

Objective:

Create a linear power supply that converts 220v AC and 50Hz frequency to variable 0 to 15v DC (3A max)

Process questions:

Is the voltage AC of Tunisia V_{rms} 220V or V_{peak} 220 ?

220v is the V_{rms} and V_{peak} is 311 V

How much optimal voltage AC do I need after the transformer to minimize heat ?

- LM317 needs $V_{in} = V_{out} + 3 \rightarrow V_{in} = 15 + 3 = 18v$
- Bridge rectifier drop 1 each diode so 2V for 1b4b42
- After rectifier + capacitor, the voltage is **not constant**.

So LM317 does **not** see only the peak.

It sees a waveform like:

Top = V_{peak}

Bottom = $V_{peak} - V_{ripple}$

$V_{min} = V_{peak}(\text{after bridge}) - V_{ripple} \geq 18V$

V_{ac} is RMS voltage at transformer so We need to calculate it:

$V_{min} \geq (1.414 * V_{ac} - 2) - V_{ripple}$

$1.414 * V_{ac} = V_{min} + V_{ripple} + 2$

$V_{ac} = (V_{min} + V_{ripple} + 2) / 1.414$

$V_{ac} = (18 + 2 + V_{ripple}) / 1.414$

$V_{ac} \geq (20 + V_{ripple}) / 1.414$

So lets choose a filter capacitor for a maximum load of 3A

$F = 100 \text{ Hz} = 50 * 2$ because of bridge rectifier

$V_{ripple} = I_{(max)} / (f * C)$

$V_{ripple} = 3 / (100 * C)$

$(100 * c) * V_{ripple} = 3$

$100 * C = 3 / V_{ripple}$

$C = 3 / 100 * V_{ripple}$

We gonna Allow a Vripple of 1-2 Vpp!!!

So minimum value of C is

$$C_{\max} = 3 / 100 * V_{\text{ripple}}(\min) = 3 / 100 = 0.03 \text{ F}$$

$$C_{\min} = 3 / 100 * V_{\text{ripple}}(\max) = 3 / 200 = 0.015 \text{ F}$$

So we need a capacitor between 0.03F and 0.015F

We can get capactions in parallel becace $C_{\text{total}} = C_1 + C_2 + \dots + C_n$

So let's choose a 0.03F capacitor with a Vripple 1V

$$\text{So our } V_{\text{ac}} \geq (20 + V_{\text{ripple}}) / 1.414$$

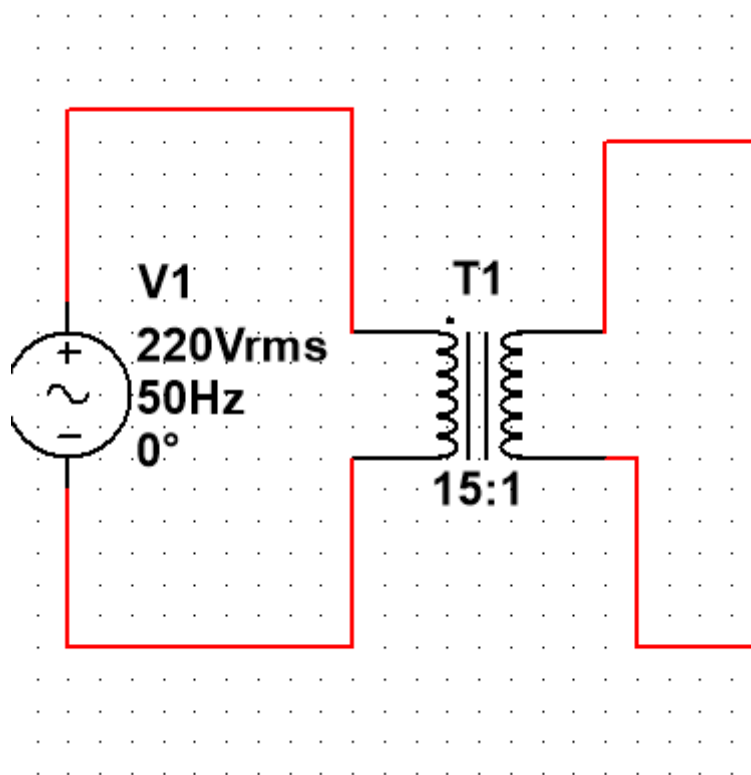
$$V_{\text{ac}} \geq (20 + 1) / 1.414$$

$$V_{\text{ac}} \geq 14.85 \text{ V}$$

So we need at least a 15VAC transformer

$$\text{So the ratio} = V_{\text{in}} / V_{\text{out}} = N_{\text{in}} / N_{\text{out}} = 220 / 15 = 14.6$$

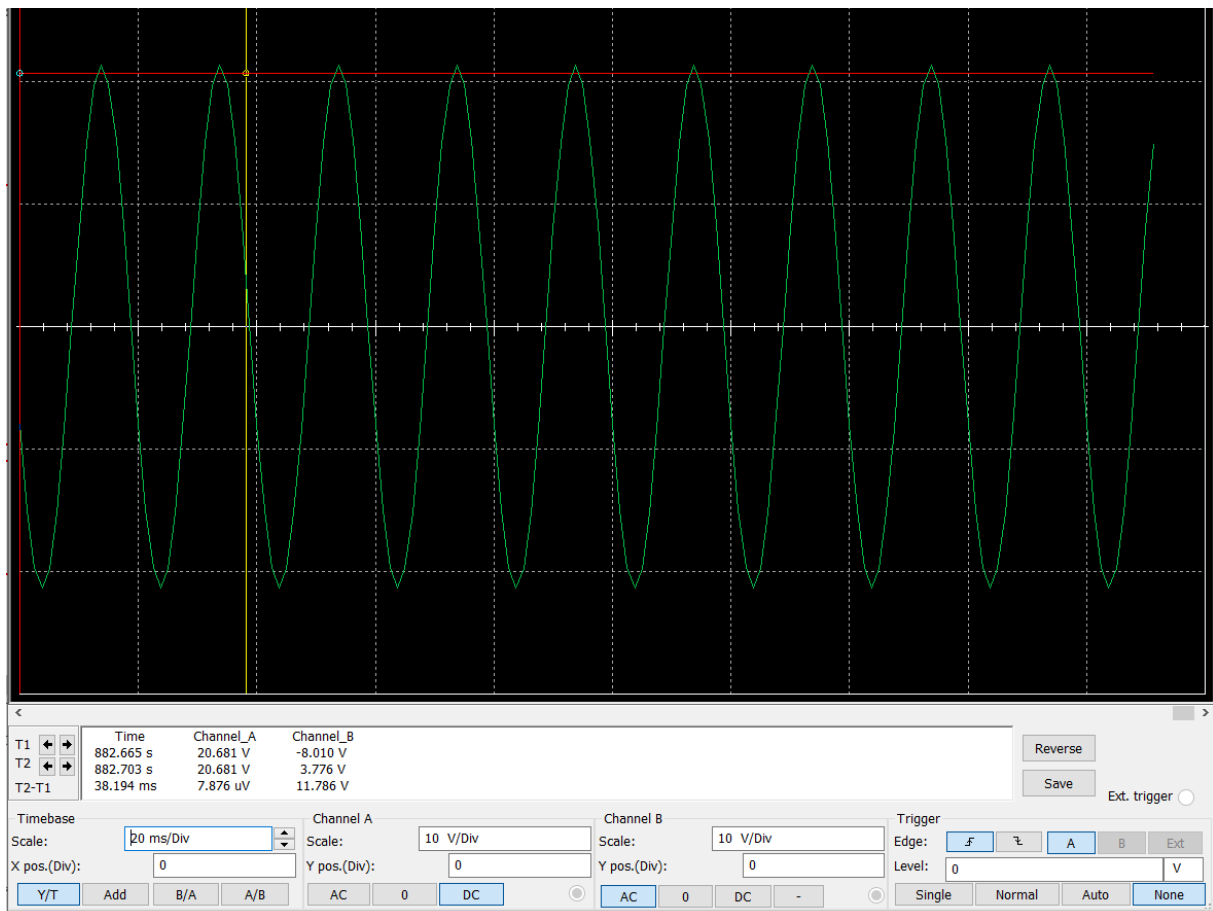
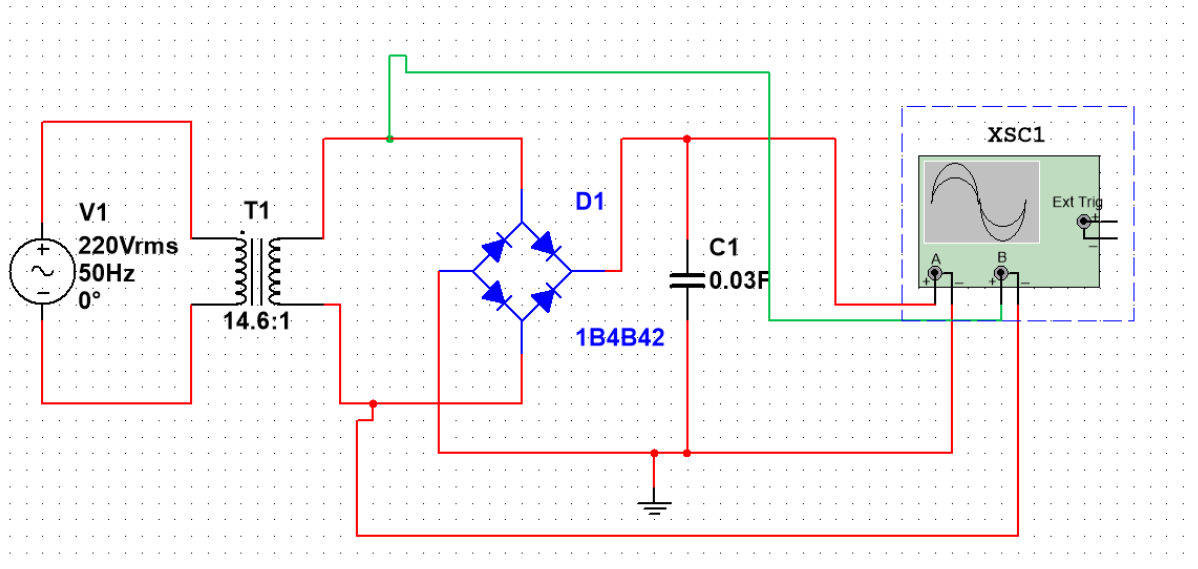
$$N_{\text{in}} = 14.6 \quad N_{\text{out}} = 1$$



Choose a bridge rectifier for AC-DC

So I choose 1B4B42 full wave rectifier

Maximum Instantaneous Forward Voltage per element at $I_F = 1.0 \text{ A} \Rightarrow 1 \text{ V}$



after the capacitor and bridge rectifier the voltage around capacitor is around 20V As expected in calculations

Variable voltage regulator choose?

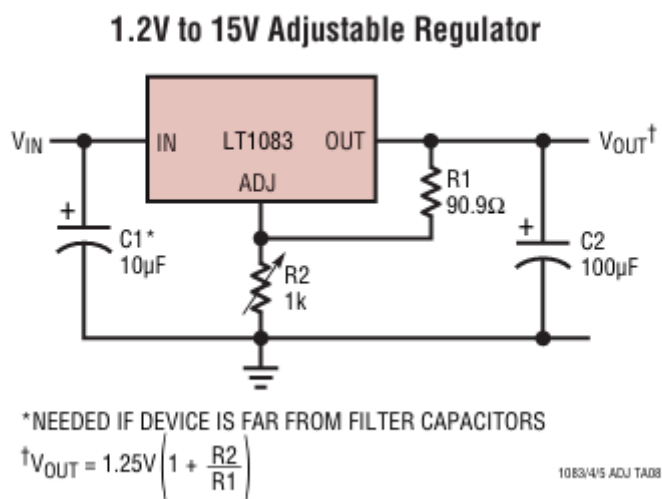
So I choose a LT1083 because It can output 7.5 A and can handle 20v in datasheet

technical-documentation/data-sheets/108345fh.pdf

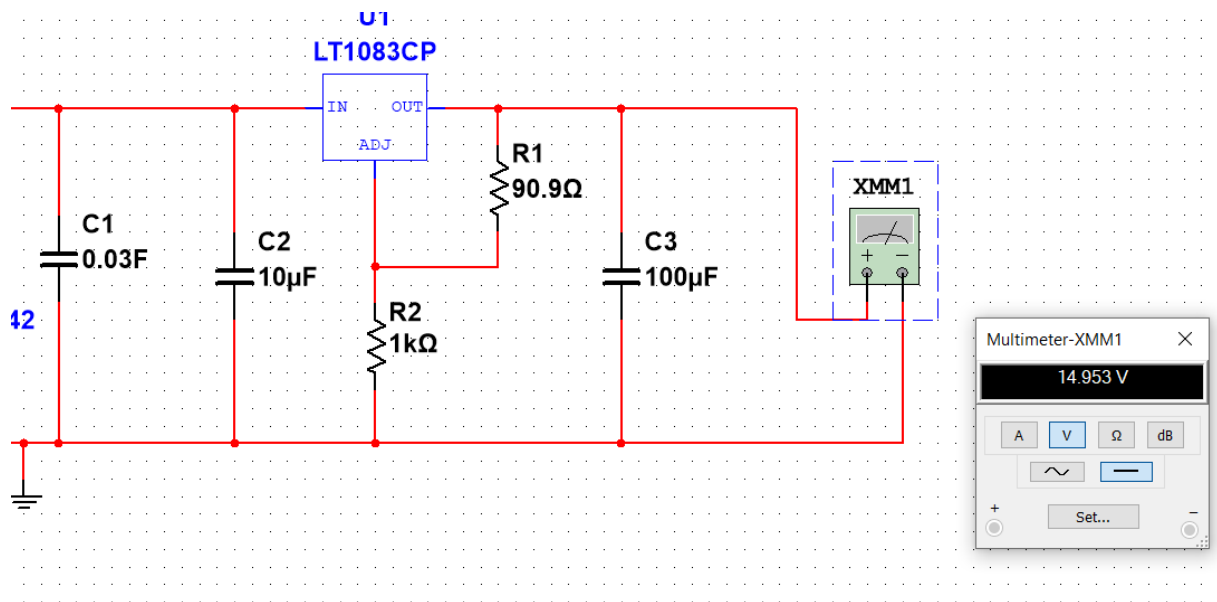
A[®] Demander à Copilot

PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS
Reference Voltage	$I_{OUT} = 10\text{mA}$, $T_J = 25^\circ\text{C}$, $(V_{IN} - V_{OUT}) = 3\text{V}$ $10\text{mA} \leq I_{OUT} \leq I_{FULL_LOAD}$ $1.5\text{V} \leq (V_{IN} - V_{OUT}) \leq 25\text{V}$ (Notes 4, 6, 7)	1.238	1.250	1.262	V
Line Regulation	$I_{LOAD} = 10\text{mA}$, $1.5\text{V} \leq (V_{IN} - V_{OUT}) \leq 15\text{V}$, $T_J = 25^\circ\text{C}$ (Notes 2, 3)	0.015	0.2		%
		0.035	0.2		%
	M-Grade: $15\text{V} \leq (V_{IN} - V_{OUT}) \leq 35\text{V}$ (Notes 2, 3)	0.05	0.5		%
	C-, I-Grades: $15\text{V} \leq (V_{IN} - V_{OUT}) \leq 30\text{V}$ (Notes 2, 3)	0.05	0.5		%
Load Regulation	$(V_{IN} - V_{OUT}) = 3\text{V}$, $10\text{mA} \leq I_{OUT} \leq I_{FULL_LOAD}$, $T_J = 25^\circ\text{C}$ (Notes 2, 3, 4, 6)	0.1	0.3		%
		0.2	0.4		%
Dropout Voltage	$\Delta V_{REG} = 1\%$, $I_{OUT} = I_{FULL_LOAD}$ (Notes 5, 6, 8)	1.3	1.5		V
Current Limit					A
LT1083	$(V_{IN} - V_{OUT}) = 5\text{V}$	8.0	9.5		A
	$(V_{IN} - V_{OUT}) = 25\text{V}$	0.4	1.0		A
LT1084	$(V_{IN} - V_{OUT}) = 5\text{V}$	5.5	6.5		A
	$(V_{IN} - V_{OUT}) = 25\text{V}$	0.3	0.6		A
LT1085	$(V_{IN} - V_{OUT}) = 5\text{V}$	3.2	4.0		A
	$(V_{IN} - V_{OUT}) = 25\text{V}$	0.2	0.5		A
Minimum Load Current	$(V_{IN} - V_{OUT}) = 25\text{V}$	5	10		mA
Thermal Regulation					%/W
LT1083	$T_A = 25^\circ\text{C}$, 30ms Pulse	0.002	0.010		%/W
LT1084		0.003	0.015		%/W
LT1085		0.004	0.020		%/W
Ripple Rejection	$f = 120\text{Hz}$, $C_{ADJ} = 25\mu\text{F}$, $C_{OUT} = 25\mu\text{F}$ Tantalum $I_{OUT} = I_{FULL_LOAD}$, $(V_{IN} - V_{OUT}) = 3\text{V}$ (Notes 6, 7, 8)	60	75		dB
Adjust Pin Current	$T_J = 25^\circ\text{C}$	55	120		μA
Adjust Pin Current Change	$10\text{mA} \leq I_{OUT} \leq I_{FULL_LOAD}$, $1.5\text{V} \leq (V_{IN} - V_{OUT}) \leq 25\text{V}$ (Note 6)	0.2	5		μA
Temperature Stability		0.5			%
Long-Term Stability	$T_A = 125^\circ\text{C}$, 1000 Hrs	0.3	1		%
RMS Output Noise (% of V_{OUT})	$T_A = 25^\circ\text{C}$, $10\text{Hz} \leq f \leq 10\text{kHz}$	0.003			%
Thermal Resistance Junction-to-Case	Control Circuitry/Power Transistor				$^\circ\text{C/W}$
LT1083	K Package		0.6/1.6		$^\circ\text{C/W}$
	P Package		0.5/1.6		$^\circ\text{C/W}$
LT1084	K Package		0.75/2.3		$^\circ\text{C/W}$
	P Package		0.65/2.3		$^\circ\text{C/W}$
	T Package		0.65/2.7		$^\circ\text{C/W}$
LT1085	K Package		0.9/3.0		$^\circ\text{C/W}$
	M, T Package		0.7/3.0		$^\circ\text{C/W}$

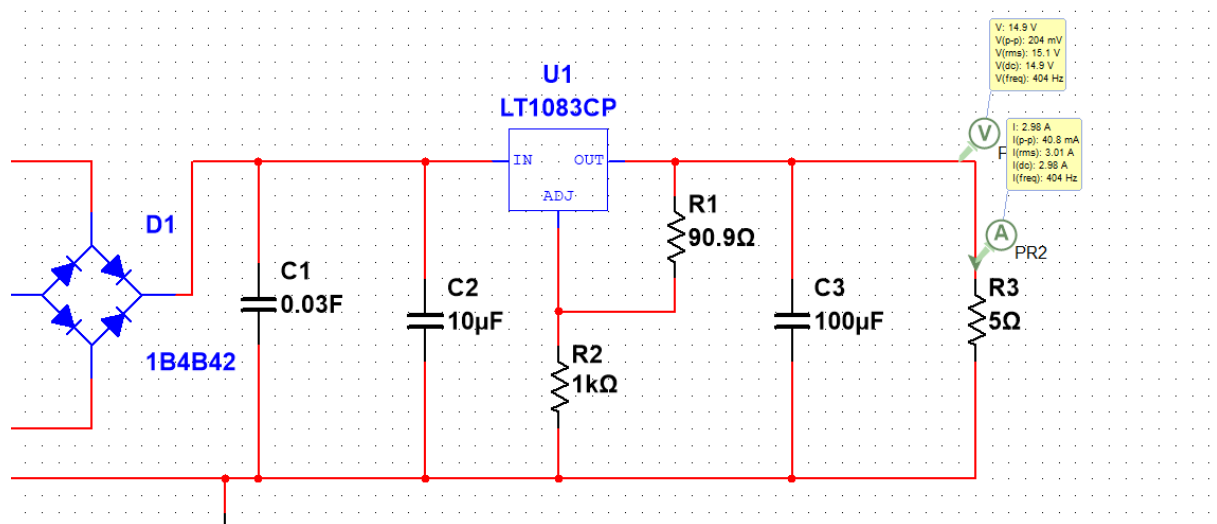
I found the circuit in LT1083 datasheet so lets use it



$$V_{out} = 1.25 \left(1 + \left(\frac{1000}{90.9} \right) \right) = 15\text{V}$$

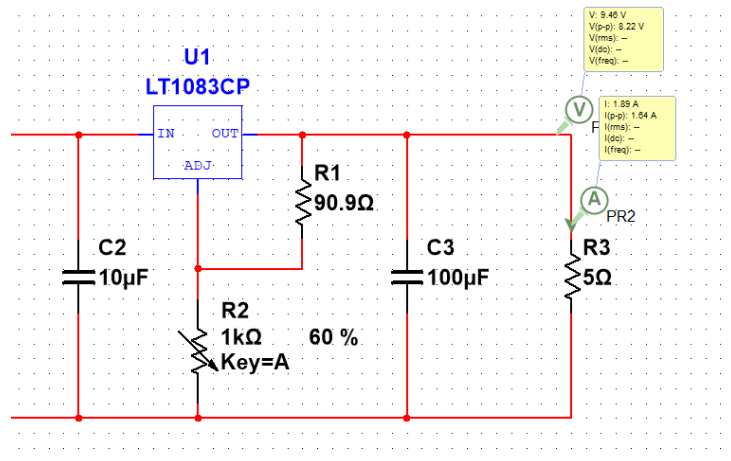


After verification the result is as expected in Multisim



So here a load using a 3A and 15V

We can now make a variable resistor on R2 instead of fixed



Ok now let's check if there is any security issue with this circuit

Security Concern

Human Safety

The transformer have a inductive isolation which is good

- We need to add a fuse on the primary
- We need MOV / surge protection
- We need double insulation

Choose Primary fuse:

$$P_{\text{max of load}} = V \times I = 15 \text{ V} \times 3 \text{ A} = 45 \text{ WATT}$$

Linear supplies are only ~50-80% efficient overall (worse at low output voltages because more voltage is "dropped" as heat in the regulator).

Input power at transformer $\approx P_{\text{dc}} / \text{efficiency}$.

Optimistic (80% eff): $45 \text{ W} / 0.8 = 56.25 \text{ W}$.

Pessimistic (50% eff, e.g., at low V_{out} like 5 V where dropout is high):
 $45 \text{ W} / 0.5 = 90 \text{ W}$.

This gives a rough input power range of ~56-90 W.

Standard rule for bridge rectifier + large cap filter (from sources like the National Semiconductor Handbook and Elliott Sound Products):

Secondary RMS current ($I_{\text{sec_rms}}$) $\approx 1.5\text{--}2 \times I_{\text{dc}}$ (3 A).

The cap charges in short bursts (high peak current) near the AC peaks, but discharges steadily to the load. This "form factor" raises RMS by ~1.57 ideally, but 1.6-1.8 is common in practice; some guides use up to 2 for safety/margin.

$$I_{\text{sec_rms}} \approx 1.5 \times 3 \text{ A} = 4.5 \text{ A (low end)}$$

$$\text{to } 2 \times 3 \text{ A} = 6 \text{ A (high end)}.$$

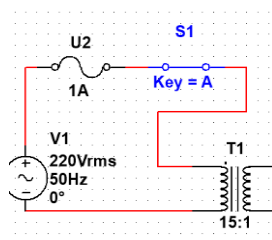
$$\text{Transformer VA} = V_{\text{sec_rms}} \times I_{\text{sec_rms}} \approx 14.6 \text{ V} \times 4.5\text{--}6 \text{ A} = 66\text{--}88 \text{ VA.}$$

Oversize (100- 132)

$$I_{\text{primary_rms}} = \text{VA} / V_{\text{primary_rms}} = \text{VA} / 220 \text{ V}.$$

$$\text{For } 66\text{--}88 \text{ VA: } 66 / 220 \approx 0.3 \text{ A to } 88 / 220 \approx 0.4 \text{ A}.$$

If oversized to 100-132 VA (common for margin/heat): $100 / 220 \approx 0.45 \text{ A}$ to $132 / 220 = 0.6 \text{ A}$.



Safety checklist:

Define Worst-Case Conditions

Ambient temp | 40 °C Load current | MAX continuous Load
type | Resistive / inductive

Good insulation transformer and slow blow fuse

Worst-case secondary voltage

$$220V +10\% = 242V$$

$$242 / 15 = 16.1 \text{ Vrms}$$

$$V_{\text{peak}} = 16.1 \times 1.414 \approx 22.8V$$

$$\text{Bridge drop} \approx 2V$$

$$V_{\text{dc}} \approx 20.8V$$

IN-RUSH CURRENT CHECK

Inrush current at power-on

Worst case: capacitor initially = 0V

$$I_{\text{inrush}} \approx V_{\text{peak}} / (R_{\text{secondary}} + R_{\text{bridge}})$$

If $C > 10,000 \mu\text{F}$ and transformer $> 30 \text{ VA}$ → inrush protection required

Add NTC thermistor (e.g. 5-10 Ω cold)

How to SELECT the NTC (STEP BY STEP)

We need 3 parameters:

Cold resistance (R25)

Current rating

Energy rating (Joules)

Decide acceptable inrush current

$$I_{\text{inrush}} \leq 2 \times I_{\text{nominal}}$$

10A

Calculate required cold resistance

$$R_{\text{ntc}} = V / I$$

$$R_{\text{ntc}} = 22 / 10 \approx 2.2 \Omega$$

2-5 Ω @ 25°C

NTC must survive continuous RMS current:

$$I_{ntc} \geq 1.5 \times I_{load}$$

$$I_{ntc} \geq 7.5 \text{ A}$$

Energy stored in capacitor:

$$E = \frac{1}{2} C V^2$$

$$E = 0.5 \times 0.03 \times 22^2$$

$$E \approx 7.3 \text{ Joules}$$

NTC must handle $\geq 2 \times$ this (safety margin): $> 15\text{J}$

Ametherm SL32 2R025

Parameter	Value	
-----	-----	
R25	**2 Ω **	
Continuous current	**25 A**	
Energy rating	**150 J**	
Diameter	32 mm	

⇒ We add it before generic diode

RECTIFIER CHECK

Current rating

$$I_{rectifier} \geq 1.8 \times I_{load} \text{ (5)}$$

$$I_{rectifier} \geq 9\text{A}$$

Heat check

$$P \approx 2 \times V_f \times I$$

$$P \approx 2 \times 0.9 \times 5 \approx 9 \text{ W}$$

Needs airflow or PCB copper area.

Capacitor C1 rating

$$V_{cap} \geq 1.5 \times V_{dc}$$

$$21.4 \times 1.5 \approx 32\text{V}$$

Ripple current rating (CRITICAL)

$$I_{\text{ripple}} \approx I_{\text{load}} \approx 5 \text{ A}$$

$$I_{\text{ripple_cap}} \geq 1.3 \times I_{\text{load}} \geq 6.5 \text{ A}$$

If not → capacitor overheats → dries → explodes.

Ripple voltage check

$$\Delta V = I / (f \times C)$$

$$\Delta V = 5 / (100 \times 0.03) \approx 1.63 \text{ V}$$

REGULATOR THERMAL CHECK (MOST IMPORTANT)

$$P = (V_{\text{in}} - V_{\text{out}}) \times I$$

$$P = (21.4 - 15) \times 5$$

$$P \approx 32 \text{ W}$$

VERY HIGH

REVERSE PROTECTION OF REGULATOR SO WE ADD A DIODE

Thermal resistance calculation

Max junction temp = 125°C

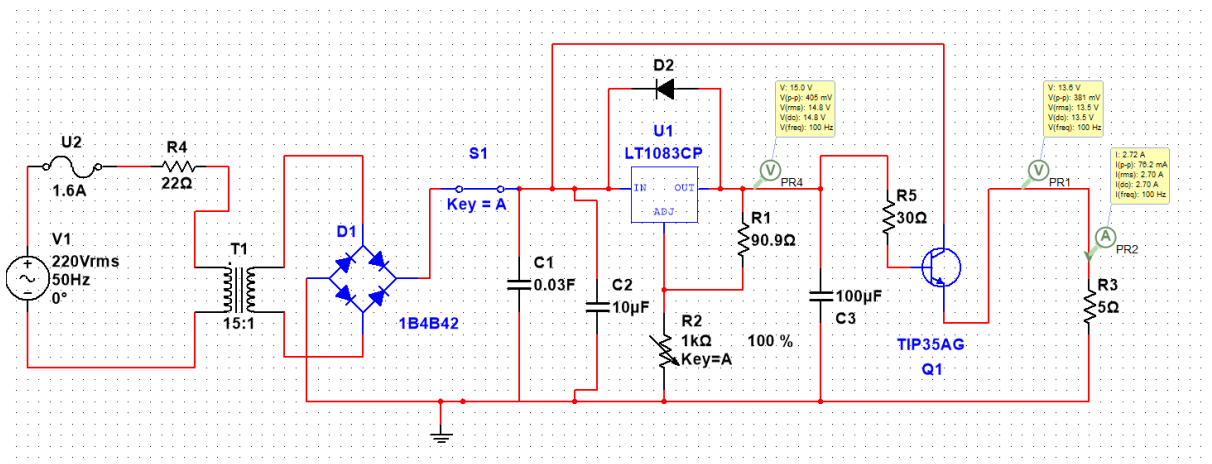
Ambient = 40°C

$$\theta_{\text{total}} \leq (125 - 40) / 22.7$$

$$\theta_{\text{total}} \leq 3.7 \text{ °C/W}$$

Junction-case ≈ 1°C/W Case-sink ≈ 0.5°C/W Remaining for heatsink:

$\theta_{\text{sink}} \leq 2.2 \text{ °C/W}$ **This is a BIG heatsink,**



SO I added a tip35 transistor to reduce heat from voltage regulator

A 22ohm after fuse acting like NTC thermistor

Also a a diode to protect regulator from reverse current