

Objective:

Create a linear power supply that converts 220v AC and 50Hz frequency to variable 0 to 15v DC (3A max)

Process questions:

Is the voltage AC of Tunisia Vrms 220V or Vpeak 220 ?

220v is the Vrms and Vpeak is 311 V

How much optimal voltage AC do I need after the transformer to minimize heat ?

- LM317 needs $V_{in} = V_{out} + 3 \rightarrow V_{in} = 15 + 3 = 18v$
- Bridge rectifier drop 1 each diode so 2V for 1b4b42
- After rectifier + capacitor, the voltage is **not constant**.

So LM317 does **not** see only the peak.

It sees a waveform like:

Top = Vpeak

Bottom = Vpeak - V ripple

$V_{min} = V_{peak}(\text{after bridge}) - V_{ripple} \geq 18V$

V_{ac} is RMS voltage at transformer so we need to calculate it:

$V_{min} \geq (1.414 * V_{ac} - 2) - V_{ripple}$

$1.414 * V_{ac} = V_{min} + V_{ripple} + 2$

$V_{ac} = (V_{min} + V_{ripple} + 2) / 1.414$

$V_{ac} = (18 + 2 + V_{ripple}) / 1.414$

$V_{ac} \geq (20 + V_{ripple}) / 1.414$

So lets choose a filter capacitor for a maximum load of 3A

$F = 100 \text{ Hz} = 50 * 2$ because of bridge rectifier

$V_{ripple} = I (\text{max}) / (f * C)$

$V_{ripple} = 3 / (100 * C)$

$(100 * C) * V_{ripple} = 3$

$100 * C = 3 / V_{ripple}$

$C = 3 / 100 * V_{ripple}$

We gonna Allow a Vripple of 1-2 Vpp!!!

So minimum value of C is

$$C_{max} = 3 / 100 * \text{Vripple(min)} = 3 / 100 = 0.03 \text{ F}$$

$$C_{min} = 3 / 100 * \text{Vripple(max)} = 3 / 200 = 0.015 \text{ F}$$

So we need a capacitor between 0.03F and 0.015F

We can get capacitors in parallel because $C_{total} = C_1 + C_2 + \dots + C_n$

So let's choose a 0.03F capacitor with a Vripple 1V

$$\text{So our } V_{ac} \geq (20 + \text{Vripple}) / 1.414$$

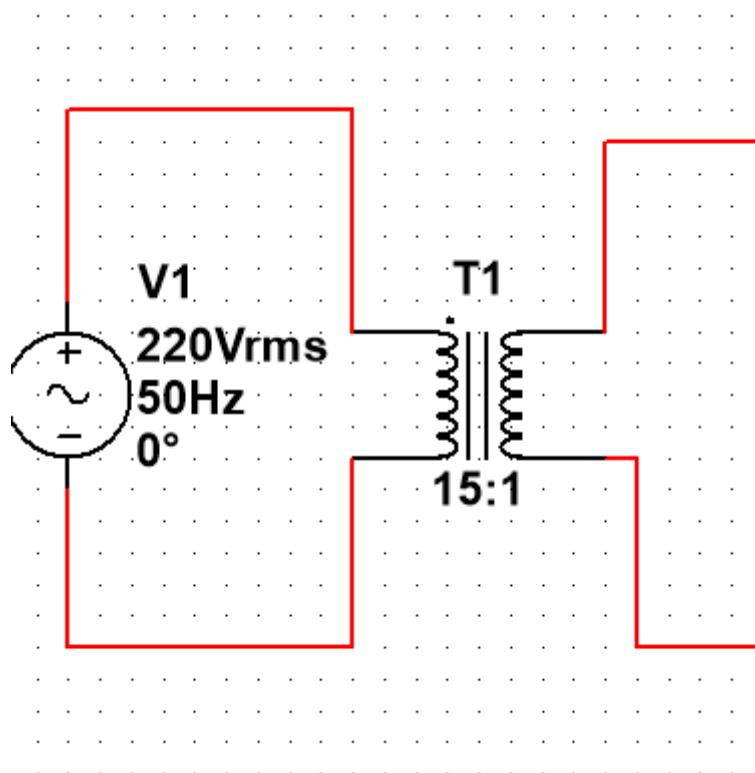
$$V_{ac} \geq (20 + 1) / 1.414$$

$$V_{ac} \geq 14.85 \text{ V}$$

So we need at least a 15VAC transformer

$$\text{So the ratio} = V_{in} / V_{out} = N_{in} / N_{out} = 220 / 15 = 14.6$$

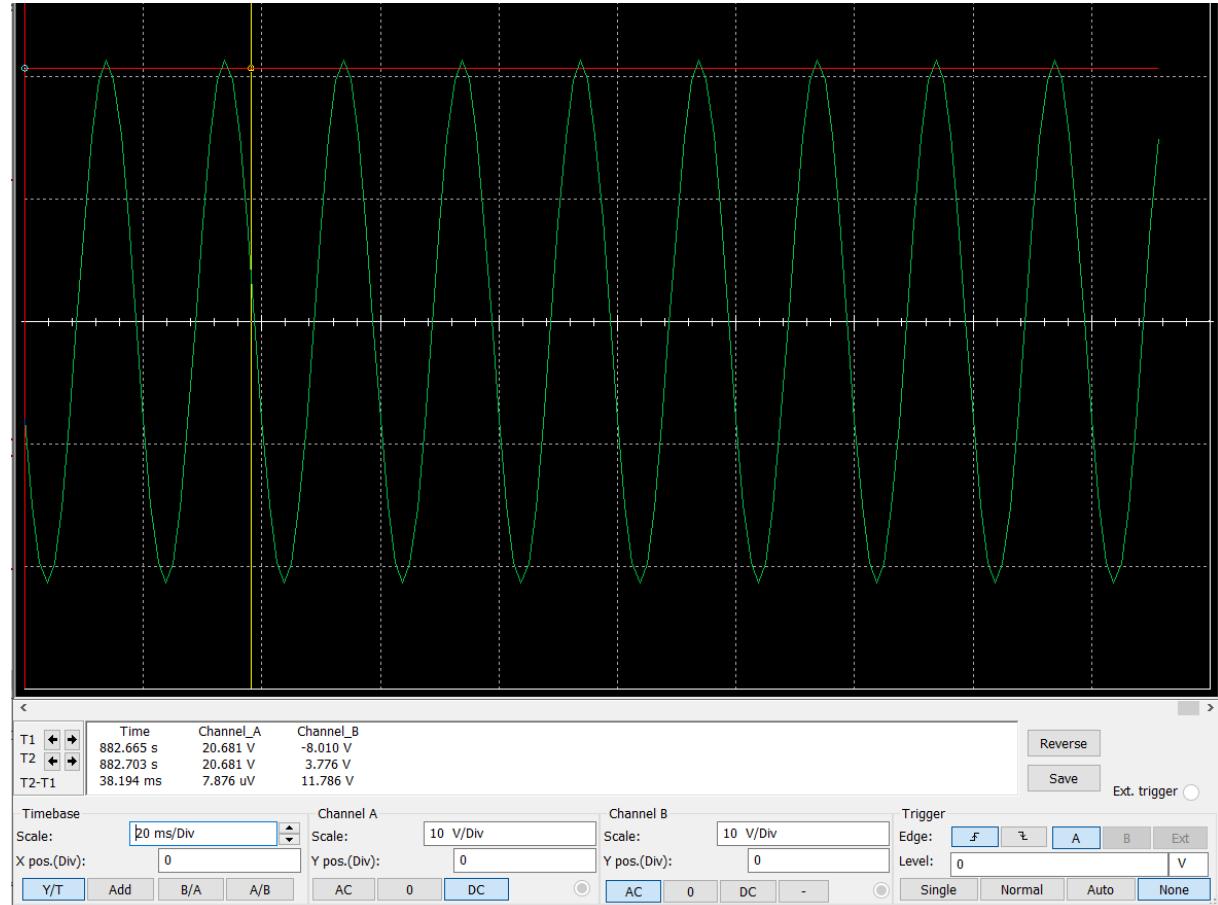
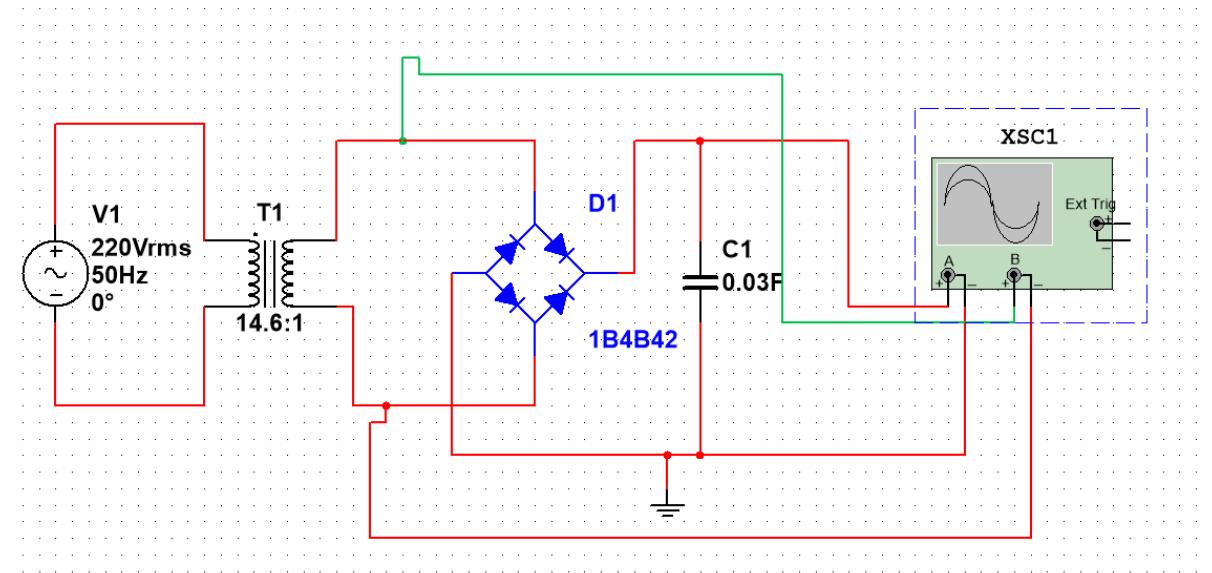
$$N_{in} = 14.6 \quad N_{out}=1$$



Choose a bridge rectifier for AC-DC

So I choose 1B4B42 full wave rectifier

Maximum Instantaneous Forward Voltage per element at IF = 1.0 A => 1V



after the capacitor and bridge rectifier the voltage around capacitor is around 20V As expected in calculations

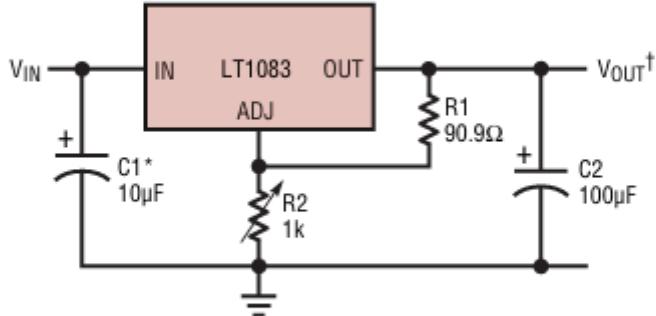
Variable voltage regulator choose?

So I choose a LT1083 because It can output 7.5 A and can handle 20v in datasheet

PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS
Reference Voltage	$I_{QD} = 10mA, T_J = 25^\circ C,$ $(V_{IN} - V_{QUT}) = 3V$ $10mA \leq I_{OUT} \leq I_{FULL_LOAD}$ $1.5V \leq (V_{IN} - V_{QUT}) \leq 25V$ (Notes 4, 6, 7)	1.238 ● 1.225	1.250 ● 1.250	1.262 ● 1.270	V
Line Regulation	$I_{QD} = 10mA, 1.5V \leq (V_{IN} - V_{QUT}) \leq 15V, T_J = 25^\circ C$ (Notes 2, 3)	● 0.015 ● 0.035	0.2 0.2	% %	%
	M-Grade: $15V \leq (V_{IN} - V_{QUT}) \leq 35V$ (Notes 2, 3)	● 0.05	0.5	%	%
C-, I-Grades: $15V \leq (V_{IN} - V_{QUT}) \leq 30V$ (Notes 2, 3)	● 0.05	0.5	%	%	
Load Regulation	$(V_{IN} - V_{QUT}) = 3V, 10mA \leq I_{OUT} \leq I_{FULL_LOAD}, T_J = 25^\circ C$ (Notes 2, 3, 4, 6)	● 0.1 ● 0.2	0.3 0.4	% %	%
Dropout Voltage	$\Delta V_{QD} = 1\%, I_{OUT} = I_{FULL_LOAD}$ (Notes 5, 6, 8)	● 1.3	1.5	V	
Current Limit					
LT1083	$(V_{IN} - V_{QUT}) = 5V$ $(V_{IN} - V_{QUT}) = 25V$	● 8.0 ● 0.4 ● 5.5 ● 0.3 ● 3.2 ● 0.2	9.5 1.0 6.5 0.6 4.0 0.5	A A A A A A	A
LT1084	$(V_{IN} - V_{QUT}) = 5V$ $(V_{IN} - V_{QUT}) = 25V$	● 8.0 ● 0.4 ● 5.5 ● 0.3 ● 3.2 ● 0.2	9.5 1.0 6.5 0.6 4.0 0.5	A A A A A A	A
LT1085	$(V_{IN} - V_{QUT}) = 5V$ $(V_{IN} - V_{QUT}) = 25V$	● 8.0 ● 0.4 ● 5.5 ● 0.3 ● 3.2 ● 0.2	9.5 1.0 6.5 0.6 4.0 0.5	A A A A A A	A
Minimum Load Current	$(V_{IN} - V_{QUT}) = 25V$	● 5	10	mA	
Thermal Regulation	$T_A = 25^\circ C, 30ms$ Pulse		0.002 0.003 0.004	0.010 0.015 0.020	%/W %/W %/W
LT1083					
LT1084					
LT1085					
Ripple Rejection	$f = 120Hz, C_{ADJ} = 25\mu F, C_{OUT} = 25\mu F$ Tantalum $I_{QUT} = I_{FULL_LOAD}, (V_{IN} - V_{QUT}) = 3V$ (Notes 6, 7, 8)	● 60	75	dB	
Adjust Pin Current	$T_J = 25^\circ C$	● 55	120	μA	μA
Adjust Pin Current Change	$10mA \leq I_{OUT} \leq I_{FULL_LOAD}, 1.5V \leq (V_{IN} - V_{QUT}) \leq 25V$ (Note 6)	● 0.2	5	μA	μA
Temperature Stability		● 0.5		%	%
Long-Term Stability	$T_A = 125^\circ C, 1000$ Hrs		0.3	1	%
RMS Output Noise (% of V_{QUT})	$T_A = 25^\circ C, 10Hz \leq f \leq 10kHz$		0.003		%
Thermal Resistance Junction-to-Case	Control Circuitry/Power Transistor				
LT1083	K Package P Package		0.6/1.6 0.5/1.6		°C/W °C/W
LT1084	K Package P Package		0.75/2.3 0.65/2.3		°C/W °C/W
LT1085	T Package K Package M, T Package		0.65/2.7 0.95/3.0 0.7/3.0		°C/W °C/W °C/W

I found the circuit in LT1083 datasheet so lets use it

1.2V to 15V Adjustable Regulator

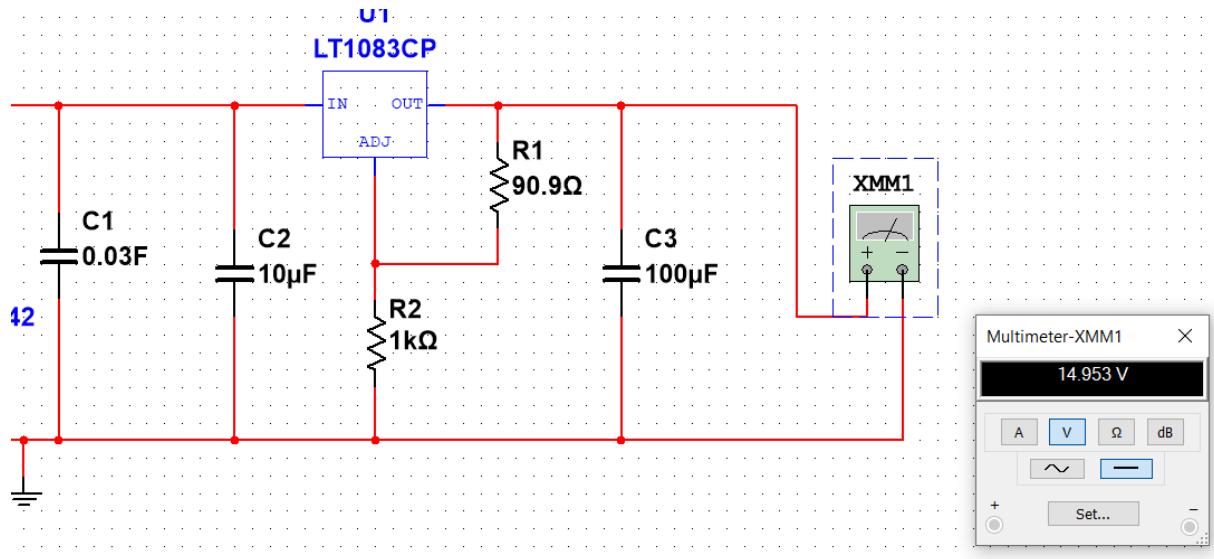


*NEEDED IF DEVICE IS FAR FROM FILTER CAPACITORS

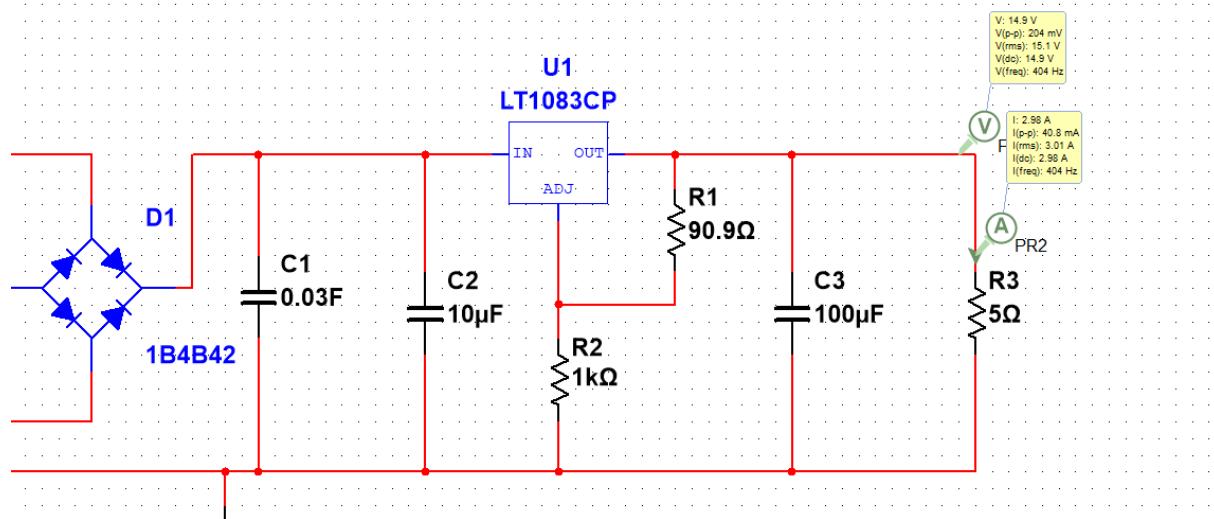
$$\dagger V_{OUT} = 1.25V \left(1 + \frac{R2}{R1} \right)$$

1083/4/5 ADJ TA08

$$V_{out} = 1.25 \left(1 + \frac{1000}{90.9} \right) = 15V$$

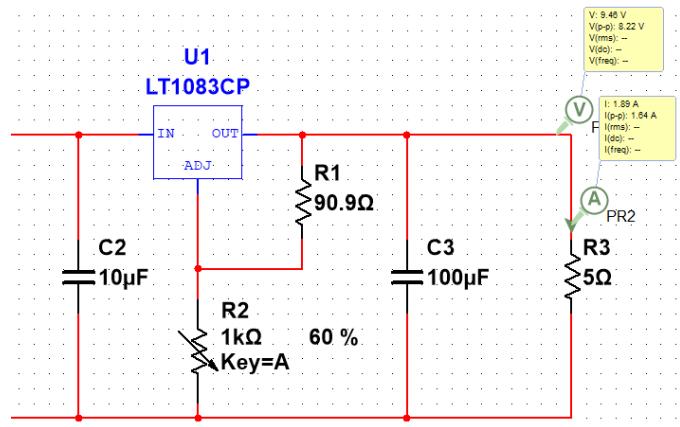


After verification the result is as expected in Multisim



So here a load using a 3A and 15V

We can now make a variable resistor on R2 instead of fixed



Ok now let's check if there is any security issue with this circuit

Security Concern

Human Safety

The transformer have a inductive isolation which is good

- We need to add a fuse on the primary
- We need MOV / surge protection
- We need double insulation

Choose Primary fuse:

$$P_{max} \text{ of load} = V * I = 15 \text{ V} * 3 \text{ A} = 45 \text{ WATT}$$

Linear supplies are only ~50-80% efficient overall (worse at low output voltages because more voltage is "dropped" as heat in the regulator).

Input power at transformer $\approx P_{dc} / \text{efficiency}$.

$$\text{Optimistic (80% eff): } 45 \text{ W} / 0.8 = 56.25 \text{ W.}$$

$$\text{Pessimistic (50% eff, e.g., at low } V_{out} \text{ like 5 V where dropout is high): } 45 \text{ W} / 0.5 = 90 \text{ W.}$$

This gives a rough input power range of ~56-90 W.

Standard rule for bridge rectifier + large cap filter (from sources like the National Semiconductor Handbook and Elliott Sound Products):

$$\text{Secondary RMS current (I_sec_rms)} \approx 1.5-2 \times I_{dc} \text{ (3 A).}$$

The cap charges in short bursts (high peak current) near the AC peaks, but discharges steadily to the load. This "form factor" raises RMS by ~1.57 ideally, but 1.6-1.8 is common in practice; some guides use up to 2 for safety/margin.

$$I_{sec_rms} \approx 1.5 \times 3 \text{ A} = 4.5 \text{ A (low end)}$$

$$\text{to } 2 \times 3 \text{ A} = 6 \text{ A (high end).}$$

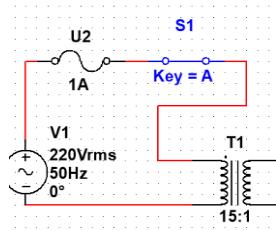
$$\text{Transformer VA} = V_{sec_rms} \times I_{sec_rms} \approx 14.6 \text{ V} \times 4.5-6 \text{ A} = 66-88 \text{ VA.}$$

Oversize (100- 132)

$$I_{primary_rms} = VA / V_{primary_rms} = VA / 220 \text{ V.}$$

$$\text{For 66-88 VA: } 66 / 220 \approx 0.3 \text{ A to } 88 / 220 \approx 0.4 \text{ A.}$$

$$\text{If oversized to 100-132 VA (common for margin/heat): } 100 / 220 \approx 0.45 \text{ A to } 132 / 220 = 0.6 \text{ A.}$$



Safety checklist:

Define Worst-Case Conditions

Ambient temp | 40 °C Load current | MAX continuous
type | Resistive / inductive Load

Good insulation transformer and slow blow fuse

Worst-case secondary voltage

$$220V +10\% = 242V$$

$$242 / 15 = 16.1 \text{ Vrms}$$

$$V_{peak} = 16.1 \times 1.414 \approx 22.8V$$

$$\text{Bridge drop} \approx 2V$$

$$V_{dc} \approx 20.8V$$

IN-RUSH CURRENT CHECK

Inrush current at power-on

Worst case: capacitor initially = 0V

$$I_{inrush} \approx V_{peak} / (R_{secondary} + R_{bridge})$$

If $C > 10,000 \mu F$ and transformer > 30 VA → inrush protection required

Add NTC thermistor (e.g. 5-10 Ω cold)

How to SELECT the NTC (STEP BY STEP)

We need 3 parameters:

Cold resistance (R₂₅)

Current rating

Energy rating (Joules)

Decide acceptable inrush current

$$I_{inrush} \leq 2 \times I_{nominal}$$

10A

Calculate required cold resistance

$$R_{ntc} = V / I$$

$$R_{ntc} = 22 / 10 \approx 2.2 \Omega$$

2-5 Ω @ 25°C

NTC must survive continuous RMS current:

$$I_{ntc} \geq 1.5 \times I_{load}$$

$$I_{ntc} \geq 7.5 \text{ A}$$

Energy stored in capacitor:

$$E = \frac{1}{2} C V^2$$

$$E = 0.5 \times 0.03 \times 22^2$$

$$E \approx 7.3 \text{ Joules}$$

NTC must handle $\geq 2 \times$ this (safety margin): $> 15\text{J}$

Ametherm SL32 2R025

Parameter	Value
R ₂₅	**2 Ω**
Continuous current	**25 A**
Energy rating	**150 J**
Diameter	32 mm

⇒ We add it before generic diode

RECTIFIER CHECK

Current rating

$$I_{rectifier} \geq 1.8 \times I_{load} (5)$$

$$I_{rectifier} \geq 9\text{A}$$

Heat check

$$P \approx 2 \times V_f \times I$$

$$P \approx 2 \times 0.9 \times 5 \approx 9 \text{ W}$$

Needs airflow or PCB copper area.

Capacitor C₁ rating

$$V_{cap} \geq 1.5 \times V_{dc}$$

$$21.4 \times 1.5 \approx 32\text{V}$$

Ripple current rating (CRITICAL)

$$I_{\text{ripple}} \approx I_{\text{load}} \approx 5 \text{ A}$$

$$I_{\text{ripple_cap}} \geq 1.3 \times I_{\text{load}} \geq 6.5 \text{ A}$$

If not \rightarrow capacitor overheats \rightarrow dries \rightarrow explodes.

Ripple voltage check

$$\Delta V = I / (f \times C)$$

$$\Delta V = 5 / (100 \times 0.03) \approx 1.63 \text{ V}$$

REGULATOR THERMAL CHECK (MOST IMPORTANT)

$$P = (V_{\text{in}} - V_{\text{out}}) \times I$$

$$P = (21.4 - 15) \times 5$$

$$P \approx 32 \text{ W}$$

VERY HIGH

REVERSE PROTECTION OF REGULATOR SO WE ADD A DIODE

Thermal resistance calculation

Max junction temp = 125°C

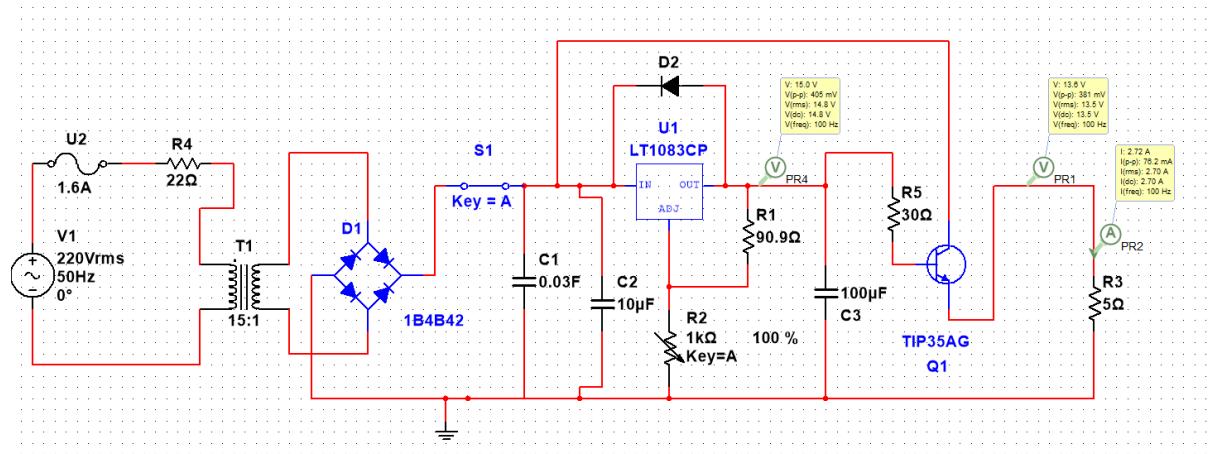
Ambient = 40°C

$$\theta_{\text{total}} \leq (125 - 40) / 22.7$$

$$\theta_{\text{total}} \leq 3.7 \text{ }^{\circ}\text{C/W}$$

Junction-case $\approx 1 \text{ }^{\circ}\text{C/W}$ Case-sink $\approx 0.5 \text{ }^{\circ}\text{C/W}$ Remaining for heatsink:

$\theta_{\text{sink}} \leq 2.2 \text{ }^{\circ}\text{C/W}$ This is a BIG heatsink,



SO I added a tip35 transistor to reduce heat from voltage regulator

A 22ohm after fuse acting like NTC thermistor

Also a diode to protect regulator from reverse current