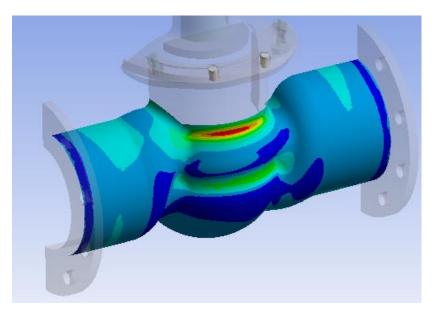
Ansys Mechanical Beyond the Basics

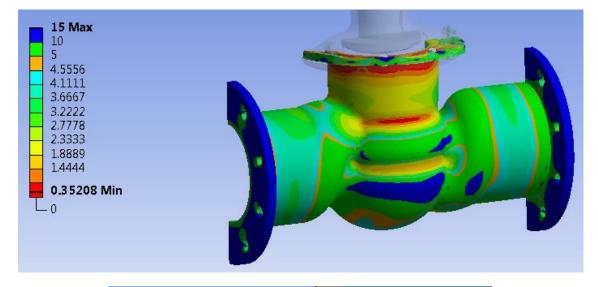
Module 06 Student Step-by-Step Guide: Expanded Results and Validation

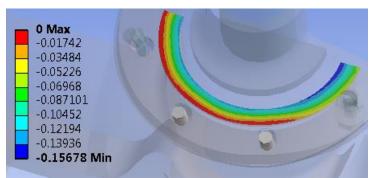
Release 2021 R2

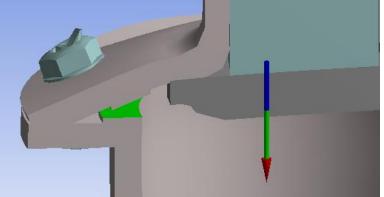


Use this guide to repeat the steps the instructor demonstrated within this module.

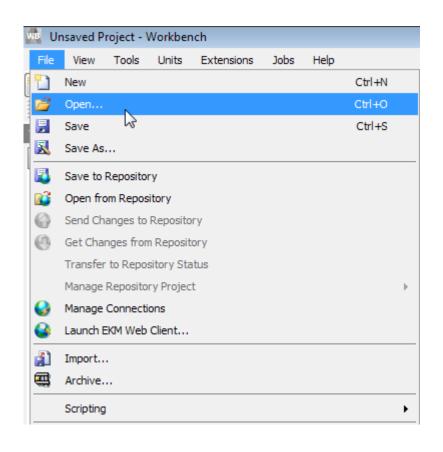


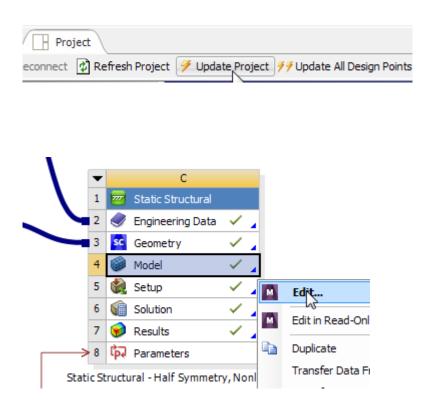






- Open Archive: "Globe_Valve_SS06_Start.wbpz"
- Update the Project to solve the model, then Open Mechanical

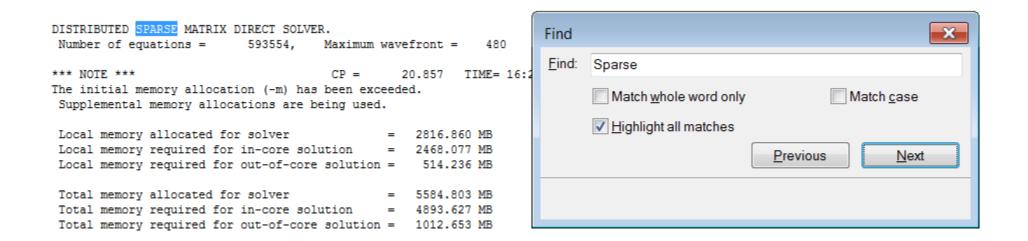






Review the **Solution Information** window:

- Note the versioning information at the beginning
- Followed by the number of parallel processors requested
- Search within Solution Information for keywords such as "sparse", "warning", and "error"
 - Ctrl-F → Sparse → Next



Review the **Solution Information** window:

• Compare the in-core solution statistics for this run against the out-of-core solution statistics for a different run using the **Image** inserted under **Solution Information**; this half symmetry model required much less computer resources



- Solution Information
 - Example of Out-of-Core Solution

```
DISTRIBUTED SPARSE MATRIX DIRECT SOLVER.

Number of equations = 3465736, Maximum wavefront = 714

Local memory allocated for solver = 3149.457 MB
Local memory required for in-core solution = 16092.762 MB
Local memory required for out-of-core solution = 3061.049 MB

Total memory required for in-core solution = 32711.935 MB
Total memory required for out-of-core solution = 6071.417 MB

3,465,736 DOF → 10-20 GB RAM / 1 M DOF Approx 34 GB RAM required

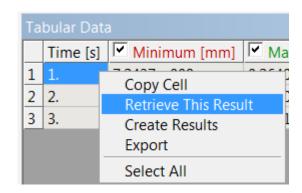
Solver only allocated 6 GB RAM

Solution requires 32 GB RAM
```

Use the **Tabular Data Window** below the Graphics window to retrieve and review results from each of the 3 steps of the solution:

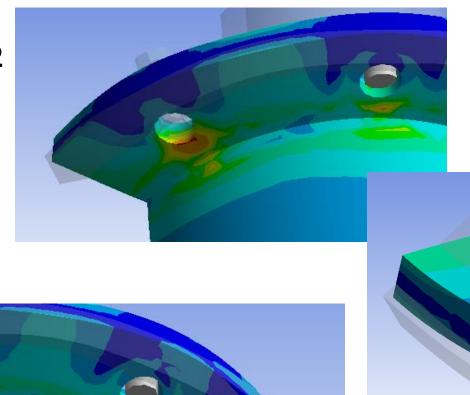
- Solution → Total Deformation
- Tabular Data → Time 1. → RMB Retrieve This Result
- Repeat for other results of interest
- Change Result Scaling as desired
- Alternatively, Set the **Display Time** in the Details of the result to the desired Time value → **RMB** – **Retrieve This Result**





Review Stress in Valve Body and identify locations of stress singularity:

Solution → Equivalent Stress 2

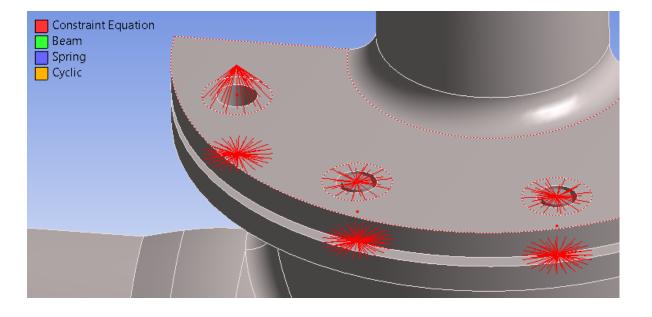




Use Solution Information to View **FE Connections**, identifying possible locations of stress singularity:

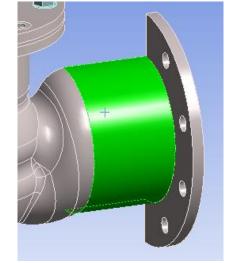
Solution Information → Graphics Tab

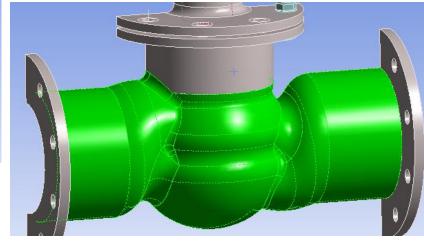


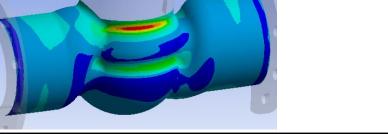


Add equivalent stress scoped to Valve Body; don't include regions of singular stress:

- RMB Solution → Insert → Stress →
 Equivalent (von-Mises)
- Select cylindrical face of valve body →
 Extend to Limits → CTR—Select upper cylindrical surface (to un-select it)
- Geometry Scope → All bodies → Apply
- RMB Equivalent Stress 3 → Evaluate All Results







Compare Averaged and Unaveraged Results on Valve Body:

 Details of Equivalent Stress 3 → **Integration Point Results** → **Display Option** → **Averaged**

 Details of Equivalent Stress 3 → Integration Point Results → Display Option → Unaveraged

Details of "Equivalent Stress 3"

34 Faces

Time

No

Unaveraged

Scoping Method

Display Time Calculate Time History Yes

Integration Point Results Display Option

Geometry

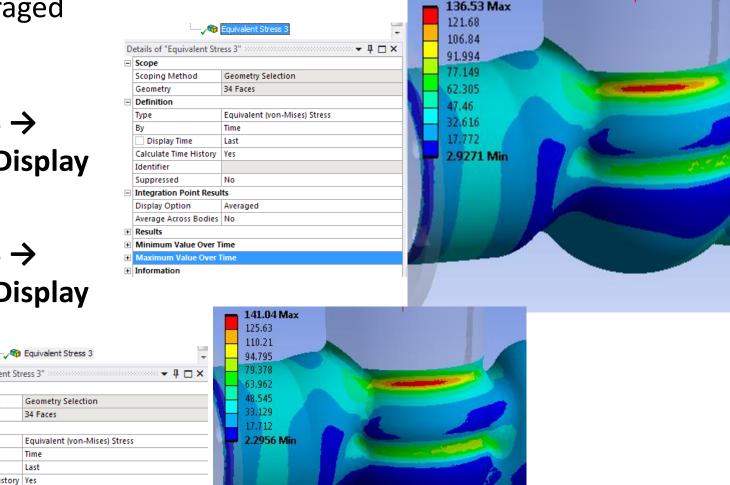
Definition

Identifier Suppressed

Type

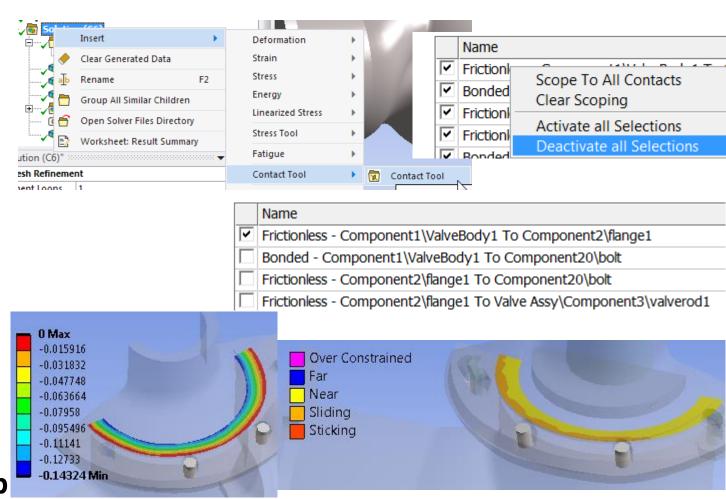
─ Scope

Evaluate All Results



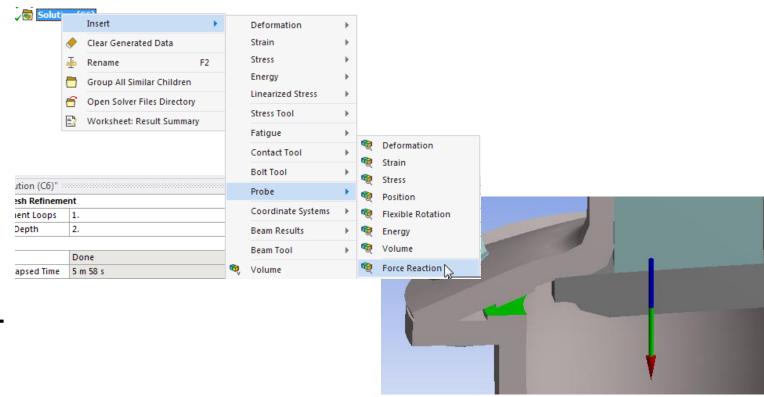
Use a Contact Tool to review Contact Status, Pressure, and Gap at the Valve Body to Flange Frictionless Contact Interface:

- Solution → Insert Contact Tool
- Deactivate All Selections
- Activate only the first Frictionless
 Contact Pair
- RMB Contact Tool → Insert →
 Pressure
- RMB Contact Tool → Insert → Gap
- Evaluate All Results



Review total clamping force between Valve Body and Flange using Force Reaction Probe:

- Solution → Probe → Force
 Reaction
- Location Method → Contact Region
- Contact Region → Frictionless –
 Valve Body1 To Flange1
- Extraction → Contact (Contact Element)
- Evaluate All Results



Tabular Data :							
	Time [s]	Force Reaction (X) [N]	Force Reaction (Y) [N]	Force Reaction (Z) [N]	Force Reaction (Total) [N]		
1	1.	-5.4428e-011	-1.9142e-010	-41171	41171		
2	2.	-5.4377e-011	-1.9122e-010	-41120	41120		
3	3.	-3.6296e-011	-1.0835e-010	-23159	23159		

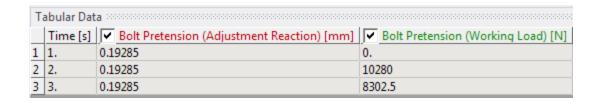


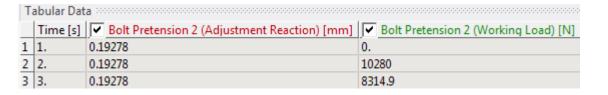
Retrieve clamping force on a per-bolt basis using Force Reaction Probe on the Bolt Pretension Loads:

Drag / Drop Bolt Pretension 4 onto Solution Folder



- Repeat for Bolt Pretension 3
- Evaluate All Results

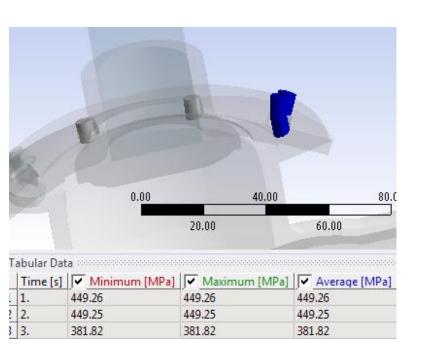


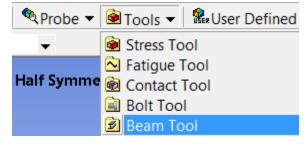


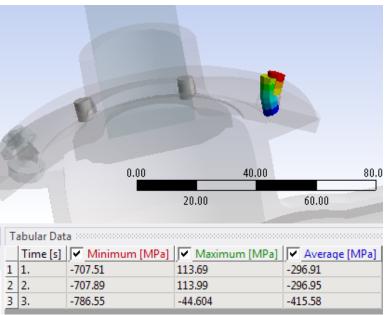


Review Stress (Direct, Min Combined, Max Combined) in line body beam using the Beam Tool:

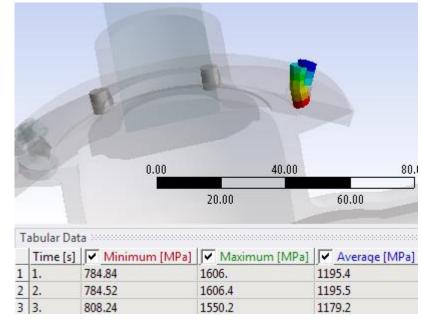
- Solution → Tools → Beam Tool
- Evaluate All Results







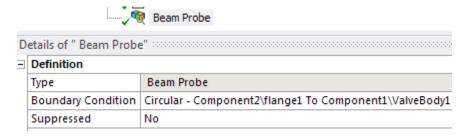






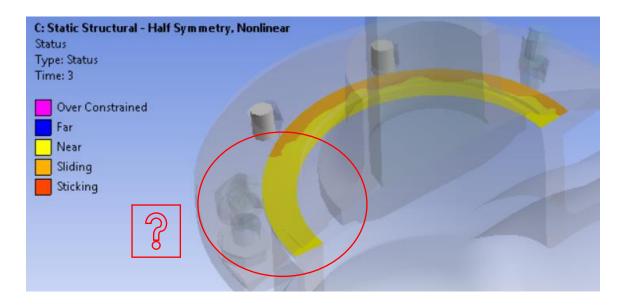
Review forces and moments in the Body-to-Body Beam connections using the Beam Probe:

- Solution → Probe → Beam
- Boundary Condition → Circular Flange1 To Valve Body1
- Evaluate All Results



Tabular Data								
Time [s] 🗸 Beam Probe (Axial Force) [N]	■ Beam Probe (Torque) [N·mm]	Beam Probe (Shear Force At I) [N]	Beam Probe (Shear Force At J) [N]	■ Beam Probe (Moment At I) [N·mm]	Beam Probe (Moment At J) [N⋅mm]		
1 1.	10280	59.786	197.35	197.35	18297	17137		
2 2.	10280	60.092	197.78	197.78	18301	17139		
3 3.	8302.5	-8.5863	727.44	727.44	22951	18658		

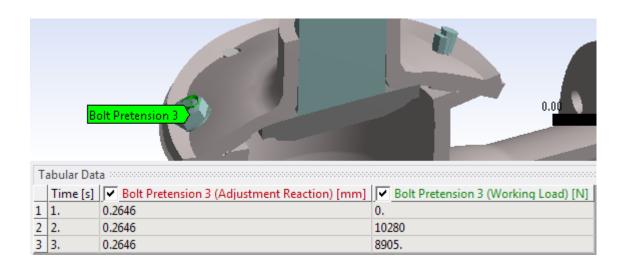
After reviewing the contact force and bolt pretension results at the bolted interface between the flange and the valve body, why does there appear to be no clamping force at the flange in the location of the 1 bolt modeled as a solid body? The contact status shows no contact in this region...



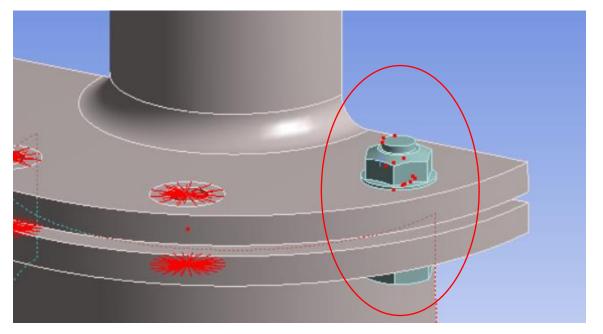
Review the clamping force in that solid body bolt:

 Drag the first Bolt Pretension load from the Static Structural branch to the Solution branch and Evaluate All Results

There is still a working load in the bolt. But it is now more than the original pretension force. It has taken on additional force, apparently due to separation of the joint. Why haven't the other bolts done the same thing?



View the **FE Connections** once again by selecting **Solution Information** and the **Graphics** tab. Look at the FE Connections generated by the Bolt Pretension load. These connections represent the constraint equations used to "tie" the bolt body back together after it has been split by the bolt pretension load. It appears that the bolt body has been split outside of the joint. Ideally, the bolt would be split somewhere between the two flange surfaces.



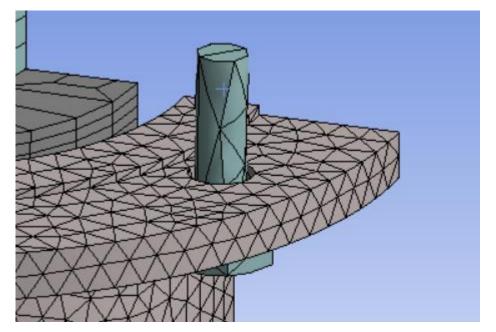
Check the mesh density on the solid body bolt. A mesh that is too coarse can be problematic for bolt pretension loads, as it does not provide a viable means of splitting the mesh.

- Hide the remaining nut body along with the flange1 body
- Select the Mesh branch to display the mesh on the bolt body

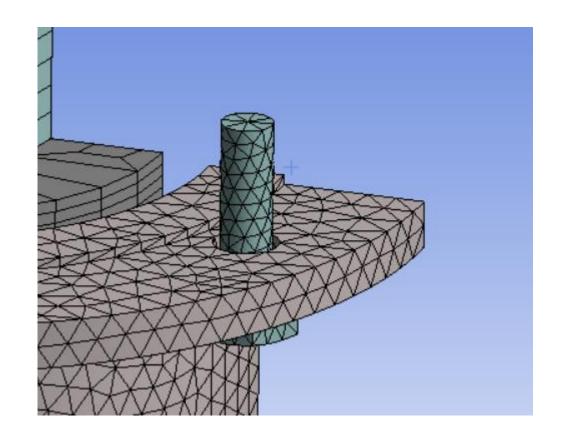
Refine the mesh on the bolt body in order to supply more elements along the length of

the bolt shaft.

- Mesh → RMB → Insert → Sizing
 - Select the bolt body
 - Element Size = 2.0 mm
- Generate Mesh

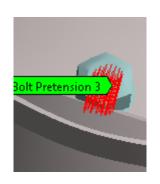


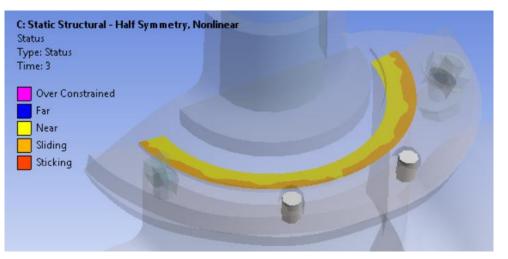
The bolt now has a more refined mesh. Re-solve the model and then review the **FE Connections, Contact Tool** and **Bolt Pretension** results once again.





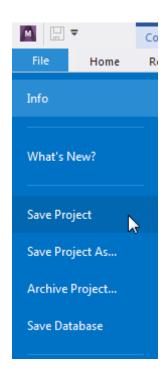
These results look much more as expected now.





Tabular Data							
	Time [s]	Bolt Pretension 3 (Adjustment Reaction) [mm]		Bolt Pretension 3 (Working Load) [N]			
1	1.	0.25657	0.				
2	2.	0.25657	102	82			
3	3.	0.25657	891	0.4			

• Save Project for use later if desired.



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