA_{20} + WA_{10}}{A_{10}(A_{21} + A_{20})}\right)} \\
N_2 - N_1 &= \frac{\frac{R(A_{10} - A_{21})}{A_{10}(A_{21} + A_{20})}}{1 + W \frac{(A_{20} + A_{10})}{A_{10}(A_{21} + A_{20})}} = \frac{\Delta N_0}{1 + \frac{W}{W_{sat}}}
\end{aligned}$$

We have $\Delta N_0 = \frac{R(A_{10} - A_{21})}{A_{10}(A_{21} + A_{20})}$ and $W_{sat} = \frac{A_{10}(A_{21} + A_{20})}{(A_{20} + A_{10})}$