

Micromechanics of thermoplastic elastomers with random microstructures^[1]

Hansohl Cho*, Jaehee Lee, Jehoon Moon

Korea Advanced Institute of Science and Technology

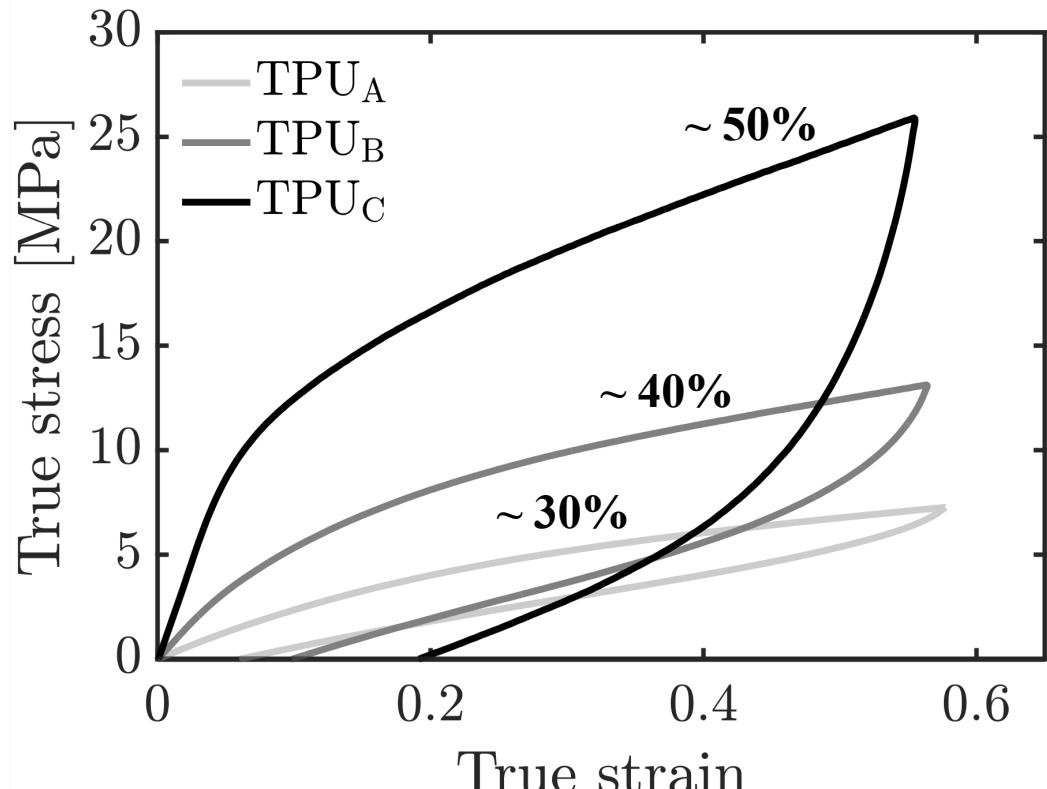
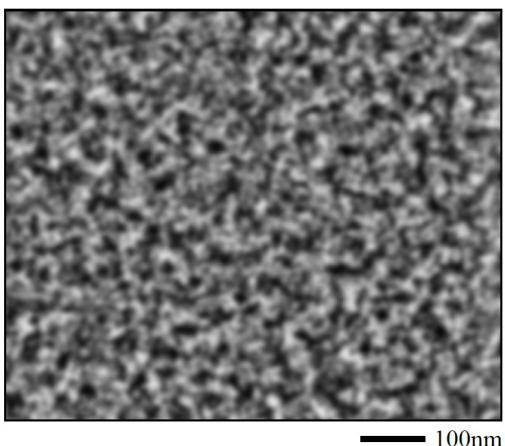
Gregory C Rutledge

Massachusetts Institute of Technology

Mary C Boyce

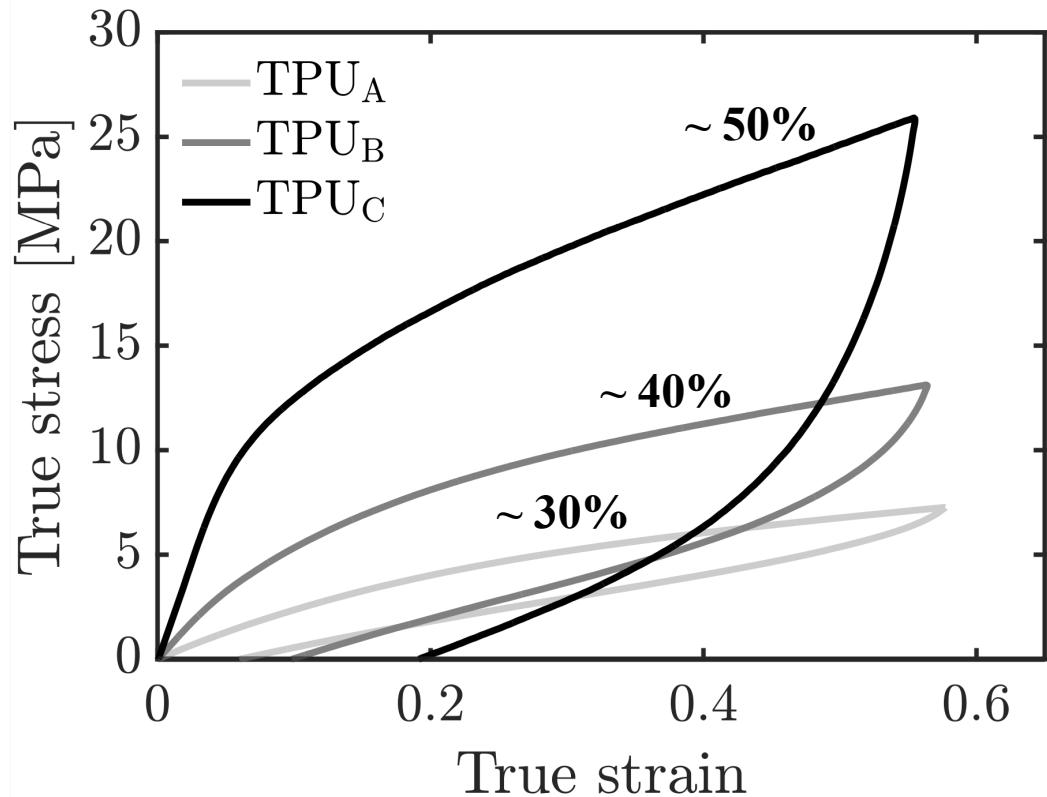
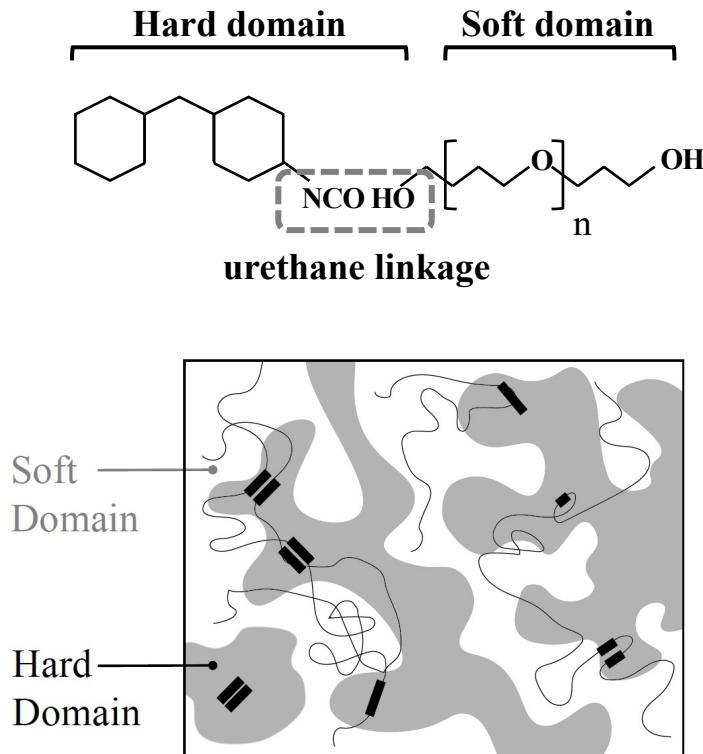
Columbia University

Thermoplastic polyurethanes (TPU)



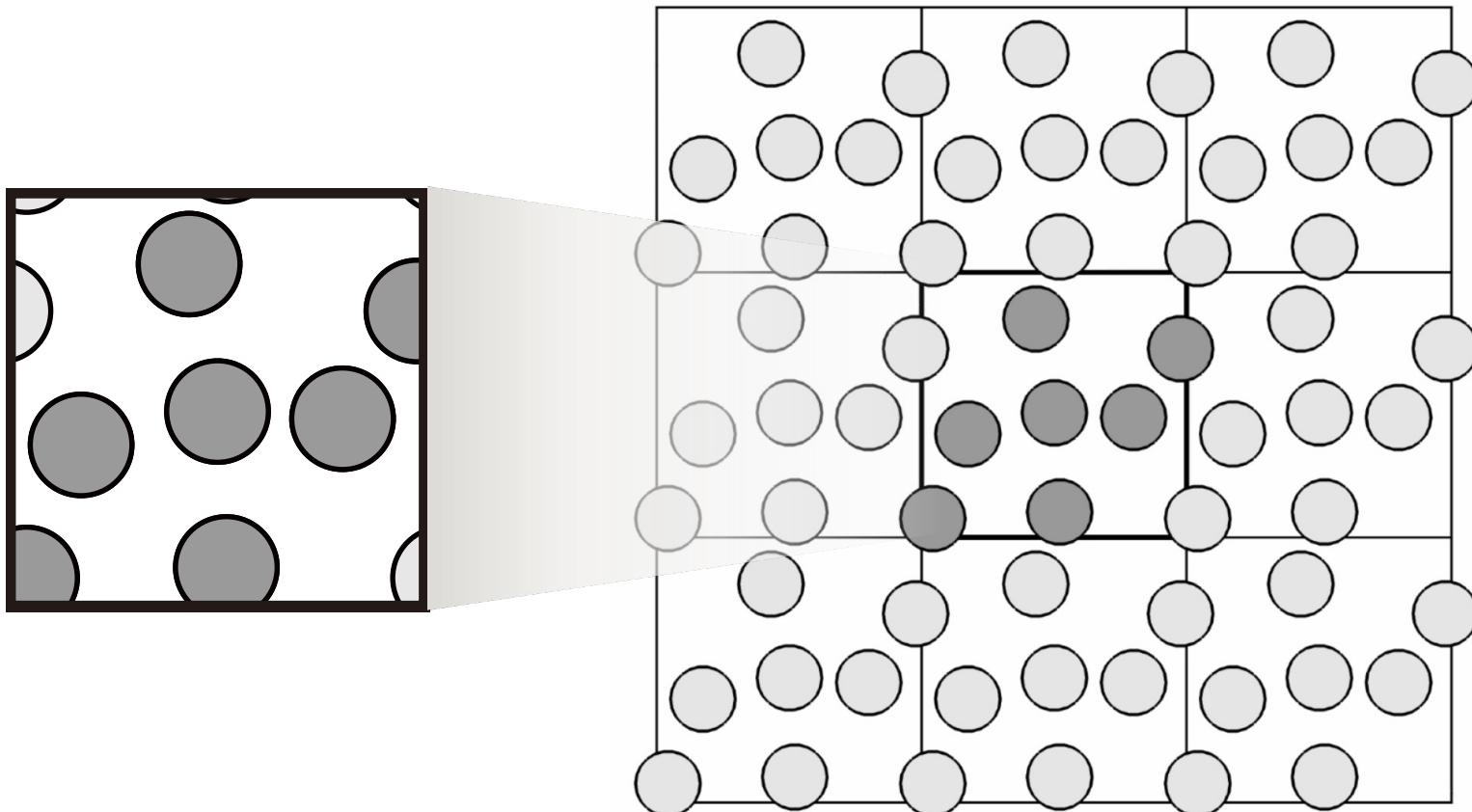
- Block copolymeric materials composed of hard and soft domains^[3-5]
- Macro- and micromechanics of “large strain” behavior of thermoplastic polyurethanes (TPU)^[1,2]

Thermoplastic polyurethanes (TPU)



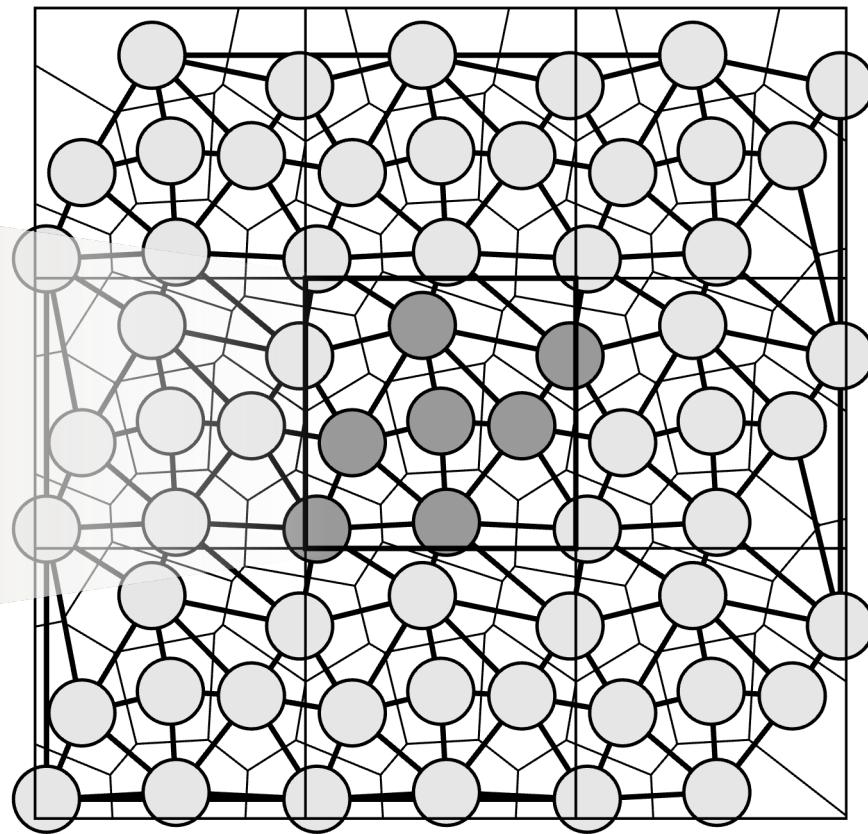
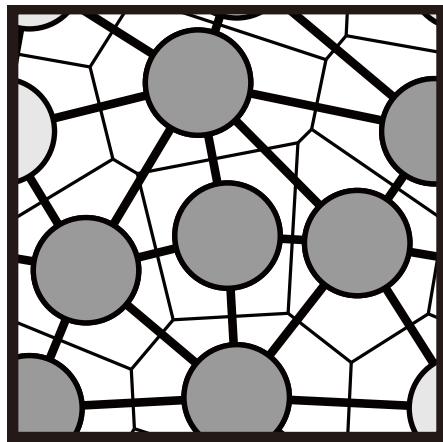
- Block copolymeric materials composed of hard and soft domains^[3-5]
- Macro- and micromechanics of “large strain” behavior of thermoplastic polyurethanes (TPU)^[1,2]

Construct “Random” microstructures



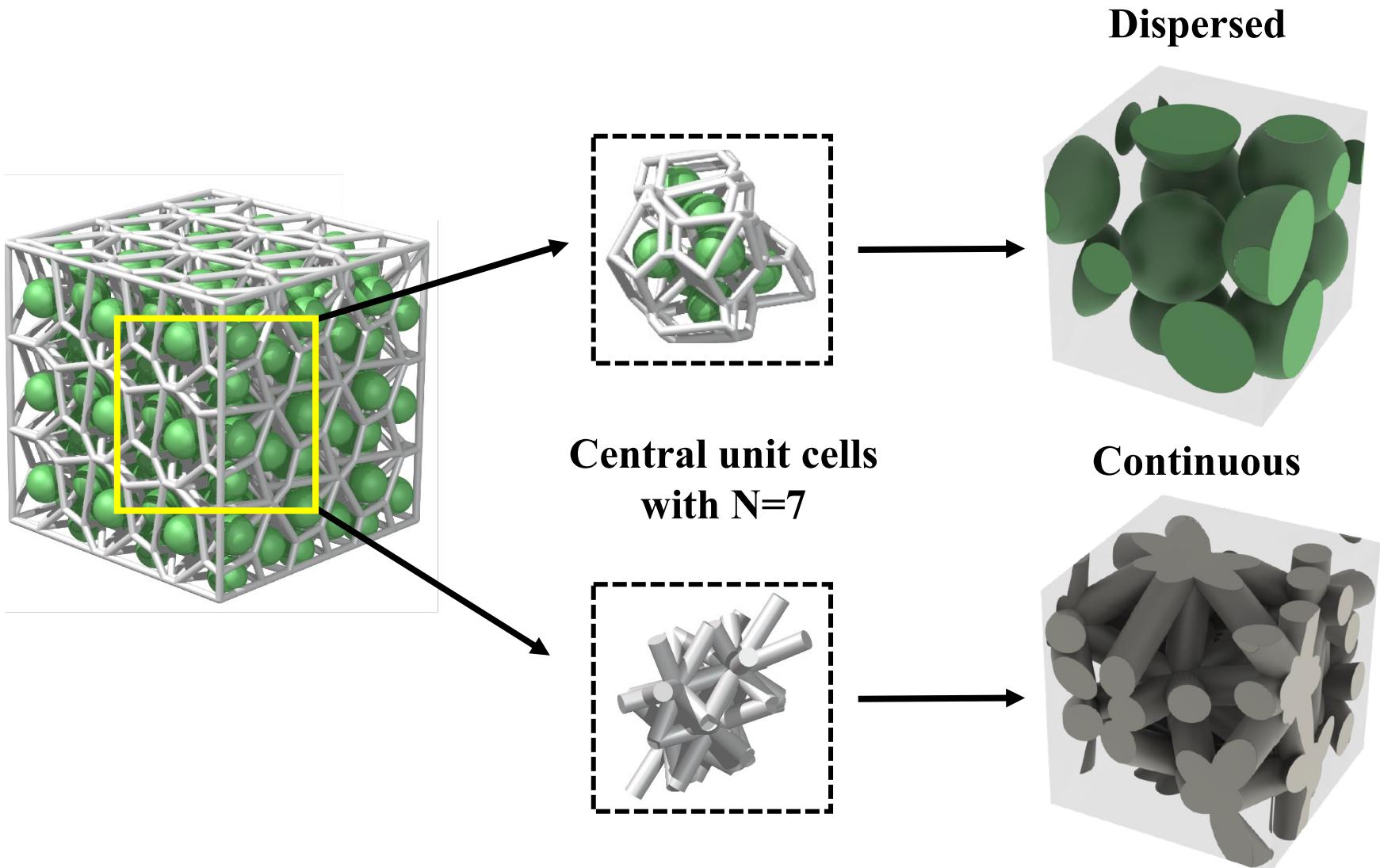
- Random packing of monodispersed spheres in periodic boundary conditions [\[6,7\]](#)

Random spatial points + tessellations



- Identification of the neighbors via Voronoi tessellations^[8]
- By connecting with the neighbors → continuous, disordered microstructures available

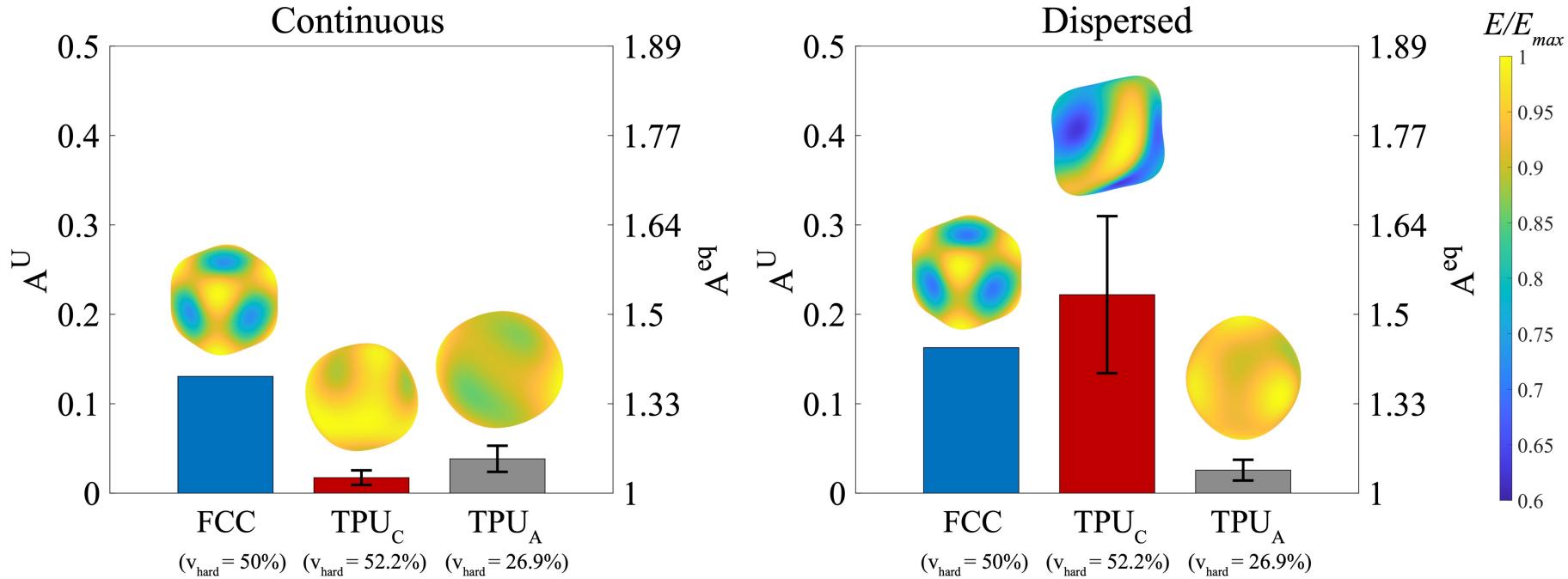
Proposed microstructures: Dispersed vs. continuous



- Only hard domains shown; we constructed two-phase materials

Identification of the N for RVEs

- Elastic anisotropy of both continuous and dispersed morphologies with $N=7$

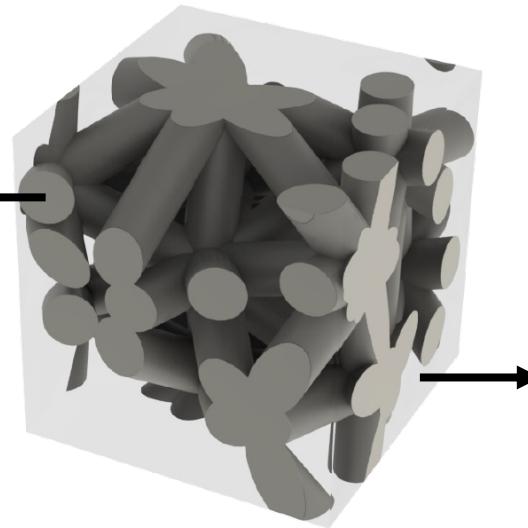
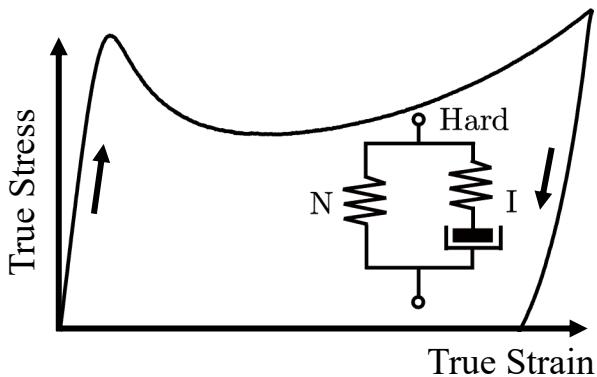


- Universal anisotropy index^[9,10]

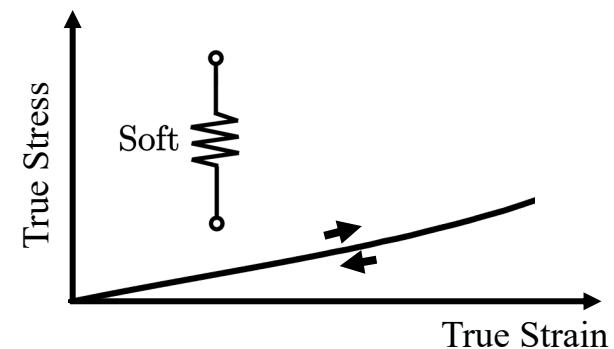
$$A^U = \mathbf{C}^V : \mathbf{S}^R - 6 = 5 \frac{G^V}{G^R} + \frac{K^V}{K^R} - 6 \geq 0 \quad (\text{Isotropic} : A^U = 0)$$

Constitutive behavior of hard and soft domains

Hard: Thermoplastic behavior



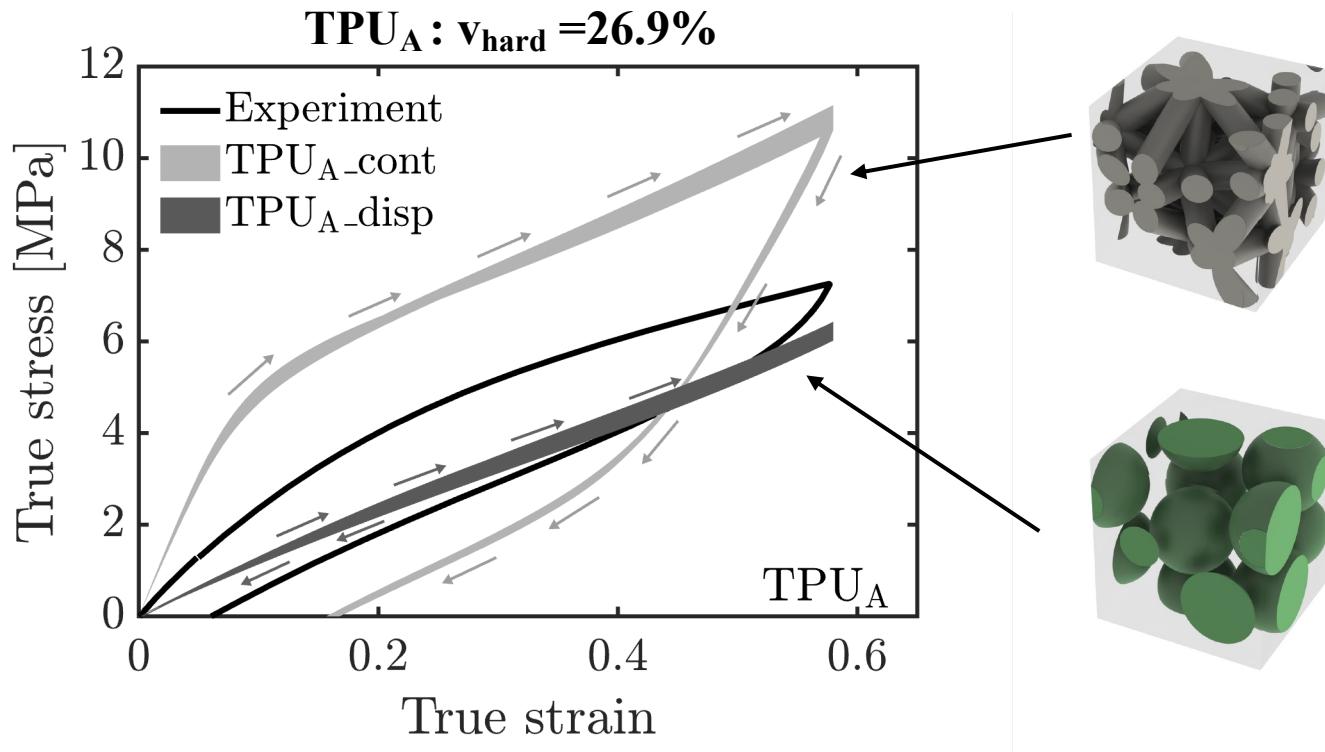
Soft: Elastomeric behavior



- High initial stiffness
- Energy dissipation
- Residual strain

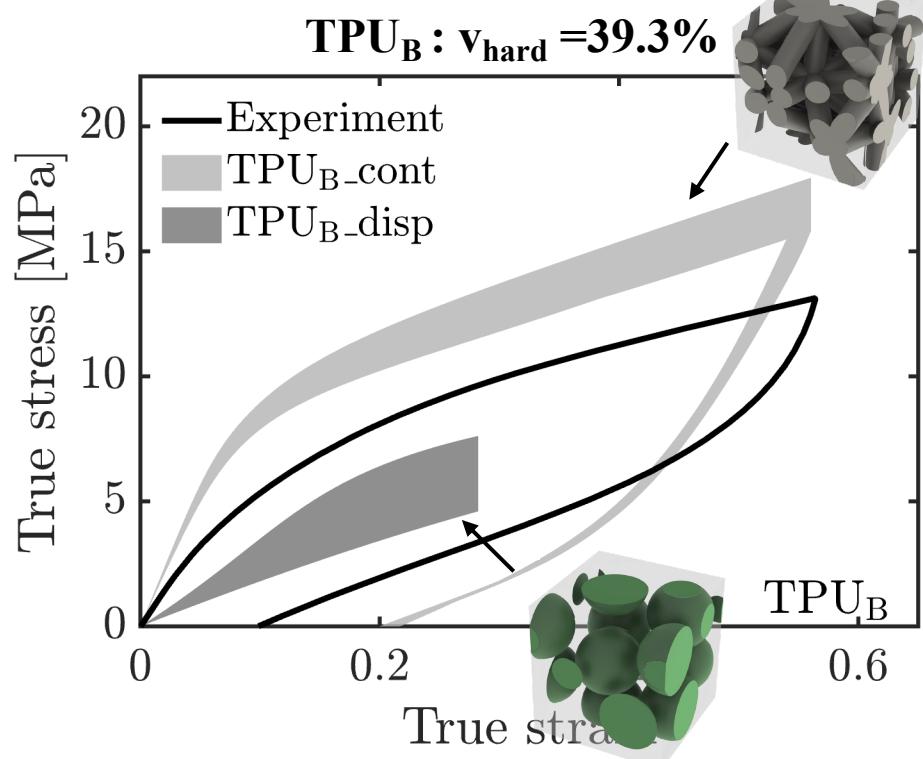
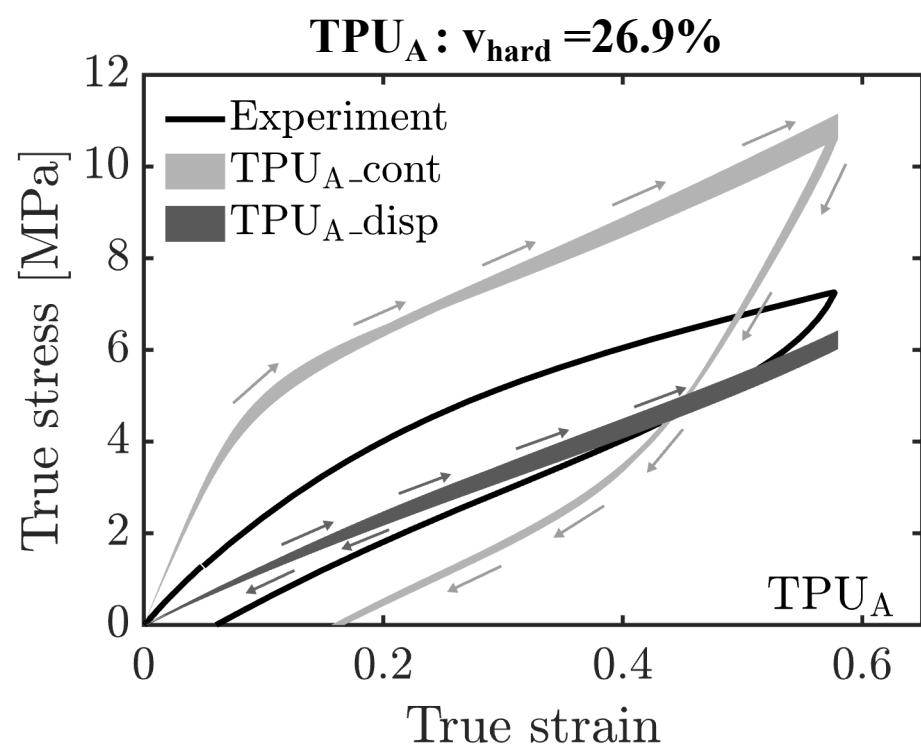
- Rubbery-like behavior
- Compliance
- Resilience

Dispersed vs. continuous: Role of connectivity



- Greater stress response, stiffer initial modulus, significant energy dissipation in the RVE with continuous hard domain [\[11,12\]](#)
- Numerical simulation results with five statistical realizations

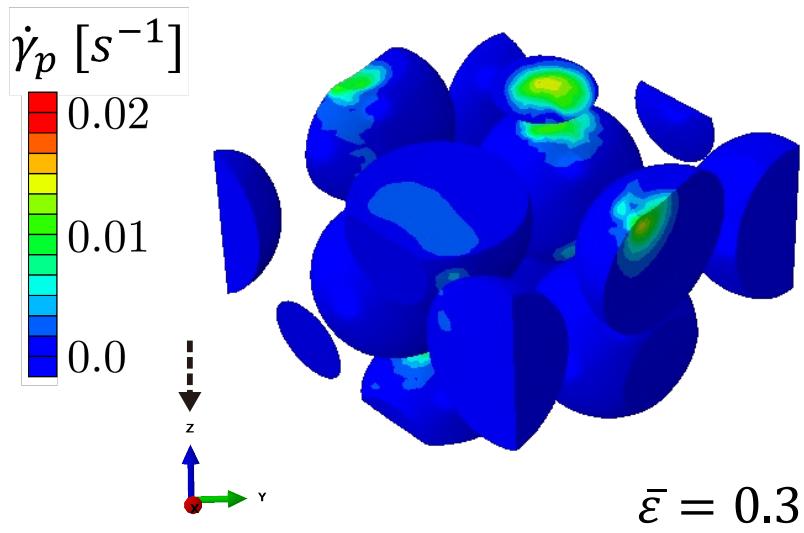
Dispersed vs. continuous: Role of connectivity



- In case of TPU_B → closer to the stress-strain response with continuous hard domain
- TPU_B (higher volume fraction; 39.3%) is likely to possess more “connected” domains

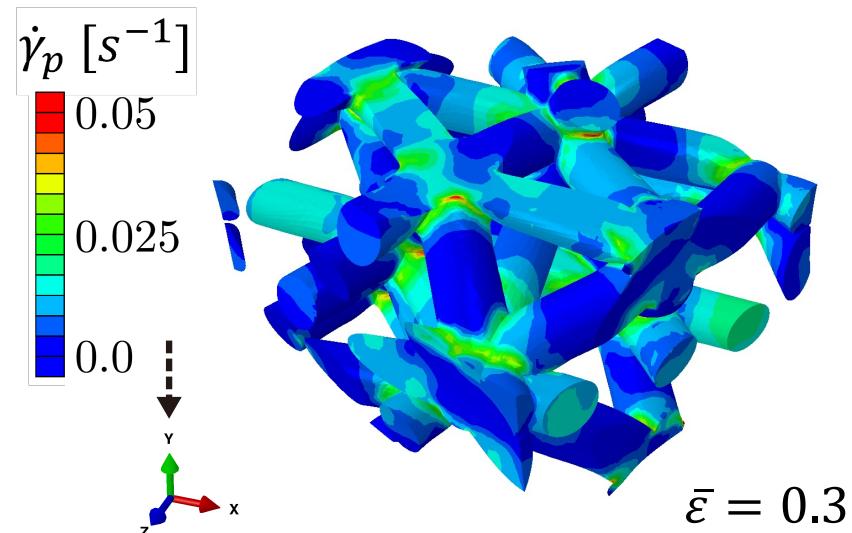
Dispersed vs. continuous: Role of connectivity

Dispersed



$\bar{\varepsilon} = 0.3$

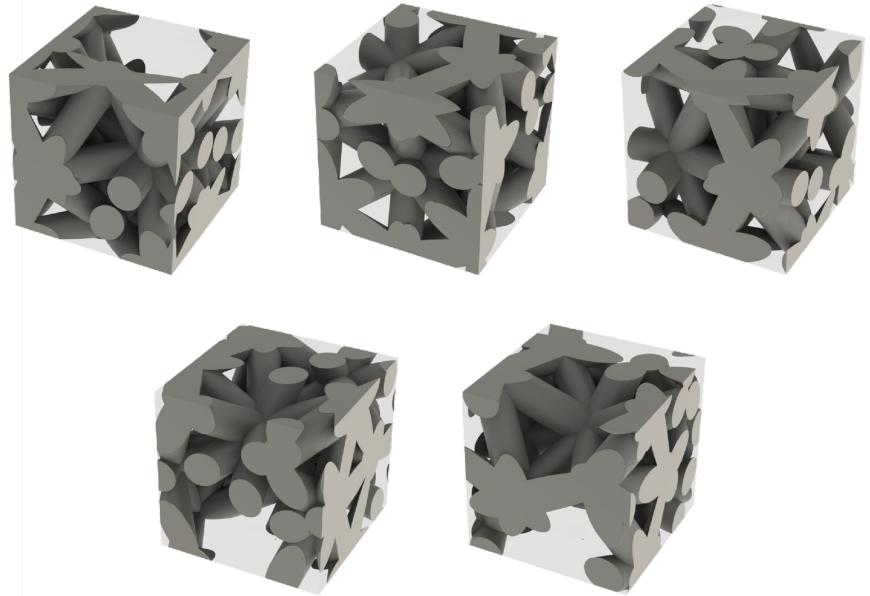
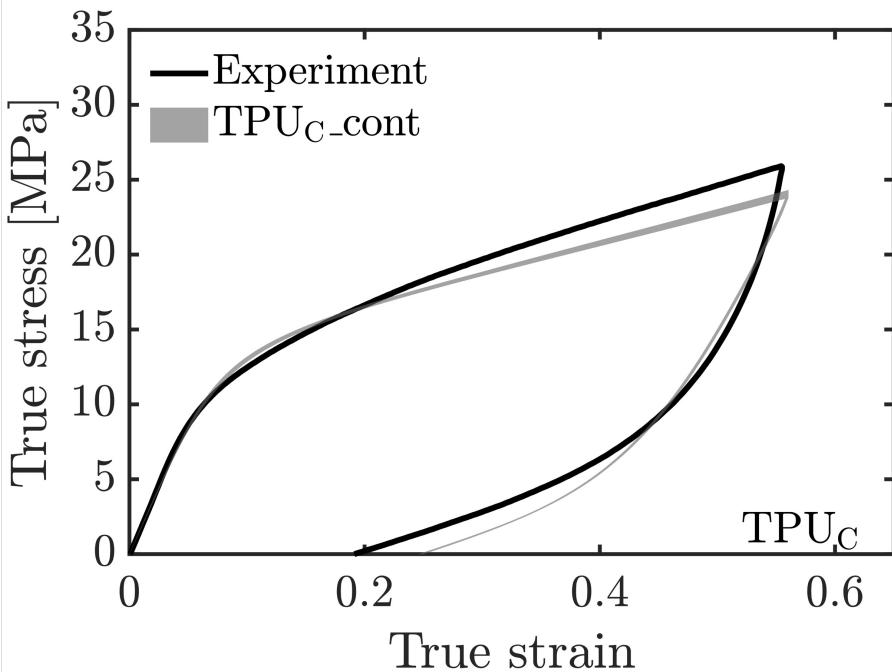
Continuous



$\bar{\varepsilon} = 0.3$

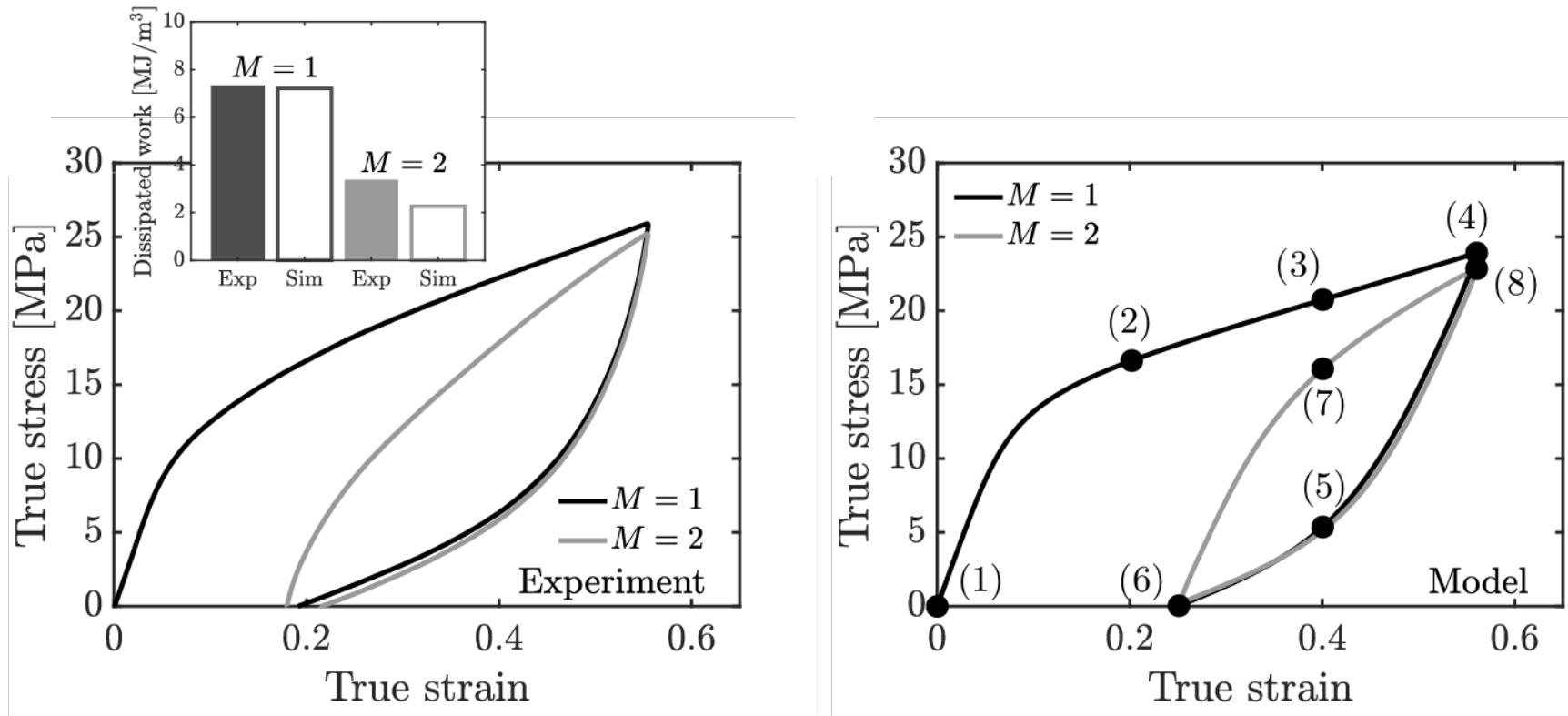
- Contours of plastic flow rates in dispersed and continuous RVEs of **TPU_B** ($v_{\text{hard}} = 39.3\%$)
- **Plastic flow** developed throughout the hard ligament, which results in the **stress-rollover** in the RVEs **with continuous hard domain**

Dispersed vs. continuous: Role of connectivity



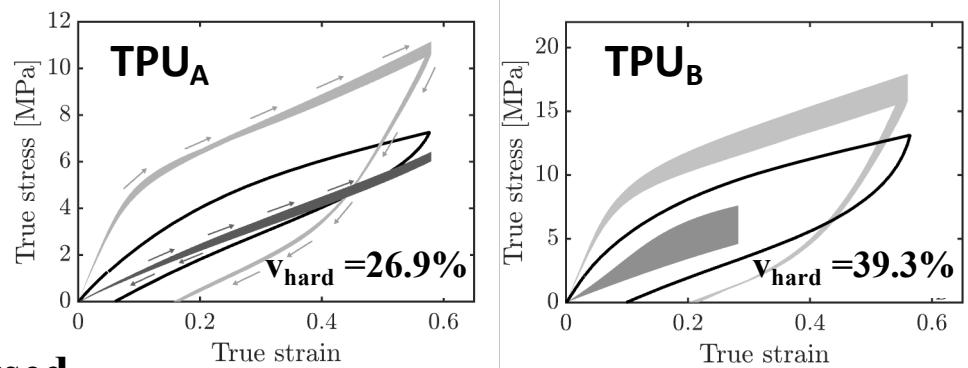
- Micromechanical model with **continuous hard domain** nicely captured the main features of TPU_C with highest volume fraction ($v_{\text{hard}} = 52.2\%$)

Cyclic loading behavior

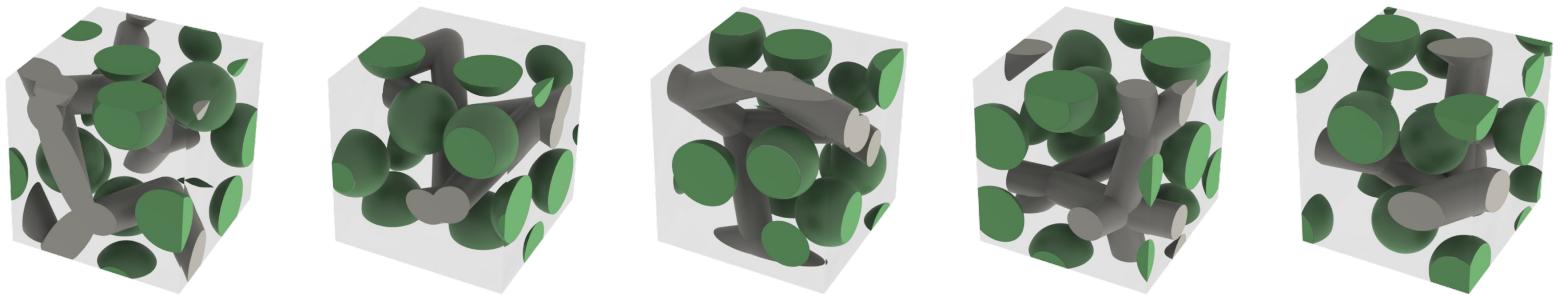


- Stretch-induced softening (Mullins' effect) was clearly manifested in the second cycle and was nicely captured by the micromechanical model [13,14]

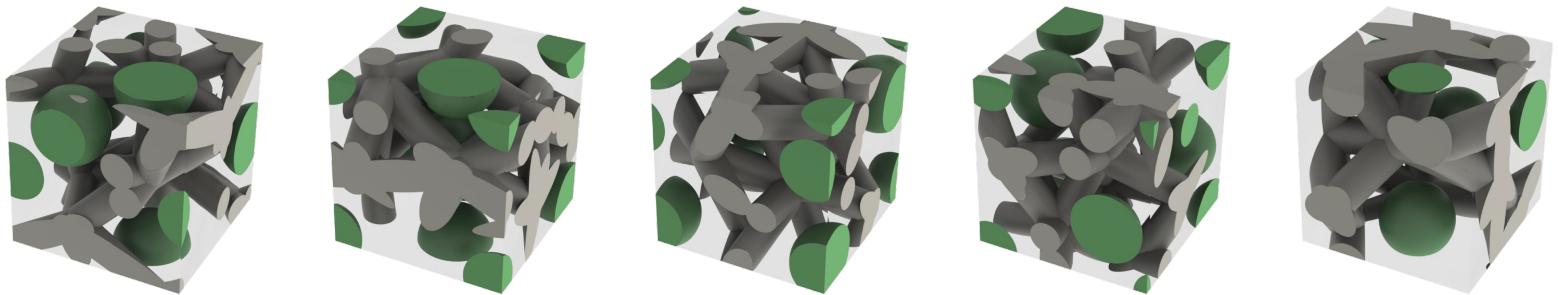
“Mixed” RVEs



(1) **TPU_A: 40% continuous / 60% dispersed**

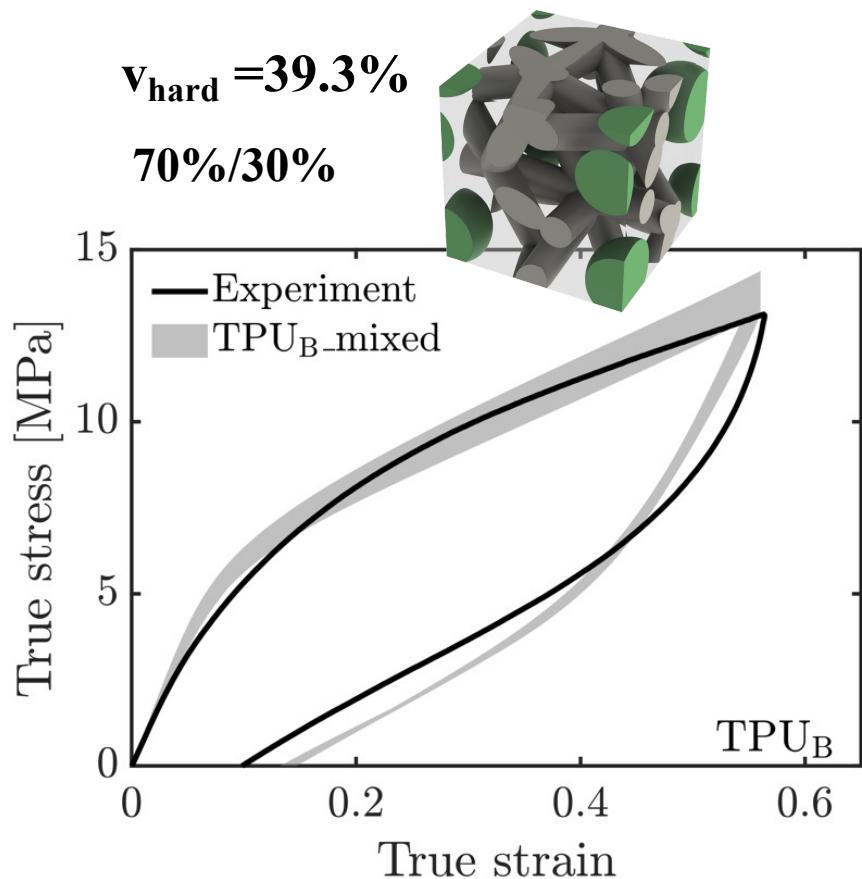
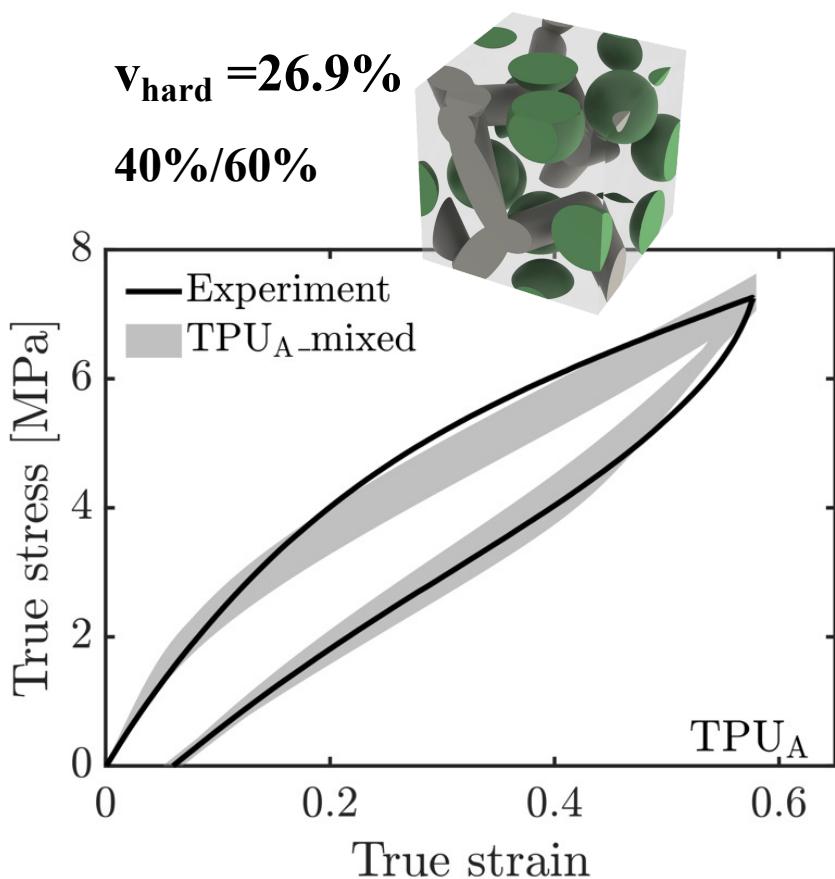


(2) **TPU_B: 70% continuous / 30% dispersed**



- Voronoi points $N=10$

“Mixed” RVEs



- Nicely captured the major features of the experimentally measured stress-strain response

Conclusion and Future works

- Micromechanical modeling of “**two-phase**” elastomers with two different disordered morphologies: **(1) dispersed** and **(2) continuous hard domains**
- **Connectivity** of hard domains impacts key elastic/inelastic features under cyclic loading
- Newly constructed **mixed RVEs** → co-existing dispersed and continuous morphologies
- Useful tool for micromechanical analysis of “**two-phase**” materials with random microstructures
 - Design of topological features for tailoring macroscopic mechanical properties [11,12]
 - Furthermore, explore the fracture behavior in a variety of elastomeric materials [15-18]

Acknowledgement

- This work is supported by BASF and National Research Foundation of Korea (2021R1A4A103278312 and RS-2023-00279843)

References

- [1] Cho, H., Lee, J., Moon, J., Pöseit, E., Rutledge, G. C., & Boyce, M. C. (2024). Large strain micromechanics of thermoplastic elastomers with random microstructures. *Journal of the Mechanics and Physics of Solids, 187, 105615.*
- [2] Cho, H., Mayer, S., Pöseit, E., Susoff, M., in't Veld, P. J., Rutledge, G. C., & Boyce, M. C. (2017). Deformation mechanisms of thermoplastic elastomers: Stress-strain behavior and constitutive modeling. *Polymer, 128, 87-99.*
- [3] Cho, H., Rinaldi, R. G., & Boyce, M. C. (2013). Constitutive modeling of the rate-dependent resilient and dissipative large deformation behavior of a segmented copolymer polyurea. *Soft Matter, 9(27), 6319-6330.*
- [4] Cho, H., Bartyczak, S., Mock Jr, W., & Boyce, M. C. (2013). Dissipation and resilience of elastomeric segmented copolymers under extreme strain rates. *Polymer, 54(21), 5952-5964.*
- [5] Lee, J., Veysset, D., Hsieh, A. J., Rutledge, G. C., & Cho, H. (2023). A polyurethane-urea elastomer at low to extreme strain rates. *International Journal of Solids and Structures, 280, 112360.*
- [6] Danielsson, M., Parks, D. M., & Boyce, M. C. (2002). Three-dimensional micromechanical modeling of voided polymeric materials. *Journal of the Mechanics and Physics of Solids, 50(2), 351-379.*
- [7] Danielsson, M., Parks, D. M., & Boyce, M. C. (2007). Micromechanics, macromechanics and constitutive modeling of the elasto-viscoplastic deformation of rubber-toughened glassy polymers. *Journal of the Mechanics and Physics of Solids, 55(3), 533-561.*
- [8] Rycroft, C. (2009). *VORO++: A three-dimensional Voronoi cell library in C++.*
- [9] Ranganathan, S. I., & Ostoja-Starzewski, M. (2008). Universal elastic anisotropy index. *Physical review letters, 101(5), 055504.*

References

- [10] Nye, J. F. (1985). Physical properties of crystals: their representation by tensors and matrices. *Oxford University Press.*
- [11] Cho, H., Weaver, J. C., Pösel, E., in't Veld, P. J., Boyce, M. C., & Rutledge, G. C. (2016). Engineering the mechanics of heterogeneous soft crystals. *Advanced Functional Materials, 26*(38), 6938-6949.
- [12] Lee, G., Lee, J., Lee, S., Rudykh, S., & Cho, H. (2024). Extreme resilience and dissipation in heterogeneous elastoplastomeric crystals. *Soft Matter, 20*(2), 315-329.
- [13] Qi, H. J., & Boyce, M. C. (2004). Constitutive model for stretch-induced softening of the stress–stretch behavior of elastomeric materials. *Journal of the Mechanics and Physics of Solids, 52*(10), 2187-2205.
- [14] Diani, J., Fayolle, B., & Gilormini, P. (2009). A review on the Mullins effect. *European Polymer Journal, 45*(3), 601-612.
- [15] Chen, C., Wang, Z., & Suo, Z. (2017). Flaw sensitivity of highly stretchable materials. *Extreme Mechanics Letters, 10*, 50-57.
- [16] Mao, Y., Talamini, B., & Anand, L. (2017). Rupture of polymers by chain scission. *Extreme Mechanics Letters, 13*, 17-24.
- [17] Narayan, S., & Anand, L. (2021). Fracture of amorphous polymers: A gradient-damage theory. *Journal of the Mechanics and Physics of Solids, 146*, 104164.
- [18] Lee, J., Lee, S., Chester, S. A., & Cho, H. (2023). Finite element implementation of a gradient-damage theory for fracture in elastomeric materials. *International Journal of Solids and Structures, 279*, 112309.