

# *hp*-Finite Element Model of Poisson and Nernst-Planck System of Equations

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## Abstract

In this paper we present a *hp*-finite element model (*hp*-FEM) of Nernst-Planck and Poisson equation system. The model is implemented in Hermes2D which is a space- and space-time adaptive *hp*-FEM solver. The time dependent adaptivity is used to control the error of the solution. Full mathematical derivation of the weak formulation of the system of equations and the solution comparison with a nonadaptive conventional FEM is presented. Furthermore, we extend the discussion on Hermes3D as a modeling tool that can help in studying and improving the IPMC materials.

*Keywords:* *hp*-FEM, Nernst-Planck, Poisson, weak form

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## 1. Introduction

The system of Poisson and Nernst-Planck (further denoted PNP) equations has been widely used to describe the charge transport — which includes the ionic migration, diffusion, and convection — in a medium. The charge transport process is a key mechanism for electromechanical transduction in some of the electroactive polymer (EAP) materials, for instance, in ionic polymer-metal composites (IPMCs) [1, 2, 3, 4, 5, 6, 7]. As the system of equations is nonlinear and for a domain with two electrodes, the charge concentration differences occur in a very narrow region near the boundaries, the required computing power for a full scale domain is, especially in 3D, rather significant. This requires a mesh that is optimal in terms of calculation time and calculation error.

The Nernst-Planck equation for a mobile species — in this case for counter ions — and without the convection term is:

$$\frac{\partial C}{\partial t} + \nabla \cdot (-D \nabla C - z \mu F C \nabla \phi) = 0, \quad (1)$$

where  $C$  is the counter ion concentration,  $D$  diffusion,  $\mu$  mobility,  $F$  Faraday constant,  $\phi$  voltage, and  $z$  charge number. The Poisson equation is

$$-\nabla^2 \phi = \frac{F \rho}{\varepsilon}, \quad (2)$$

where  $\varepsilon$  is an absolute dielectric permittivity and the charge density  $\rho$  is expressed

$$\rho = C - C_0 \quad (3)$$

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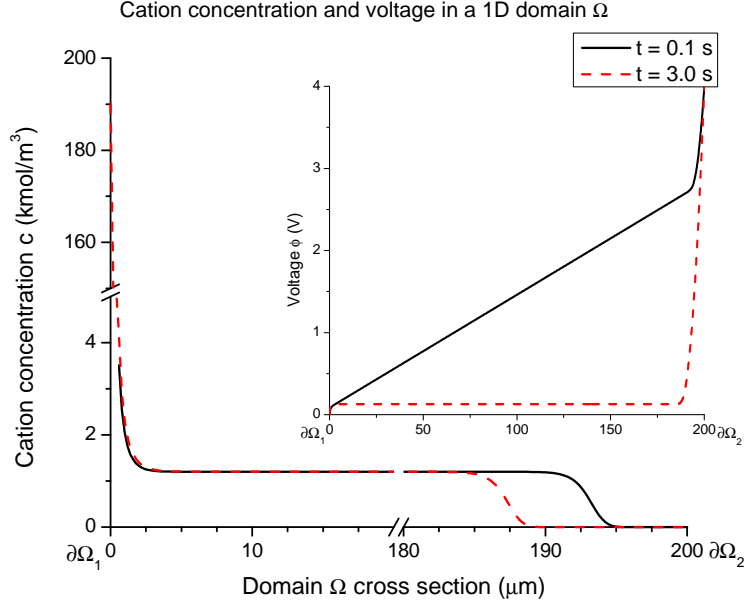


Figure 1: Calculated concentration  $C$  and voltage  $\phi$  in a 1D domain  $\Omega \subset \mathbb{R}$ . Dirichlet boundary conditions ( $V_{\partial\Omega_1} = 0$  V and  $V_{\partial\Omega_2} = 4$  V) were applied to the Poisson equation Eq. (2) and Neumann boundaries to the Nernst-Planck equation Eq. (1).

with  $C_0$  being a constant anion concentration.

In the following section we give a brief overview of the motivation of the study and a practical application of the results. Thereafter the weak-form [8] derivation of the PNP system of equations and time dependent adaptive  $hp$ -FEM solutions of the system is presented for different adaptivity algorithms. Also, advantages of a multi-mesh solution over a single-mesh solution are discussed.

## 2. Motivation

Fig. 1 shows a solution for  $C$  and  $\phi$  in the time dependent NPN system at  $t = 0.1$  s and  $t = 3.0$  s. Solution constants are shown in Table 1. It can be seen that the solution has two notable characteristics. Firstly,  $\nabla C$  at  $\partial\Omega_2$  is moving in time, whereas  $\nabla C$  at  $\partial\Omega_1$  is very sharp. For the large part of the domain  $\Omega$   $\nabla C = 0$ . At the same time,  $\phi$  is a rather smooth function in  $\Omega$ . This clearly makes the choice of mesh for the time dependent NPN system difficult. By creating a too fine mesh, the problem gets too big. By choosing a coarser mesh, the calculation error goes up. Furthermore, from the shape of the solution in Fig. 1 can be seen that the polynomial degree of the elements in the middle of the domain  $\Omega$  and near the boundaries  $\partial\Omega_1$ ,  $\partial\Omega_2$  should be different — namely higher degree near the boundaries. Overall shape of the solutions suggest that using different meshes for variables  $C$  and  $\phi$  can be beneficial in terms of resources and calculation time.

All the aforementioned difficulties can be solved by using a time dependent adaptive multimesh  $hp$ -FEM solver. Automatic time dependent adaptivity in conjunction with  $hp$ -FEM helps to limit the error of the calculations by choosing a suitable mesh and polynomial degrees of the elements at each time step. In this work Hermes2D [9] was used to study the problem size, error convergence and solution time of NPN system with different adaptivity algorithms.

Table 1: Constants used in the Poisson-Nernst-Planck system of equations.

Constant	Value	Unit	Description
$D$	$10 \times 10^{-11}$	$\frac{m^2}{s}$	Diffusion constant
$z$	1	-	Charge number
$F$	96,485	$\frac{C}{mol}$	Faraday number
$R$	8.31	$\frac{J}{mol \cdot K}$	The gas constant
$\mu$ ( $= \frac{D}{RT}$ )	$4.11 \times 10^{-14}$	$\frac{s}{mol \cdot K}$	Mobility
$C_0$	1,200	$\frac{mol}{m^3}$	Anion concentration
$\varepsilon$	0.025	$\frac{F}{m}$	Electric permittivity

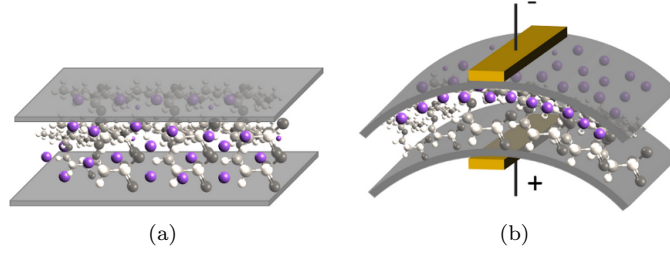


Figure 2: Conceptual model of the actuation of IPMC. Initial counter ion distribution (a) and the distribution and resulting bending after applying a voltage (b).

### 2.1. Practical application

IPMCs have been studied in past two decades in view of using them as noiseless mechatrical or electromechanical transducers. The advantages of the IPMCs over other electroactive polymer actuators are low voltage bending, high strains ( $> 1\%$ ), and ability to work in wet environments. A typical IPMC consists of a thin sheet of polymer (often Nafion or Teflon) which is sandwiched between noble metal electrodes such as platinum or gold. When fabricated, the polymer membrane is saturated with certain solvent and ions, e.g water and  $H^+$ . When a voltage is applied to the electrodes, the counter ions start migrating due to the imposed electric field. By dragging along the solvent, the osmotic pressure difference near the electrodes occur which in turn results in bending of the material (see Fig. 2). The derived and implemented model helps to predict the actuation of the material. Furthermore, it is expected that the *hp*-FEM implementation results in a smaller problem size, thus likely allowing faster calculation in both 2D and 3D.

## 3. Model

The model for solving NPN system is implemented in Hermes2D. In this work a rectangular 2D domain  $\Omega \subset \mathbb{R}^2$  with boundaries  $\partial\Omega_{1...4} \subset \partial\Omega$  is considered (see Fig. 3). As there is now flow considered in or out of the domain and there is no constant concentration at the boundaries, zero Neumann boundary conditions

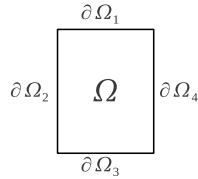


Figure 3: Calculation domain  $\Omega \subset \mathbb{R}^2$  with boundaries  $\partial\Omega_{1...4} \subset \partial\Omega$ .

are used for Eq. (1):

$$-D \frac{\partial C}{\partial n} - z\mu F C \frac{\partial \phi}{\partial n} = 0. \quad (4)$$

As a positive voltage  $V_{pos}$  is applied on  $\Omega_1$  and  $V_{neg} = 0$  is applied on  $\Omega_3$ , Dirichlet boundary conditions are used for Eq. (2) for boundaries  $\Omega_1$  and  $\Omega_3$ :

$$\phi_{\partial\Omega_1} = V_{pos}, \quad (5)$$

$$\phi_{\partial\Omega_3} = 0, \quad (6)$$

and Neumann boundaries for  $\Omega_2$  and  $\Omega_4$ :

$$\frac{\partial \phi_{\Omega_2}}{\partial n} = \frac{\partial \phi_{\Omega_4}}{\partial n} = 0. \quad (7)$$

### 3.1. Weak form of Poisson-Nernst-Planck system

To make the derivation of the weak forms more convenient, the following helper constants will be used:

$$K = z\mu F, \quad (8)$$

$$L = \frac{F}{\varepsilon}. \quad (9)$$

So Eq. (1) and Eq. (2) become after substituting Eq. (3) and the constants  $K$  and  $L$ :

$$\frac{\partial C}{\partial t} - D \nabla^2 C - K \nabla \cdot (C \nabla \phi) = 0, \quad (10)$$

$$-\nabla^2 \phi - L(C - C_0) = 0. \quad (11)$$

The boundary condition Eq. (4) becomes:

$$-D \frac{\partial C}{\partial n} - KC \frac{\partial \phi}{\partial n} = 0. \quad (12)$$

The space for solution is  $V = H^1(\Omega)$  where  $H^1(\Omega) = \{v \in L^2(\Omega); \nabla v \in [L^2(\Omega)]^2\}$ . Let's choose a test function  $v^C \in V$ . The weak form the Nernst-Planck equation Eq. (10) is found by multiplying it with the test function  $v^C$  and then integrating over the domain  $\Omega$ :

$$\int_{\Omega} \frac{\partial C}{\partial t} v^C d\mathbf{x} - \int_{\Omega} D \nabla^2 C v^C d\mathbf{x} - \int_{\Omega} K \nabla C \cdot \nabla \phi v^C d\mathbf{x} - \int_{\Omega} KC \nabla^2 \phi v^C d\mathbf{x} = 0. \quad (13)$$

After adding the weak form of the boundary term (Eq. (12)) and applying the Green's first identity to the terms that contain Laplacian  $\nabla^2$  we get

$$\int_{\Omega} \frac{\partial C}{\partial t} v^C d\mathbf{x} + D \int_{\Omega} \nabla C \cdot \nabla v^C d\mathbf{x} - K \int_{\Omega} \nabla C \cdot \nabla \phi v^C d\mathbf{x} + K \int_{\Omega} \nabla (C v^C) \cdot \nabla \phi d\mathbf{x} \quad (14)$$

$$-D \int_{\partial\Omega} \frac{\partial C}{\partial n} v^C d\mathbf{S} - \int_{\partial\Omega} K \frac{\partial \phi}{\partial n} C v^C d\mathbf{S} = 0. \quad (15)$$

After expanding the nonlinear term and given that the boundary terms do not contribute, the weak form becomes

$$\int_{\Omega} \frac{\partial C}{\partial t} v^C d\mathbf{x} + D \int_{\Omega} \nabla C \cdot \nabla v^C d\mathbf{x} - K \int_{\Omega} \nabla C \cdot \nabla \phi v^C d\mathbf{x} + K \int_{\Omega} \nabla \phi \cdot \nabla C v^C d\mathbf{x} + K \int_{\Omega} C (\nabla \phi \cdot \nabla v^C) d\mathbf{x} = 0. \quad (16)$$

As the second and third term cancel out, the final weak form of the Nernst-Planck equation is

$$\int_{\Omega} \frac{\partial C}{\partial t} v^C d\mathbf{x} + D \int_{\Omega} \nabla C \cdot \nabla v^C d\mathbf{x} + K \int_{\Omega} C (\nabla \phi \cdot \nabla v^C) d\mathbf{x} = 0. \quad (17)$$

Similarly the weak form of Poisson equation Eq. 11 with a test function  $v^\phi \in V$  is:

$$-\int_{\Omega} \nabla^2 \phi v^\phi d\mathbf{x} - \int_{\Omega} LC v^\phi d\mathbf{x} + \int_{\Omega} LC_0 v^\phi d\mathbf{x} = 0. \quad (18)$$

After expanding the  $\nabla^2$  terms, the final form becomes

$$\int_{\Omega} \nabla \phi \cdot \nabla v^\phi d\mathbf{x} - \int_{\Omega} LC v^\phi d\mathbf{x} + \int_{\Omega} LC_0 v^\phi d\mathbf{x} = 0. \quad (19)$$

### 3.2. Implementation in Hermes2D

To implement the system of equations Eq. (17) and Eq. (19), the residuals and the Jacobian matrix must be derived. For that, Crank-Nicolson time stepping was used

$$\frac{\partial C}{\partial t} \approx \frac{C^{n+1} - C^n}{\tau}, \quad (20)$$

where  $\tau$  is a time step. For the variables  $C^{n+1}$  and  $\phi^{n+1}$  the following notation will be used:

$$C^{n+1} = \sum_{k=1}^{N^C} y_k^C v_k^C, \quad (21)$$

$$\phi^{n+1} = \sum_{k=1}^{N^\phi} y_k^\phi v_k^\phi, \quad (22)$$

where  $v_k^C$  and  $v_k^\phi$  are piecewise polynomial functions in  $V$ . Considering the Crank-Nicolson time stepping and the notation (21), the time discretized Eq. (17) becomes

$$\begin{aligned} F_i^C(Y) &= \int_{\Omega} \frac{C^{n+1}}{\tau} v_i^C d\mathbf{x} - \int_{\Omega} \frac{C^n}{\tau} v_i^C d\mathbf{x} \\ &\quad + \frac{1}{2} \left[ D \int_{\Omega} \nabla C^{n+1} \cdot \nabla v_i^C d\mathbf{x} + D \int_{\Omega} \nabla C^n \cdot \nabla v_i^C d\mathbf{x} \right] \\ &\quad + \frac{1}{2} \left[ K \int_{\Omega} C^{n+1} (\nabla \phi^{n+1} \cdot \nabla v_i^C) d\mathbf{x} + K \int_{\Omega} C^n (\nabla \phi^n \cdot \nabla v_i^C) d\mathbf{x} \right], \end{aligned} \quad (23)$$

and in the notation (22), Eq. (19) becomes

$$F_i^\phi(Y) = \int_{\Omega} \nabla \phi^{n+1} \cdot \nabla v_i^\phi d\mathbf{x} - \int_{\Omega} LC^{n+1} v_i^\phi d\mathbf{x} + \int_{\Omega} LC_0 v_i^\phi d\mathbf{x}. \quad (24)$$

For the implementation the  $2 \times 2$  Jacobian matrix  $DF/DY$  with elements corresponding to

$$\frac{\partial F_i^C}{\partial y_j^C}, \frac{\partial F_i^C}{\partial y_j^\phi}, \frac{\partial F_i^\phi}{\partial y_j^C}, \frac{\partial F_i^\phi}{\partial y_j^\phi}, \quad (25)$$

must be derived:

$$\frac{\partial F_i^C}{\partial y_j^C} = \int_{\Omega} \frac{1}{\tau} v_j^C v_i^C d\mathbf{x} + \frac{1}{2} D \int_{\Omega} \nabla v_j^C \cdot \nabla v_i^C d\mathbf{x} + \frac{1}{2} K \int_{\Omega} v_j^C (\nabla \phi^{n+1} \cdot \nabla v_i^C) d\mathbf{x}, \quad (26)$$

$$\frac{\partial F_i^C}{\partial y_j^\phi} = \frac{1}{2} K \int_{\Omega} C^{n+1} (\nabla v_j^\phi \cdot \nabla v_i^C) d\mathbf{x}, \quad (27)$$

$$\frac{\partial F_i^\phi}{\partial y_j^C} = - \int_{\Omega} L v_j^C v_i^\phi d\mathbf{x}, \quad (28)$$

$$\frac{\partial F_i^\phi}{\partial y_j^\phi} = \int_{\Omega} \nabla v_j^\phi \cdot \nabla v_i^\phi d\mathbf{x}. \quad (29)$$

In Hermes2D Eq. (23) and (24) define the residuum  $F$  and Eq. (26)—(29) define the Jacobian matrix  $J$ .

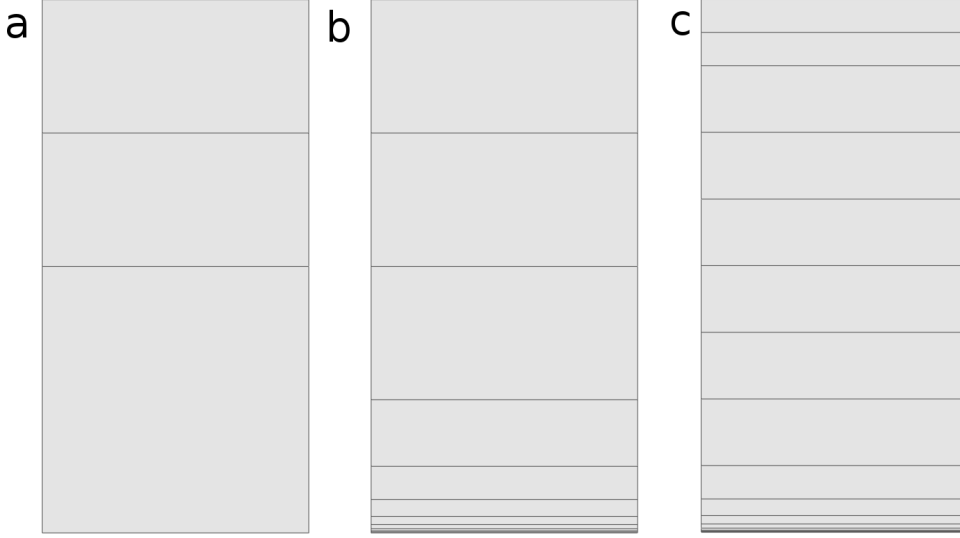


Figure 4: Initial coarse mesh (a), half refined mesh (b) and refined mesh (c). The coarse mesh and refined mesh were used in the initial calculations, the latter one in case of  $p$ -adaptivity (including HP\_ANISO\_P). The half-refined mesh was used later to optimize  $hp$ -adaptive mode solutions.

### 3.3. Adaptive multi-mesh solution

The defined Jacobian  $J$  and residuum  $F$  can be simply solved in Hermes2D by using Newton's iteration. However, we were more interested in the automatic adaptivity and the calculation differences with a single-mesh and multi-mesh.

In case of the single mesh, the same basis function base was used, i.e.  $v_i^\phi = v_i^C$ . For multi mesh, the meshes and therefore the basis functions were different. Regardless of the meshing, automatic adaptivity was applied during each time step, till the error converged to the acceptable level. In analogy to the most successful adaptive ODE solvers, Hermes2D uses a pair of approximations with different orders of accuracy to obtain this information: coarse mesh solution and fine mesh solution. The initial coarse mesh is read from the mesh file, and the initial fine mesh is created through its global refinement both in  $h$  and  $p$ . For more information, see [9]. In the calculations, the coarse mesh solution was not calculated at each time step, but the fine mesh solution was projected to the coarse mesh by using orthogonal projection. This yielded better convergence and also faster calculation.

Hermes2D supports 8 different refinement modes, namely, 3 isotropic and 5 anisotropic refinements. The isotropic refinements are  $h$ -isotropic (H\_ISO),  $p$ -isotropic (P\_ISO),  $hp$ -isotropic (HP\_ISO). Anisotropic refinement modes are  $h$ -anisotropic (H\_ANISO),  $hp$ -anisotropic- $h$  (HP\_ANISO\_H),  $p$ -anisotropic (P\_ANISO),  $hp$ -anisotropic- $p$  (HP\_ANISO\_P), and  $hp$ -anisotropic (HP\_ANISO). Once the refinement mode is selected (by user), Hermes2D selects a particular refinement scheme from several candidates based on the score. More information can be found in [9].

## 4. Results

We ran the calculation for all the adaptivity types in both single-mesh and multi-mesh configurations. The following numeric results were recorded for each adaptivity type: converged error at each time step, cumulative CPU time at each time step, and the problem size in terms of number of degrees of freedoms (NDOFs) at each time step. Two types of initial meshes were used — in case of only  $p$ -adaptivity, more refined mesh was used. When also the element size refinement was enabled (all  $h$  adaptivity types), very coarse initial mesh was used. In any case, the initial mesh was loaded at each time step.

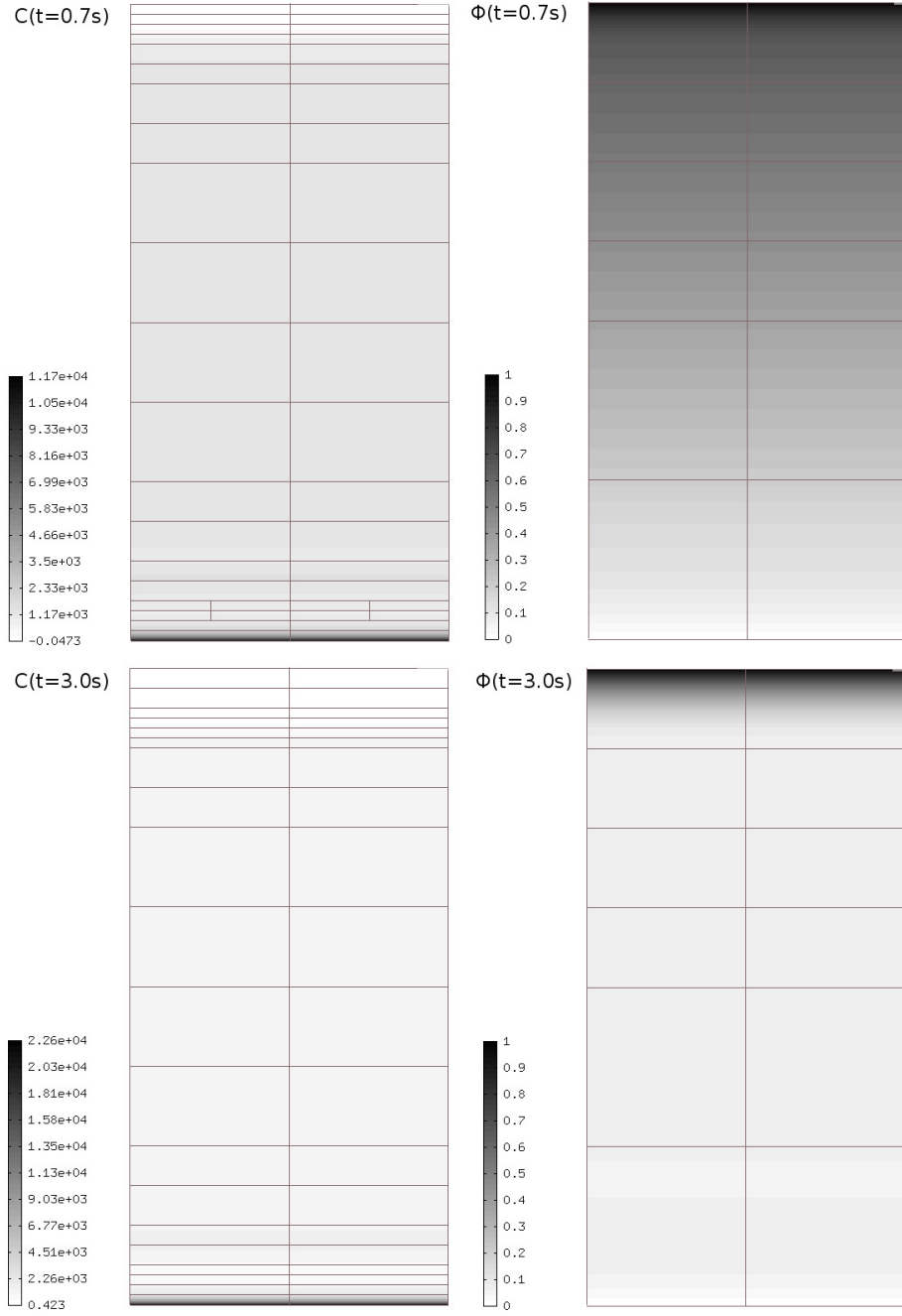


Figure 5: Concentration  $C$  and voltage  $\phi$  at two different time steps (HP\_ANISO adaptivity was used).

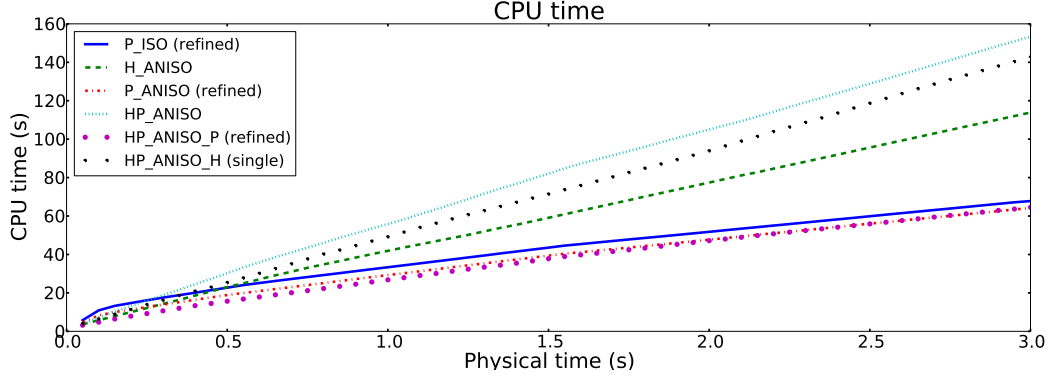


Figure 6: Cumulative CPU time for different adaptivity modes.

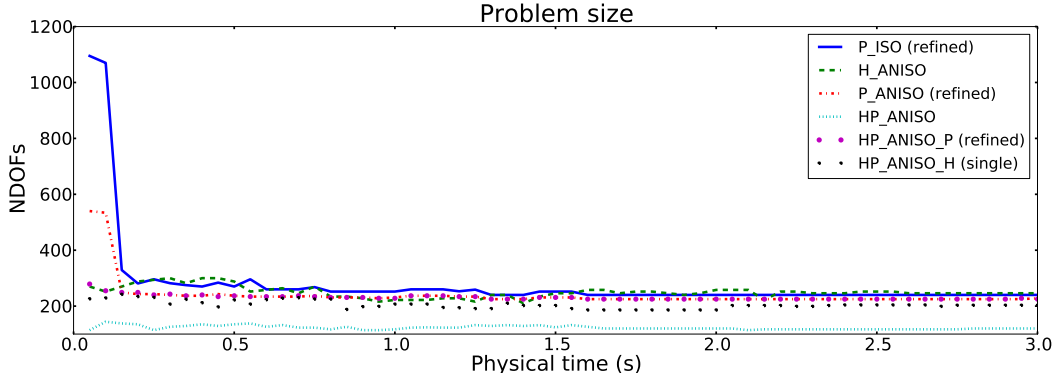


Figure 7: NDOFs at each time step for different adaptivity modes.

Example of the solution at  $t = 0.7$  s and  $t = 3.0$  s with adaptivity type HP\_ANISO is shown in Fig. 5. The time  $t = 0.7$  s was chosen because by that time, some ionic migration has already taken place, i.e. concentration gradient near the  $\partial\Omega_1$  and  $\partial\Omega_3$  has formed. The automatic mesh refinements at different time steps are clearly visible — especially near the top boundary, where the concentration gradient is moving in time (as seen in Fig. 1).

Some initial observations helped to select the graphs for this work — it would have been unreasonable to present all recorded results for each adaptivity type. First of all, the multi-mesh configuration resulted smaller problem size, faster calculation, and better or similar error convergence than the single-mesh configuration for all but HP\_ANISO\_H adaptivity type. In this case the single-mesh configuration resulted slightly but not significantly smaller problem size, therefore, single-mesh results of HP\_ANISO\_H are considered in further comparisons. It must be also noted that in case of the isotropic refinements, only P\_ISO adaptivity mode resulted in a reasonable problem size. Secondly, H\_ISO did not converge very well in terms of the calculation time and the problem size. The term “reasonable problem size” means that the number of degrees of freedom in time converges to so that  $N_{dof} < 500$ , and the term “reasonable calculation time” means that the calculation (step  $\tau = 0.01$  s, physical time  $t_{end} = 3.0$  s) time  $t$  on a given system was  $t < 500$  s. Although these parameters are empirical, they serve as an upper limit, given that the most adaptivity modes gave significantly smaller results, e.g.  $t \ll 500$  s and  $N_{dof} \ll 500$ . Therefore, the multi-mesh calculation results H\_ISO, H\_ANISO, P\_ANISO, HP\_ANISO, HP\_ANISO\_P and the single-mesh calculation results of HP\_ANISO\_H adaptivity mode will be compared. In all of the cases, the relative error at each time step remained below the threshold which were set to  $e_{th} = 0.5\%$  between the coarse mesh and fine mesh solutions.

Fig. 6 shows the cumulative CPU time for different adaptivity modes at each time step. All the calcu-



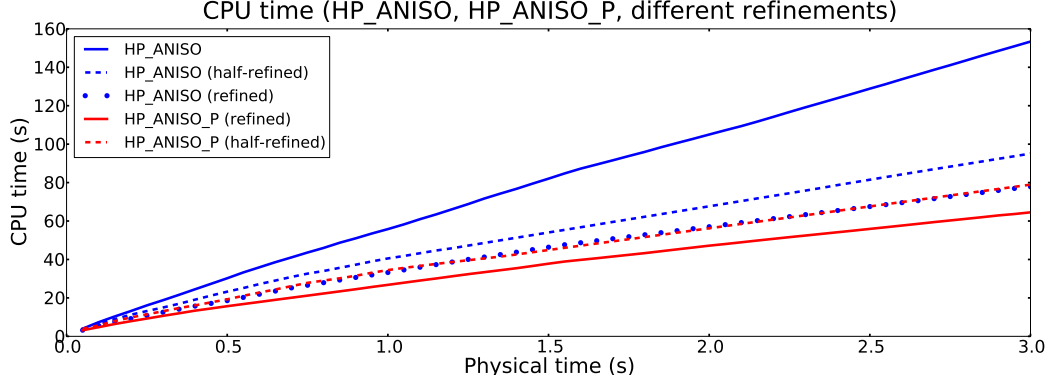


Figure 8: Cumulative CPU time for HP\_ANISO and HP\_ANISO\_P with different initial meshes.

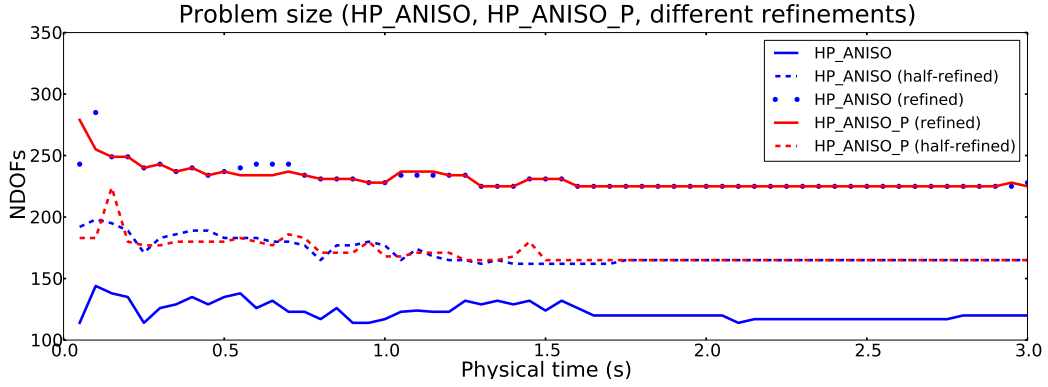


Figure 9: NDOFs at each time step for HP\_ANISO and HP\_ANISO\_P with different meshes.

lations were done on the same computer. Here we see that HP\_ANISO requires the most resources which can be understood from the fact that this adaptivity mode has the largest number of candidates (see XXX) from which the refinement method is chosen. At the same time, HP\_ANISO\_H is the fastest. Fig. 7 shows the NDOFs at each time step for different adaptivity modes. There we see that the HP\_ANISO results in the smallest problem size —  $N_{dof} \approx 125$ . All the other adaptivity modes result in the problem size approximately ( $N_{dof} \approx 300$ ), however,  $p$ -adaptivity modes P\_ISO and P\_ANISO start off with relatively large  $N_{dof}$ . We can see from the graphs and also from the Fig. 5 that  $p$ -adaptivity is used for the most part of the problem. The initially high  $N_{dof}$  for  $p$ -adaptive modes indicate that only first time steps benefit greatly from the  $h$ -adaptivity. P\_ISO, HP\_ANISO\_H and HP\_ANISO\_P are the fastest in terms of CPU time, however, we have to consider that P\_ISO and HP\_ANISO\_P start off from more refined mesh.

So far we have seen that HP\_ANISO results in the smallest problem size, but takes most CPU time. When it comes to a large domain or 3D modeling the problem size becomes the most important factor. Therefore, we consider HP\_ANISO the most suitable adaptivity type to the given problem. Thus some ways to optimize the time factor was considered. We neglected HP\_ANISO\_H as this uses single mesh only and for large 3D domains, we believe the multi-mesh approach would be more reasonable. The performance of HP\_ANISO\_P with refined mesh and half-refined mesh, and performance of HP\_ANISO with unrefined, half-refined, and refined meshes was calculated (see Fig. 4). The results are shown in Fig. 8 and Fig. 9.

TODO(more explanation) It can be seen that some initial refinements help to reduce the CPU time, however, it increases the problem size.

## 5. Conclusion, future works

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