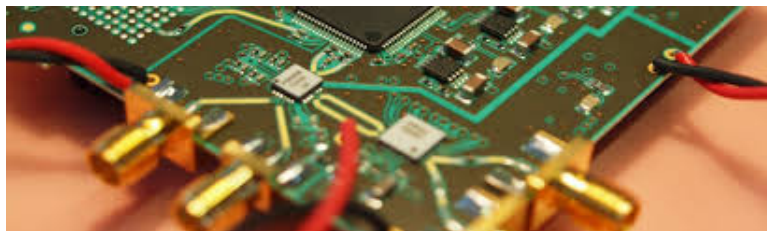


# A Terabit sampling system with a photonics time-stretch ADC

Master Thesis  
of

Olena Manzhura

at the Institute for Data Processing and Electronics (IPE)



Reviewer: Prof. Dr. Anke-Susanne Müller (LAS)  
Second Reviewer: Dr. Michele Caselle (IPE)

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Karlsruhe, den 14.05.2021, \_\_\_\_\_  
Olena Manzhura

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Prof. Dr. Anke-Susanne Müller (LAS)



# Abstract



# **Zusammenfassung**





## Résumé



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# List of abbreviations

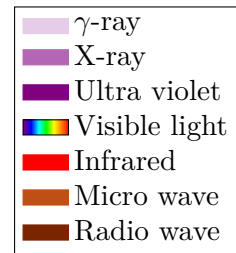
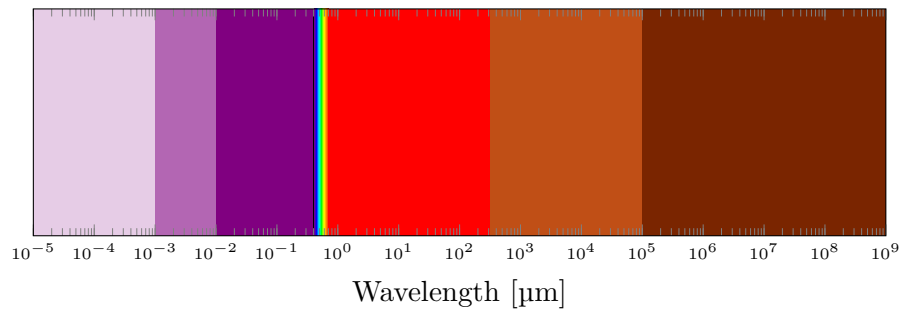
<b>KIT</b>	Karlsruhe Institute of Technology
<b>IPE</b>	Institut für Prozessdatenverarbeitung und Elektronik
<b>KARA</b>	Karlsruhe Research Accelerator
<b>KAPTURE</b>	Karlsruhe Pulse Taking Ultra-fast Readout Electronics
<b>ADC</b>	Analog-To-Digital-Converter
<b>TAH</b>	Track-And-Hold
<b>PLL</b>	Phase-Locked-Loop
<b>DLL</b>	Delay-Locked-Loop
<b>FMC</b>	FPGA Mezzanine Card

# 1. Introduction



## 2. Theoretical Fundamentals

### 2.1. Synchrotron



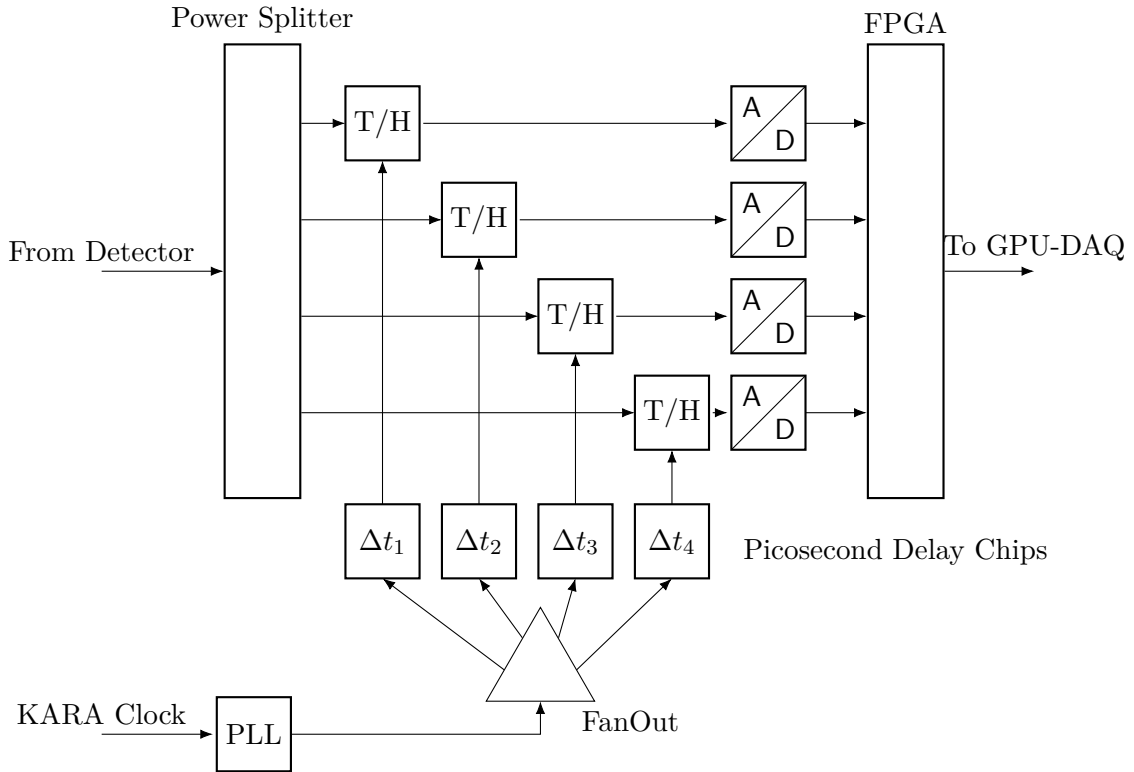
**Figure 2.1.:** Electro-Magnetic spectrum

### 2.1.1. KARA

- Located at the Karlsruhe Institute of Technology (KIT)
- Up to 184 electron packages (bunches) can be filled with a distance between two adjacent bunches of 2 ns
- Operated by the Institute of Beam Physics and Technology (IBPT)

#### 2.1.1.1. KAPTURE-2

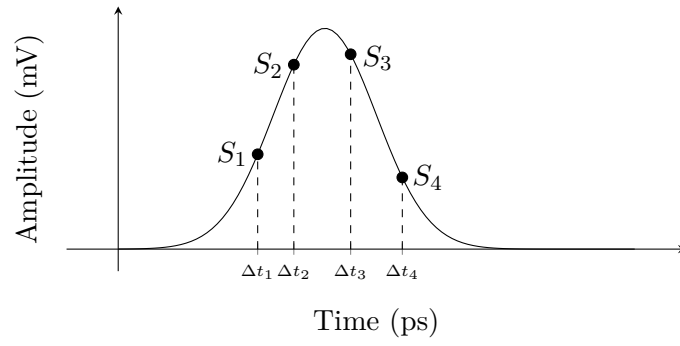
KAPTURE (**K**arlsruhe **P**ulse **T**aking **U**ltra-fast **R**eadout **E**lectronics) is a system – integrated in KARA – designed to continuously sample ultra-short pulses generated by terahertz detectors. The newer version, KAPTURE-2, was designed for more accurate sampling for pulse repetition rates up to 2 GHz. The acquired data is processed by a FPGA and GPU architecture [CAB<sup>+</sup>17]. The general structure of the board is shown in Figure 2.2.



**Figure 2.2.:** General schema of KAPTURE (cf. [CAB<sup>+</sup>17, p.2])

The pulse from the THz detector is fed into a power splitter, which splits the signal into four identical pulses and distributes them to four channels, consisting of a respective Track-And-Hold (TAH) unit and a 12-bit ADC@500 MS/s. The sampling time of each unit can be adjusted individually with a Picosecond Delay Chip with a resolution of 3 ps (maximal delay range: 100 ps). The clock signal is provided by KARA, which is cleared from jitter by a Phase-Locked-Loop (PLL). The clean clock signal is distributed to the delay chips with a fan-out. [CAB<sup>+</sup>17]

This results in the sampling of the signal as shown in Figure 2.3.



**Figure 2.3.:** Signal with sample points

## **2.2. Optical Time Stretching Technique**

### **2.2.1. Applications**

### 2.3. Analog-To-Digital-Converter



## 2.4. New Readout System

### 2.4.1. Xilinx Zynq UltraScale+ RFSoc

### 2.4.2. Requirements

#### Delay chip

The necessary step size for the delay chips, when using 16 ADC@2 GS/s in time-interleaving mode, is:  $\frac{2 \text{ GS/s}}{16} = 31 \text{ ps}$

## 3. Development of the system

### 3.1. Architecture

In a first step, a new front-end board needs to be developed for the new system. This will be plugged onto the Xilinx ZCU216 Evaluation Board.

#### Power Supply for Track-And-Hold amplifiers

For the Track-And-Hold amplifiers a new power supply unit – the ADP1741 (Analog Devices) – should be used. It is necessary to think about the amount of power supply chips needed. As a rule of thumb, the power supply should provide twice the maximum power needed by the components it drives. The power consumption/maximum current for the respective components on the THERESA board is listed in Table 3.1.

**Table 3.1.:** Power consumption of components on the board

Component	$V_{cc}$ (V)	$I_{max}$ (A)	$P_{max}$ (W)	$\#_{parts}$	$I_{tot}^1$ (A)
HMC5649 (T/H-Amplifier)	2	0.221	0.442	16	3.536
	–5	–0.242	1.21		3.872
HMC856 (Delay)	–3.3	0.185	–0.611	16	2.96
HMC987LP5E (Fan-Out)	3.3	0.234 <sup>2</sup>	0.772	2	0.468
LMC0480 (PLL)	3.3	0.590 <sup>3</sup>	1.947	1	0.590
VCXO	3.3	0.03	0.198	1	0.03

<sup>1</sup>for 16 ADCs

<sup>2</sup>All Outputs and RF-Buffer

<sup>3</sup>All CLKs

The maximal current which the ADP1741 can provide @2 V is 2 A. This means, with one Track-And-Hold amplifier requiring a maximal current of 0.221 A, one ADP1741 can handle four units according to the rule mentioned beforehand ( $I_{max\_ADP1741} = 2 \text{ A} > 2 * I_{tot}$ ,  $I_{tot} = 4 \times 0.221 \text{ A} = 0.884 \text{ A}$ ).

#### NB6L295

Dual Channel Programmable Delay Chip.

- Two individual variable delay channels
- Dual Delay: minimal delay 3.2 ns
- Total Delay Range: 3.2 ns to 8.8 ns per Delay Channel
- 11 ps Increments in 511 steps
- 100 ps Typical Rise and Fall Times

### 3.2. PCB-Layout

#### Surface Coplanar Waveguide with Ground

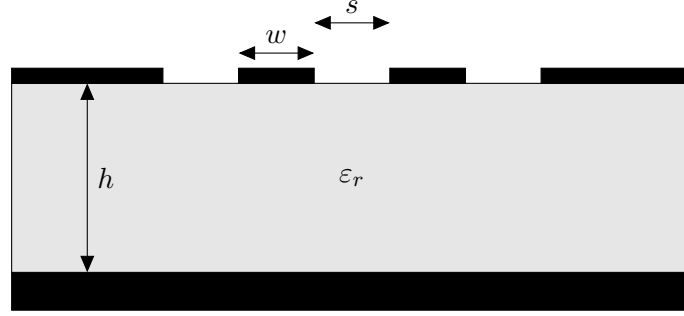


Figure 3.1.: Edge-Coupled Coplanar Waveguide

#### Surface Coplanar Waveguide with Ground

The characteristic impedance of a coplanar waveguide is given as follows [Wad91]:

$$Z_0 = \frac{60.0\pi}{\sqrt{\epsilon_{eff}}} \frac{1.0}{\frac{K(k)}{K(k')} + \frac{K(k_1)}{K(k'_1)}} \quad (3.1)$$

It comprises of the following components, with  $K(k)$  being an elliptical integral of the first kind (see also [BSMM99, p. 430]):

$$k = a/b \quad (3.2)$$

$$k' = \sqrt{1.0 - k^2} \quad (3.3)$$

$$k'_1 = \sqrt{1.0 - k_1^2} \quad (3.4)$$

$$k_1 = \frac{\tanh(\frac{\pi a}{4.0h})}{\tanh(\frac{\pi b}{4.0h})} \quad (3.5)$$

$$\epsilon_{eff} = \frac{1.0 + \epsilon_r \frac{K(k')}{K(k)} \frac{K(k_1)}{K(k'_1)}}{1.0 + \frac{K(k')}{K(k)} \frac{K(k_1)}{K(k'_1)}} \quad (3.6)$$

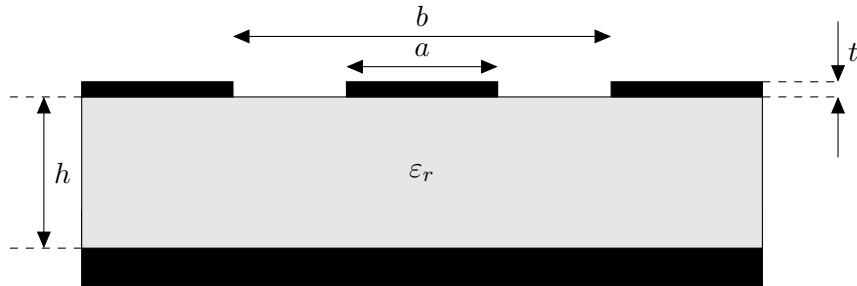


Figure 3.2.: Coplanar Waveguide with Ground

## **4. Conclusions and Outlook**



# Appendix

## A. First Appendix Section

**LVC MOS** Low voltage complementary metal oxide semiconductor

**LVDS** Low-voltage differential signaling

**LVPECL** Low-voltage positive emitter-coupled logic



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