

# Time Series Decomposition for Long-Short Multivariate Self-Supervised Forecasting

Technical Report

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## Abstract

Self-Supervised Learning (SSL) has become a powerful paradigm in Artificial Intelligence, enabling the training of machine learning models using unlabeled data. However, in time series analysis, SSL models generally underperform in terms of accuracy compared to supervised models, due to the complex temporal patterns present in time series data, such as trends, seasonality, and noise. To address this, we experiment a straightforward data-centric approach inspired by supervised models that decompose time series into two additive components, and we investigate whether a similar decomposition can improve the performance of SSL models. We introduce a pipeline that applies time series decomposition to SSL architectures. This pipeline is adapted to four SSL forecasting models and evaluated on ten benchmark datasets. Our results demonstrate that time series decomposition significantly enhances the accuracy of SSL models in forecasting tasks, and in short-term prediction, it narrows the gap with state-of-the-art supervised models.

## Keywords

Self-Supervised Learning, Time Series Forecasting, Time Series Decomposition

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## 1 Experimental Evaluation

The following sections present supplementary results in the form of tables, offering additional insights that complement and enrich the main findings.

**Settings.** The experiments have been performed on a Workstation with an NVIDIA L40S GPU with 48 GB of VRAM, 256 GB of RAM, and a dual AMD EPYC 9254 24-Core Processor. According to the literature in the field, the predictions are computed via direct multi-step forecasting [1]. Moreover, we used the hyperparameters defined for each model as indicated in the original papers. The only exception was the moving average, whose kernel size we determined through a grid search, exploring the values {9, 25, 64, 96, 128, 224} on the validation set.

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Table 1: The datasets used in the experiments.

Datasets	Signals	Series	Timestamps		Gran.
			Train	Val & Test	
ETTh1 & ETTh2	7	1	8640	2880	1hour
ETTm1 & ETTm2	7	1	34560	11520	15min
Exchange	8	1	4552	1518	1day
Electricity	1	321	15782	5261	1hour
Traffic	862	1	17544	10526	1hour
Weather	21	1	31617	10539	10min
ILI	7	1	579	193	1week
WTH	12	1	21038	7013	1hour

**Datasets.** We conducted experiments on ten widely used in the literature real-world datasets in the field of time series forecasting:

- (1) **ETT (Electricity Transformer Temperature)**<sup>1</sup>: It consists of two hourly sampled datasets (ETTh1/ETTh2) and two 15-minute-sampled datasets (ETTm1/ETTm2) of electricity transformer temperatures, containing features such as oil temperature and load.
- (2) **Exchange**<sup>2</sup>: It collects the daily exchange rates of 8 countries from 1990 to 2016.
- (3) **WTH**<sup>3</sup>: This dataset contains hourly observations of 12 climate-related variables, including temperature, humidity, wind speed, and solar radiation, across nearly 1,600 locations in the United States.
- (4) **Electricity**<sup>4</sup>: This dataset consists of hourly electricity consumption data from 321 residential and industrial clients over the period from 2012 to 2014.
- (5) **Traffic**<sup>5</sup>: It is a dataset containing 48 months of hourly road occupancy rates, gathered between 2015 and 2016 by 862 sensors from the California Department of Transportation in the San Francisco Bay area.
- (6) **Weather**<sup>6</sup>: It includes 21 indicators of weather, such as air temperature, and humidity.
- (7) **ILI (Influenza-like Illness)**<sup>7</sup>: It contains weekly reports from the Centers for Disease Control and Prevention (CDC) in the U.S., tracking the number of patients with influenza-like illness (ILI) from 1997 to 2022.

Table 1 shows a quantitative description of the datasets regarding the number of signals, series, timestamps and granularity.

<sup>1</sup><https://github.com/zhouhaoyi/ETDataset>

<sup>2</sup><https://github.com/laiguokun/multivariate-time-series-data>

<sup>3</sup><https://drive.google.com/drive/folders/1ohGYWWohJlOlb2gsGTeEq3Wii2egnEPR>

<sup>4</sup><https://archive.ics.uci.edu/ml/datasets/ElectricityLoadDiagrams20112014>

<sup>5</sup><http://pems.dot.ca.gov/>

<sup>6</sup><https://www.bgc-jena.mpg.de/wetter/>

<sup>7</sup><https://gis.cdc.gov/grasp/fluview/fluportaldashboard.html>

*Supervised Forecasting Baselines.* We selected PatchTST [2] and DLinear [3] as supervised forecasting models. PatchTST is a state-of-the-art transformer-based model; DLinear achieves competitive accuracy through moving average decomposition and a single linear layer.

## 1.1 Forecasting Evaluation

The effectiveness of our decomposition pipeline is evaluated using Mean Squared Error (MSE) and Mean Absolute Error (MAE), defined as  $MSE = \frac{1}{N} \sum_{i=1}^N (y_i - \hat{y}_i)^2$  and  $MAE = \frac{1}{N} \sum_{i=1}^N |y_i - \hat{y}_i|$ , where  $y$  and  $\hat{y}$  denote the true and predicted values, respectively. The experiment measures the forecasting error of SSL models with and without our pipeline across five prediction lengths, which vary by dataset and are chosen according to the literature for SSL forecasting models.

*List of Tables.* . The following list provides an overview of the tables included in this document.

- **Table 2:** MSE values for each dataset and prediction length, evaluated using grid search with a moving average kernel size.
- **Table 3:** MAE values for each dataset and prediction length, evaluated using grid search with a moving average kernel size.
- **Table 4:** Percentage improvements for each dataset in terms of MAE and MSE.
- **Table 5:** Results for TS2Vec with different kernel size  $K$ .
- **Table 6:** Results for SimTS with different kernel size  $K$ .

- **Table 7:** Results for CoST with different kernel size  $K$ .
- **Table 8:** Results for MaskAE with different kernel size  $K$ .
- **Table 9:** Short-term forecasting results across all models and baselines with a fixed kernel size of 25.

## 1.2 Ablation Study

To understand the contribution of the time series decomposition, we run the selected SSL models again using the embeddings generated by the trend and the error components of the decomposition pipeline alone. In this case, we selected the same kernel size (25 timestamps) for the moving average in all experiments. The findings do not change considering different kernel sizes.

*List of Tables.* . The following list provides an overview of the tables included in this document.

- **Table 10a:** Ablation for TS2Vec and SimTS in terms of MSE.
- **Table 10b:** Ablation for TS2Vec and SimTS in terms of MAE.
- **Table 11a:** Ablation for CoST and MaskAE in terms of MSE.
- **Table 11b:** Ablation for CoST and MasLAE in terms of MAE.

## References

- [1] Chevillon, G.: Direct multi-step estimation and forecasting. *Journal of Economic Surveys* **21**(4), 746–785 (2007). <https://doi.org/https://doi.org/10.1111/j.1467-6419.2007.00518.x>, <https://onlinelibrary.wiley.com/doi/abs/10.1111/j.1467-6419.2007.00518.x>
- [2] Nie, Y., Nguyen, N.H., Sinthong, P., Kalagnanam, J.: A time series is worth 64 words: Long-term forecasting with transformers. In: *ICLR. OpenReview.net* (2023)
- [3] Zeng, A., Chen, M., Zhang, L., Xu, Q.: Are transformers effective for time series forecasting? In: *AAAI*. pp. 11121–11128. AAAI Press (2023)

**Table 2: Effectiveness of the SSL (with and without our decomposition pipeline) and Supervised Forecasting Models measured with the MSE. In bold the best result per model. Underlined the best result per dataset and prediction length  $L$ .**

D	L	Ts2Vec		SimTS		CoST		MAE		PatchTST	DLinear
		TED4STL	Orig.	TED4STL	Orig.	TED4STL	Orig.	TED4STL	Orig.		
ETTh1	24	<b>0.333</b>	0.549	<b>0.231</b>	0.374	<b>0.298</b>	0.383	<b>0.867</b>	1.484	0.327	0.320
	48	<b>0.375</b>	0.598	<b>0.284</b>	0.424	<b>0.403</b>	0.434	<b>1.150</b>	1.544	0.351	0.343
	168	<b>0.498</b>	0.758	<b>0.497</b>	0.644	<b>0.589</b>	0.633	<b>1.144</b>	1.320	0.406	0.399
	336	<b>0.771</b>	0.899	<b>0.796</b>	0.844	0.903	<b>0.792</b>	<b>1.165</b>	1.289	<u>0.431</u>	0.447
	720	1.090	<b>1.060</b>	1.069	<b>1.014</b>	1.027	<b>0.904</b>	<b>1.160</b>	1.370	<u>0.449</u>	0.504
ETTh2	24	<b>0.150</b>	0.389	<b>0.118</b>	0.346	<b>0.188</b>	0.453	<b>1.892</b>	2.994	0.170	0.167
	48	<b>0.267</b>	0.562	<b>0.178</b>	0.586	<b>0.329</b>	0.699	<b>1.947</b>	2.820	0.219	0.221
	168	<b>1.217</b>	1.845	<b>1.221</b>	1.661	<b>1.281</b>	1.538	<b>2.400</b>	3.141	<u>0.324</u>	0.375
	336	<b>1.736</b>	2.291	<b>1.554</b>	1.932	<b>1.481</b>	1.743	<b>2.631</b>	2.741	<u>0.331</u>	0.463
	720	<b>2.143</b>	2.717	<b>1.812</b>	2.148	<b>1.716</b>	1.955	<b>2.698</b>	3.302	0.379	0.733
ETTm1	24	<b>0.131</b>	0.391	<b>0.078</b>	0.240	<b>0.117</b>	0.246	<b>0.227</b>	2.028	0.195	0.213
	48	<b>0.227</b>	0.498	<b>0.123</b>	0.319	<b>0.181</b>	0.330	<b>0.332</b>	1.840	0.261	0.272
	96	<b>0.330</b>	0.564	<b>0.211</b>	0.369	<b>0.275</b>	0.377	<b>0.453</b>	1.692	0.292	0.301
	288	<b>0.457</b>	0.633	<b>0.373</b>	0.464	<b>0.437</b>	0.471	<b>0.784</b>	1.683	<u>0.356</u>	0.365
	672	<b>0.640</b>	0.731	<b>0.555</b>	0.617	<b>0.617</b>	0.622	<b>1.121</b>	1.706	0.408	0.423
ETTm2	24	<b>0.079</b>	0.155	<b>0.056</b>	0.113	<b>0.076</b>	0.134	<b>0.313</b>	2.576	0.095	0.098
	48	<b>0.112</b>	0.219	<b>0.070</b>	0.168	<b>0.101</b>	0.196	<b>0.461</b>	2.499	0.125	0.129
	96	<b>0.172</b>	0.325	<b>0.106</b>	0.272	<b>0.155</b>	0.305	<b>0.643</b>	2.600	0.165	0.172
	288	<b>0.600</b>	0.690	<b>0.606</b>	0.713	<b>0.639</b>	0.754	<b>1.188</b>	2.685	0.261	0.293
	672	2.011	<b>1.831</b>	<b>1.519</b>	1.658	1.866	<b>1.589</b>	2.922	<b>2.955</b>	<u>0.356</u>	0.419
exchange	24	<b>0.058</b>	0.099	<b>0.039</b>	0.086	<b>0.059</b>	0.133	<b>2.257</b>	2.029	0.028	0.025
	48	<b>0.104</b>	0.184	<b>0.059</b>	0.192	<b>0.117</b>	0.250	2.452	<b>2.223</b>	0.047	0.042
	96	<b>0.267</b>	0.390	<b>0.161</b>	0.439	<b>0.334</b>	0.505	2.452	<b>2.227</b>	0.093	<u>0.089</u>
	288	1.455	<b>1.352</b>	<b>1.258</b>	1.312	<b>1.272</b>	1.278	2.776	<b>2.250</b>	0.307	<u>0.274</u>
	672	<b>2.290</b>	3.501	2.405	<b>1.889</b>	2.204	<b>1.942</b>	3.247	<b>2.305</b>	0.824	<u>0.766</u>
WTH	24	<b>0.223</b>	0.310	<b>0.204</b>	0.294	<b>0.203</b>	0.299	<b>0.252</b>	1.612	0.322	0.352
	48	<b>0.251</b>	0.377	<b>0.236</b>	0.356	<b>0.236</b>	0.360	<b>0.286</b>	1.719	0.398	0.419
	168	<b>0.384</b>	0.499	<b>0.353</b>	0.465	<b>0.351</b>	0.465	<b>0.541</b>	1.462	0.509	0.513
	336	<b>0.464</b>	0.535	<b>0.441</b>	0.500	<b>0.437</b>	0.498	<b>0.593</b>	1.529	0.556	0.552
	720	<b>0.515</b>	0.571	<b>0.504</b>	0.537	<b>0.501</b>	0.533	<b>0.573</b>	1.503	0.629	0.618
electricity	24	<b>0.207</b>	0.285	<b>0.090</b>	0.139	0.149	<b>0.135</b>	<b>0.978</b>	1.143	0.095	0.110
	48	<b>0.224</b>	0.307	<b>0.106</b>	0.154	0.169	<b>0.152</b>	<b>0.972</b>	1.136	0.110	0.125
	168	<b>0.262</b>	0.331	<b>0.139</b>	0.176	0.199	<b>0.175</b>	<b>0.979</b>	1.130	0.144	0.150
	336	<b>0.288</b>	0.348	<b>0.170</b>	0.195	0.219	<b>0.195</b>	<b>0.983</b>	1.124	<u>0.166</u>	0.169
	720	<b>0.321</b>	0.375	<b>0.213</b>	0.233	0.254	<b>0.231</b>	<b>0.971</b>	1.106	0.209	0.204
weather	24	<b>0.124</b>	0.316	<b>0.071</b>	0.241	<b>0.114</b>	0.258	<b>0.408</b>	2.015	0.091	0.106
	48	<b>0.176</b>	0.808	<b>0.113</b>	0.526	<b>0.160</b>	0.496	<b>0.553</b>	2.000	0.117	0.139
	96	<b>0.223</b>	1.297	<b>0.123</b>	0.957	<b>0.186</b>	0.787	<b>0.928</b>	2.053	0.152	0.174
	288	<b>0.879</b>	1.608	<b>1.108</b>	1.296	1.085	<b>1.082</b>	<b>1.280</b>	1.919	<u>0.234</u>	0.249
	672	<b>1.727</b>	2.424	1.849	<b>1.749</b>	1.808	<b>1.535</b>	<b>1.502</b>	1.785	<u>0.315</u>	0.322
traffic	24	<b>0.818</b>	0.914	<b>0.731</b>	0.756	0.787	<b>0.721</b>	<b>0.875</b>	1.816	0.320	0.373
	48	<b>0.848</b>	0.958	<b>0.765</b>	0.793	0.816	<b>0.745</b>	<b>0.900</b>	1.752	<u>0.342</u>	0.395
	96	<b>0.890</b>	1.017	<b>0.783</b>	0.809	0.833	<b>0.755</b>	<b>0.915</b>	1.796	<u>0.367</u>	0.413
	288	<b>0.906</b>	1.036	<b>0.798</b>	0.815	0.840	<b>0.764</b>	<b>0.972</b>	1.604	<u>0.395</u>	0.435
	672	<b>0.920</b>	1.073	0.814	0.827	0.856	<b>0.777</b>	<b>1.006</b>	1.692	<u>0.427</u>	0.462
ili	24	<b>2.903</b>	3.625	<b>1.975</b>	2.640	<b>2.389</b>	2.872	<b>8.299</b>	8.860	<u>1.301</u>	2.280
	36	<b>3.493</b>	3.821	<b>2.139</b>	2.905	<b>1.978</b>	3.155	<b>7.565</b>	9.049	<u>1.658</u>	2.235
	48	<b>4.015</b>	4.058	<b>2.547</b>	3.183	<b>2.363</b>	3.439	<b>7.387</b>	8.757	<u>1.657</u>	2.298
	60	<b>4.002</b>	4.319	<b>3.335</b>	3.572	<b>2.487</b>	3.831	<b>7.564</b>	9.195	<u>1.436</u>	2.573

**Table 3: Effectiveness of the SSL (with and without our decomposition pipeline) and Supervised Forecasting Models measured with the MAE. In bold the best result per model. Underlined the best result per dataset and prediction length  $L$ .**

D	L	Ts2Vec		SimTS		CoST		MAE		PatchTST	DLinear
		TED4STL	Orig.	TED4STL	Orig.	TED4STL	Orig.	TED4STL	Orig.		
ETT <sub>h1</sub>	24	<b>0.392</b>	0.509	<b>0.335</b>	0.418	<b>0.381</b>	0.427	<b>0.681</b>	0.958	0.372	0.364
	48	<b>0.424</b>	0.543	<b>0.368</b>	0.452	<b>0.439</b>	0.463	<b>0.842</b>	0.997	0.385	0.377
	168	<b>0.484</b>	0.638	<b>0.491</b>	0.581	<b>0.548</b>	0.578	<b>0.829</b>	0.913	0.416	0.410
	336	<b>0.632</b>	0.713	<b>0.646</b>	0.690	<b>0.711</b>	0.670	<b>0.844</b>	0.895	0.435	0.448
	720	<b>0.790</b>	0.795	<b>0.786</b>	<b>0.786</b>	0.789	0.748	<b>0.836</b>	0.934	0.466	0.515
ETT <sub>h2</sub>	24	<b>0.284</b>	0.459	<b>0.254</b>	0.441	<b>0.327</b>	0.507	<b>1.115</b>	1.339	0.265	0.263
	48	<b>0.387</b>	0.572	<b>0.319</b>	0.586	<b>0.428</b>	0.640	<b>1.105</b>	1.311	0.299	0.302
	168	<b>0.832</b>	1.060	<b>0.763</b>	1.002	<b>0.854</b>	0.983	<b>1.213</b>	1.406	0.369	0.412
	336	<b>1.057</b>	1.210	<b>0.978</b>	1.098	<b>0.962</b>	1.050	<b>1.271</b>	1.317	0.380	0.473
	720	<b>1.236</b>	1.396	<b>1.080</b>	1.185	<b>1.042</b>	1.089	<b>1.242</b>	1.436	0.422	0.606
ETT <sub>m1</sub>	24	<b>0.258</b>	0.407	<b>0.197</b>	0.322	<b>0.240</b>	0.329	<b>0.343</b>	1.106	0.275	0.287
	48	<b>0.330</b>	0.472	<b>0.244</b>	0.377	<b>0.295</b>	0.386	<b>0.413</b>	1.074	0.321	0.326
	96	<b>0.388</b>	0.518	<b>0.321</b>	0.413	<b>0.361</b>	0.419	<b>0.490</b>	1.002	0.343	0.345
	288	<b>0.470</b>	0.569	<b>0.425</b>	0.480	<b>0.465</b>	0.485	<b>0.655</b>	1.000	0.387	0.386
	672	<b>0.579</b>	0.628	<b>0.535</b>	0.572	0.575	<b>0.574</b>	<b>0.819</b>	1.041	0.417	0.422
ETT <sub>m2</sub>	24	<b>0.201</b>	0.273	<b>0.172</b>	0.234	<b>0.201</b>	0.259	<b>0.434</b>	1.160	0.193	0.198
	48	<b>0.241</b>	0.332	<b>0.191</b>	0.295	<b>0.234</b>	0.320	<b>0.531</b>	1.201	0.224	0.229
	96	<b>0.298</b>	0.409	<b>0.242</b>	0.383	<b>0.292</b>	0.405	<b>0.634</b>	1.261	0.255	0.265
	288	<b>0.582</b>	0.629	<b>0.574</b>	0.645	<b>0.592</b>	0.661	<b>0.886</b>	1.287	0.319	0.361
	672	1.072	<b>1.030</b>	<b>0.949</b>	0.999	1.035	<b>0.982</b>	1.380	<b>1.346</b>	0.378	0.434
exchange	24	<b>0.179</b>	0.235	<b>0.152</b>	0.214	<b>0.184</b>	0.277	<b>1.170</b>	1.151	0.116	0.110
	48	<b>0.245</b>	0.319	<b>0.187</b>	0.319	<b>0.256</b>	0.383	1.193	<b>1.187</b>	0.151	0.142
	96	<b>0.380</b>	0.463	<b>0.300</b>	0.491	<b>0.435</b>	0.548	1.226	<b>1.190</b>	0.213	0.216
	288	0.967	<b>0.887</b>	<b>0.894</b>	0.914	<b>0.903</b>	0.883	1.305	<b>1.193</b>	0.402	0.398
	672	<b>1.158</b>	1.362	1.231	<b>1.100</b>	1.168	<b>1.075</b>	1.399	<b>1.171</b>	0.676	0.673
WTH	24	<b>0.290</b>	0.365	<b>0.278</b>	0.356	<b>0.282</b>	0.361	<b>0.332</b>	1.151	0.361	0.385
	48	<b>0.323</b>	0.419	<b>0.311</b>	0.408	<b>0.318</b>	0.412	<b>0.361</b>	1.187	0.422	0.438
	168	<b>0.432</b>	0.509	<b>0.412</b>	0.492	<b>0.417</b>	0.492	<b>0.545</b>	1.190	0.506	0.510
	336	<b>0.488</b>	0.535	<b>0.476</b>	0.518	<b>0.475</b>	0.518	<b>0.580</b>	1.193	0.534	0.537
	720	<b>0.528</b>	0.559	<b>0.520</b>	0.544	<b>0.519</b>	0.542	<b>0.568</b>	1.171	0.576	0.580
electricity	24	<b>0.310</b>	0.373	<b>0.208</b>	0.243	0.265	<b>0.241</b>	<b>0.799</b>	0.873	0.191	0.209
	48	<b>0.337</b>	0.389	<b>0.223</b>	0.258	0.283	<b>0.257</b>	<b>0.798</b>	0.869	0.206	0.224
	168	<b>0.366</b>	0.407	<b>0.251</b>	0.276	0.307	<b>0.275</b>	<b>0.799</b>	0.866	0.237	0.247
	336	<b>0.385</b>	0.420	<b>0.278</b>	0.296	0.326	<b>0.296</b>	<b>0.801</b>	0.865	0.262	0.268
	720	<b>0.401</b>	0.439	<b>0.316</b>	0.329	0.354	<b>0.328</b>	<b>0.802</b>	0.860	0.298	0.300
weather	24	<b>0.236</b>	0.349	<b>0.155</b>	0.306	<b>0.212</b>	0.337	<b>0.480</b>	1.048	0.121	0.156
	48	<b>0.285</b>	0.584	<b>0.209</b>	0.484	<b>0.259</b>	0.488	<b>0.561</b>	1.075	0.158	0.197
	96	<b>0.336</b>	0.788	<b>0.220</b>	0.695	<b>0.292</b>	0.642	<b>0.771</b>	1.114	0.199	0.233
	288	<b>0.670</b>	0.939	<b>0.711</b>	0.859	<b>0.727</b>	0.794	<b>0.907</b>	1.102	0.272	0.304
	672	<b>0.999</b>	1.220	1.066	<b>1.033</b>	1.027	<b>0.977</b>	<b>0.993</b>	1.057	0.331	0.362
traffic	24	<b>0.473</b>	0.541	0.438	<b>0.431</b>	0.470	<b>0.423</b>	<b>0.490</b>	0.923	0.231	0.271
	48	<b>0.490</b>	0.556	0.453	<b>0.451</b>	0.482	<b>0.437</b>	<b>0.506</b>	0.899	0.240	0.279
	96	<b>0.508</b>	0.564	<b>0.465</b>	0.475	0.484	<b>0.438</b>	<b>0.504</b>	0.913	0.250	0.287
	288	<b>0.509</b>	0.571	<b>0.463</b>	0.472	0.482	<b>0.434</b>	<b>0.521</b>	0.837	0.263	0.297
	672	<b>0.511</b>	0.600	<b>0.464</b>	0.474	0.487	<b>0.435</b>	<b>0.532</b>	0.868	0.284	0.314
ili	24	<b>1.102</b>	1.209	<b>0.904</b>	1.048	<b>0.998</b>	1.077	<b>2.101</b>	2.160	0.734	1.061
	36	<b>1.249</b>	1.272	<b>0.958</b>	1.075	<b>0.969</b>	1.122	<b>1.960</b>	2.163	0.898	1.059
	48	1.333	<b>1.324</b>	<b>1.016</b>	1.124	<b>1.014</b>	1.178	<b>1.924</b>	2.125	0.879	1.079
	60	<b>1.316</b>	1.374	<b>1.150</b>	1.204	<b>1.024</b>	1.261	<b>1.941</b>	2.175	0.790	1.157

**Table 4: Percentage improvements in terms of MSE and MAE referred to Table 3 and Table 2**

(a) MSE percentage Improvements						(b) MAE percentage Improvements					
	MSE				Avg		MAE				Avg
	TS2Vec	SimTS	CoST	MaskAE			TS2Vec	SimTS	CoST	MaskAE	
ETTh1	20.59%	<b>12.81%</b>	-2.34%	<b>21.71%</b>	13.20%	ETTh1	<b>14.90%</b>	<b>10.26%</b>	<b>0.62%</b>	<b>14.14%</b>	9.98%
ETTh2	<b>29.36%</b>	<b>26.83%</b>	<b>21.80%</b>	<b>22.87%</b>	25.22%	ETTh2	<b>19.18%</b>	<b>21.30%</b>	<b>15.35%</b>	<b>12.68%</b>	17.13%
ETTm1	<b>36.64%</b>	<b>33.32%</b>	<b>20.53%</b>	<b>67.40%</b>	39.47%	ETTm1	<b>21.99%</b>	<b>20.49%</b>	<b>11.67%</b>	<b>47.91%</b>	25.52%
ETTm2	<b>7.65%</b>	<b>19.34%</b>	<b>4.70%</b>	<b>58.51%</b>	22.55%	ETTm2	<b>10.37%</b>	<b>16.76%</b>	<b>10.40%</b>	<b>38.24%</b>	18.94%
Exch.	<b>24.48%</b>	-0.07%	<b>2.97%</b>	-19.47%	1.98%	Exch.	<b>10.33%</b>	<b>9.02%</b>	<b>6.96%</b>	-6.80%	4.88%
WTH	<b>19.92%</b>	<b>19.25%</b>	<b>19.83%</b>	<b>71.32%</b>	32.58%	WTH	<b>13.62%</b>	<b>13.86%</b>	<b>13.46%</b>	<b>59.51%</b>	25.11%
Electr.	<b>20.91%</b>	<b>20.08%</b>	-11.49%	<b>13.41%</b>	10.73%	Electr.	<b>11.29%</b>	<b>9.04%</b>	-9.77%	<b>7.71%</b>	4.57%
Weath.	<b>51.51%</b>	<b>31.56%</b>	<b>19.36%</b>	<b>52.20%</b>	38.66%	Weath.	<b>34.92%</b>	<b>30.11%</b>	<b>22.25%</b>	<b>31.23%</b>	29.63%
Traff.	<b>12.33%</b>	<b>2.76%</b>	-9.85%	<b>46.10%</b>	12.83%	Traff.	<b>12.08%</b>	<b>0.92%</b>	-10.99%	<b>42.50%</b>	11.13%
Ili	<b>8.91%</b>	<b>18.74%</b>	<b>30.68%</b>	<b>14.07%</b>	18.10%	Ili	<b>3.47%</b>	<b>9.50%</b>	<b>13.65%</b>	<b>8.08%</b>	8.67%
Avg	23.23%	18.46%	9.62%	34.81%	21.53%	Avg	15.22%	14.13%	7.36%	25.52%	15.56%

Table 5: TS2Vec with different kernel size

D	L	ks=9		ks=25		ks=64		ks=96		ks=128		ks=224		Orig.	
		MAE	MSE	MAE	MSE	MAE	MSE	MAE	MSE	MAE	MSE	MAE	MSE	MAE	MSE
ETTh1	24	0.463	0.463	0.402	0.347	<b>0.392</b>	<b>0.333</b>	0.405	0.351	0.406	0.355	0.417	0.378	0.509	0.549
	48	0.511	0.539	0.466	0.453	0.427	0.392	0.424	0.375	<b>0.420</b>	<b>0.374</b>	0.428	0.394	0.543	0.598
	168	0.621	0.727	0.591	0.666	0.567	0.630	0.535	0.575	0.519	0.556	<b>0.484</b>	<b>0.498</b>	0.638	0.758
	336	0.707	0.887	0.697	0.862	0.685	0.844	0.677	0.832	0.667	0.821	<b>0.632</b>	<b>0.771</b>	0.713	0.899
	720	0.791	<b>1.026</b>	0.793	1.040	<b>0.790</b>	1.054	0.790	1.060	0.789	1.068	0.790	1.090	0.795	1.060
ETTh2	24	0.393	0.304	0.324	0.212	<b>0.284</b>	<b>0.150</b>	0.303	0.170	0.305	0.179	0.385	0.288	0.459	0.389
	48	0.562	0.584	0.476	0.424	0.406	0.303	0.392	0.271	<b>0.387</b>	<b>0.267</b>	0.417	0.314	0.572	0.562
	168	0.975	1.618	0.994	1.659	0.970	1.603	0.921	1.431	0.920	1.386	<b>0.832</b>	<b>1.217</b>	1.060	1.845
	336	1.128	2.055	1.144	2.074	1.150	2.094	1.106	1.933	1.118	1.940	<b>1.057</b>	<b>1.736</b>	1.210	2.291
	720	1.262	2.354	1.288	2.383	1.299	2.390	1.272	2.293	1.274	2.280	<b>1.236</b>	<b>2.143</b>	1.396	2.717
ETTh1	24	0.375	0.358	0.296	0.207	<b>0.258</b>	<b>0.131</b>	0.313	0.208	0.320	0.212	0.334	0.256	0.407	0.391
	48	0.465	0.496	0.395	0.364	0.335	0.253	0.333	0.237	<b>0.330</b>	<b>0.227</b>	0.368	0.305	0.472	0.498
	96	0.502	0.536	0.450	0.446	0.414	0.381	0.407	0.360	<b>0.388</b>	0.330	0.389	<b>0.326</b>	0.518	0.564
	288	0.566	0.634	0.532	0.574	0.509	0.528	0.505	0.513	0.487	0.487	<b>0.470</b>	<b>0.457</b>	0.569	0.633
	672	0.637	0.754	0.613	0.710	0.590	0.662	0.595	0.665	0.579	0.640	<b>0.565</b>	<b>0.615</b>	0.628	0.731
ETTh2	24	0.251	0.139	0.213	0.097	<b>0.201</b>	<b>0.079</b>	0.225	0.100	0.228	0.102	0.229	0.104	0.273	0.155
	48	0.319	0.217	0.274	0.160	0.245	0.121	<b>0.240</b>	0.113	0.241	<b>0.112</b>	0.260	0.128	0.332	0.219
	96	0.403	0.342	0.359	0.273	0.328	0.220	0.318	0.198	<b>0.298</b>	<b>0.172</b>	0.309	<b>0.172</b>	0.409	0.325
	288	0.639	0.736	0.610	0.668	0.589	0.640	0.580	0.613	<b>0.563</b>	<b>0.583</b>	0.582	0.600	0.629	0.690
	672	<b>1.012</b>	<b>1.749</b>	1.021	1.794	1.035	1.855	1.043	1.897	1.038	1.877	1.072	2.011	1.030	1.831
Exch.	24	0.213	0.082	0.208	0.077	<b>0.179</b>	<b>0.058</b>	0.192	0.070	0.209	0.076	0.184	0.067	0.235	0.099
	48	0.332	0.177	0.316	0.172	0.267	0.125	0.248	0.117	0.245	0.104	<b>0.229</b>	<b>0.093</b>	0.319	0.184
	96	0.525	0.438	0.522	0.429	0.472	0.406	0.462	0.398	0.440	0.347	<b>0.380</b>	<b>0.267</b>	0.463	0.390
	288	0.967	1.455	0.966	1.448	0.954	<b>1.374</b>	<b>0.941</b>	1.422	0.942	1.446	0.951	1.461	0.887	1.352
	672	1.158	2.290	<b>1.093</b>	<b>1.970</b>	1.187	2.385	1.233	2.698	1.268	2.876	1.297	2.920	1.362	3.501
WTH	24	0.333	0.273	0.307	0.242	<b>0.290</b>	<b>0.223</b>	0.305	0.236	0.319	0.250	0.342	0.278	0.365	0.310
	48	0.396	0.346	0.376	0.322	0.337	0.272	<b>0.323</b>	<b>0.251</b>	0.331	0.260	0.369	0.305	0.419	0.377
	168	0.492	0.471	0.482	0.459	0.465	0.435	0.452	0.414	0.444	0.405	<b>0.432</b>	<b>0.384</b>	0.509	0.499
	336	0.519	0.507	0.514	0.500	0.504	0.486	0.498	0.475	0.495	0.473	<b>0.488</b>	<b>0.464</b>	0.535	0.535
	720	0.543	0.543	0.541	0.538	0.536	0.531	0.533	0.525	0.532	0.523	<b>0.528</b>	<b>0.515</b>	0.559	0.571
Electr.	24	0.310	0.207	<b>0.317</b>	<b>0.202</b>	0.322	0.203	0.335	0.223	0.336	0.226	0.353	0.251	0.373	0.285
	48	0.332	0.234	0.342	0.236	<b>0.337</b>	<b>0.224</b>	0.342	0.228	0.340	0.227	0.357	0.252	0.389	0.307
	168	0.362	0.270	0.374	0.280	0.372	0.275	0.375	0.278	0.367	0.267	<b>0.366</b>	<b>0.262</b>	0.407	0.331
	336	0.378	0.290	0.391	0.302	0.389	0.298	0.393	0.302	0.386	0.292	<b>0.385</b>	<b>0.288</b>	0.420	0.348
	720	<b>0.401</b>	<b>0.321</b>	0.413	0.333	0.411	0.331	0.416	0.336	<b>0.410</b>	0.327	0.410	0.325	0.439	0.375
Weath.	24	0.393	0.391	0.311	0.260	<b>0.236</b>	<b>0.124</b>	0.291	0.177	0.251	0.140	0.253	0.138	0.349	0.316
	48	0.679	1.090	0.566	0.795	0.345	0.287	0.285	0.176	<b>0.284</b>	<b>0.166</b>	0.297	0.180	0.584	0.808
	96	0.930	1.817	0.843	1.521	0.618	0.844	0.500	0.545	0.400	0.338	<b>0.336</b>	<b>0.223</b>	0.788	1.297
	288	1.056	2.073	0.992	1.845	0.856	1.400	0.776	1.169	0.723	1.022	<b>0.670</b>	<b>0.879</b>	0.939	1.608
	672	1.337	3.016	1.280	2.774	1.172	2.338	1.108	2.103	1.056	1.921	<b>0.999</b>	<b>1.727</b>	1.220	2.424
Traff.	24	0.572	0.963	0.554	0.893	0.507	0.841	0.498	0.847	<b>0.473</b>	0.818	0.480	<b>0.813</b>	0.541	0.914
	48	0.583	0.994	0.532	0.916	0.516	0.881	0.515	0.884	<b>0.490</b>	<b>0.848</b>	0.499	<b>0.848</b>	0.556	0.958
	96	0.598	1.043	0.551	0.967	0.532	0.926	0.533	0.932	<b>0.508</b>	0.890	0.510	<b>0.879</b>	0.564	1.017
	288	0.605	1.072	0.556	0.988	0.533	0.940	0.533	0.945	<b>0.509</b>	0.906	0.509	<b>0.891</b>	0.571	1.036
	672	0.611	1.092	0.570	1.012	0.534	0.953	0.534	0.955	<b>0.511</b>	0.920	0.512	<b>0.907</b>	0.600	1.073
Ili	24	1.999	8.380	1.102	2.903	1.419	3.555	<b>1.049</b>	<b>2.350</b>	1.093	2.767	1.190	3.552	1.209	3.625
	36	1.672	6.235	1.249	3.493	1.336	3.662	1.113	<b>2.856</b>	<b>1.090</b>	2.874	1.176	3.478	1.272	3.821
	48	1.548	5.446	1.333	4.015	1.497	4.551	1.213	3.421	<b>1.172</b>	<b>3.333</b>	1.256	3.873	1.324	4.058
	60	1.467	5.029	1.316	4.002	1.425	4.302	1.221	3.543	<b>1.192</b>	<b>3.511</b>	1.264	3.959	1.374	4.319
Sum		33.887	63.061	30.850	49.302	30.020	47.893	28.600	43.071	28.093	42.518	28.273	44.282	32.730	54.442
Avg		0.692	1.287	0.630	1.006	0.613	0.977	0.584	0.879	0.573	0.868	0.577	0.904	0.668	1.111

Table 6: SimTS with different kernel size

D	L	ks=9		ks=25		ks=64		ks=96		ks=128		ks=224		Orig.	
		MAE	MSE	MAE	MSE	MAE	MSE	MAE	MSE	MAE	MSE	MAE	MSE	MAE	MSE
ETTh1	24	0.392	0.339	0.352	0.274	<b>0.335</b>	<b>0.231</b>	0.344	0.250	0.351	0.265	0.362	0.288	0.418	0.374
	48	0.438	0.404	0.417	0.373	0.388	0.319	<b>0.368</b>	<b>0.284</b>	0.371	0.293	0.378	0.310	0.452	0.424
	168	0.578	0.636	0.565	0.615	0.544	0.585	0.533	0.571	0.518	0.546	<b>0.491</b>	<b>0.497</b>	0.581	0.644
	336	0.688	0.838	0.681	0.827	0.669	0.806	<b>0.661</b>	<b>0.795</b>	0.662	0.816	0.646	0.796	0.690	0.844
	720	0.784	1.013	0.781	1.004	0.778	1.002	<b>0.776</b>	<b>1.001</b>	0.775	1.001	0.786	1.069	0.786	1.014
ETTh2	24	0.415	0.320	0.353	0.243	<b>0.254</b>	<b>0.118</b>	0.259	0.122	0.277	0.140	0.302	0.174	0.441	0.346
	48	0.565	0.556	0.526	0.498	0.411	0.328	0.339	0.210	<b>0.319</b>	<b>0.178</b>	0.342	0.219	0.586	0.586
	168	0.993	1.648	0.985	1.626	0.959	1.544	0.931	1.457	0.899	1.358	<b>0.763</b>	<b>1.221</b>	1.002	1.661
	336	1.090	1.923	1.087	1.912	1.072	1.863	1.055	1.809	1.035	1.743	<b>0.978</b>	<b>1.554</b>	1.098	1.932
	720	1.171	2.127	1.168	2.115	1.160	2.078	1.149	2.037	1.136	1.992	<b>1.080</b>	<b>1.812</b>	1.185	2.148
ETTm1	24	0.295	0.209	0.238	0.138	<b>0.197</b>	<b>0.078</b>	0.219	0.100	0.241	0.121	0.281	0.168	0.322	0.240
	48	0.366	0.308	0.334	0.265	0.269	0.167	<b>0.244</b>	<b>0.123</b>	0.255	0.134	0.302	0.190	0.377	0.319
	96	0.409	0.368	0.391	0.344	0.358	0.292	0.336	0.254	<b>0.321</b>	<b>0.225</b>	<b>0.321</b>	<b>0.211</b>	0.413	0.369
	288	0.478	0.463	0.470	0.452	0.454	0.425	0.446	0.410	0.438	0.397	<b>0.425</b>	<b>0.373</b>	0.480	0.464
	672	0.570	0.616	0.566	0.610	0.556	0.592	0.552	0.585	0.547	0.577	<b>0.535</b>	<b>0.555</b>	0.572	0.617
ETTm2	24	0.219	0.100	0.195	0.078	<b>0.172</b>	<b>0.056</b>	0.176	0.060	0.179	0.064	0.201	0.081	0.234	0.113
	48	0.285	0.158	0.265	0.139	0.222	0.096	0.201	0.077	<b>0.191</b>	<b>0.070</b>	0.212	0.086	0.295	0.168
	96	0.376	0.265	0.363	0.249	0.327	0.206	0.302	0.176	0.274	0.145	<b>0.242</b>	<b>0.106</b>	0.383	0.272
	288	0.640	0.705	0.634	0.695	0.618	0.671	0.606	0.652	0.610	0.672	<b>0.574</b>	<b>0.606</b>	0.645	0.713
	672	0.994	1.658	0.992	1.651	0.984	1.627	0.977	1.606	0.970	1.585	<b>0.949</b>	<b>1.519</b>	0.999	1.658
Exch.	24	0.203	0.078	0.177	0.062	0.152	0.039	0.156	0.043	<b>0.150</b>	<b>0.038</b>	0.176	0.052	0.214	0.086
	48	0.313	0.186	0.296	0.169	0.243	0.119	0.201	0.074	<b>0.187</b>	<b>0.059</b>	0.212	0.078	0.319	0.192
	96	0.486	0.432	0.475	0.417	0.442	0.368	0.410	0.333	0.380	0.282	<b>0.300</b>	<b>0.161</b>	0.491	0.439
	288	0.909	1.302	0.907	1.298	0.900	1.283	0.897	1.276	<b>0.894</b>	1.269	<b>0.894</b>	<b>1.258</b>	0.914	1.312
	672	<b>1.094</b>	<b>1.872</b>	<b>1.094</b>	1.873	1.099	1.893	1.106	1.920	1.117	1.957	1.231	2.405	1.100	1.889
WTH	24	0.335	0.267	0.301	0.229	<b>0.278</b>	<b>0.204</b>	0.293	0.221	0.306	0.235	0.329	0.260	0.356	0.294
	48	0.394	0.339	0.370	0.309	0.326	0.255	<b>0.311</b>	<b>0.236</b>	0.314	0.241	0.346	0.276	0.408	0.356
	168	0.487	0.461	0.479	0.451	0.460	0.425	0.447	0.407	0.436	0.391	<b>0.412</b>	<b>0.353</b>	0.492	0.465
	336	0.515	0.497	0.511	0.492	0.501	0.478	0.495	0.469	0.489	0.461	<b>0.476</b>	<b>0.441</b>	0.518	0.500
	720	0.540	0.532	0.538	0.530	0.534	0.524	0.530	0.519	0.527	0.515	<b>0.520</b>	<b>0.504</b>	0.544	0.537
Electr.	24	0.231	0.130	0.210	0.103	<b>0.208</b>	<b>0.090</b>	0.217	0.101	0.222	0.108	0.231	0.120	0.243	0.139
	48	0.254	0.151	0.240	0.135	0.228	0.114	<b>0.223</b>	<b>0.106</b>	0.227	0.110	0.236	0.121	0.258	0.154
	168	0.279	0.178	0.273	0.172	0.268	0.163	0.264	0.157	0.259	0.151	<b>0.251</b>	<b>0.139</b>	0.276	0.176
	336	0.300	0.198	0.296	0.194	0.293	0.189	0.289	0.184	0.286	0.180	<b>0.278</b>	<b>0.170</b>	0.296	0.195
	720	0.332	0.235	0.329	0.231	0.327	0.227	0.324	0.224	0.321	0.221	<b>0.316</b>	<b>0.213</b>	0.329	0.233
Weath.	24	0.291	0.213	0.232	0.141	<b>0.155</b>	<b>0.071</b>	0.160	0.075	0.169	0.084	0.175	0.094	0.306	0.241
	48	0.489	0.538	0.436	0.444	0.287	0.212	0.209	0.113	<b>0.182</b>	<b>0.093</b>	0.192	0.104	0.484	0.526
	96	0.719	1.046	0.691	0.998	0.573	0.757	0.464	0.528	0.362	0.333	<b>0.220</b>	<b>0.123</b>	0.695	0.957
	288	1.013	1.773	1.032	1.910	0.967	1.750	0.895	1.548	0.834	1.379	<b>0.711</b>	<b>1.108</b>	0.859	1.296
	672	1.227	2.430	1.221	2.417	1.186	2.305	1.139	2.114	1.107	1.979	1.066	1.849	<b>1.033</b>	<b>1.749</b>
Traff.	24	0.440	0.745	<b>0.438</b>	<b>0.731</b>	0.445	0.732	0.448	0.737	0.447	0.742	0.443	0.748	0.431	0.756
	48	0.457	0.780	<b>0.453</b>	0.765	0.459	<b>0.764</b>	0.462	0.764	0.462	0.766	0.456	0.768	0.451	0.793
	96	0.469	0.802	<b>0.464</b>	0.790	0.470	0.796	0.472	0.797	0.469	0.793	0.465	<b>0.783</b>	0.475	0.809
	288	0.469	0.813	0.464	0.803	0.467	0.806	0.468	0.806	0.467	0.804	<b>0.463</b>	<b>0.798</b>	0.472	0.815
	672	0.471	0.826	0.467	0.817	0.468	0.819	0.469	0.819	0.467	0.818	<b>0.464</b>	<b>0.814</b>	0.474	0.827
Ili	24	1.007	2.471	0.904	1.975	<b>0.912</b>	<b>1.862</b>	0.955	2.116	0.988	2.296	0.994	2.488	1.048	2.640
	36	1.049	2.803	0.981	2.422	<b>0.958</b>	<b>2.139</b>	0.978	2.235	1.012	2.407	1.018	2.620	1.075	2.905
	48	1.106	3.124	1.055	2.809	<b>1.016</b>	2.547	1.040	<b>2.546</b>	1.054	2.618	1.058	2.825	1.124	3.183
	60	1.189	3.542	1.150	3.335	<b>1.096</b>	2.969	1.121	2.982	1.118	<b>2.952</b>	1.124	3.149	1.204	3.572
Sum		28.809	43.414	27.847	41.130	26.438	37.983	25.913	37.028	25.621	36.603	25.224	36.651	28.848	42.939
Avg		0.588	0.886	0.568	0.839	0.540	0.775	0.529	0.756	0.523	0.747	0.515	0.748	0.589	0.876

Table 7: CoST with different kernel size

D	L	ks=9		ks=25		ks=64		ks=96		ks=128		ks=224		Orig.	
		MAE	MSE	MAE	MSE	MAE	MSE	MAE	MSE	MAE	MSE	MAE	MSE	MAE	MSE
ETTth1	24	0.416	0.366	0.440	0.416	<b>0.381</b>	<b>0.298</b>	0.425	0.400	0.433	0.400	0.451	0.438	0.427	0.383
	48	0.457	0.426	0.484	0.485	<b>0.433</b>	<b>0.386</b>	0.437	0.411	0.439	0.403	0.455	0.439	0.463	0.434
	168	0.585	0.648	0.609	0.694	0.591	0.660	0.578	0.644	0.576	0.638	<b>0.548</b>	<b>0.589</b>	0.578	0.633
	336	0.691	0.850	0.712	0.890	0.701	0.871	0.698	0.869	0.708	0.893	0.711	0.903	<b>0.670</b>	<b>0.792</b>
	720	0.789	1.027	0.822	1.109	0.813	1.092	0.818	1.106	0.820	1.116	0.828	1.160	<b>0.748</b>	<b>0.904</b>
ETTth2	24	0.441	0.350	0.395	0.284	0.327	0.188	<b>0.319</b>	<b>0.184</b>	0.341	0.210	0.416	0.300	0.507	0.453
	48	0.593	0.610	0.562	0.556	0.476	0.411	0.428	0.329	<b>0.423</b>	0.315	0.432	<b>0.314</b>	0.640	0.699
	168	1.004	1.638	0.997	1.611	0.965	1.514	0.946	1.460	0.919	1.439	<b>0.854</b>	<b>1.281</b>	0.983	1.538
	336	1.070	1.856	1.071	1.863	1.057	1.827	1.045	1.789	1.032	1.741	<b>0.962</b>	<b>1.481</b>	1.050	1.743
	720	1.139	2.055	1.136	2.041	1.117	1.980	1.104	1.937	1.093	1.885	<b>1.042</b>	<b>1.716</b>	1.089	1.955
ETTm1	24	0.305	0.217	0.269	0.165	<b>0.240</b>	<b>0.117</b>	0.379	0.326	0.300	0.185	0.364	0.287	0.329	0.246
	48	0.375	0.316	0.354	0.287	0.304	0.202	0.386	0.336	<b>0.295</b>	<b>0.181</b>	0.366	0.288	0.386	0.330
	96	0.416	0.373	0.408	0.362	0.390	0.331	0.441	0.425	<b>0.361</b>	0.279	<b>0.361</b>	<b>0.275</b>	0.419	0.377
	288	0.485	0.471	0.483	0.467	0.483	0.465	0.514	0.530	0.475	0.451	<b>0.465</b>	<b>0.437</b>	0.485	0.471
	672	0.576	0.625	0.577	0.626	0.585	0.634	0.603	0.671	0.583	0.628	0.575	<b>0.617</b>	<b>0.574</b>	0.622
ETTm2	24	0.237	0.114	0.221	0.097	<b>0.201</b>	<b>0.076</b>	0.217	0.090	0.220	0.093	0.248	0.123	0.259	0.134
	48	0.301	0.177	0.287	0.160	0.258	0.125	0.247	0.111	<b>0.234</b>	<b>0.101</b>	0.250	0.121	0.320	0.196
	96	0.390	0.287	0.380	0.275	0.353	0.238	0.334	0.211	0.313	0.185	<b>0.292</b>	<b>0.155</b>	0.405	0.305
	288	0.653	0.750	0.646	0.735	0.633	0.715	0.625	0.700	0.611	0.670	<b>0.592</b>	<b>0.639</b>	0.661	0.754
	672	1.067	1.937	1.067	1.947	1.068	1.950	1.066	1.948	1.058	1.928	1.035	1.866	<b>0.982</b>	<b>1.589</b>
Exch.	24	0.261	0.118	0.243	0.105	0.199	0.070	0.184	0.059	<b>0.181</b>	<b>0.056</b>	0.244	0.098	0.277	0.133
	48	0.378	0.248	0.361	0.230	0.317	0.182	0.283	0.146	<b>0.256</b>	<b>0.117</b>	0.292	0.140	0.383	0.250
	96	0.556	0.518	0.546	0.506	0.517	0.465	0.502	0.438	0.476	0.399	<b>0.435</b>	<b>0.334</b>	0.548	0.505
	288	0.923	1.340	0.923	1.339	0.919	1.327	0.902	1.289	0.902	1.283	0.903	<b>1.272</b>	<b>0.883</b>	1.278
	672	1.098	1.969	1.099	1.972	1.103	1.987	1.123	2.064	1.132	2.089	1.168	2.204	<b>1.075</b>	<b>1.942</b>
WTH	24	0.337	0.271	0.304	0.231	<b>0.282</b>	<b>0.203</b>	0.313	0.234	0.344	0.263	0.386	0.308	0.361	0.299
	48	0.397	0.343	0.374	0.314	0.324	0.248	<b>0.318</b>	<b>0.236</b>	0.342	0.261	0.385	0.306	0.412	0.360
	168	0.488	0.460	0.481	0.451	0.461	0.425	0.450	0.407	0.440	0.391	<b>0.417</b>	<b>0.351</b>	0.492	0.465
	336	0.514	0.494	0.510	0.489	0.501	0.475	0.495	0.467	0.490	0.459	<b>0.475</b>	<b>0.437</b>	0.518	0.498
	720	0.539	0.530	0.537	0.528	0.532	0.521	0.529	0.516	0.526	0.513	<b>0.519</b>	<b>0.501</b>	0.542	0.533
Electr.	24	0.265	0.149	0.387	0.271	0.308	0.181	0.465	0.371	0.376	0.264	0.435	0.342	<b>0.241</b>	<b>0.135</b>
	48	0.283	0.169	0.405	0.298	0.321	0.198	0.464	0.369	0.370	0.250	0.431	0.331	<b>0.257</b>	<b>0.152</b>
	168	0.307	0.199	0.425	0.332	0.356	0.247	0.489	0.418	0.394	0.291	0.437	0.341	<b>0.275</b>	<b>0.175</b>
	336	0.326	0.219	0.438	0.351	0.373	0.271	0.500	0.439	0.415	0.321	0.455	0.372	<b>0.296</b>	<b>0.195</b>
	720	0.354	0.254	0.459	0.383	0.398	0.305	0.517	0.469	0.436	0.354	0.477	0.408	<b>0.328</b>	<b>0.231</b>
Weath.	24	0.310	0.226	0.272	0.179	<b>0.212</b>	<b>0.114</b>	0.220	0.118	0.285	0.171	0.284	0.176	0.337	0.258
	48	0.472	0.484	0.434	0.424	0.313	0.239	<b>0.259</b>	<b>0.160</b>	0.293	0.181	<b>0.293</b>	0.187	0.488	0.496
	96	0.655	0.841	0.632	0.800	0.541	0.631	0.464	0.485	0.428	0.403	<b>0.292</b>	<b>0.186</b>	0.642	0.787
	288	0.916	1.477	0.905	1.448	0.857	1.333	0.830	1.285	0.806	1.257	0.727	1.085	<b>0.794</b>	<b>1.082</b>
	672	1.199	2.327	1.191	2.299	1.152	2.182	1.121	2.092	1.076	1.944	1.027	1.808	<b>0.977</b>	<b>1.535</b>
Traff.	24	0.470	0.787	0.631	1.036	0.551	0.905	0.700	1.172	0.604	0.994	0.670	1.163	<b>0.423</b>	<b>0.721</b>
	48	0.482	0.816	0.621	1.046	0.548	0.925	0.719	1.221	0.608	1.007	0.666	1.154	<b>0.437</b>	<b>0.745</b>
	96	0.484	0.833	0.632	1.082	0.549	0.951	0.716	1.258	0.617	1.050	0.671	1.159	<b>0.438</b>	<b>0.755</b>
	288	0.482	0.840	0.634	1.094	0.555	0.969	0.719	1.280	0.609	1.071	0.674	1.196	<b>0.434</b>	<b>0.764</b>
	672	0.487	0.856	0.658	1.138	0.570	0.999	0.731	1.311	0.623	1.118	0.678	1.225	<b>0.435</b>	<b>0.777</b>
Ili	24	1.058	2.811	0.998	2.389	<b>0.997</b>	<b>1.991</b>	0.988	2.146	1.032	2.392	1.034	2.528	1.077	2.872
	36	1.111	3.127	1.075	2.860	<b>0.969</b>	<b>1.978</b>	0.997	2.178	1.013	2.316	1.014	2.568	1.122	3.155
	48	1.165	3.413	1.136	3.188	1.014	2.363	1.036	2.389	<b>1.003</b>	<b>2.331</b>	1.010	2.657	1.178	3.439
	60	1.247	3.814	1.208	3.545	1.098	2.871	1.096	2.827	<b>1.024</b>	<b>2.487</b>	1.042	2.883	1.261	3.831
Sum		29.549	45.023	30.441	45.394	28.210	39.631	29.739	42.316	28.331	39.774	28.788	41.148	28.903	42.926
Avg		0.603	0.919	0.621	0.926	0.576	0.809	0.607	0.864	0.578	0.812	0.588	0.840	0.590	0.876



Table 8: MaskAE with different kernel size

D	L	ks=9		ks=25		ks=64		ks=96		ks=128		ks=224		Orig.	
		MAE	MSE	MAE	MSE	MAE	MSE	MAE	MSE	MAE	MSE	MAE	MSE	MAE	MSE
ETTth1	24	0.821	1.136	0.783	1.047	0.711	0.921	0.689	0.898	0.681	0.867	<b>0.678</b>	<b>0.864</b>	0.958	1.484
	48	<b>0.839</b>	1.162	0.851	1.166	0.841	1.152	0.842	<b>1.150</b>	0.840	1.151	0.840	1.160	0.997	1.544
	168	0.827	1.147	0.825	<b>1.144</b>	0.831	1.147	0.829	<b>1.144</b>	<b>0.826</b>	<b>1.144</b>	0.828	1.151	0.913	1.320
	336	0.838	<b>1.158</b>	0.844	1.165	<b>0.836</b>	1.160	0.846	1.167	0.847	1.168	0.850	1.172	0.895	1.289
	720	0.836	1.160	0.836	<b>1.158</b>	<b>0.835</b>	1.159	0.836	1.160	0.837	1.163	0.837	1.165	0.934	1.370
ETTth2	24	1.286	2.617	1.245	2.385	1.125	1.908	1.222	2.170	1.115	1.892	<b>1.095</b>	<b>1.885</b>	1.339	2.994
	48	1.233	2.422	1.152	2.091	1.105	1.947	1.128	2.132	1.118	2.137	<b>1.019</b>	<b>1.787</b>	1.311	2.820
	168	1.236	2.491	1.265	2.598	1.303	2.745	1.257	2.550	<b>1.213</b>	<b>2.400</b>	1.222	2.418	1.406	3.141
	336	1.334	2.715	1.402	2.932	1.370	2.900	1.369	2.927	1.351	2.925	<b>1.271</b>	<b>2.631</b>	1.317	2.741
	720	1.303	2.895	1.290	2.875	1.296	2.876	1.274	2.781	1.269	2.770	<b>1.242</b>	<b>2.698</b>	1.436	3.302
ETTm1	24	0.498	0.497	0.468	0.424	<b>0.343</b>	<b>0.227</b>	0.374	0.277	0.392	0.317	0.409	0.345	1.106	2.028
	48	0.680	0.902	0.563	0.650	0.451	0.406	0.422	0.346	<b>0.413</b>	<b>0.332</b>	0.420	0.357	1.074	1.840
	96	0.666	0.886	0.631	0.779	0.595	0.668	0.597	0.696	0.552	0.586	<b>0.490</b>	<b>0.453</b>	1.002	1.692
	288	0.764	1.032	0.738	0.971	0.781	1.029	0.719	0.896	0.709	0.903	<b>0.655</b>	<b>0.784</b>	1.000	1.683
	672	0.760	1.039	0.769	1.073	0.819	1.121	0.788	1.046	0.845	1.151	<b>0.740</b>	<b>1.003</b>	1.041	1.706
ETTm2	24	0.575	0.530	0.494	0.388	0.517	0.424	<b>0.434</b>	<b>0.313</b>	0.455	0.347	0.507	0.426	1.160	2.576
	48	0.844	1.048	0.801	1.025	0.643	0.629	0.532	0.439	0.531	0.461	<b>0.531</b>	<b>0.435</b>	1.201	2.499
	96	0.841	1.127	0.862	1.140	0.849	1.060	0.724	0.785	0.748	0.847	<b>0.634</b>	<b>0.643</b>	1.261	2.600
	288	0.898	1.216	0.869	1.157	<b>0.886</b>	1.188	0.912	1.241	1.060	1.642	0.954	1.316	1.287	2.685
	672	1.221	2.388	1.258	2.484	<b>1.182</b>	<b>2.181</b>	1.196	2.280	1.380	2.922	1.480	3.276	1.346	2.955
Exch.	24	1.170	2.257	1.174	2.273	1.268	2.513	1.306	2.656	1.327	2.742	1.367	2.903	<b>1.151</b>	<b>2.029</b>
	48	1.193	2.452	1.189	2.445	1.219	2.432	1.296	2.667	1.302	2.683	1.348	2.886	<b>1.187</b>	<b>2.223</b>
	96	1.226	2.448	1.226	2.452	1.270	2.555	1.306	2.692	1.345	2.849	1.396	3.079	<b>1.190</b>	<b>2.227</b>
	288	1.305	2.776	1.298	2.743	1.285	2.685	1.316	2.802	1.330	2.860	1.324	2.771	<b>1.193</b>	<b>2.250</b>
	672	1.391	3.229	1.382	3.185	1.362	3.084	1.399	3.247	1.440	3.431	1.496	3.698	<b>1.171</b>	<b>2.305</b>
WTH	24	0.389	0.322	0.355	0.277	<b>0.332</b>	<b>0.252</b>	0.355	0.278	0.369	0.293	0.376	0.305	1.151	1.612
	48	0.451	0.408	0.425	0.364	0.373	0.300	<b>0.361</b>	<b>0.286</b>	0.369	0.296	0.415	0.352	1.187	1.719
	168	0.573	0.587	0.584	0.604	0.575	0.590	0.579	0.595	0.566	0.589	<b>0.545</b>	<b>0.541</b>	1.190	1.462
	336	0.580	0.593	0.574	0.587	0.584	0.599	0.579	0.592	<b>0.572</b>	<b>0.586</b>	0.578	0.587	1.193	1.529
	720	<b>0.561</b>	<b>0.559</b>	0.562	0.560	<b>0.561</b>	0.560	0.568	0.573	0.563	0.565	0.567	0.567	1.171	1.503
Electr.	24	0.801	0.987	0.802	0.981	0.803	0.987	0.804	0.988	0.803	0.986	<b>0.799</b>	<b>0.978</b>	0.873	1.143
	48	0.797	0.974	<b>0.797</b>	0.978	0.799	0.975	0.798	<b>0.972</b>	0.800	0.973	0.801	0.981	0.869	1.136
	168	0.802	0.993	<b>0.799</b>	0.979	0.803	0.989	0.802	<b>0.977</b>	0.804	0.992	0.801	0.984	0.866	1.130
	336	0.800	0.976	<b>0.798</b>	<b>0.973</b>	0.801	0.983	0.802	0.983	0.802	0.986	0.800	0.978	0.865	1.124
	720	0.804	0.976	<b>0.802</b>	<b>0.971</b>	0.804	0.978	0.806	0.974	0.804	0.976	0.803	0.977	0.860	1.106
Weath.	24	0.687	0.833	0.630	0.695	0.480	0.408	0.496	0.432	<b>0.430</b>	<b>0.343</b>	0.704	0.914	1.048	2.015
	48	0.706	0.839	0.664	0.779	0.601	0.607	0.561	<b>0.553</b>	0.552	0.566	<b>0.547</b>	0.554	1.075	2.000
	96	0.969	1.629	1.028	1.788	0.869	1.248	0.776	0.982	0.833	1.113	<b>0.771</b>	<b>0.928</b>	1.114	2.053
	288	0.939	1.375	1.008	1.564	0.954	1.430	0.982	1.510	0.990	1.544	<b>0.907</b>	<b>1.280</b>	1.102	1.919
	672	0.995	1.517	<b>0.993</b>	<b>1.502</b>	1.119	1.897	1.185	2.111	1.091	1.813	1.119	1.919	1.057	1.785
Traff.	24	<b>0.490</b>	<b>0.875</b>	0.788	1.429	0.549	0.983	0.818	1.498	0.576	1.034	0.631	1.142	0.923	1.816
	48	<b>0.506</b>	<b>0.900</b>	0.810	1.481	0.573	1.031	0.644	1.136	0.588	1.052	0.588	1.065	0.899	1.752
	96	<b>0.504</b>	<b>0.915</b>	0.816	1.503	0.796	1.462	0.817	1.507	0.591	1.083	0.753	1.382	0.913	1.796
	288	<b>0.521</b>	<b>0.972</b>	0.822	1.522	0.819	1.524	0.832	1.553	0.560	1.042	0.593	1.095	0.837	1.604
	672	<b>0.532</b>	<b>1.006</b>	0.819	1.533	0.579	1.067	0.835	1.576	0.655	1.223	0.827	1.575	0.868	1.692
Ili	24	1.989	7.856	2.097	8.458	<b>1.928</b>	<b>7.314</b>	2.101	8.299	2.223	9.321	2.276	9.847	2.160	8.860
	36	1.990	7.861	2.109	8.724	<b>1.960</b>	<b>7.565</b>	2.122	8.814	2.009	8.078	2.170	9.333	2.163	9.049
	48	2.000	7.917	2.085	8.461	<b>1.924</b>	<b>7.387</b>	1.992	7.702	2.155	8.819	2.164	8.998	2.125	8.757
	60	1.964	7.725	2.045	8.211	<b>1.941</b>	<b>7.564</b>	2.039	8.120	2.066	8.279	2.068	8.338	2.175	9.195
	Sum	29.549	45.023	30.441	45.394	28.210	39.631	29.739	42.316	28.331	39.774	28.788	41.148	28.903	42.926
	Avg	0.603	0.919	0.621	0.926	0.576	0.809	0.607	0.864	0.578	0.812	0.588	0.840	0.590	0.876

Table 9: Short-term forecasting for prediction length from 6 to 22 timestamps.

D	L	TS2Vec				SimTS				CoST				MaskAE				PatchTST		DLinear	
		TED4STL		Orig.		TED4STL		Orig.		TED4STL		Orig.		TED4STL		Orig.		MAE	MSE	MAE	MSE
		MAE	MSE	MAE	MSE	MAE	MSE	MAE	MSE	MAE	MSE	MAE	MSE	MAE	MSE	MAE	MSE				
ETTh1	6	0.329	0.231	0.445	0.436	<b>0.243</b>	<b>0.118</b>	0.341	0.259	0.387	0.332	0.355	0.272	0.658	0.831	1.087	1.743	0.327	0.255	0.313	0.242
	8	0.328	0.227	0.462	0.462	<b>0.245</b>	<b>0.119</b>	0.363	0.292	0.388	0.331	0.376	0.305	0.681	0.834	1.075	1.786	0.344	0.282	0.333	0.271
	10	0.331	0.230	0.475	0.483	<b>0.253</b>	<b>0.127</b>	0.382	0.318	0.389	0.330	0.389	0.326	0.632	0.752	0.976	1.537	0.353	0.297	0.342	0.286
	12	0.341	0.244	0.489	0.507	<b>0.267</b>	<b>0.142</b>	0.391	0.332	0.393	0.333	0.400	0.343	0.663	0.786	1.004	1.576	0.359	0.307	0.349	0.297
	14	0.352	0.264	0.498	0.523	<b>0.286</b>	<b>0.170</b>	0.398	0.343	0.401	0.346	0.408	0.355	0.744	0.964	0.986	1.562	0.364	0.315	0.354	0.305
	16	0.361	0.282	0.500	0.529	<b>0.304</b>	<b>0.198</b>	0.404	0.353	0.413	0.367	0.414	0.364	0.628	0.764	0.998	1.584	0.367	0.319	0.357	0.310
	18	0.373	0.301	0.501	0.530	<b>0.320</b>	<b>0.224</b>	0.409	0.361	0.423	0.386	0.418	0.370	0.727	0.965	1.016	1.654	0.369	0.322	0.359	0.314
ETTh2	6	0.384	0.319	0.504	0.535	<b>0.333</b>	<b>0.245</b>	0.413	0.366	0.432	0.403	0.422	0.375	0.735	0.945	1.018	1.586	0.371	0.326	0.362	0.317
	8	0.393	0.333	0.506	0.536	<b>0.344</b>	<b>0.262</b>	0.416	0.371	0.440	0.416	0.425	0.379	0.824	1.148	1.010	1.590	0.372	0.327	0.363	0.318
	10	0.218	0.097	0.316	0.195	<b>0.197</b>	<b>0.072</b>	0.293	0.166	0.260	0.124	0.337	0.205	1.139	1.953	1.311	2.811	0.211	0.106	0.209	0.105
	12	0.221	0.099	0.341	0.222	<b>0.202</b>	<b>0.076</b>	0.317	0.189	0.271	0.135	0.363	0.237	0.985	1.502	1.285	2.782	0.221	0.116	0.219	0.114
	14	0.226	0.102	0.362	0.247	<b>0.217</b>	<b>0.088</b>	0.337	0.211	0.284	0.146	0.387	0.268	0.964	1.426	1.323	2.914	0.230	0.125	0.228	0.123
	16	<b>0.234</b>	<b>0.109</b>	0.385	0.277	0.239	0.110	0.355	0.232	0.298	0.160	0.408	0.295	0.989	1.460	1.228	2.489	0.238	0.133	0.235	0.131
	18	<b>0.245</b>	<b>0.121</b>	0.401	0.299	0.257	0.129	0.372	0.254	0.317	0.182	0.427	0.324	0.998	1.517	1.264	2.650	0.244	0.141	0.244	0.140
ETTm1	6	<b>0.257</b>	<b>0.134</b>	0.415	0.319	0.279	0.154	0.388	0.275	0.338	0.209	0.446	0.353	1.144	2.062	1.238	2.410	0.249	0.147	<b>0.249</b>	0.146
	8	0.271	<b>0.150</b>	0.429	0.340	0.301	0.180	0.404	0.296	0.356	0.232	0.463	0.380	1.080	1.717	1.296	2.784	<b>0.255</b>	0.154	<b>0.255</b>	<b>0.153</b>
	10	0.284	0.164	0.443	0.363	0.317	0.197	0.418	0.317	0.376	0.262	0.478	0.405	1.307	2.661	1.333	2.963	<b>0.258</b>	0.160	0.260	<b>0.159</b>
	12	0.300	0.183	0.461	0.390	0.336	0.221	0.429	0.329	0.396	0.292	0.494	0.430	1.117	1.910	1.311	2.836	<b>0.262</b>	0.165	0.263	<b>0.164</b>
	14	0.170	0.061	0.250	0.145	<b>0.141</b>	<b>0.042</b>	0.204	0.098	0.170	0.059	0.211	0.101	0.258	0.137	1.172	2.189	0.177	0.079	0.185	0.089
	16	0.177	0.066	0.283	0.184	<b>0.144</b>	<b>0.043</b>	0.224	0.119	0.173	0.060	0.231	0.121	0.258	0.140	1.095	1.992	0.193	0.095	0.202	0.106
	18	0.189	0.075	0.314	0.227	<b>0.148</b>	<b>0.046</b>	0.243	0.139	0.179	0.064	0.249	0.141	0.243	0.119	1.126	2.114	0.207	0.108	0.217	0.123
ETTm2	6	0.204	0.089	0.342	0.269	<b>0.157</b>	<b>0.052</b>	0.258	0.157	0.188	0.071	0.264	0.159	0.274	0.156	1.101	2.080	0.218	0.122	0.230	0.138
	8	0.220	0.108	0.367	0.308	<b>0.169</b>	<b>0.063</b>	0.272	0.174	0.200	0.082	0.278	0.176	0.295	0.189	1.059	1.902	0.231	0.137	0.242	0.153
	10	0.237	0.128	0.387	0.342	<b>0.183</b>	<b>0.076</b>	0.285	0.189	0.213	0.096	0.291	0.192	0.332	0.223	1.079	1.930	0.241	0.149	0.252	0.167
	12	0.253	0.148	0.406	0.373	<b>0.197</b>	<b>0.090</b>	0.296	0.204	0.226	0.111	0.302	0.208	0.367	0.272	1.118	2.104	0.251	0.162	0.266	0.183
	14	0.268	0.168	0.421	0.400	<b>0.211</b>	<b>0.106</b>	0.306	0.217	0.239	0.126	0.312	0.221	0.380	0.301	1.075	1.955	0.260	0.178	0.274	0.193
	16	0.282	0.188	0.434	0.424	<b>0.225</b>	<b>0.123</b>	0.315	0.230	0.251	0.142	0.321	0.234	0.407	0.351	1.056	1.838	0.269	0.185	0.277	0.202
	18	0.146	0.044	0.219	0.103	<b>0.130</b>	<b>0.034</b>	0.162	0.060	0.162	0.051	0.191	0.075	0.364	0.213	1.142	2.389	0.140	0.055	0.142	0.056
Exch.	8	0.151	0.046	0.235	0.118	<b>0.136</b>	<b>0.037</b>	0.173	0.068	0.165	0.053	0.201	0.082	0.498	0.393	1.084	2.272	0.150	0.062	0.153	0.063
	10	0.157	0.050	0.248	0.130	<b>0.143</b>	<b>0.041</b>	0.183	0.075	0.171	0.056	0.210	0.090	0.467	0.344	1.154	2.563	0.158	0.067	0.160	0.069
	12	0.166	0.057	0.260	0.142	<b>0.150</b>	<b>0.044</b>	0.192	0.081	0.178	0.061	0.219	0.097	0.437	0.299	1.142	2.438	0.164	0.072	0.168	0.074
	14	0.175	0.064	0.270	0.152	<b>0.157</b>	<b>0.049</b>	0.200	0.087	0.186	0.067	0.227	0.104	0.512	0.399	1.149	2.427	0.171	0.078	0.174	0.079
	16	0.185	0.073	0.279	0.162	<b>0.165</b>	<b>0.055</b>	0.208	0.093	0.194	0.073	0.234	0.110	0.367	0.235	1.096	2.262	0.175	0.081	0.178	0.083
	18	0.193	0.080	0.287	0.170	<b>0.173</b>	<b>0.061</b>	0.215	0.098	0.201	0.079	0.240	0.116	0.447	0.338	1.212	2.661	0.179	0.085	0.184	0.087
	20	0.199	0.086	0.295	0.178	<b>0.181</b>	<b>0.067</b>	0.222	0.103	0.209	0.085	0.247	0.122	0.480	0.362	1.213	2.722	0.185	0.088	0.190	0.091
WTH	6	0.206	0.091	0.302	0.186	<b>0.187</b>	<b>0.072</b>	0.228	0.108	0.217	0.092	0.254	0.128	0.452	0.347	1.120	2.351	0.189	0.092	<b>0.192</b>	<b>0.095</b>
	8	0.125	0.029	0.159	0.045	0.109	0.021	0.112	0.023	0.153	0.041	0.177	0.054	1.197	2.572	1.149	2.011	0.075	0.012	<b>0.059</b>	<b>0.009</b>
	10	0.131	0.032	0.172	0.054	0.115	0.024	0.125	0.029	0.162	0.046	0.190	0.063	1.140	2.379	1.137	1.993	0.080	0.014	<b>0.066</b>	<b>0.010</b>
	12	0.137	0.034	0.179	0.058	0.122	0.027	0.138	0.035	0.173	0.052	0.204	0.072	1.155	2.304	1.122	2.043	0.095	0.015	<b>0.074</b>	<b>0.013</b>
	14	0.149	0.039	0.184	0.061	0.120	0.026	0.149	0.041	0.184	0.059	0.215	0.081	1.215	2.509	1.113	1.926	0.091	0.018	<b>0.083</b>	<b>0.016</b>
	16	0.156	0.043	0.196	0.070	0.128	0.031	0.161	0.048	0.196	0.068	0.227	0.090	1.157	2.324	1.131	2.141	0.095	0.019	<b>0.083</b>	<b>0.016</b>
	18	0.164	0.048	0.201	0.073	0.137	0.036	0.172	0.056	0.207	0.076	0.237	0.098	1.198	2.343	1.130	2.006	0.099	0.021	<b>0.088</b>	<b>0.018</b>
Electr.	6	0.173	0.054	0.212	0.081	0.147	0.042	0.182	0.062	0.218	0.084	0.245	0.105	1.157	2.485	1.184	2.206	0.104	0.023	<b>0.093</b>	<b>0.019</b>
	8	0.192	0.064	0.222	0.090	0.158	0.049	0.193	0.070	0.228	0.092	0.255	0.113	1.245	2.622	1.163	2.106	0.108	0.025	0.099	<b>0.021</b>
	10	0.201	0.071	0.224	0.092	0.166	0.054	0.203	0.078	0.240	0.102	0.266	0.124	1.178	2.437	1.153	2.071	0.112	0.026	0.103	<b>0.023</b>
	12	0.231	0.170	0.283	0.230	<b>0.223</b>	<b>0.151</b>	0.279	0.222	0.242	0.168	0.287	0.227	0.273	0.191	1.046	1.828	0.270	0.232	0.298	0.259
	14	0.236	0.173	0.299	0.244	<b>0.227</b>	<b>0.154</b>	0.294	0.235	0.243	0.168	0.302	0.240	0.259	0.173	1.041	1.792	0.288	0.248	0.315	0.276
	16	0.242	0.177	0.312	0.257	<b>0.233</b>	<b>0.158</b>	0.307	0.246	0.245	0.169	0.313	0.250	0.273	0.185	1.054	1.839	0.301	0.261	0.329	0.291
	18	0.250	0.183	0.322	0.267	<b>0.242</b>	<b>0.165</b>	0.317	0.256	0.250	0.172	0.323	0.259	0.295	0.209	1.119	2.031	0.314	0.273	0.341	0.303
Weath.	6	0.260	0.193	0.332	0.276	<b>0.253</b>	<b>0.177</b>	0.326	0.264	0.260	0.182	0.331	0.267	0.301	0.216	1.109	1.989	0.324	0.283	0.350	0.313

**Table 10: Ablation for the 1st pipeline application with kernel size of 25 timestamps - bold: best results, underlined: second best results.**

(a) MSE ablation									
D	L	Ts2Vec				SimTS			
		TED4STL	Trend	Err	Orig.	TED4STL	Trend	Err	Orig.
ETTh1	24	<b>0.342</b>	0.515	1.081	0.549	<b>0.274</b>	0.418	0.952	0.374
	48	<b>0.440</b>	0.574	1.118	0.598	<b>0.373</b>	0.486	0.970	0.424
	168	<b>0.668</b>	<u>0.728</u>	1.146	0.758	<b>0.615</b>	0.696	1.007	<u>0.644</u>
	336	<b>0.863</b>	0.898	1.119	0.899	<b>0.827</b>	0.892	1.015	<u>0.844</u>
	720	<b>1.044</b>	1.098	1.046	1.060	1.004	1.083	<b>0.947</b>	1.014
ETTh2	24	<b>0.202</b>	0.206	3.489	0.389	<b>0.243</b>	0.278	3.530	0.346
	48	<b>0.412</b>	0.407	3.476	0.562	<b>0.498</b>	0.529	3.523	0.586
	168	<b>1.655</b>	1.742	3.508	1.845	<b>1.626</b>	1.635	3.534	1.661
	336	<b>2.079</b>	<u>2.213</u>	3.471	2.291	<b>1.912</b>	1.918	3.506	1.932
	720	<b>2.389</b>	2.471	3.503	2.717	<b>2.115</b>	2.134	3.574	2.148
ETTm1	24	<b>0.200</b>	0.308	1.110	0.391	<b>0.138</b>	0.147	1.063	0.240
	48	<b>0.352</b>	0.479	1.120	0.498	<b>0.265</b>	0.270	1.072	0.319
	96	<b>0.441</b>	0.567	1.123	0.564	<b>0.344</b>	0.347	1.068	0.369
	288	<b>0.570</b>	0.654	1.121	0.633	<b>0.452</b>	0.456	1.069	0.464
	672	<b>0.700</b>	0.763	1.113	0.731	<b>0.610</b>	0.616	1.087	0.617
ETTm2	24	<b>0.097</b>	0.105	3.433	0.155	<b>0.078</b>	0.079	3.499	0.113
	48	<b>0.162</b>	0.181	3.431	0.219	<b>0.139</b>	0.141	3.501	0.168
	96	<b>0.287</b>	<u>0.312</u>	3.429	0.325	<b>0.249</b>	<u>0.250</u>	3.502	0.272
	288	<b>0.681</b>	0.673	3.434	0.690	<b>0.695</b>	0.703	3.498	0.713
	672	<b>1.796</b>	1.984	3.443	1.831	<b>1.651</b>	1.647	3.498	1.658
Exch.	24	<b>0.076</b>	0.072	5.092	0.099	<b>0.062</b>	0.067	5.0905	0.086
	48	<b>0.171</b>	0.159	5.093	0.184	<b>0.169</b>	0.172	5.0882	0.192
	96	0.429	0.442	5.069	<b>0.390</b>	<b>0.417</b>	0.421	5.0648	0.439
	288	1.449	<u>1.321</u>	5.025	<b>1.352</b>	<b>1.298</b>	<u>1.309</u>	5.0447	1.312
	672	<b>1.970</b>	2.149	5.174	3.501	<b>1.873</b>	1.897	5.1729	1.889
WTH	24	<b>0.241</b>	0.262	0.701	0.310	0.229	<b>0.219</b>	0.751	0.294
	48	<b>0.320</b>	0.334	0.712	0.377	0.309	<b>0.305</b>	0.761	0.356
	168	<b>0.458</b>	0.477	0.742	0.499	<u>0.451</u>	<b>0.449</b>	0.774	0.465
	336	<b>0.500</b>	0.511	0.747	0.535	<u>0.492</u>	<b>0.490</b>	0.774	0.500
	720	<b>0.536</b>	<u>0.543</u>	0.746	0.571	<b>0.530</b>	<b>0.530</b>	0.771	0.537
Electr.	24	<b>0.202</b>	0.387	0.454	0.285	<b>0.103</b>	0.486	0.423	0.139
	48	<b>0.237</b>	0.419	0.463	<u>0.307</u>	<b>0.135</b>	0.508	0.430	<u>0.154</u>
	168	<b>0.281</b>	0.456	0.472	<u>0.331</u>	<b>0.172</b>	0.523	0.427	0.176
	336	<b>0.302</b>	0.474	0.473	<u>0.348</u>	<b>0.194</b>	0.532	0.421	0.195
	720	<b>0.334</b>	0.498	0.474	0.375	<b>0.231</b>	0.530	0.414	0.233
Weath.	24	0.259	<b>0.196</b>	4.368	0.316	0.141	<b>0.128</b>	4.129	0.241
	48	0.792	<b>0.588</b>	4.355	0.808	<u>0.444</u>	<b>0.421</b>	4.139	0.526
	96	1.518	<b>1.043</b>	4.422	<u>1.297</u>	0.998	<b>0.920</b>	4.108	<u>0.957</u>
	288	1.842	1.628	4.368	<b>1.608</b>	1.910	<b>1.292</b>	4.076	1.296
	672	2.772	2.532	4.557	<b>2.424</b>	2.417	<b>1.752</b>	4.115	1.749
Traff.	24	0.883	1.052	<b>0.870</b>	0.914	<b>0.731</b>	1.328	0.754	<u>0.756</u>
	48	<b>0.920</b>	1.069	0.915	0.958	<b>0.765</b>	1.337	0.784	0.793
	96	<b>0.969</b>	1.080	<u>0.974</u>	1.017	<b>0.790</b>	1.347	0.802	0.809
	288	0.994	1.091	<b>0.990</b>	1.036	<b>0.803</b>	1.365	0.809	<u>0.815</u>
	672	1.009	1.107	<b>1.001</b>	1.073	<b>0.817</b>	1.420	0.821	0.827
Ili	24	<b>2.919</b>	8.167	4.816	3.625	<b>1.975</b>	2.048	5.118	2.640
	36	<b>3.506</b>	4.207	5.033	<u>3.821</u>	<u>2.422</u>	<b>2.394</b>	5.246	2.905
	48	<b>4.027</b>	4.317	5.302	<u>4.058</u>	<u>2.809</u>	<b>2.712</b>	5.439	3.183
	60	<b>4.016</b>	<u>4.248</u>	5.471	4.319	<u>3.335</u>	<b>3.089</b>	5.617	3.572

(b) MAE ablation									
D	L	Ts2Vec				SimTS			
		TED4STL	Trend	Err	Orig.	TED4STL	Trend	Err	Orig.
ETTh1	24	<b>0.400</b>	0.477	0.810	0.509	<b>0.352</b>	0.439	0.794	0.418
	48	<b>0.461</b>	0.512	0.820	0.543	<b>0.417</b>	0.481	0.798	0.452
	168	<b>0.593</b>	<u>0.605</u>	0.828	0.638	<b>0.565</b>	0.608	0.804	<u>0.581</u>
	336	<b>0.698</b>	0.701	0.821	0.713	<b>0.681</b>	0.715	0.800	0.690
	720	<b>0.794</b>	0.799	0.783	0.795	<u>0.781</u>	0.818	<b>0.762</b>	0.786
ETTh2	24	<b>0.316</b>	0.326	1.440	0.459	<b>0.353</b>	<u>0.382</u>	1.445	0.441
	48	<b>0.469</b>	0.469	1.435	0.572	<b>0.526</b>	<u>0.547</u>	1.444	0.586
	168	<b>0.994</b>	1.009	1.441	1.060	<b>0.985</b>	0.993	1.449	1.002
	336	<b>1.148</b>	<u>1.180</u>	1.432	1.210	<b>1.087</b>	<u>1.095</u>	1.444	1.098
	720	<b>1.293</b>	1.299	1.445	1.396	<b>1.168</b>	1.183	1.465	1.185
ETTm1	24	<b>0.289</b>	0.363	0.831	0.407	<b>0.238</b>	0.248	0.819	0.322
	48	<b>0.389</b>	0.465	0.833	0.472	<b>0.334</b>	0.340	0.819	0.377
	96	<b>0.448</b>	0.529	0.832	0.518	<b>0.391</b>	0.396	0.817	0.413
	288	<b>0.532</b>	0.579	0.828	0.569	<b>0.470</b>	0.475	0.815	0.480
	672	<b>0.611</b>	0.639	0.820	<u>0.628</u>	<b>0.566</b>	0.571	0.818	0.572
ETTm2	24	<b>0.213</b>	0.227	1.426	0.273	0.195	<b>0.194</b>	1.432	0.234
	48	<b>0.277</b>	0.300	1.425	0.332	<b>0.265</b>	0.267	1.432	0.295
	96	<b>0.372</b>	<u>0.396</u>	1.425	0.409	<b>0.363</b>	<u>0.365</u>	1.433	0.383
	288	<b>0.617</b>	0.620	1.425	0.629	<b>0.634</b>	<u>0.638</u>	1.433	0.645
	672	<b>1.020</b>	1.077	1.427	1.030	<b>0.992</b>	0.996	1.435	0.999
Exch.	24	<b>0.206</b>	0.200	1.834	0.235	<b>0.177</b>	0.184	1.8334	0.214
	48	<b>0.314</b>	0.303	1.833	0.319	<b>0.296</b>	0.298	1.8339	0.319
	96	0.522	0.497	1.831	<b>0.463</b>	<b>0.475</b>	0.478	1.8279	0.491
	288	0.967	0.880	1.818	<b>0.887</b>	<b>0.907</b>	<u>0.911</u>	1.819	0.914
	672	<b>1.094</b>	1.104	1.855	1.362	<b>1.094</b>	1.102	1.8546	1.100
WTH	24	<b>0.306</b>	0.329	0.643	0.365	0.301	<b>0.292</b>	0.670	0.356
	48	<b>0.374</b>	0.391	0.650	0.419	0.370	<b>0.365</b>	0.674	0.408
	168	<b>0.481</b>	0.496	0.665	0.509	<b>0.479</b>	0.478	0.680	0.492
	336	<b>0.513</b>	0.523	0.667	0.535	0.511	<b>0.510</b>	0.679	0.518
	720	<b>0.539</b>	<u>0.547</u>	0.668	0.559	<b>0.538</b>	<b>0.538</b>	0.678	0.544
Electr.	24	<b>0.317</b>	0.472	0.488	0.373	<b>0.210</b>	0.524	0.463	0.243
	48	<b>0.343</b>	0.488	0.494	<u>0.389</u>	<b>0.240</b>	0.535	0.466	<u>0.258</u>
	168	<b>0.375</b>	0.508	0.499	<u>0.407</u>	<b>0.273</b>	0.544	0.465	0.276
	336	<b>0.392</b>	0.518	0.501	<u>0.420</u>	<b>0.296</b>	0.549	0.462	<b>0.296</b>
	720	<b>0.414</b>	0.530	0.504	<u>0.439</u>	<b>0.329</b>	0.549	0.458	<b>0.329</b>
Weath.	24	0.310	<b>0.271</b>	1.659	0.349	<u>0.232</u>	<b>0.212</b>	1.642	0.306
	48	0.565	<b>0.487</b>	1.646	0.584	<u>0.436</u>	<b>0.414</b>	1.644	0.484
	96	0.842	<b>0.709</b>	1.661	<u>0.788</u>	<u>0.691</u>	<b>0.665</b>	1.635	0.695
	288	0.991	0.955	1.652	<b>0.939</b>	1.032	<b>0.854</b>	1.628	0.859
	672	1.279	1.246	1.690	<b>1.220</b>	1.221	<b>1.032</b>	1.639	1.033
Traff.	24	0.550	0.589	<b>0.523</b>	<u>0.541</u>	<u>0.438</u>	0.740	0.449	<b>0.431</b>
	48	<b>0.530</b>	0.586	0.539	0.556	<u>0.453</u>	0.738	0.461	<b>0.451</b>
	96	<b>0.550</b>	0.585	0.559	0.564	<b>0.464</b>	0.742	0.466	0.475
	288	<u>0.564</u>	0.589	<b>0.562</b>	0.571	<b>0.464</b>	0.746	0.464	<u>0.472</u>
	672	0.568	0.594	<b>0.566</b>	0.600	<b>0.467</b>	0.778	0.466	0.474
Ili	24	<b>1.104</b>	2.015	1.579	1.209	<b>0.904</b>	0.934	1.632	1.048
	36	<b>1.251</b>	1.356	1.594	<u>1.272</u>	<b>0.981</b>	<u>0.984</u>	1.635	1.075
	48	<b>1.335</b>	1.371	1.627	<u>1.324</u>	<u>1.055</u>	<b>1.040</b>	1.660	1.124
	60	<b>1.318</b>	<u>1.369</u>	1.650	1.374	<u>1.150</u>	<b>1.115</b>	1.690	1.204

**Table 11: Ablation for the 2st pipeline application with kernel size of 25 timestamps - bold: best results, underlined: second best results.**

(a) MSE ablation									(b) MAE ablation										
D	L	CoST				MaskAE				D	L	CoST				MaskAE			
		TED4STL	Trend	Err	Orig.	TED4STL	Trend	Err	Orig.			TED4STL	Trend	Err	Orig.	TED4STL	Trend	Err	Orig.
ETT <sub>h1</sub>	24	0.392	0.427	0.414	<b>0.383</b>	<b>1.047</b>	1.245	1.281	1.484	ETT <sub>h1</sub>	24	<b>0.426</b>	0.447	0.441	0.427	<b>0.783</b>	0.852	0.877	0.958
	48	0.466	0.491	0.489	<b>0.434</b>	<b>1.166</b>	1.237	1.243	1.544		48	0.475	0.491	0.489	<b>0.463</b>	<b>0.851</b>	0.894	0.862	0.997
	168	0.668	0.677	0.676	<b>0.633</b>	<b>1.144</b>	1.245	1.266	1.320		168	0.599	0.605	0.607	<b>0.578</b>	<b>0.825</b>	0.897	0.872	0.913
	336	0.854	0.853	0.829	<b>0.792</b>	<b>1.165</b>	1.293	1.296	1.289		336	0.700	0.700	0.694	<b>0.670</b>	<b>0.844</b>	0.915	0.882	0.895
	720	1.029	1.041	0.996	<b>0.904</b>	<b>1.158</b>	1.385	1.271	1.370		720	0.797	0.803	0.786	<b>0.748</b>	<b>0.836</b>	0.974	0.869	0.934
ETT <sub>h2</sub>	24	0.320	0.319	<b>0.312</b>	0.453	<b>2.385</b>	2.418	3.292	2.994	ETT <sub>h2</sub>	24	<b>0.414</b>	0.415	0.415	0.507	<b>1.245</b>	1.285	1.369	1.339
	48	0.606	0.605	<b>0.585</b>	0.699	<b>2.091</b>	2.372	3.262	2.820		48	0.582	0.582	<b>0.577</b>	0.640	<b>1.152</b>	1.271	1.373	1.311
	168	1.701	1.701	1.638	<b>1.538</b>	<b>2.598</b>	2.636	3.364	3.141		168	1.028	1.028	0.998	<b>0.983</b>	<b>1.265</b>	1.322	1.391	1.406
	336	1.935	1.935	1.883	<b>1.743</b>	2.932	<b>2.356</b>	3.395	2.741		336	1.116	1.116	1.087	<b>1.050</b>	1.402	<b>1.210</b>	1.398	1.317
	720	2.098	2.098	2.081	<b>1.955</b>	<b>2.875</b>	2.705	3.432	3.302		720	1.173	1.173	1.147	<b>1.089</b>	<b>1.290</b>	1.291	1.406	1.436
ETT <sub>m1</sub>	24	<b>0.154</b>	0.157	0.156	0.246	<b>0.424</b>	0.249	1.249	2.028	ETT <sub>m1</sub>	24	<b>0.258</b>	0.263	0.262	0.329	<b>0.468</b>	0.347	0.848	1.106
	48	<b>0.277</b>	0.280	0.279	0.330	<b>0.650</b>	0.521	1.272	1.840		48	<b>0.346</b>	0.350	0.349	0.386	<b>0.563</b>	0.507	0.862	1.074
	96	<b>0.353</b>	0.354	0.354	0.377	<b>0.779</b>	0.673	1.275	1.692		96	<b>0.401</b>	0.403	0.403	0.419	<b>0.631</b>	0.601	0.868	1.002
	288	<b>0.463</b>	0.463	0.464	0.471	<b>0.971</b>	0.978	1.257	1.683		288	<b>0.480</b>	0.480	0.481	0.485	<b>0.738</b>	0.748	0.868	1.000
	672	0.622	0.623	<b>0.620</b>	0.622	<b>1.073</b>	1.229	1.259	1.706		672	0.575	0.576	0.576	<b>0.574</b>	<b>0.769</b>	0.880	0.864	1.041
ETT <sub>m2</sub>	24	<b>0.099</b>	<b>0.099</b>	<b>0.099</b>	0.134	<b>0.388</b>	0.176	3.335	2.576	ETT <sub>m2</sub>	24	<b>0.225</b>	<b>0.225</b>	0.225	0.259	<b>0.494</b>	0.317	1.386	1.160
	48	<b>0.163</b>	<b>0.163</b>	0.164	0.196	<b>1.025</b>	0.691	3.026	2.499		48	<b>0.290</b>	<b>0.290</b>	0.292	0.320	<b>0.801</b>	0.657	1.322	1.201
	96	<b>0.274</b>	<b>0.274</b>	<b>0.274</b>	0.305	<b>1.140</b>	1.344	3.346	2.600		96	<b>0.380</b>	<b>0.380</b>	0.382	0.405	<b>0.862</b>	0.968	1.401	1.261
	288	0.737	0.736	<b>0.731</b>	0.754	<b>1.157</b>	1.418	3.232	2.685		288	<b>0.647</b>	<b>0.647</b>	<b>0.647</b>	0.661	<b>0.869</b>	1.005	1.366	1.287
	672	1.663	1.663	1.683	<b>1.589</b>	<b>2.484</b>	2.844	3.192	2.955		672	1.003	1.003	1.010	<b>0.982</b>	<b>1.258</b>	1.362	1.352	1.346
Exch.	24	<b>0.111</b>	<b>0.111</b>	0.129	0.133	2.273	2.215	4.096	<b>2.029</b>	Exch.	24	<b>0.252</b>	<b>0.252</b>	0.271	0.277	1.174	1.149	1.606	<b>1.151</b>
	48	<b>0.226</b>	<b>0.226</b>	0.254	0.250	2.445	2.363	4.146	2.223		48	<b>0.362</b>	<b>0.362</b>	0.385	0.383	1.189	1.169	1.607	<b>1.187</b>
	96	<b>0.489</b>	<b>0.489</b>	0.512	0.505	2.452	2.425	4.155	2.227		96	<b>0.541</b>	<b>0.541</b>	0.554	0.548	1.226	1.184	1.616	<b>1.190</b>
	288	1.315	1.315	1.349	<b>1.278</b>	2.743	2.419	4.268	<b>2.250</b>		288	0.903	0.903	0.919	<b>0.883</b>	1.298	1.205	1.648	<b>1.193</b>
	672	2.020	2.020	2.015	<b>1.942</b>	3.185	3.065	4.138	<b>2.305</b>		672	1.104	1.104	1.098	<b>1.075</b>	1.382	1.344	1.610	<b>1.171</b>
WTH	24	0.232	0.233	<b>0.228</b>	0.299	<b>0.277</b>	0.264	0.462	1.612	WTH	24	0.305	0.306	<b>0.303</b>	0.361	<b>0.355</b>	0.334	0.492	1.151
	48	<b>0.315</b>	0.316	<b>0.314</b>	0.360	<b>0.364</b>	0.366	0.581	1.719		48	<b>0.375</b>	0.376	<b>0.375</b>	0.412	<b>0.425</b>	0.419	0.571	1.187
	168	<b>0.452</b>	<b>0.452</b>	<b>0.452</b>	0.465	<b>0.604</b>	0.639	0.564	1.462		168	<b>0.482</b>	<b>0.482</b>	<b>0.482</b>	0.492	<b>0.584</b>	0.605	0.559	1.190
	336	0.491	0.491	<b>0.490</b>	0.498	<b>0.587</b>	0.619	0.594	1.529		336	<b>0.512</b>	<b>0.512</b>	<b>0.512</b>	0.518	<b>0.574</b>	0.597	0.571	1.193
	720	<b>0.530</b>	<b>0.530</b>	<b>0.530</b>	0.533	<b>0.560</b>	0.582	0.549	1.503		720	<b>0.539</b>	<b>0.539</b>	<b>0.539</b>	0.542	<b>0.562</b>	0.574	0.552	1.171
Electr.	24	0.296	0.296	0.253	<b>0.135</b>	<b>0.981</b>	0.994	0.985	1.143	Electr.	24	0.409	0.409	0.370	<b>0.241</b>	<b>0.802</b>	0.810	0.803	0.873
	48	0.320	0.319	0.277	<b>0.152</b>	<b>0.978</b>	0.982	0.988	1.136		48	0.423	0.423	0.387	<b>0.257</b>	<b>0.797</b>	0.806	0.805	0.869
	168	0.355	0.355	0.314	<b>0.175</b>	<b>0.979</b>	0.989	0.996	1.130		168	0.444	0.444	0.411	<b>0.275</b>	<b>0.799</b>	0.810	0.810	0.866
	336	0.378	0.375	0.334	<b>0.195</b>	<b>0.973</b>	0.993	0.989	1.124		336	0.459	0.457	0.425	<b>0.296</b>	<b>0.798</b>	0.812	0.810	0.865
	720	0.407	0.404	0.367	<b>0.231</b>	<b>0.971</b>	0.990	0.991	1.106		720	0.476	0.475	0.446	<b>0.328</b>	<b>0.802</b>	0.808	0.809	0.860
Weath.	24	<b>0.176</b>	<b>0.176</b>	0.175	0.258	0.695	<b>0.200</b>	1.942	2.015	Weath.	24	<b>0.273</b>	<b>0.273</b>	0.275	0.337	0.630	<b>0.287</b>	1.066	1.048
	48	<b>0.432</b>	<b>0.432</b>	0.447	0.496	0.779	<b>0.577</b>	1.977	2.000		48	<b>0.442</b>	<b>0.442</b>	0.452	0.488	0.664	<b>0.546</b>	1.138	1.075
	96	0.827	0.827	0.860	<b>0.787</b>	1.788	1.364	1.536	2.053		96	0.645	0.645	0.658	<b>0.642</b>	1.028	<b>0.863</b>	0.992	1.114
	288	1.437	1.437	1.740	<b>1.082</b>	1.564	<b>1.120</b>	1.451	1.919		288	0.895	0.895	0.989	<b>0.794</b>	1.008	<b>0.806</b>	0.965	1.102
	672	2.134	2.134	2.505	<b>1.535</b>	1.502	1.262	<b>1.175</b>	1.785		672	1.145	1.145	1.248	<b>0.977</b>	0.993	0.896	<b>0.862</b>	1.057
Traff.	24	0.910	0.966	0.924	<b>0.721</b>	1.429	<b>1.209</b>	1.293	1.816	Traff.	24	0.559	0.595	0.566	<b>0.423</b>	0.788	<b>0.649</b>	0.693	0.923
	48	0.938	0.989	0.958	<b>0.745</b>	1.481	<b>1.083</b>	1.210	1.752		48	0.567	0.599	0.577	<b>0.437</b>	0.810	<b>0.585</b>	0.658	0.899
	96	0.967	1.018	0.992	<b>0.755</b>	1.503	<b>1.324</b>	1.385	1.796		96	0.574	0.604	0.589	<b>0.438</b>	0.816	<b>0.711</b>	0.738	0.913
	288	0.986	1.043	1.008	<b>0.764</b>	1.522	1.548	<b>1.235</b>	1.604		288	0.577	0.610	0.590	<b>0.434</b>	0.822	0.816	<b>0.656</b>	0.837
	672	0.990	1.068	1.044	<b>0.777</b>	1.533	1.524	<b>1.481</b>	1.692		672	0.577	0.622	0.606	<b>0.435</b>	0.819	0.796	<b>0.778</b>	0.868
Ili	24	<b>2.166</b>	2.190	2.263	2.872	<b>8.345</b>	9.406	7.626	8.860	Ili	24	<b>0.961</b>	0.974	0.978	1.077	<b>2.082</b>	2.193	1.989	2.160
	36	<b>2.608</b>	2.673	2.735	3.155	<b>8.902</b>	9.451	8.432	9.049		36	<b>1.030</b>	1.048	1.057	1.122	<b>2.128</b>	2.201	2.069	2.163
	48	<b>2.984</b>	3.047	3.090	3.439	<b>8.353</b>	10.546	8.191	8.757		48	<b>1.094</b>	1.110	1.123	1.178	<b>2.069</b>	2.404	2.050	2.125
	60	<b>3.356</b>	3.380	3.478	3.831	<b>8.254</b>	9.399	8.252	9.195		60	<b>1.169</b>	1.179	1.202	1.261	<b>2.053</b>	2.217	2.050	2.175