

Case Study

Modelling the Steady State Temperature Distribution in a Ceramic Plate

Mathematical model

- The law of conservation of energy, along with Fourier's law of heat conduction, leads to the following **partial differential equation**:

$$\rho c \frac{\partial T}{\partial t} = k \nabla^2 T + g$$

- For the **steady state** problem, we obtain the **Poisson equation**:

$$\nabla^2 T + \frac{g}{k} = 0$$

- If the source is zero everywhere, we obtain the **Laplace equation**:

$$\nabla^2 T = 0$$

Two dimensions

- Two-dimensional Laplacian

$$\nabla^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2}$$

- Poisson equation

$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{g}{k} = 0$$

- Laplace equation

$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} = 0$$

Boundary Conditions

Three types of boundaries in heat conduction problems:

Prescribed Temperature (Dirichlet condition):

$$T(x, b) = f(x)$$

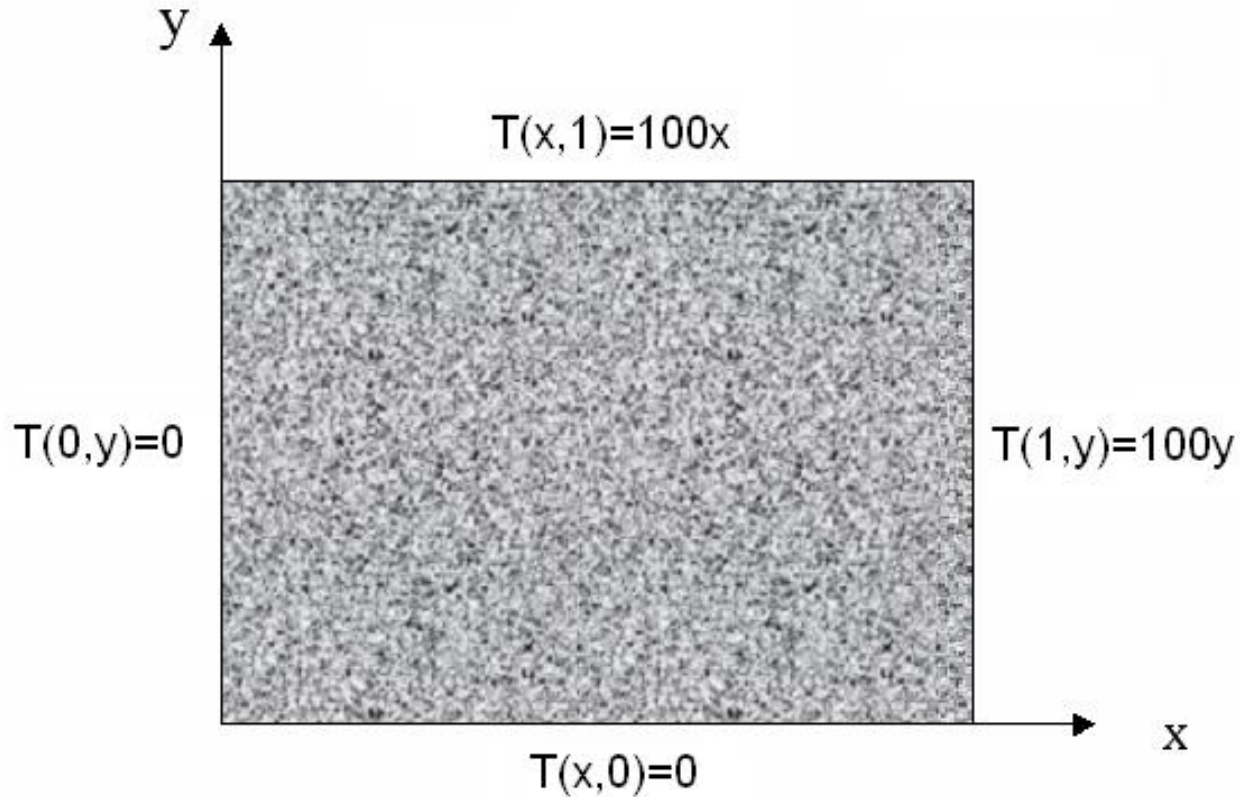
Insulated (Neumann condition):

$$\nabla T \cdot \hat{\mathbf{n}} = 0$$

Convective (Robin condition):

$$k \nabla T \cdot \hat{\mathbf{n}} = h (T_{\infty} - T)$$

First example: Laplace equation



Ceramic plate with Dirichlet boundary conditions

Summary of the Mathematical Model

$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} = 0, \quad 0 < x < 1 \quad , \quad 0 < y < 1$$

subject to

$$\text{at } x = 0 \quad : \quad T = 0$$

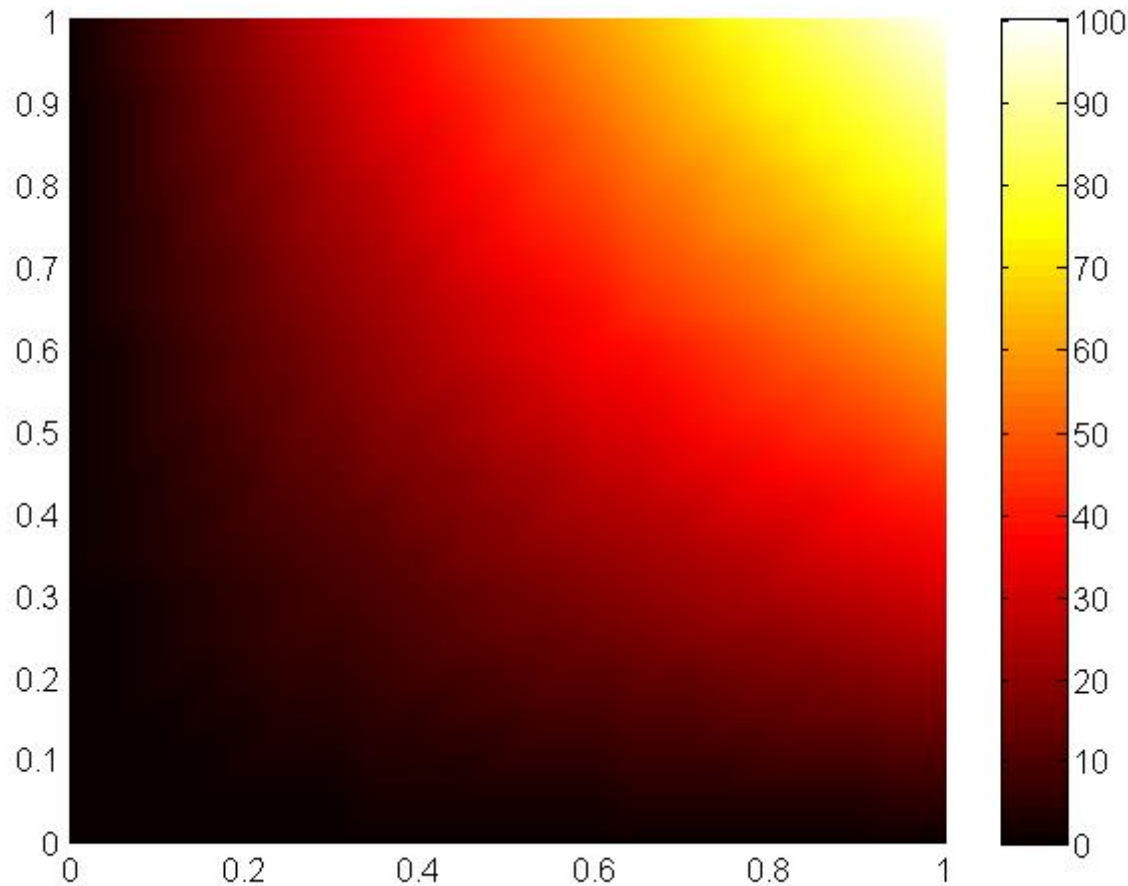
$$\text{at } x = 1 \quad : \quad T = 100y$$

$$\text{at } y = 0 \quad : \quad T = 0$$

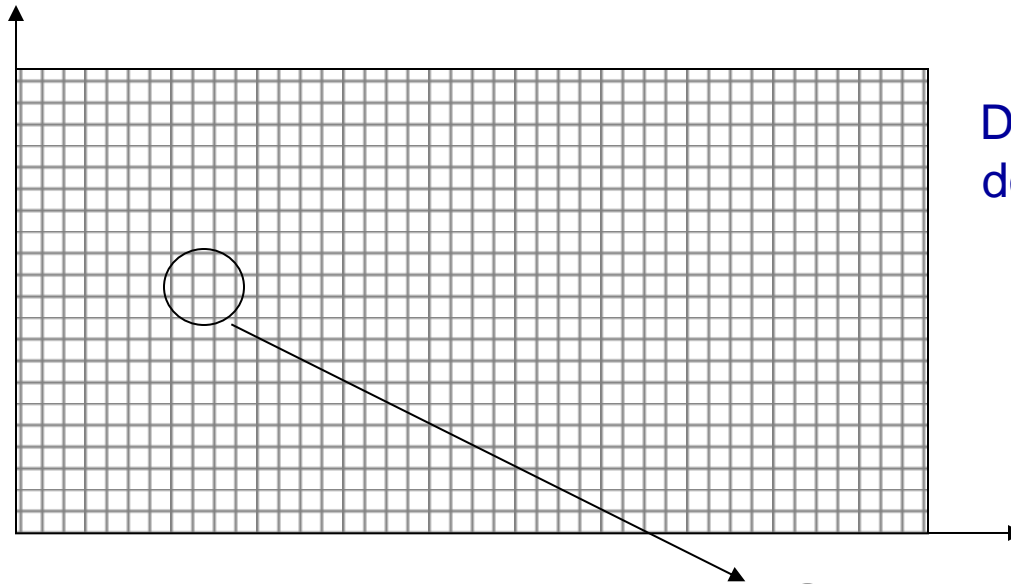
$$\text{at } y = 1 \quad : \quad T = 100x$$

Analytical Solution

$$T(x, y) = 100xy$$



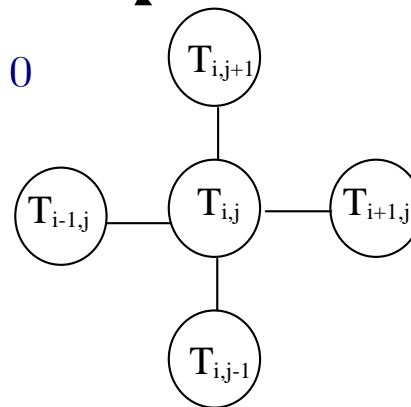
Conversion to a Matrix Problem



Discretise the domain using a mesh

$$-T_{i,j-1} - T_{i-1,j} + 4T_{i,j} - T_{i+1,j} - T_{i,j+1} = 0$$

Finite Difference Stencil used for each internal node on the mesh

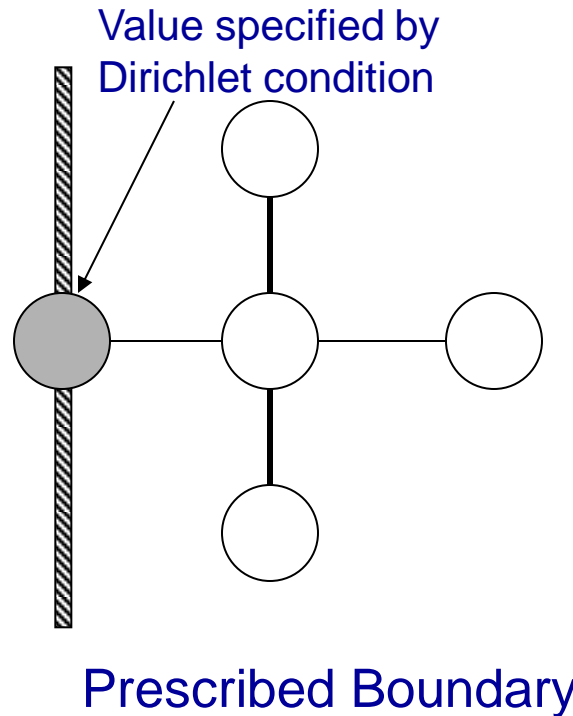


The model is converted to a matrix problem by discretising the domain and forming *finite difference equations*.

Treatment of Boundary Nodes

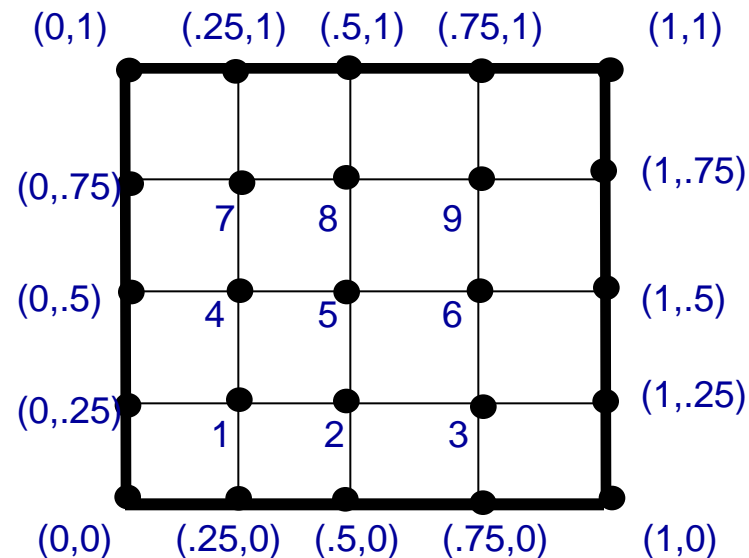
Prescribed boundary:

Dirichlet condition gives required value for use in FDE

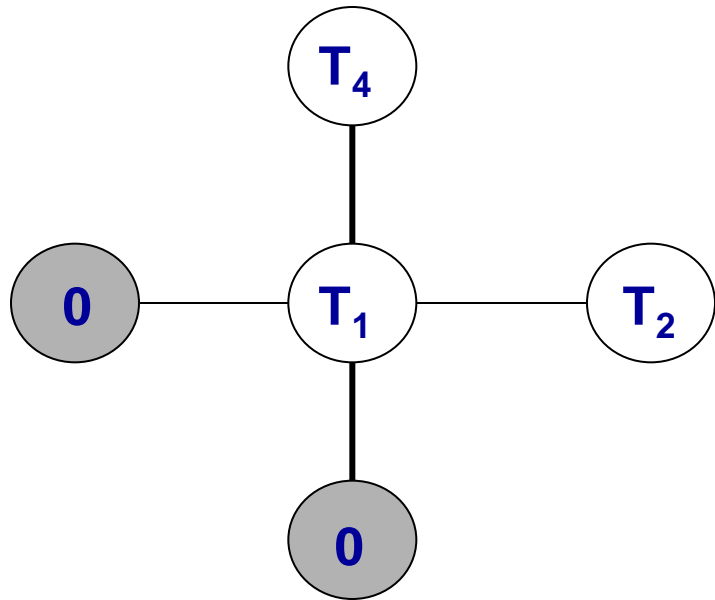


How does this process generate a matrix?

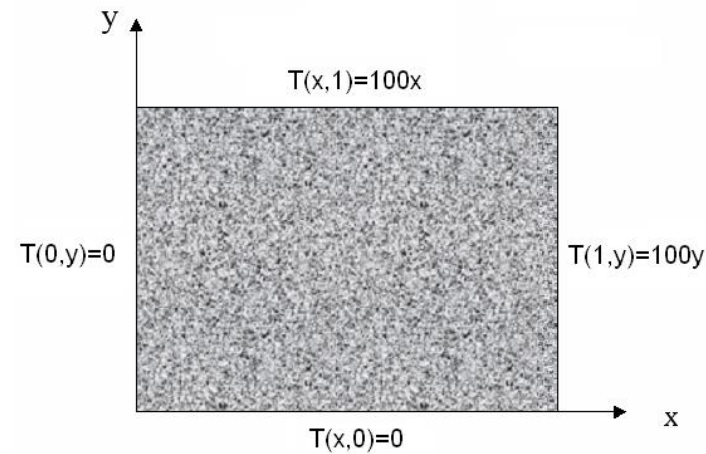
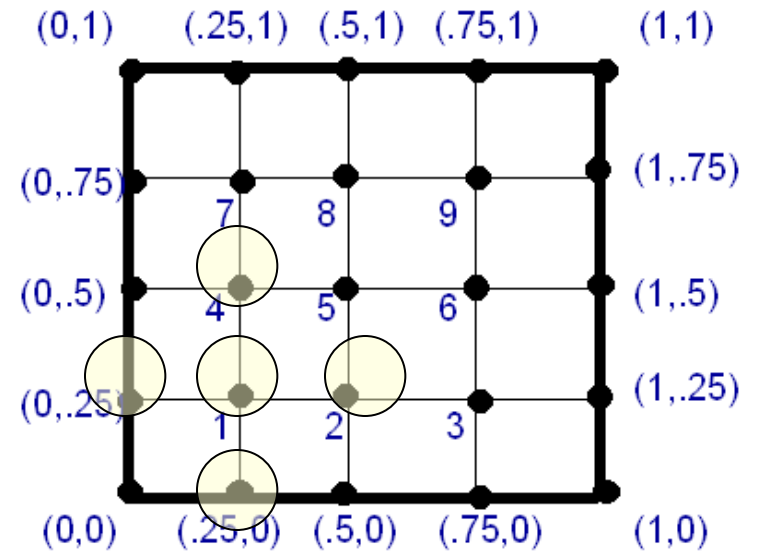
- Introduce a node numbering scheme and map (i,j) coordinates to these nodes:



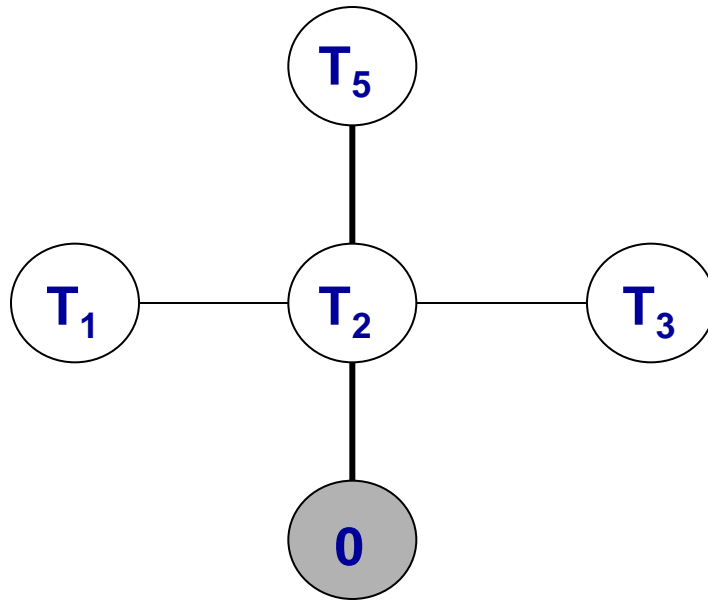
Node 1



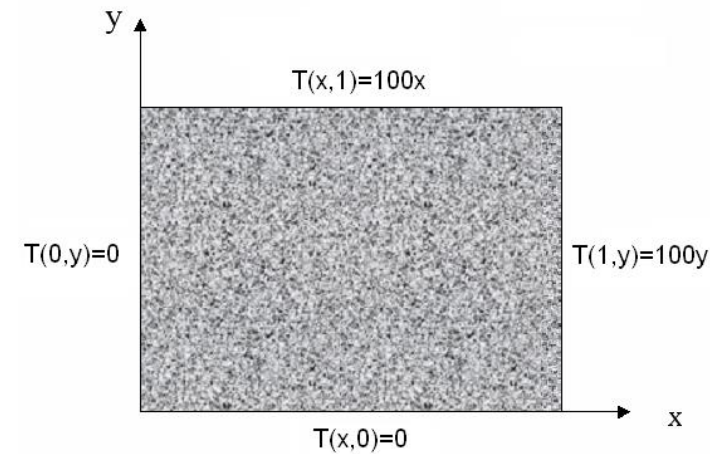
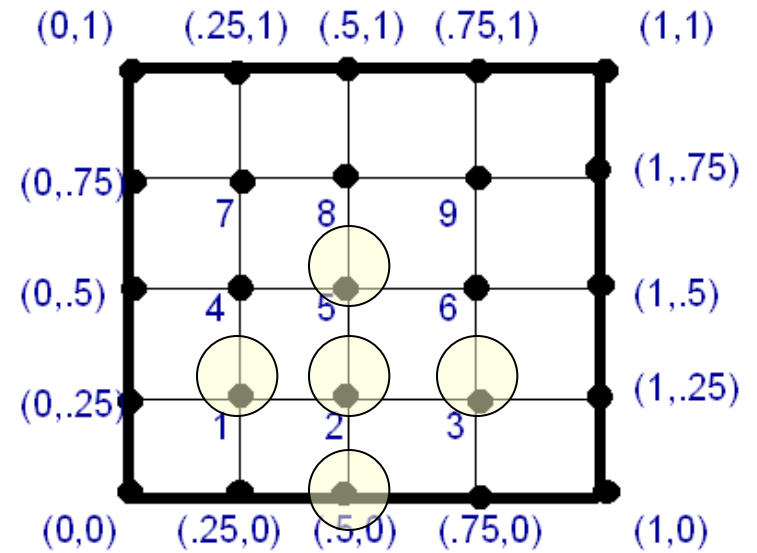
$$4T_1 - T_2 - T_4 = 0$$



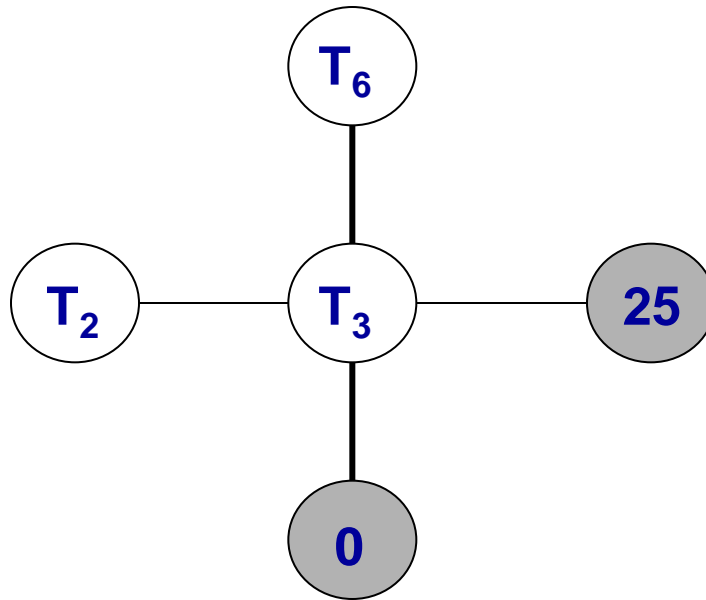
Node 2



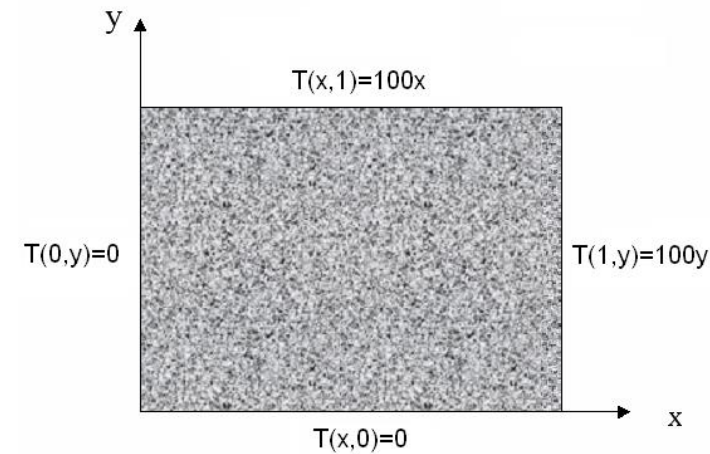
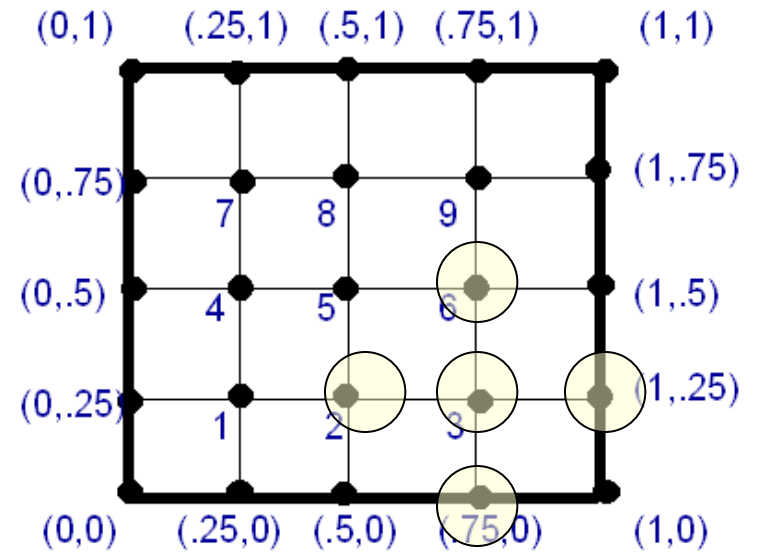
$$-T_1 + 4T_2 - T_3 - T_5 = 0$$



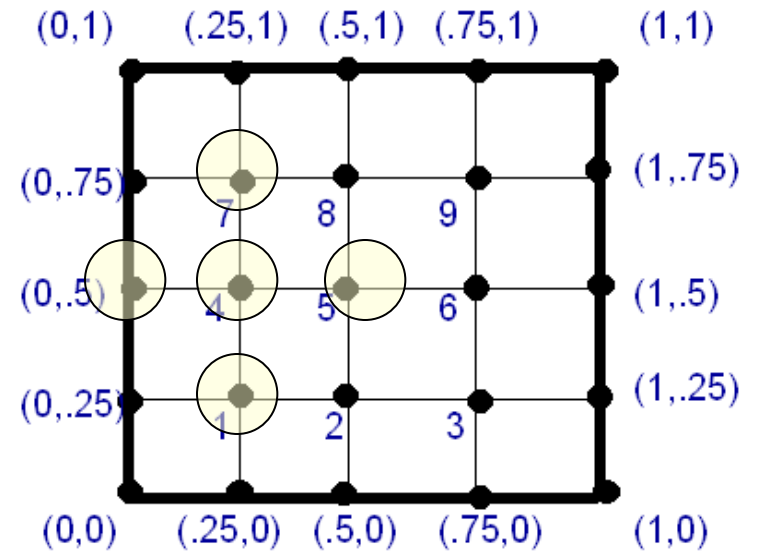
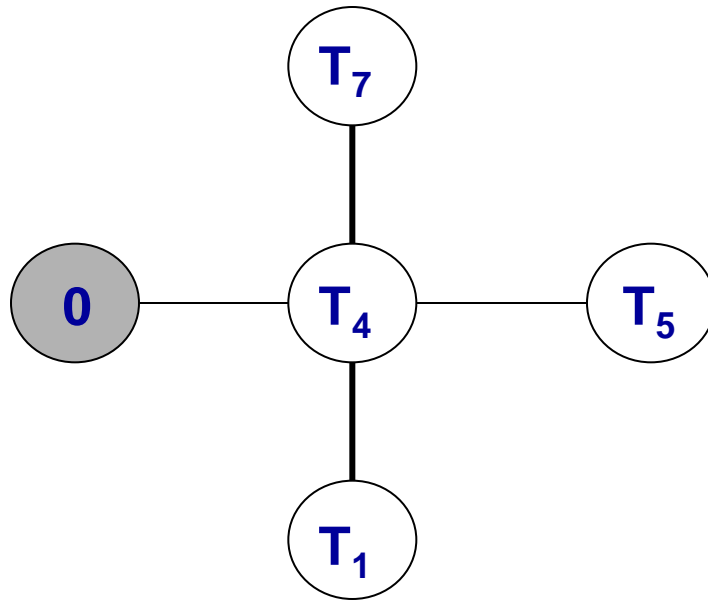
Node 3



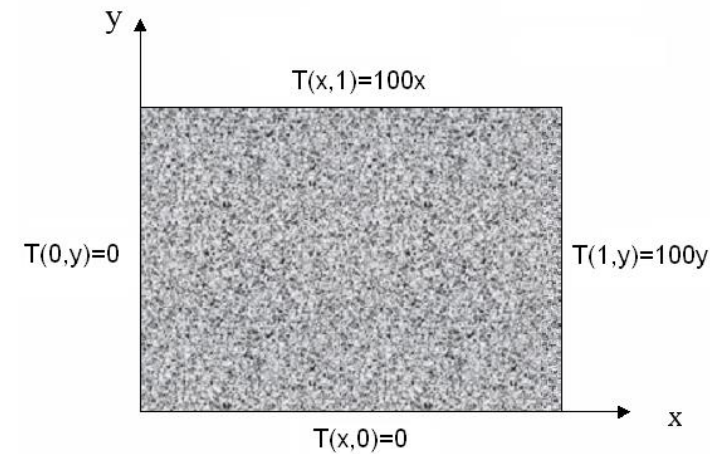
$$-T_2 + 4T_3 - T_6 = 25$$



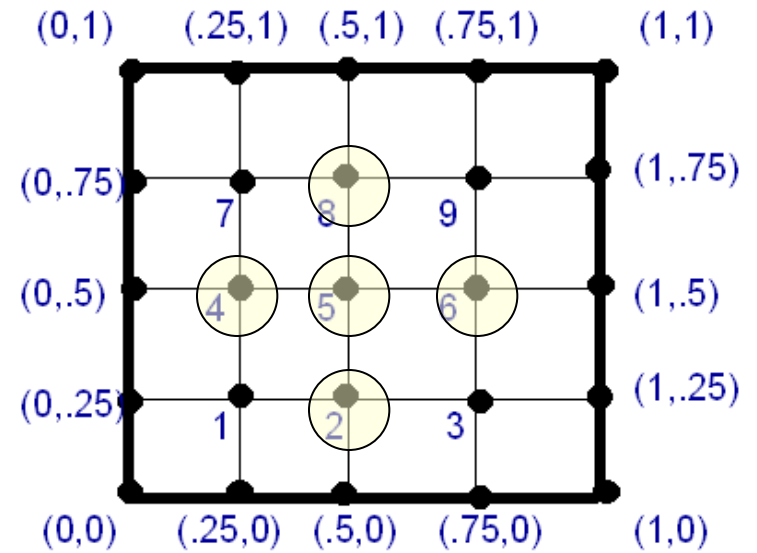
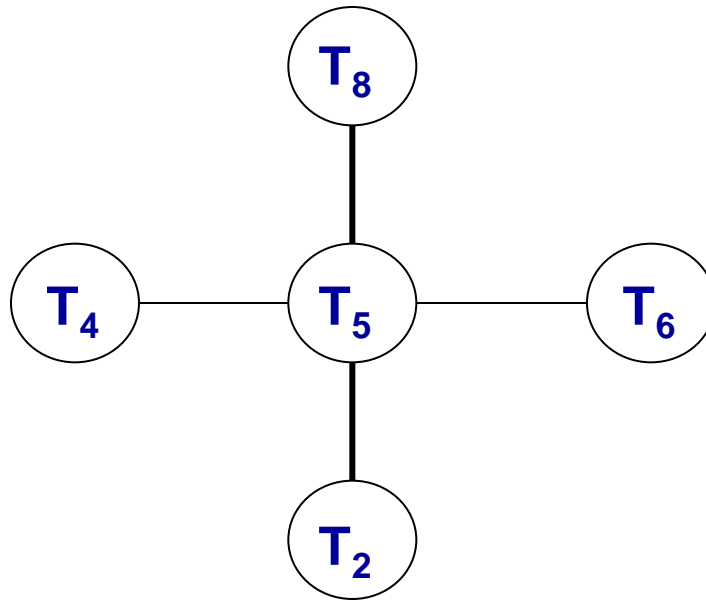
Node 4



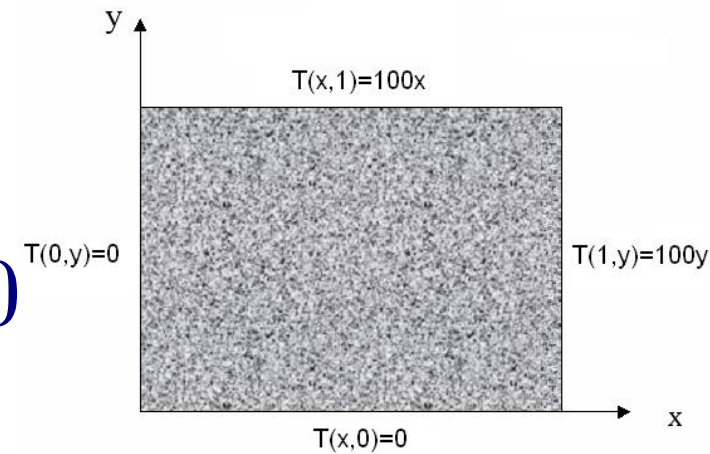
$$-T_1 + 4T_4 - T_5 - T_7 = 0$$



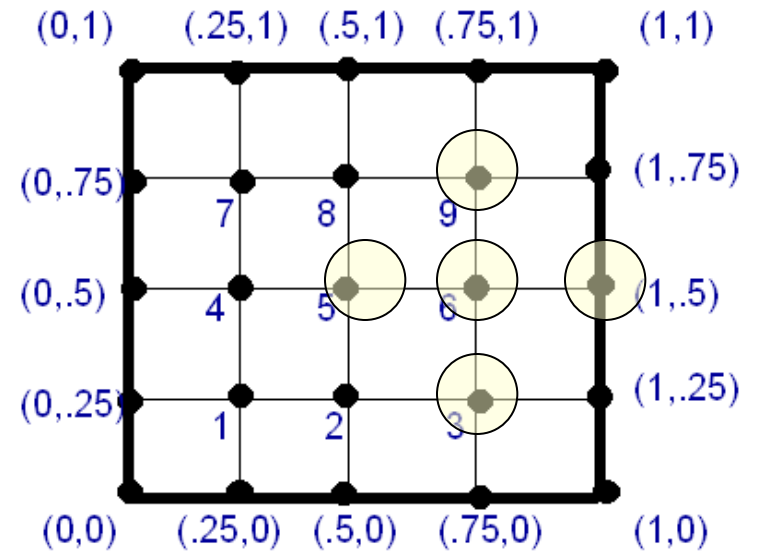
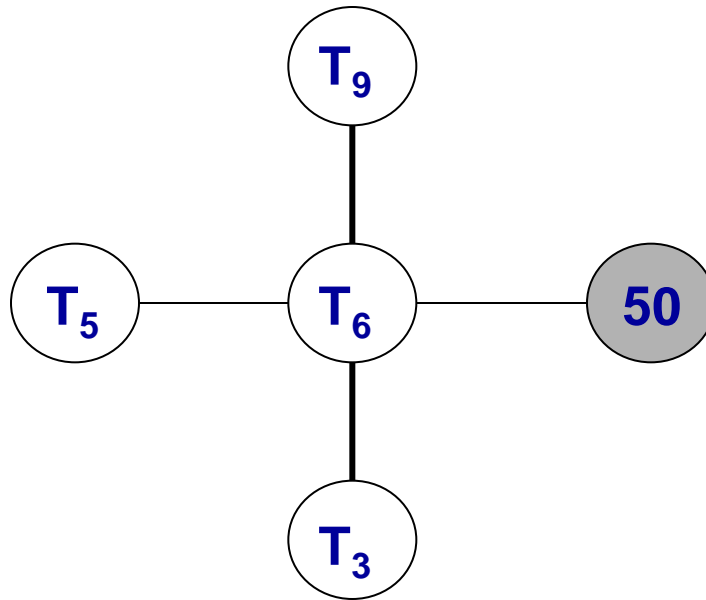
Node 5



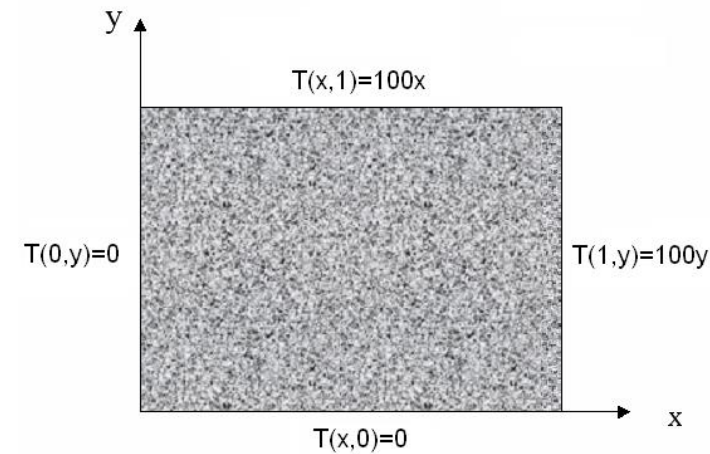
$$-T_2 - T_4 + 4T_5 - T_6 - T_8 = 0$$



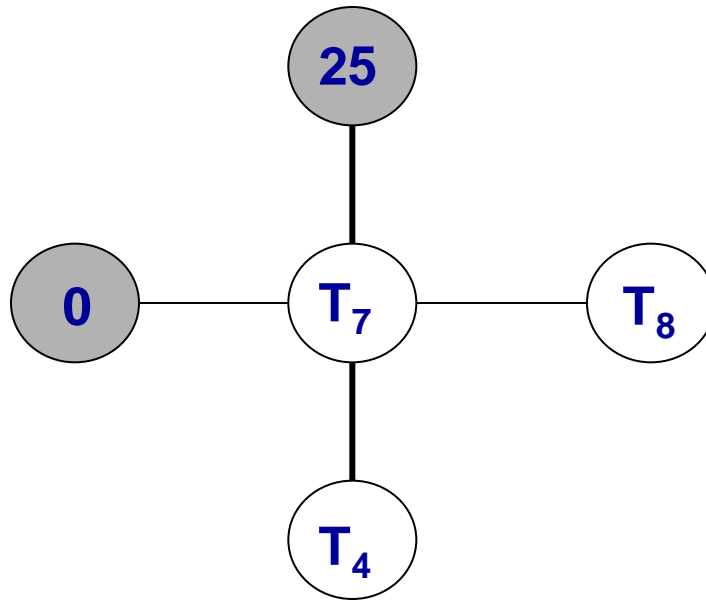
Node 6



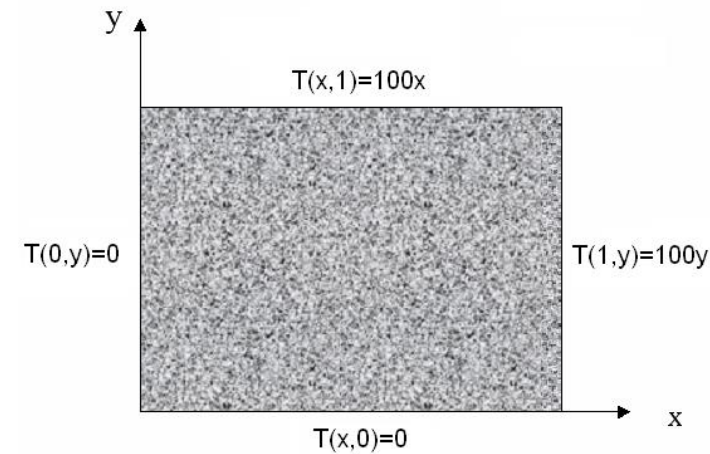
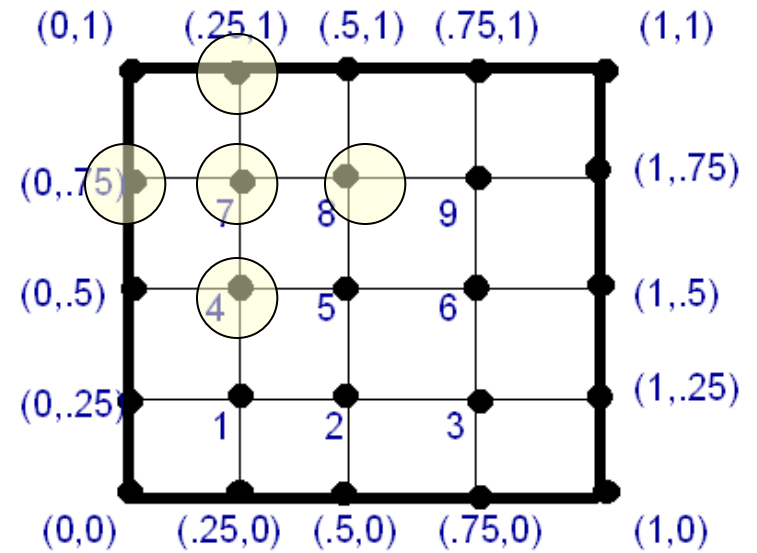
$$-T_3 - T_5 + 4T_6 - T_9 = 50$$



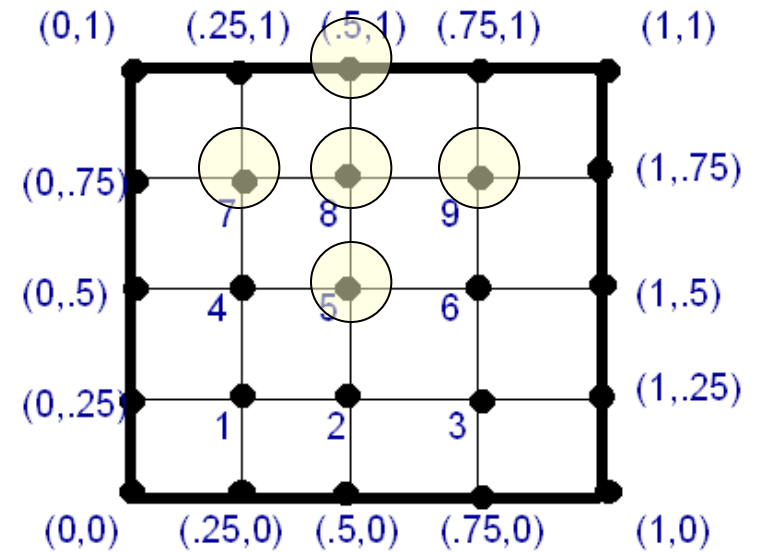
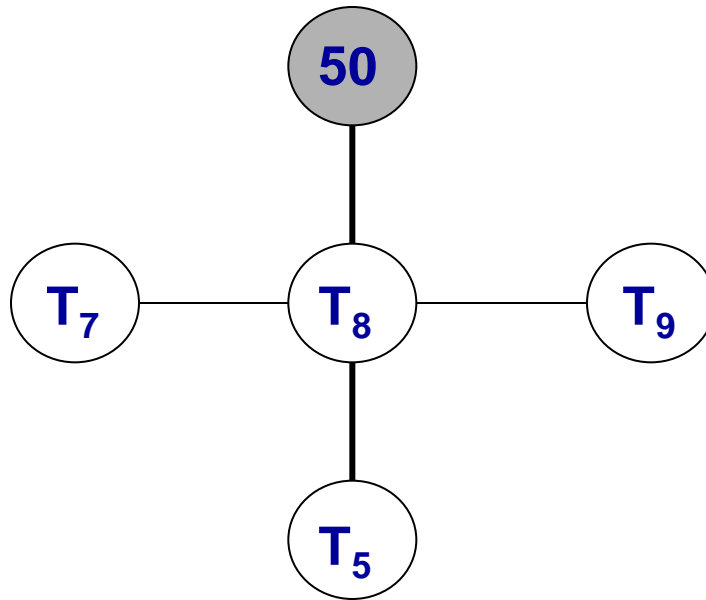
Node 7



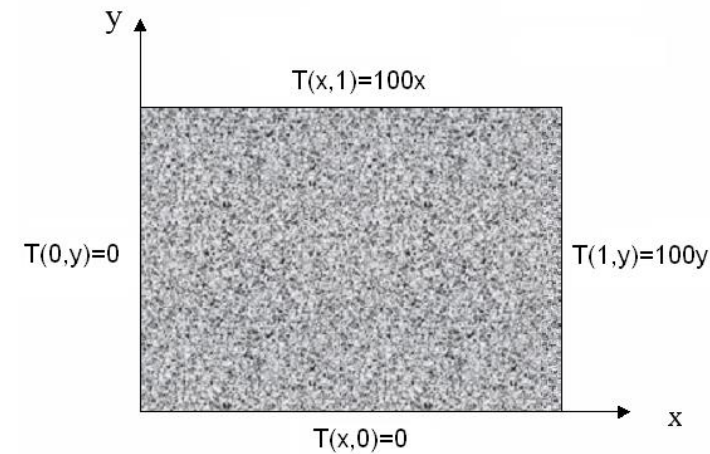
$$-T_4 + 4T_7 - T_8 = 25$$



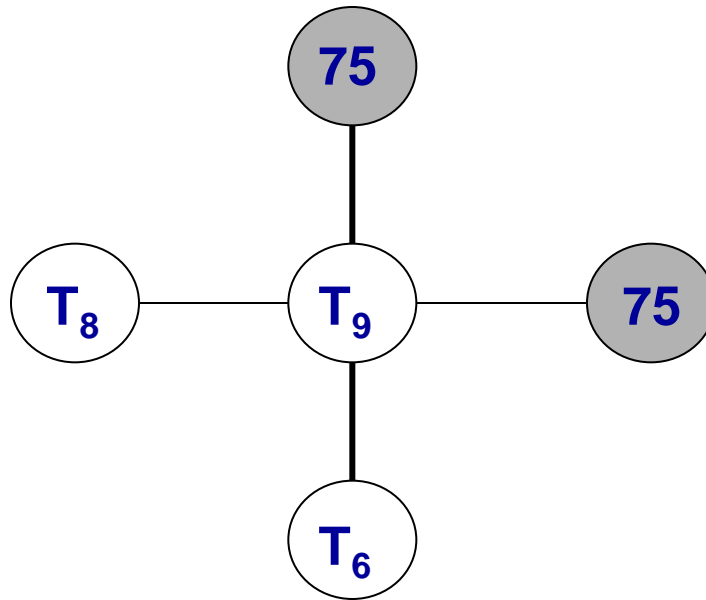
Node 8



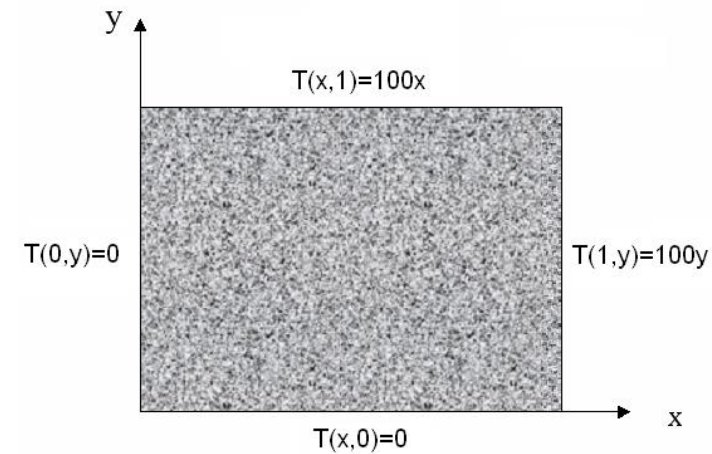
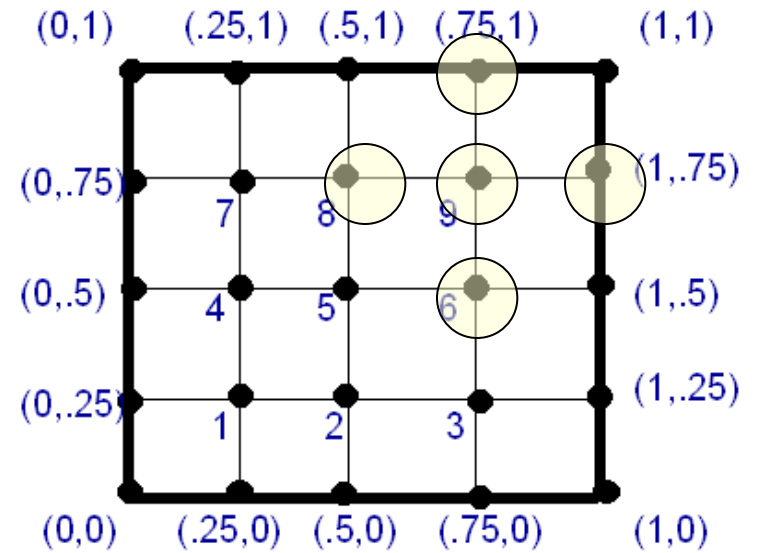
$$-T_5 - T_7 + 4T_8 - T_9 = 50$$



Node 9



$$-T_6 - T_8 + 4T_9 = 150$$



Discrete Laplace equation: $\mathbf{Ax} = \mathbf{b}$

$$\mathbf{A} = \begin{bmatrix} 4 & -1 & 0 & -1 & 0 & 0 & 0 & 0 & 0 \\ -1 & 4 & -1 & 0 & -1 & 0 & 0 & 0 & 0 \\ 0 & -1 & 4 & 0 & 0 & -1 & 0 & 0 & 0 \\ -1 & 0 & 0 & 4 & -1 & 0 & -1 & 0 & 0 \\ 0 & -1 & 0 & -1 & 4 & -1 & 0 & -1 & 0 \\ 0 & 0 & -1 & 0 & -1 & 4 & 0 & 0 & -1 \\ 0 & 0 & 0 & -1 & 0 & 0 & 4 & -1 & 0 \\ 0 & 0 & 0 & 0 & -1 & 0 & -1 & 4 & -1 \\ 0 & 0 & 0 & 0 & 0 & -1 & 0 & -1 & 4 \end{bmatrix} \quad \mathbf{b} = \begin{bmatrix} 0 \\ 0 \\ 25 \\ 0 \\ 0 \\ 50 \\ 25 \\ 50 \\ 150 \end{bmatrix}$$

Discrete Laplace equation: $\mathbf{Ax} = \mathbf{b}$

$$\mathbf{A} = \begin{bmatrix} 4 & -1 & 0 & -1 & 0 & 0 & 0 & 0 & 0 \\ -1 & 4 & -1 & 0 & -1 & 0 & 0 & 0 & 0 \\ 0 & -1 & 4 & 0 & 0 & -1 & 0 & 0 & 0 \\ -1 & 0 & 0 & 4 & -1 & 0 & -1 & 0 & 0 \\ 0 & -1 & 0 & -1 & 4 & -1 & 0 & -1 & 0 \\ 0 & 0 & -1 & 0 & -1 & 4 & 0 & 0 & -1 \\ 0 & 0 & 0 & -1 & 0 & 0 & 4 & -1 & 0 \\ 0 & 0 & 0 & 0 & -1 & 0 & -1 & 4 & -1 \\ 0 & 0 & 0 & 0 & 0 & -1 & 0 & -1 & 4 \end{bmatrix} \quad \mathbf{b} = \begin{bmatrix} 0 \\ 0 \\ 25 \\ 0 \\ 0 \\ 50 \\ 25 \\ 50 \\ 150 \end{bmatrix}$$

Banded structure

Discrete Laplace equation: $\mathbf{Ax} = \mathbf{b}$

$$\mathbf{A} = \begin{bmatrix} 4 & -1 & 0 & -1 & 0 & 0 & 0 & 0 & 0 \\ -1 & 4 & -1 & 0 & -1 & 0 & 0 & 0 & 0 \\ 0 & -1 & 4 & 0 & 0 & -1 & 0 & 0 & 0 \\ -1 & 0 & 0 & 4 & -1 & 0 & -1 & 0 & 0 \\ 0 & -1 & 0 & -1 & 4 & -1 & 0 & -1 & 0 \\ 0 & 0 & -1 & 0 & -1 & 4 & 0 & 0 & -1 \\ 0 & 0 & 0 & -1 & 0 & 0 & 4 & -1 & 0 \\ 0 & 0 & 0 & 0 & -1 & 0 & -1 & 4 & -1 \\ 0 & 0 & 0 & 0 & 0 & -1 & 0 & -1 & 4 \end{bmatrix} \quad \mathbf{b} = \begin{bmatrix} 0 \\ 0 \\ 25 \\ 0 \\ 0 \\ 50 \\ 25 \\ 50 \\ 150 \end{bmatrix}$$

Block structure

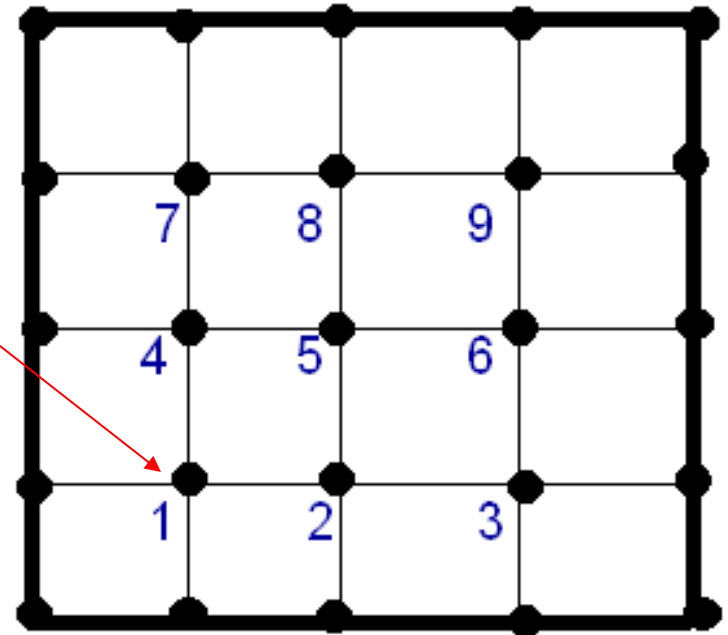
Solution Strategy

- Coefficient matrix is:
 - large: for $n \times n$ mesh, $\mathbf{A} \in \mathbb{R}^{N \times N}$, $N = O(n^2)$
 - sparse: most elements are zero
 - structured: banded / block pattern
- How do we handle this matrix efficiently?
 - efficient storage
 - naïve implementation requires $O(N^2)$ storage
 - efficient algorithms
 - naïve implementation requires $O(N^3)$ flops
- Chapter 2!

Numerical solution

$\mathbf{x} =$

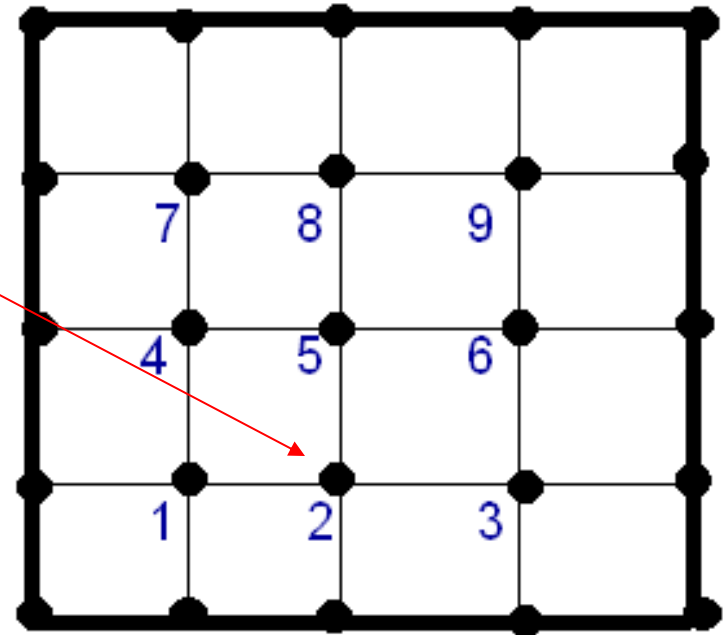
$\begin{bmatrix} 6.25 \\ 12.50 \\ 18.75 \\ 12.50 \\ 25.00 \\ 37.50 \\ 18.75 \\ 37.50 \\ 56.25 \end{bmatrix}$



Numerical solution

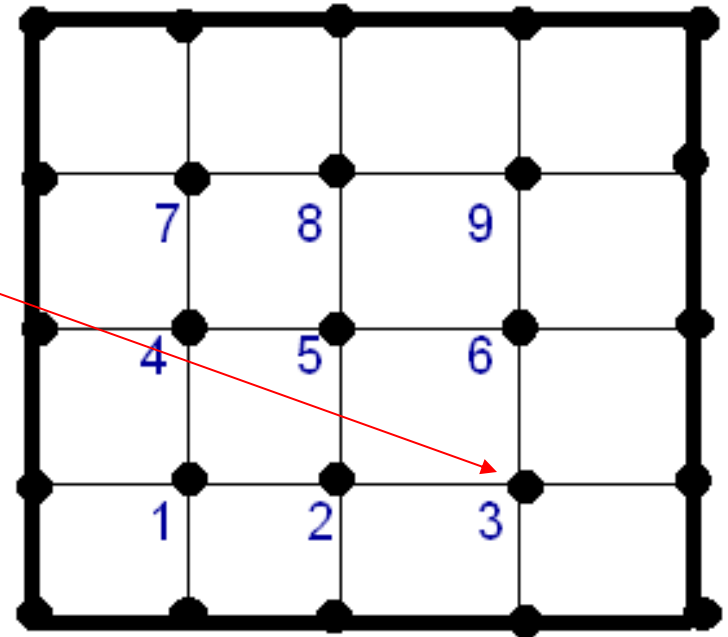
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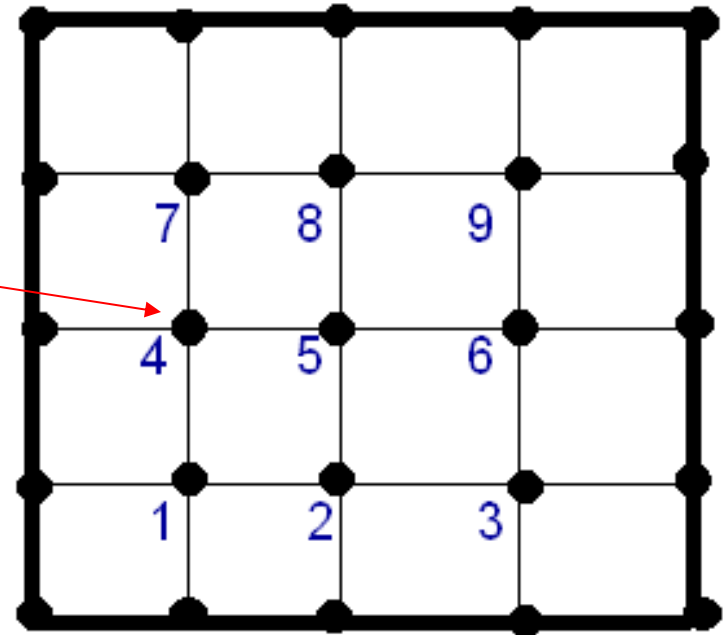
Numerical solution

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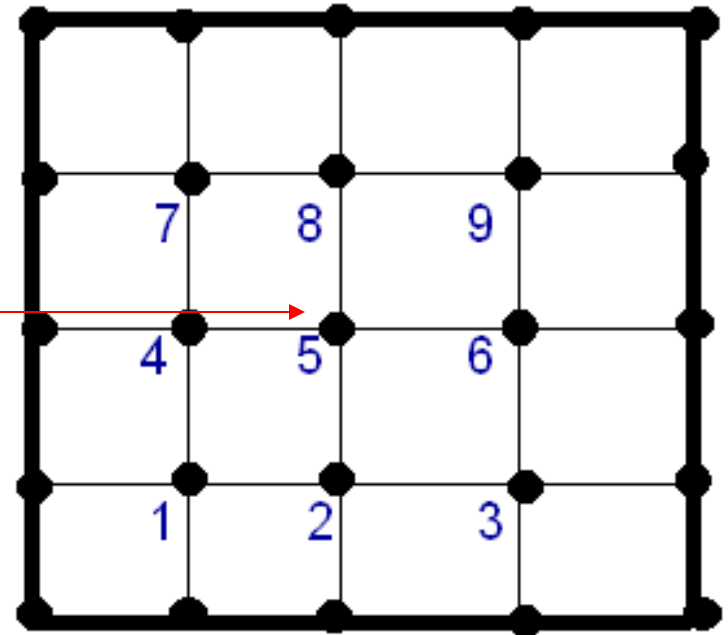
Numerical solution

$$\mathbf{x} = \begin{bmatrix} 6.25 \\ 12.50 \\ 18.75 \\ 12.50 \\ 25.00 \\ 37.50 \\ 18.75 \\ 37.50 \\ 56.25 \end{bmatrix}$$



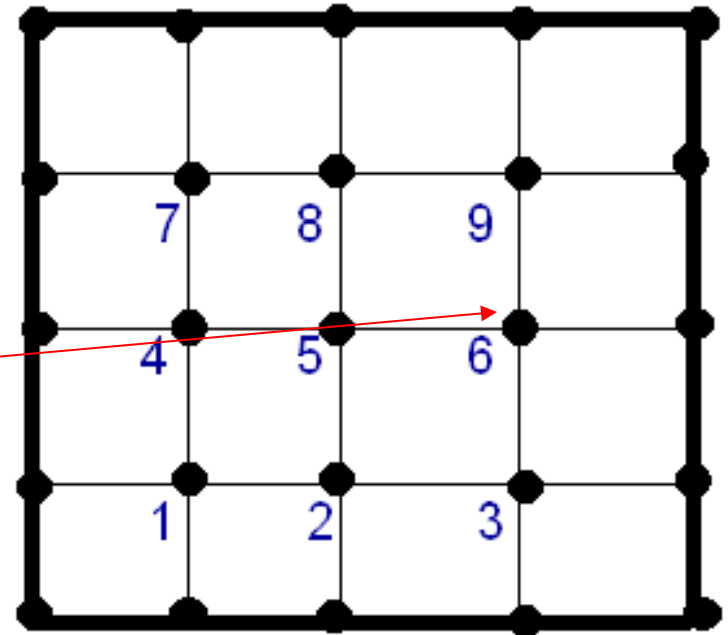
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Numerical solution

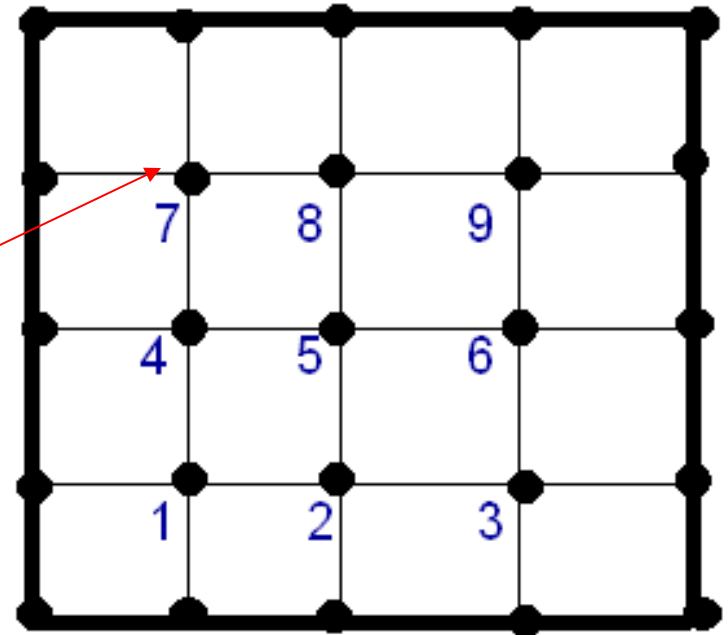
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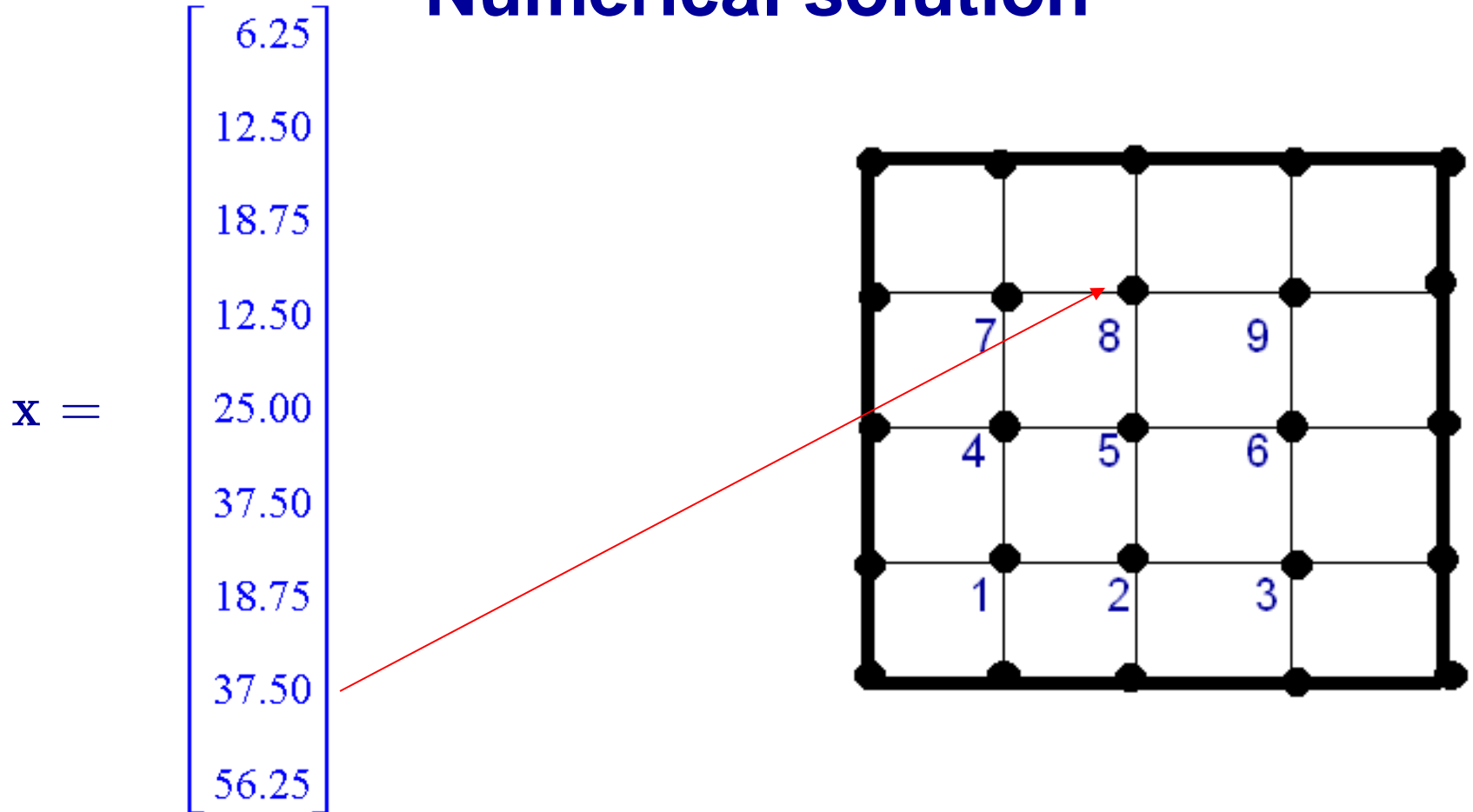
Numerical solution

$\mathbf{x} =$

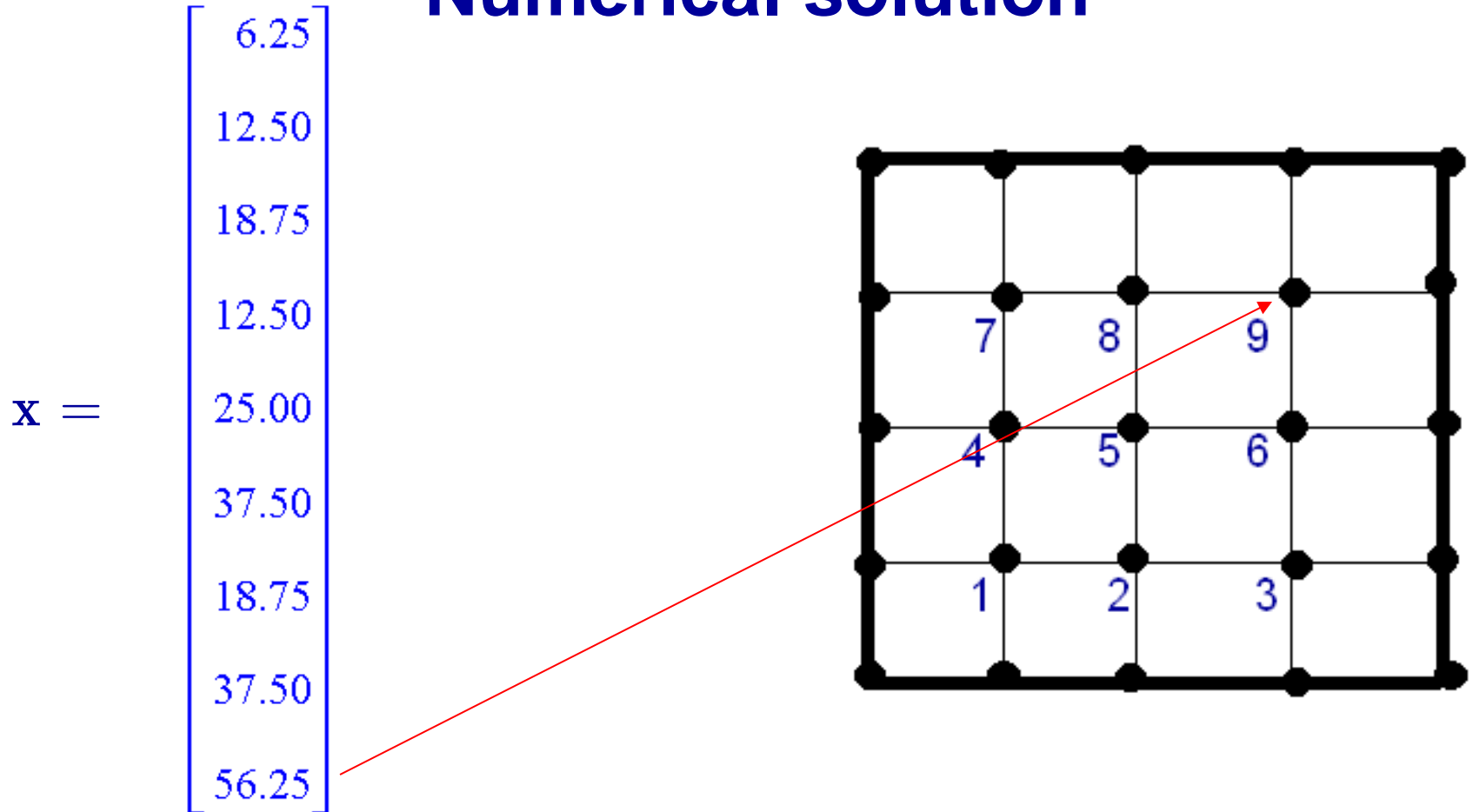
$\begin{bmatrix} 6.25 \\ 12.50 \\ 18.75 \\ 12.50 \\ 25.00 \\ 37.50 \\ 18.75 \\ 37.50 \\ 56.25 \end{bmatrix}$



Numerical solution

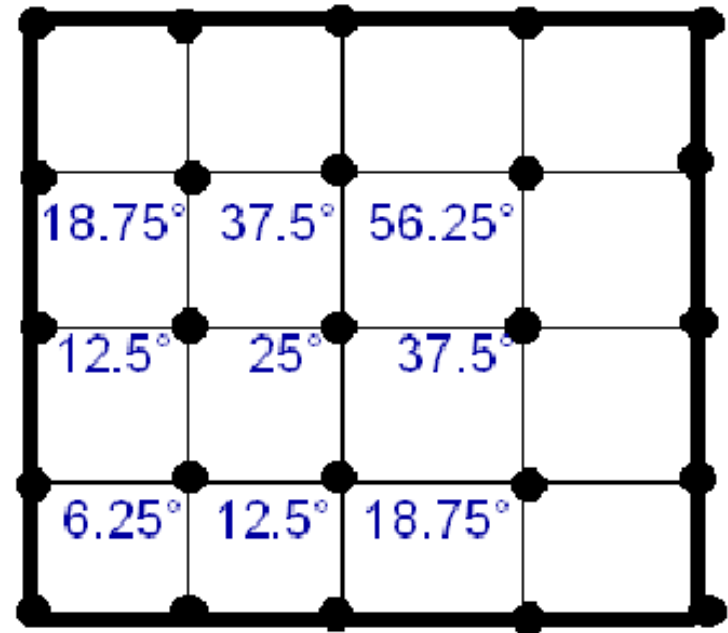


Numerical solution



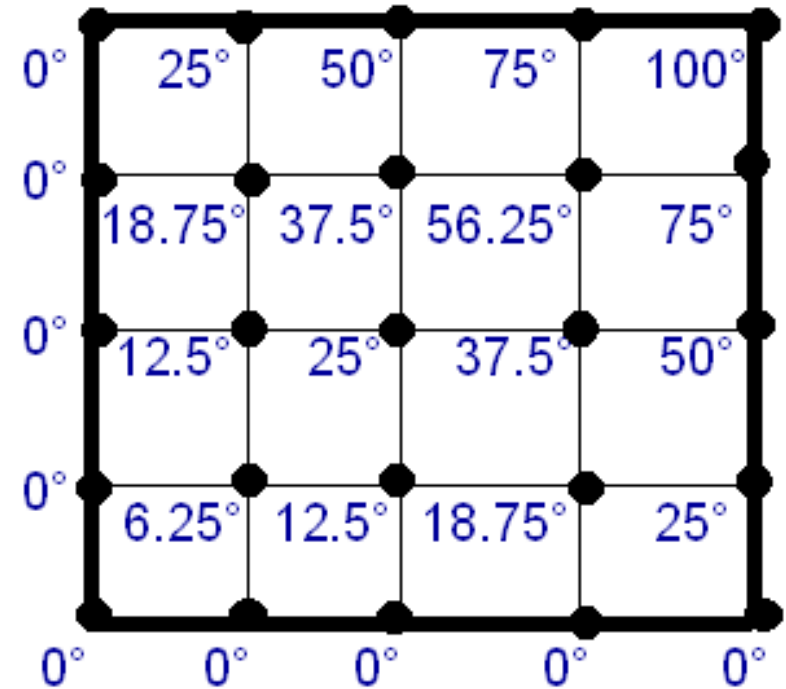
Numerical solution

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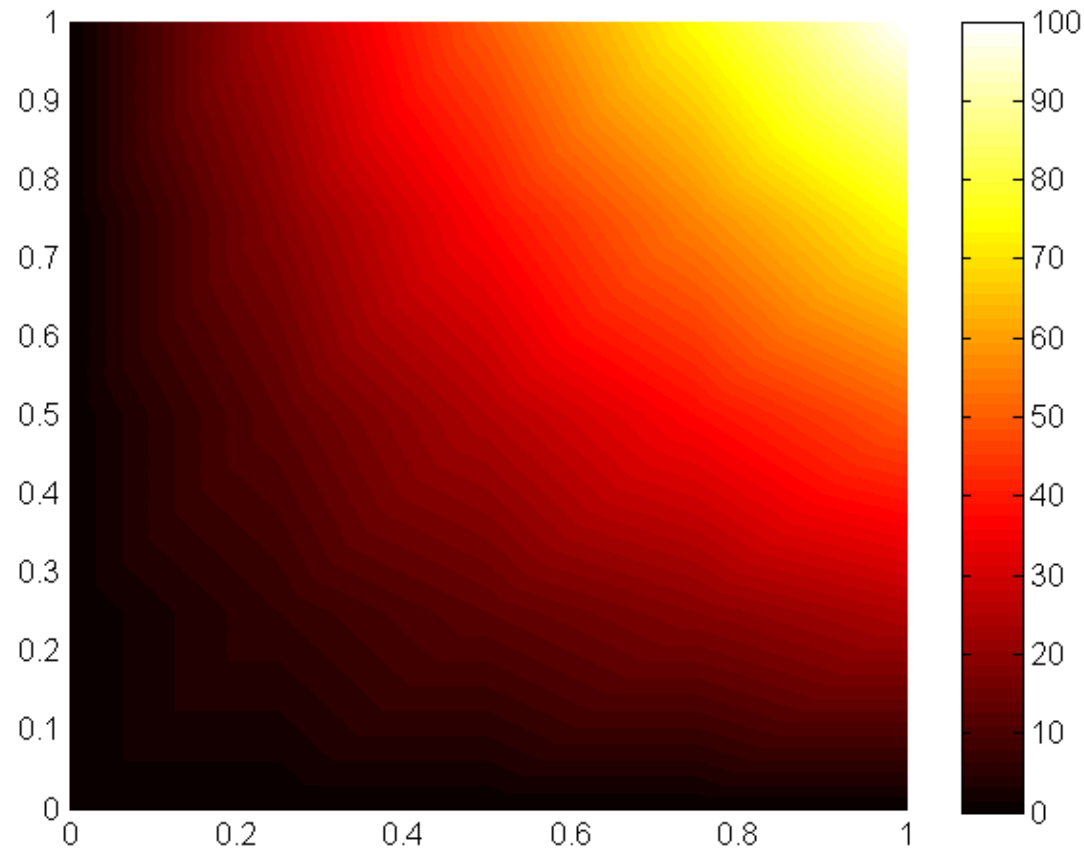
Numerical solution

$$\mathbf{x} = \begin{bmatrix} 6.25 \\ 12.50 \\ 18.75 \\ 12.50 \\ 25.00 \\ 37.50 \\ 18.75 \\ 37.50 \\ 56.25 \end{bmatrix}$$



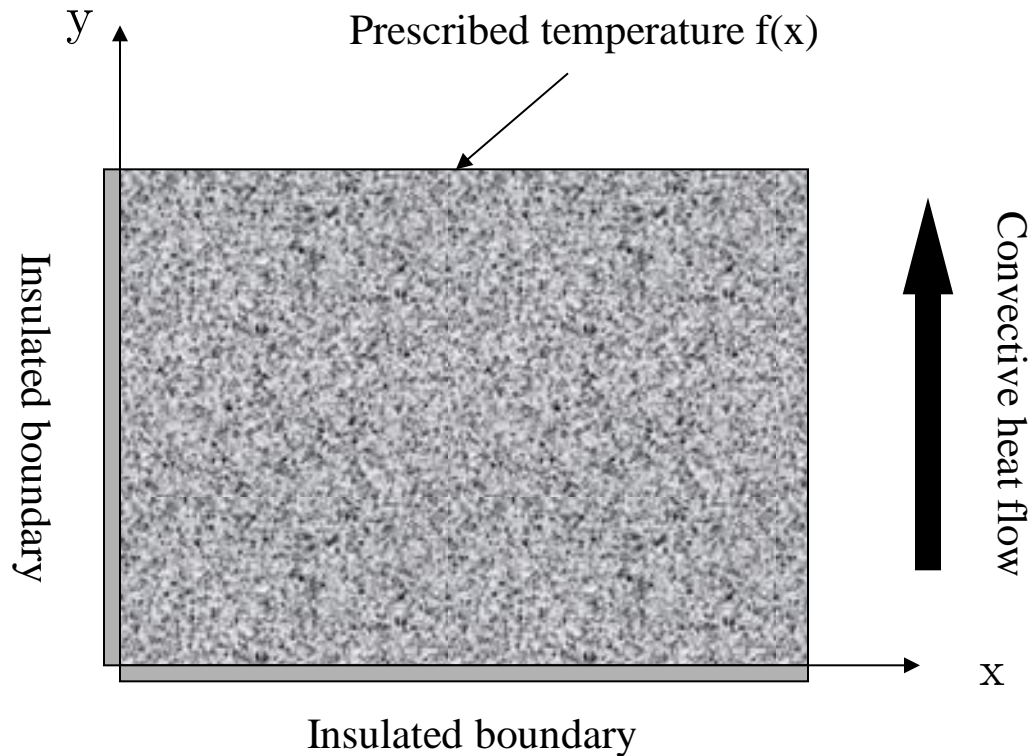
Don't forget the boundary conditions!

Numerical solution



For this problem, the numerical solution is exact (do you know why?)

Second example: Poisson equation



Ceramic plate with Dirichlet, Neumann and Robin boundary conditions

Second example: Poisson equation

- Prescribed boundary:

$$f(x) = 200 - 150x^2$$

- Insulated boundaries:

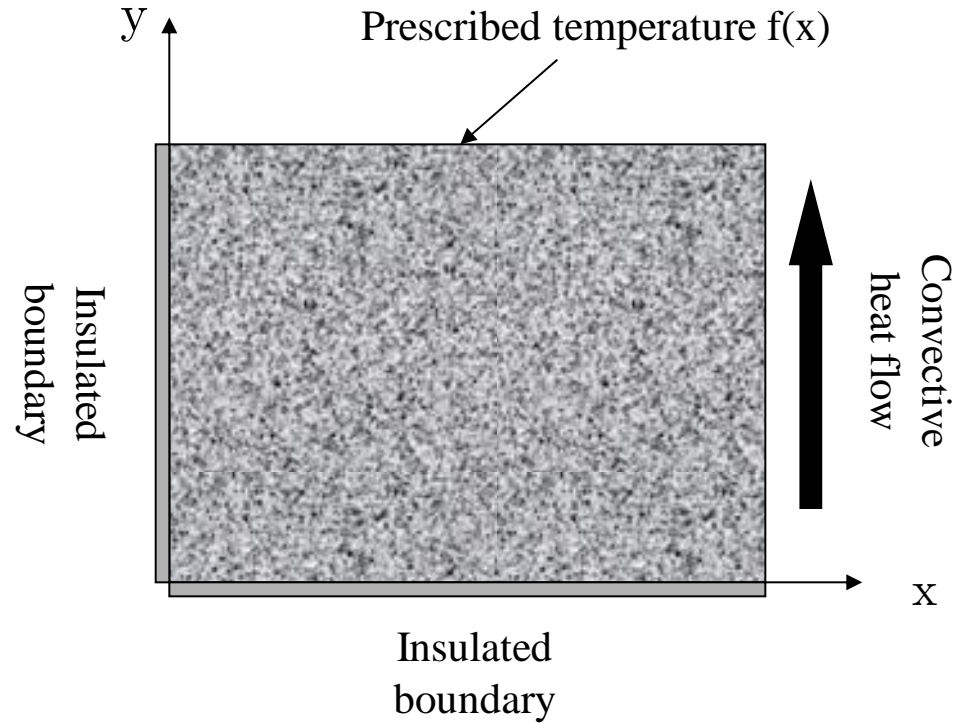
$$\nabla T \cdot \hat{\mathbf{n}} = 0$$

- Convective boundary:

$$k \nabla T \cdot \hat{\mathbf{n}} = h (T_{\infty} - T)$$

- Uniform heat source:

$$g(x, y) = g_0 \text{ (constant)}$$



Summary of the Mathematical Model

$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{g_0}{k} = 0, \quad 0 < x < a, \quad 0 < y < b$$

subject to

$$\text{at } x = 0 : \quad \frac{\partial T}{\partial x} = 0$$

$$\text{at } x = a : \quad k \frac{\partial T}{\partial x} + hT = hT_\infty$$

$$\text{at } y = 0 : \quad \frac{\partial T}{\partial y} = 0$$

$$\text{at } y = b : \quad T(x, b) = f(x)$$

Analytical Solution

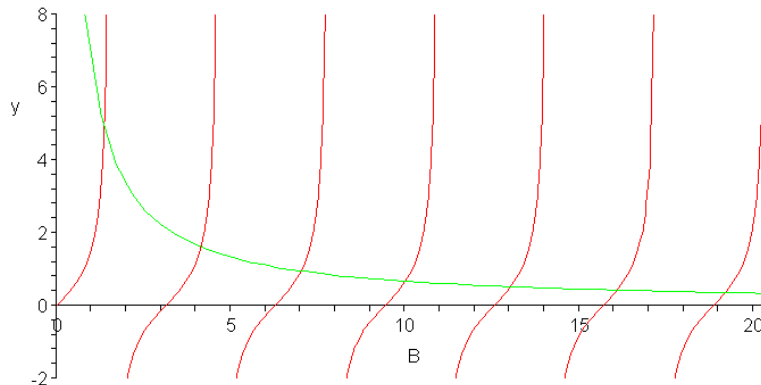
(Not examinable! You'll learn about this in MXB322.)

$$T(x, y) = \varphi(x, y) + \frac{g_0}{2k}(a^2 - x^2) + \frac{g_0 a}{h} + T_\infty$$

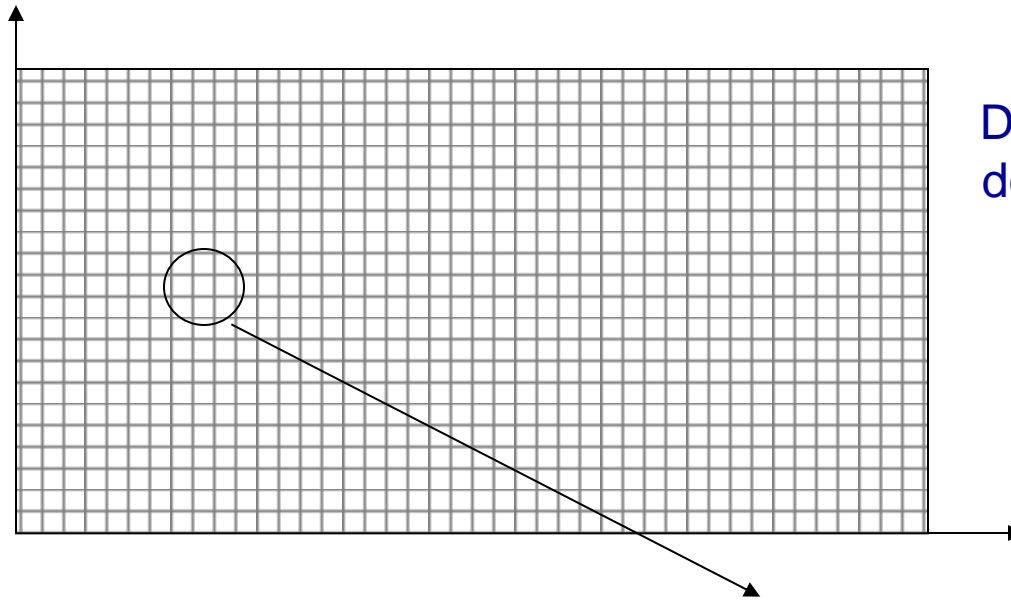
$$\varphi(x, y) = 2 \sum_{m=1}^{\infty} \frac{\beta_m^2 + H^2}{a(\beta_m^2 + H^2) + H} \frac{\cosh \beta_m y}{\cosh \beta_m b} \cos \beta_m x \int_0^a \tilde{\varphi}(\xi) \cos \beta_m \xi d\xi$$

where β_m are the roots of $\tan \beta_m a = H / \beta_m$

$$\text{and } \tilde{\varphi}(x) = f(x) - \frac{g_0}{2k}(a^2 - x^2) - \frac{g_0 a}{h} - T_\infty, \quad H = \frac{h}{k}$$



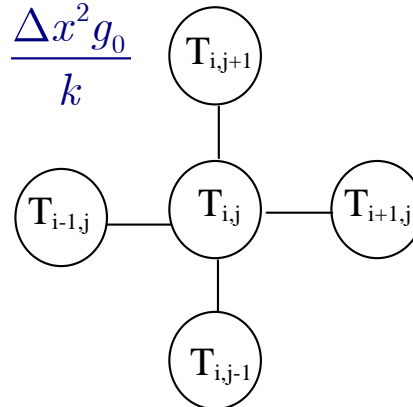
Conversion to a Matrix Problem



Discretise the domain using a mesh

$$-T_{i,j-1} - T_{i-1,j} + 4T_{i,j} - T_{i+1,j} - T_{i,j+1} = \frac{\Delta x^2 g_0}{k}$$

Finite Difference Stencil used for each internal node on the mesh

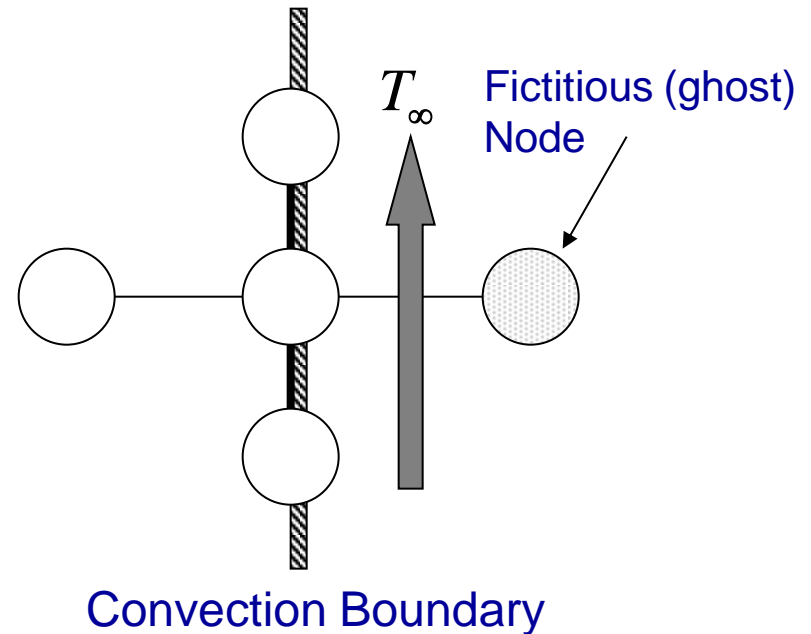
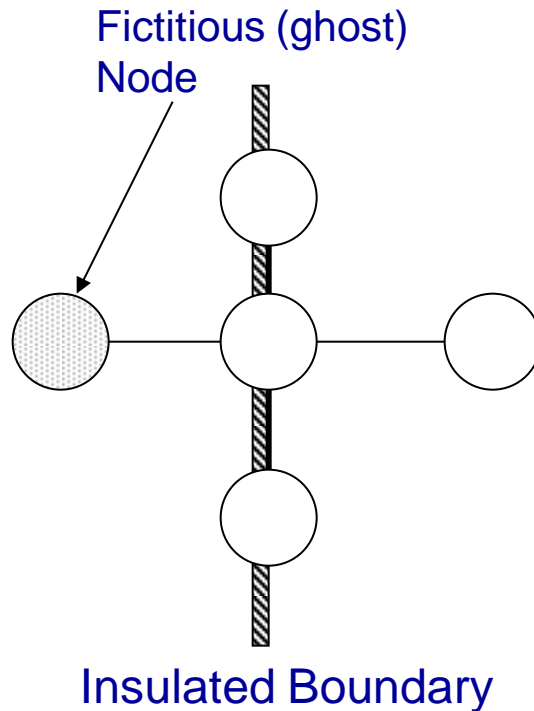


The model is converted to a matrix problem by discretising the domain and forming *finite difference equations*.

Treatment of Boundary Nodes

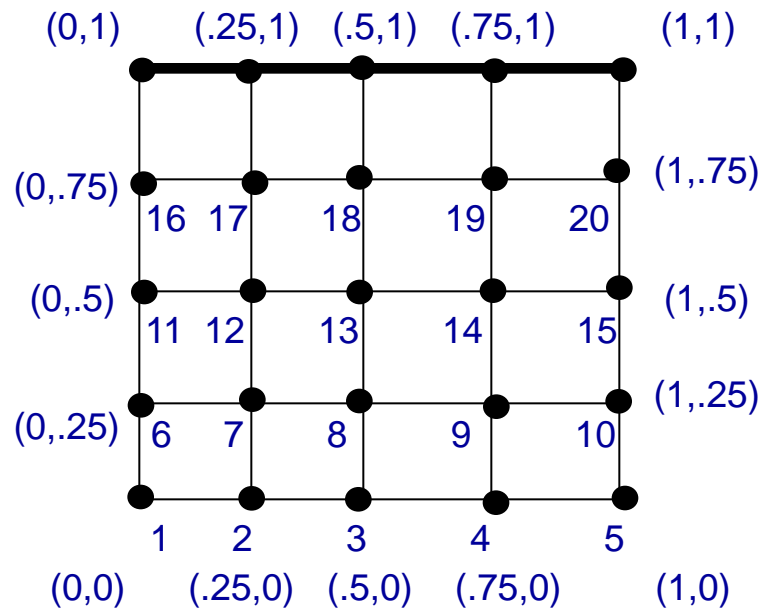
Insulated / Convection boundary:

Use Neumann / Robin condition to construct fictitious node

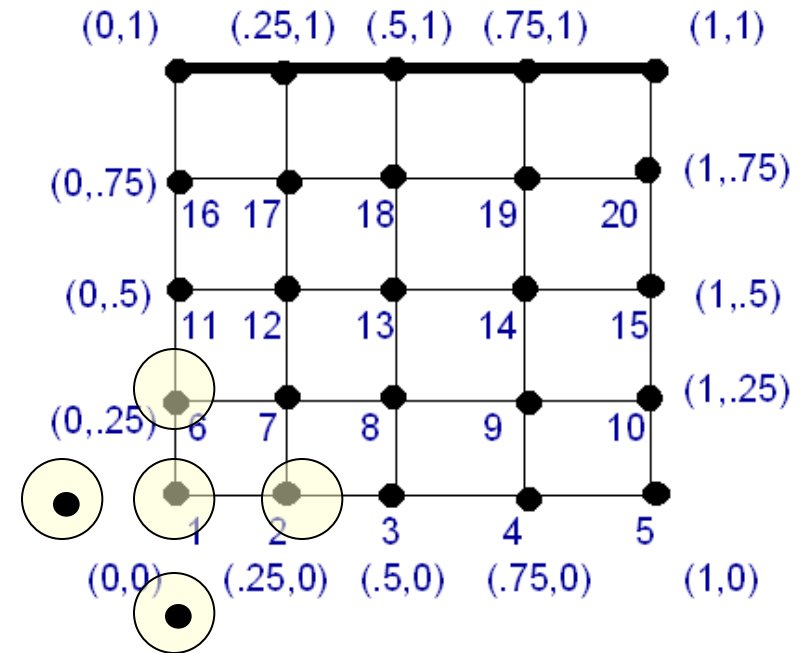
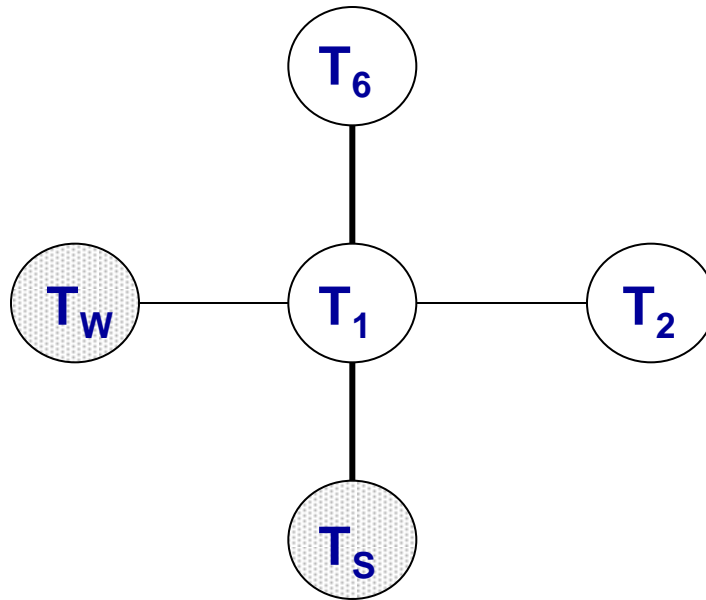


How does this process generate a matrix?

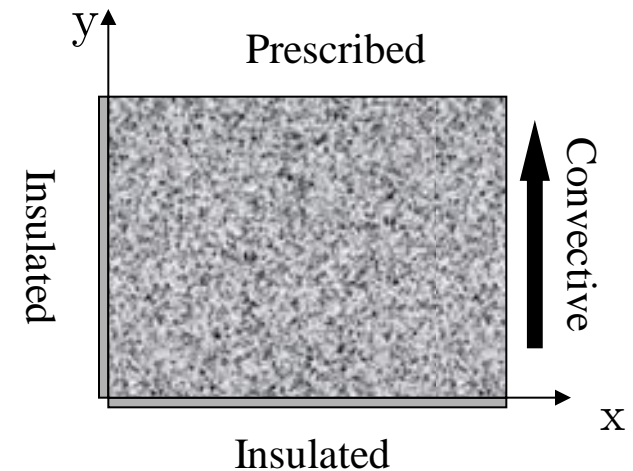
- Introduce a node numbering scheme and map (i,j) coordinates to these nodes:



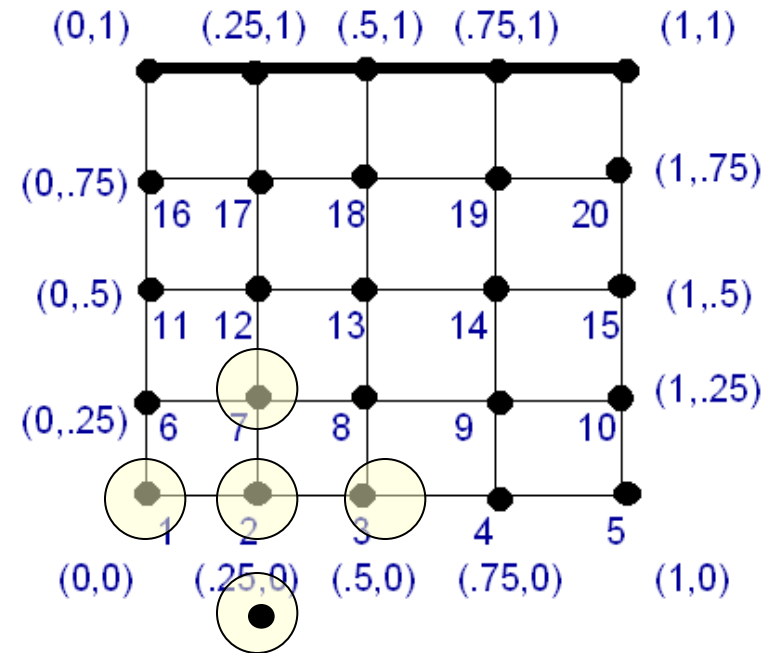
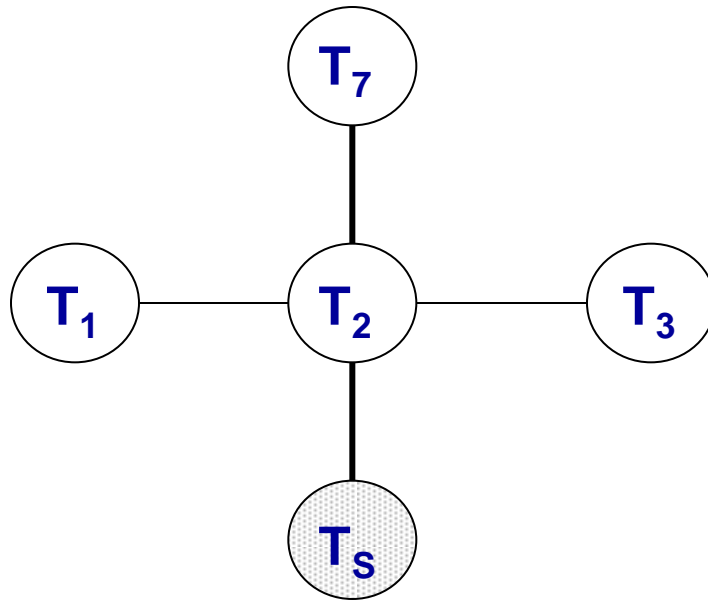
Node 1



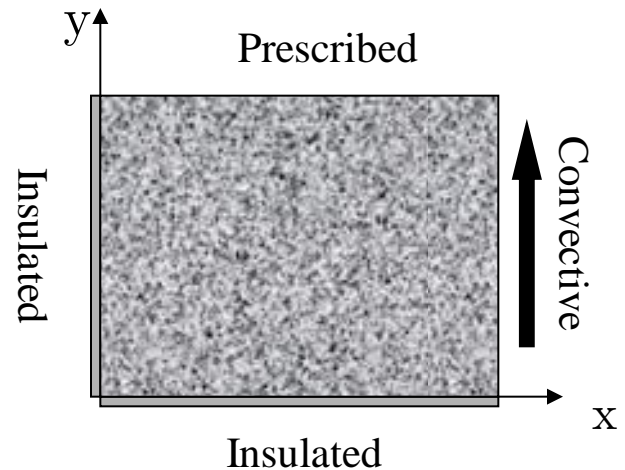
$$-T_s - T_w + 4T_1 - T_2 - T_6 = \frac{\Delta x^2 g_0}{k}$$



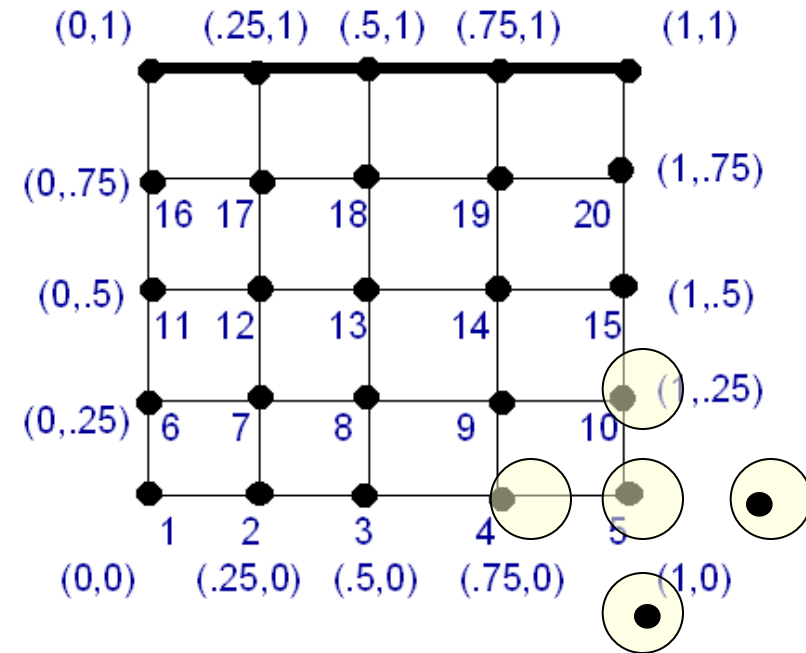
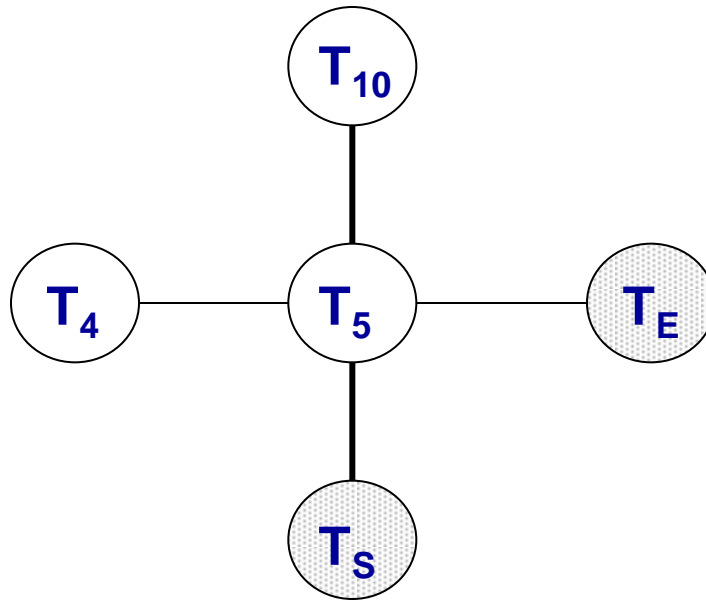
Node 2 (3,4 similar)



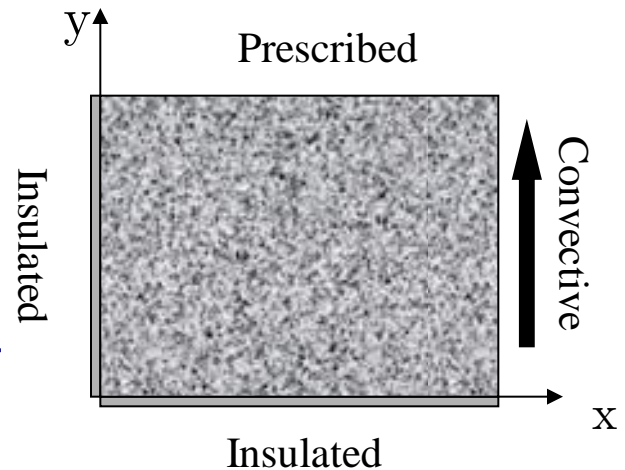
$$-T_s - T_1 + 4T_2 - T_3 - T_7 = \frac{\Delta x^2 g_0}{k}$$



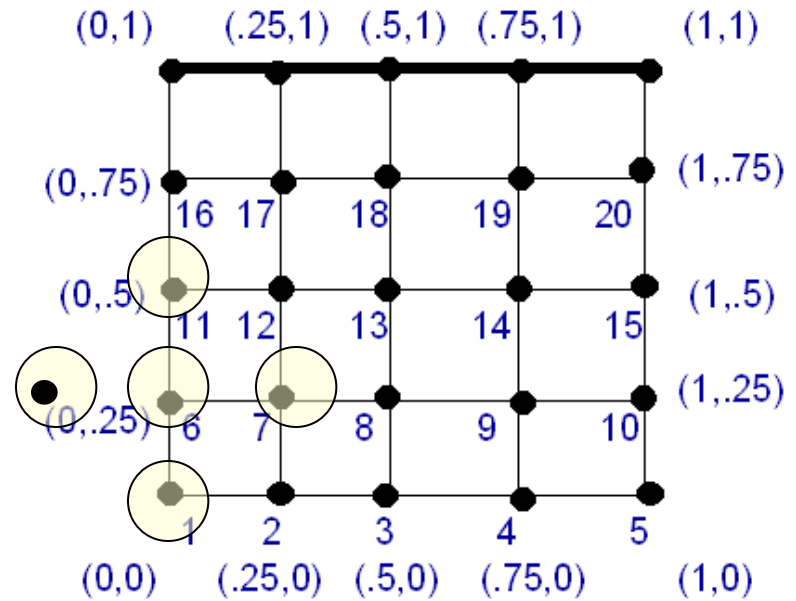
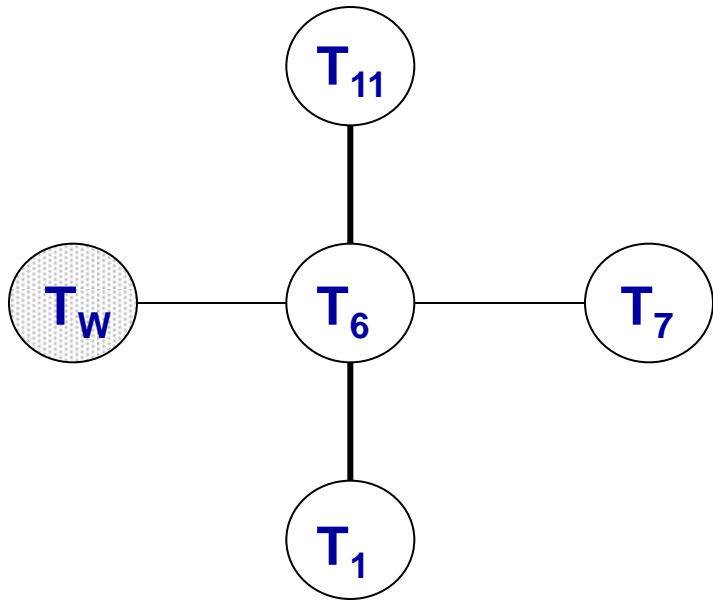
Node 5



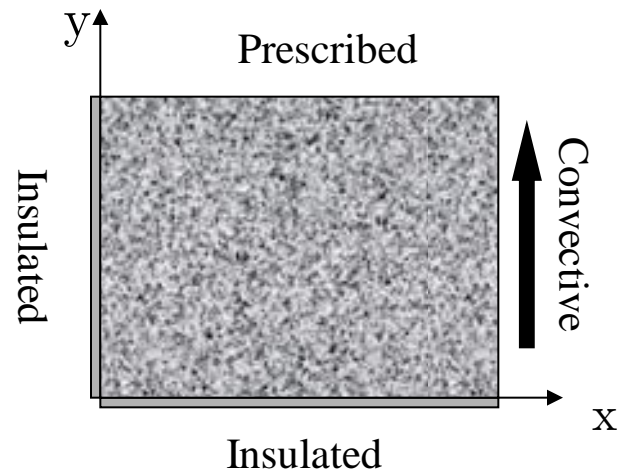
$$-T_S - T_4 + 4T_5 - T_E - T_{10} = \frac{\Delta x^2 g_0}{k}$$



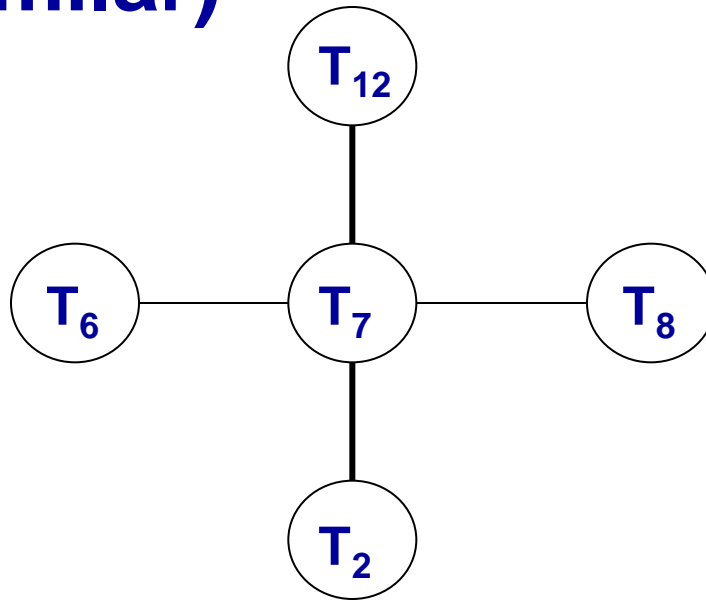
Node 6 (11 similar)



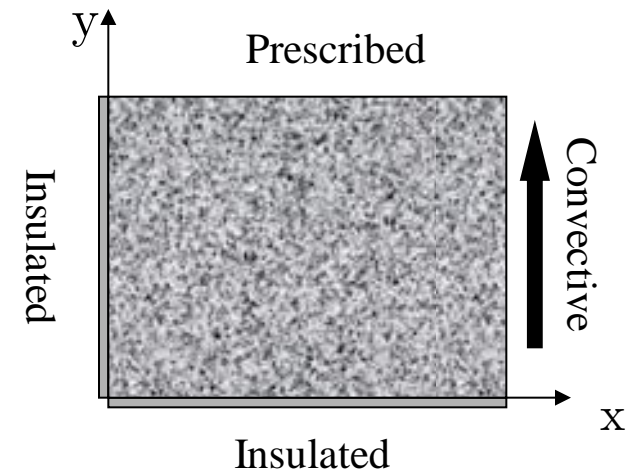
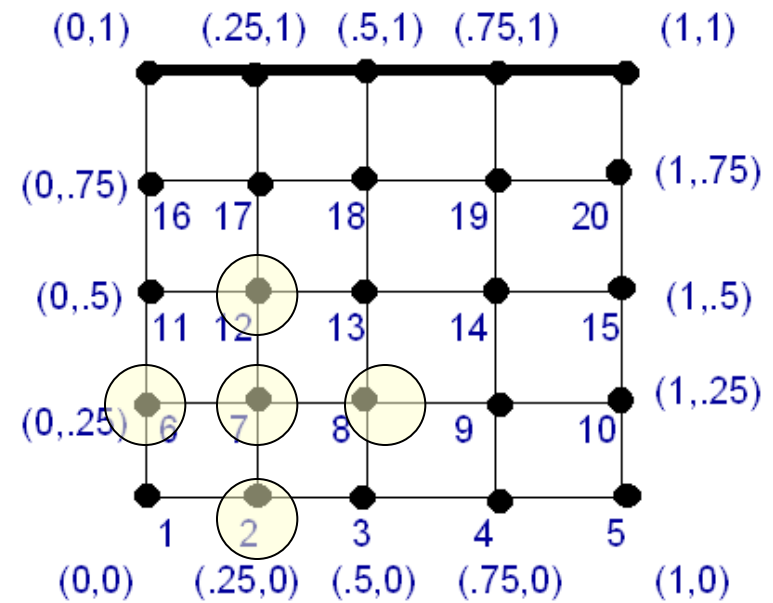
$$-T_1 - T_w + 4T_6 - T_7 - T_{11} = \frac{\Delta x^2 g_0}{k}$$



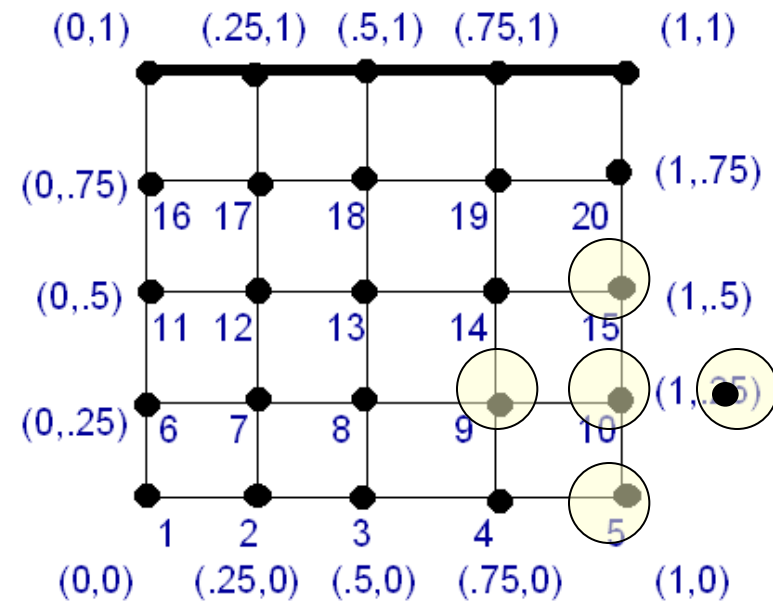
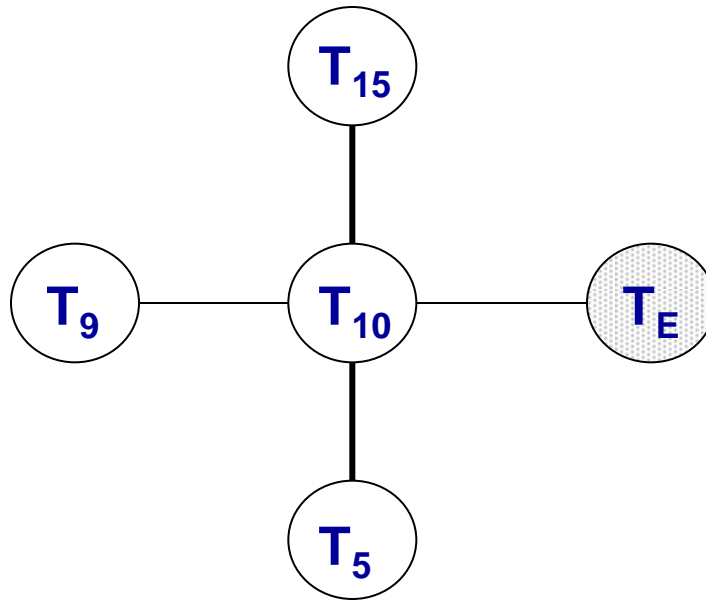
**Node 7 (8,9,12,13,14
similar)**



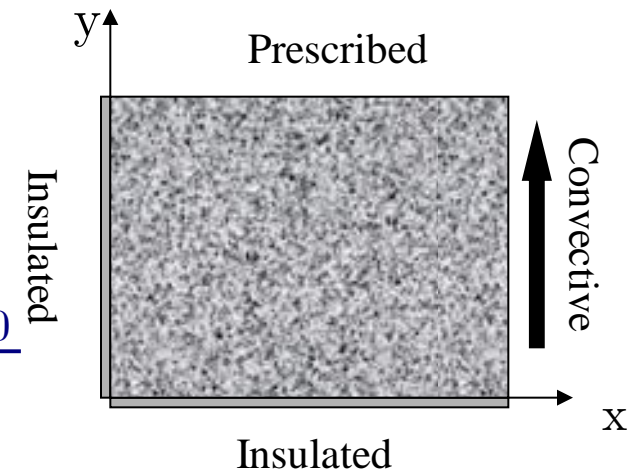
$$-T_2 - T_6 + 4T_7 - T_8 - T_{12} = \frac{\Delta x^2 g_0}{k}$$



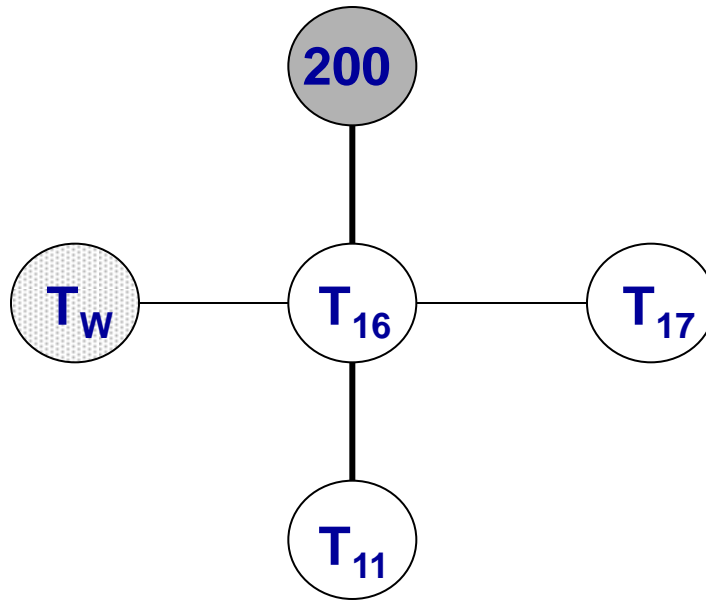
Node 10 (15 similar)



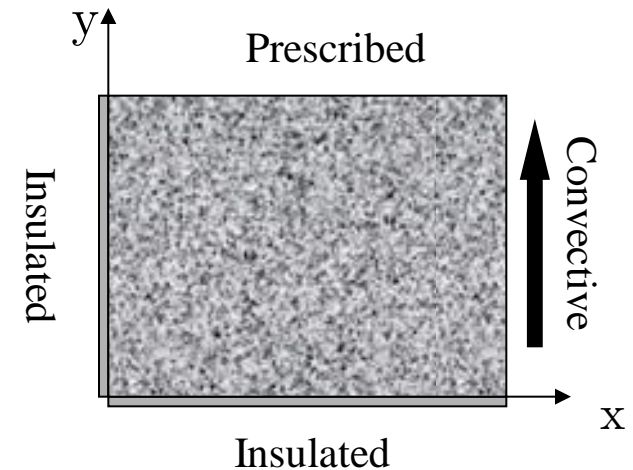
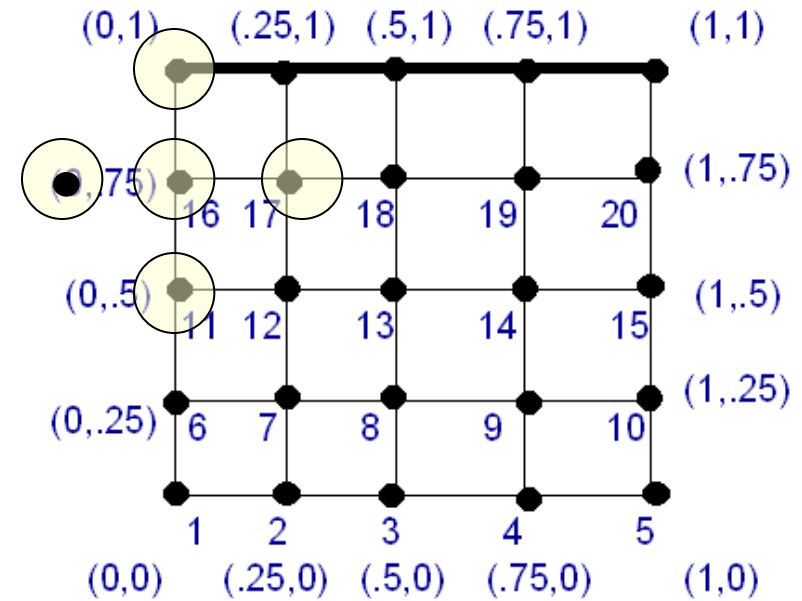
$$-T_5 - T_9 + 4T_{10} - T_E - T_{15} = \frac{\Delta x^2 g_0}{k}$$



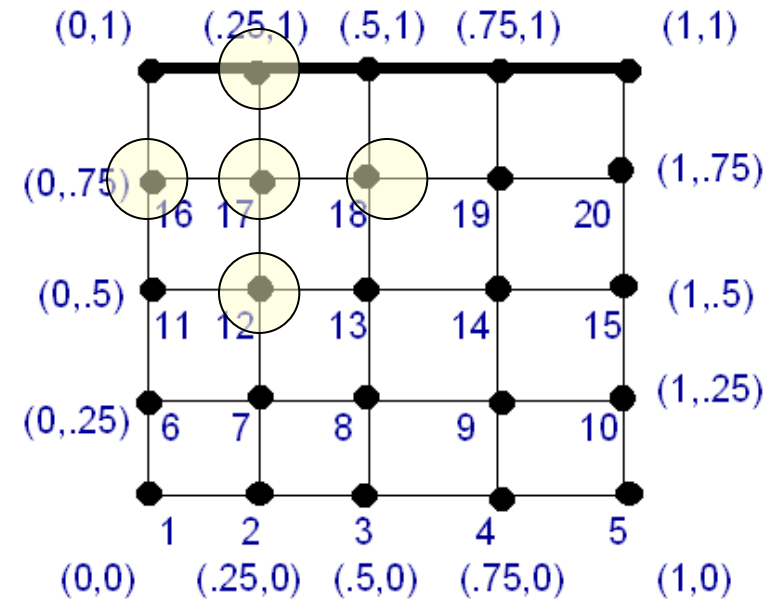
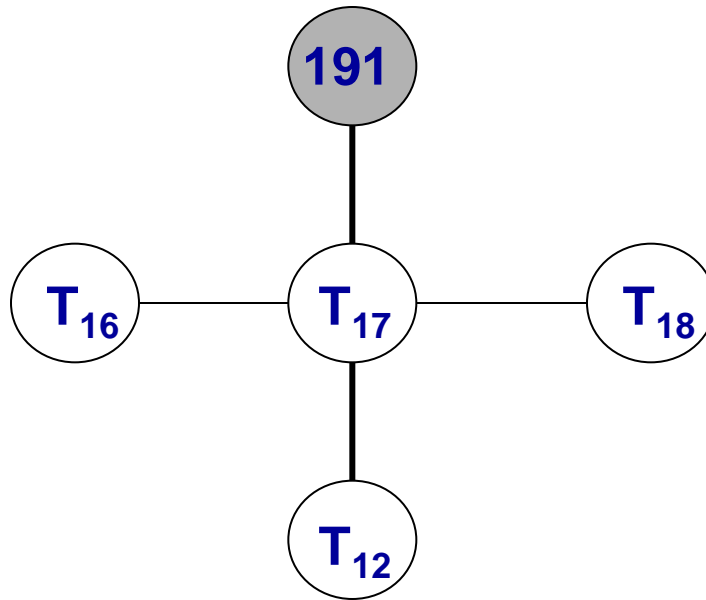
Node 16



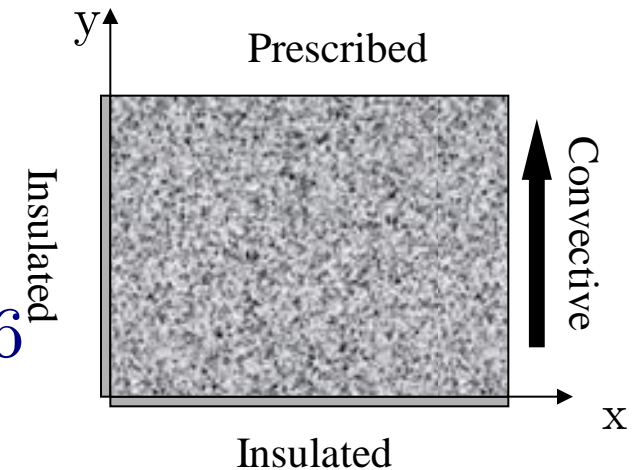
$$-T_{11} - T_w + 4T_{16} - T_{17} = \frac{\Delta x^2 g_0}{k} + 200$$



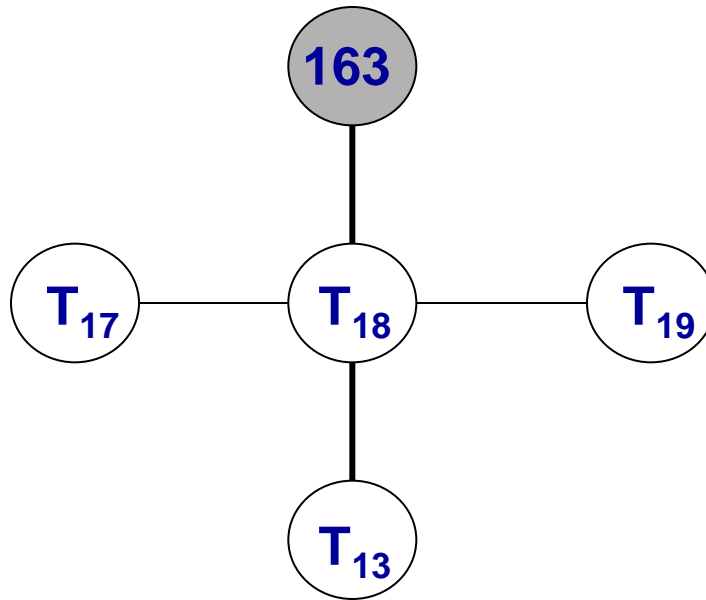
Node 17



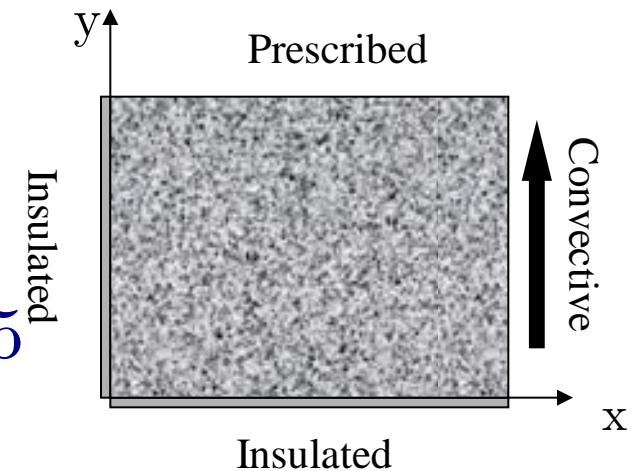
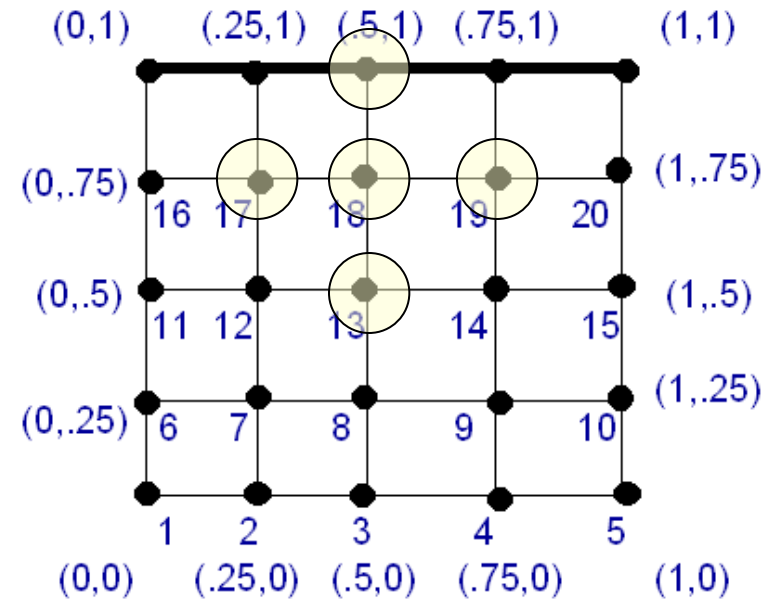
$$-T_{12} - T_{16} + 4T_{17} - T_{18} = \frac{\Delta x^2 g_0}{k} + 190.6$$



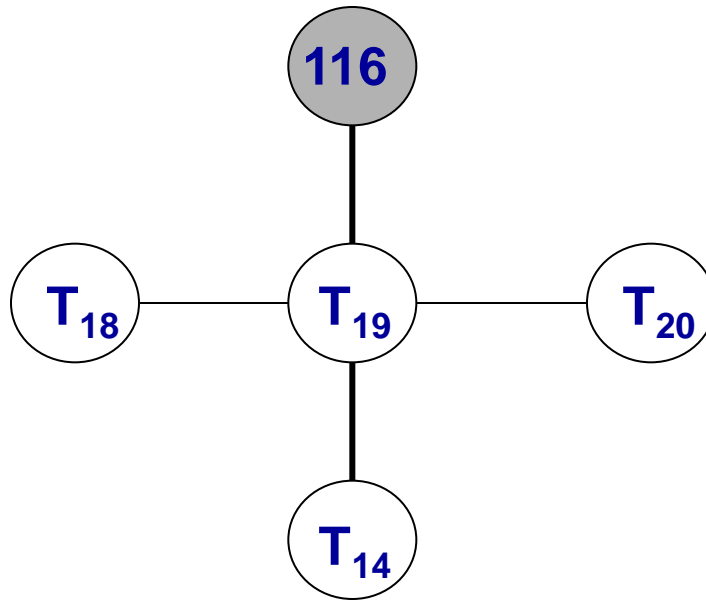
Node 18



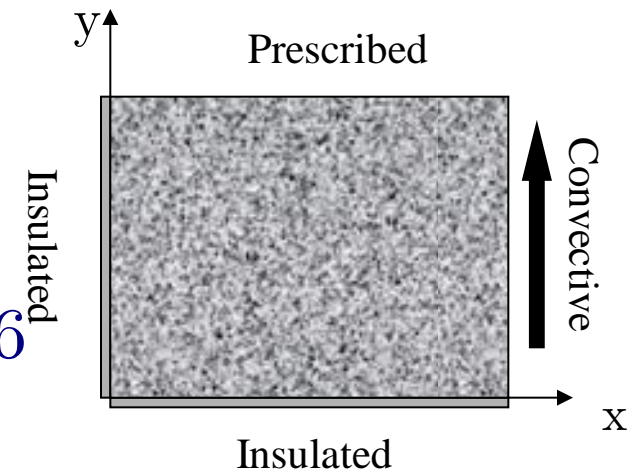
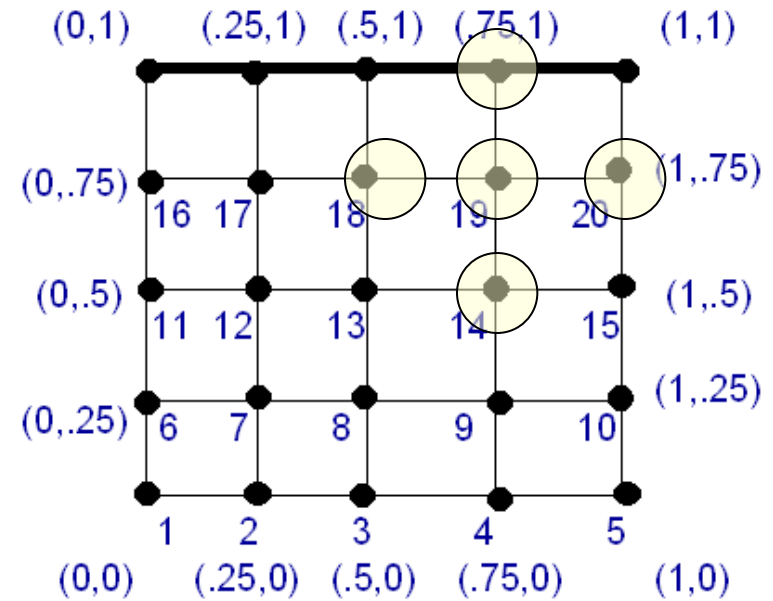
$$-T_{13} - T_{17} + 4T_{18} - T_{19} = \frac{\Delta x^2 g_0}{k} + 162.5$$



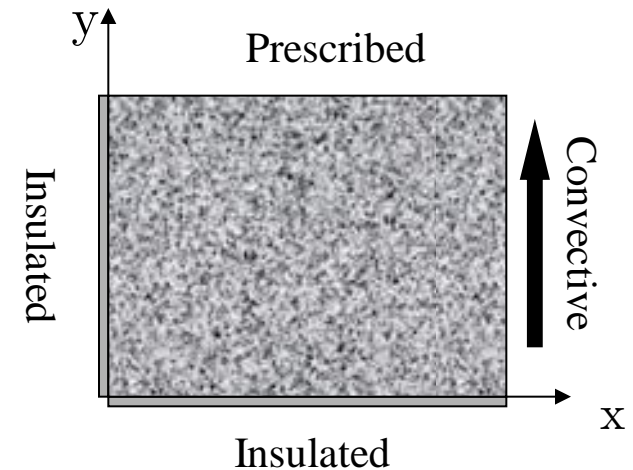
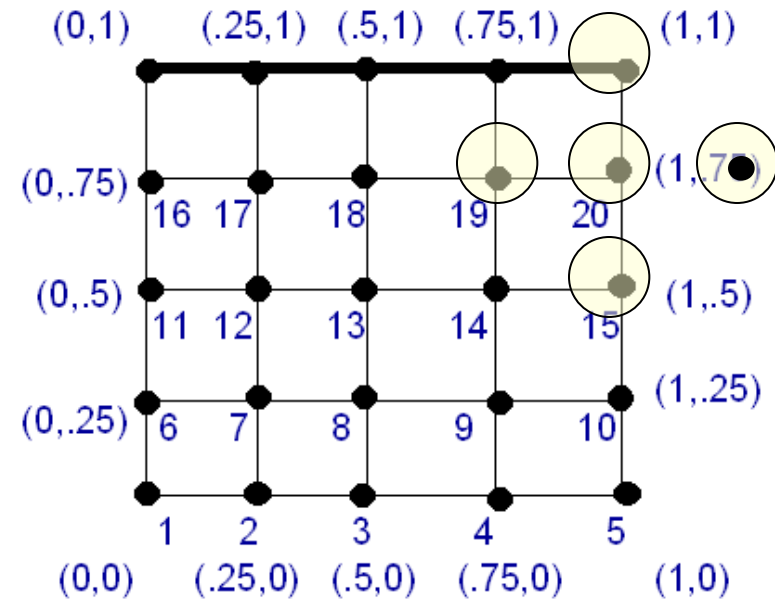
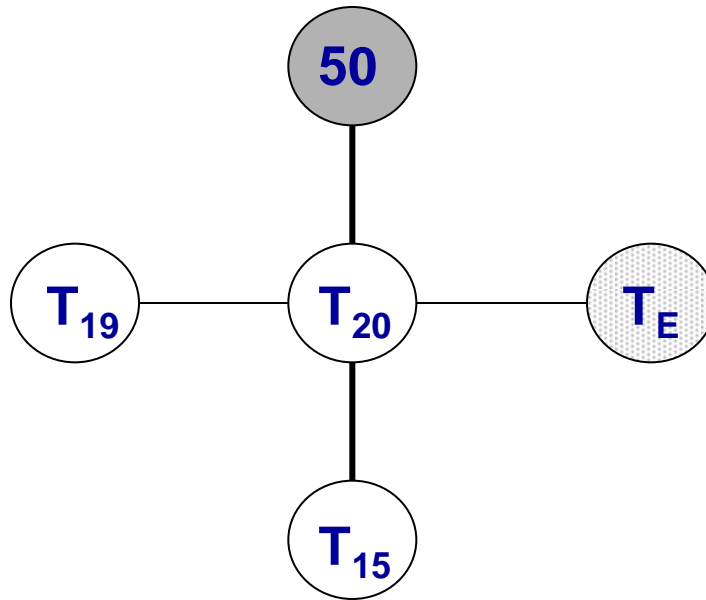
Node 19



$$-T_{14} - T_{18} + 4T_{19} - T_{20} = \frac{\Delta x^2 g_0}{k} + 115.6$$



Node 20



$$-T_{15} - T_{19} + 4T_{20} - T_E = \frac{\Delta x^2 g_0}{k} + 50$$

Fictitious (or “ghost”) Nodes

- Use second order central differences
 - Maintains second order local accuracy
 - Destroys symmetry of the matrix
- Use first order forward/backward differences
 - Maintains symmetry of the matrix
 - Only first order local accuracy (but globally still a second order method)
- For this example, we'll use second order boundary FDEs

Summary of Finite Difference Equations (FDEs)

$$(0, 0) : 4T_{0,0} - 2T_{1,0} - 2T_{0,1} = \frac{\Delta x^2 g_0}{k}$$

$$(i, 0) : -T_{i-1,0} + 4T_{i,0} - T_{i+1,0} - 2T_{i,1} = \frac{\Delta x^2 g_0}{k}$$

$$(N, 0) : -2T_{N-1,0} + (4 + 2\Delta x H) T_{N,0} - 2T_{N,1} = \frac{\Delta x^2 g_0}{k} + 2\Delta x H T_\infty$$

$$(0, j) : -T_{0,j-1} + 4T_{0,j} - 2T_{1,j} - T_{0,j+1} = \frac{\Delta x^2 g_0}{k}$$

$$(i, j) : -T_{i,j-1} - T_{i-1,j} + 4T_{i,j} - T_{i+1,j} - T_{i,j+1} = \frac{\Delta x^2 g_0}{k}$$

$$(N, j) : -T_{N,j-1} - 2T_{N-1,j} + (4 + 2\Delta x H) T_{N,j} - T_{N,j+1} = \frac{\Delta x^2 g_0}{k} + 2\Delta x H T_\infty$$

$$(0, N-1) : -T_{0,N-2} + 4T_{0,N-1} - 2T_{1,N-1} = \frac{\Delta x^2 g_0}{k} + f(0)$$

$$(i, N-1) : -T_{i,N-2} - T_{i-1,N-1} + 4T_{i,N-1} - T_{i+1,N-1} = \frac{\Delta x^2 g_0}{k} + f(i\Delta x)$$

$$(N, N-1) : -T_{N,N-2} - 2T_{N-1,N-1} + (4 + 2\Delta x H) T_{N,N-1} = \frac{\Delta x^2 g_0}{k} + 2\Delta x H T_\infty + f(a)$$

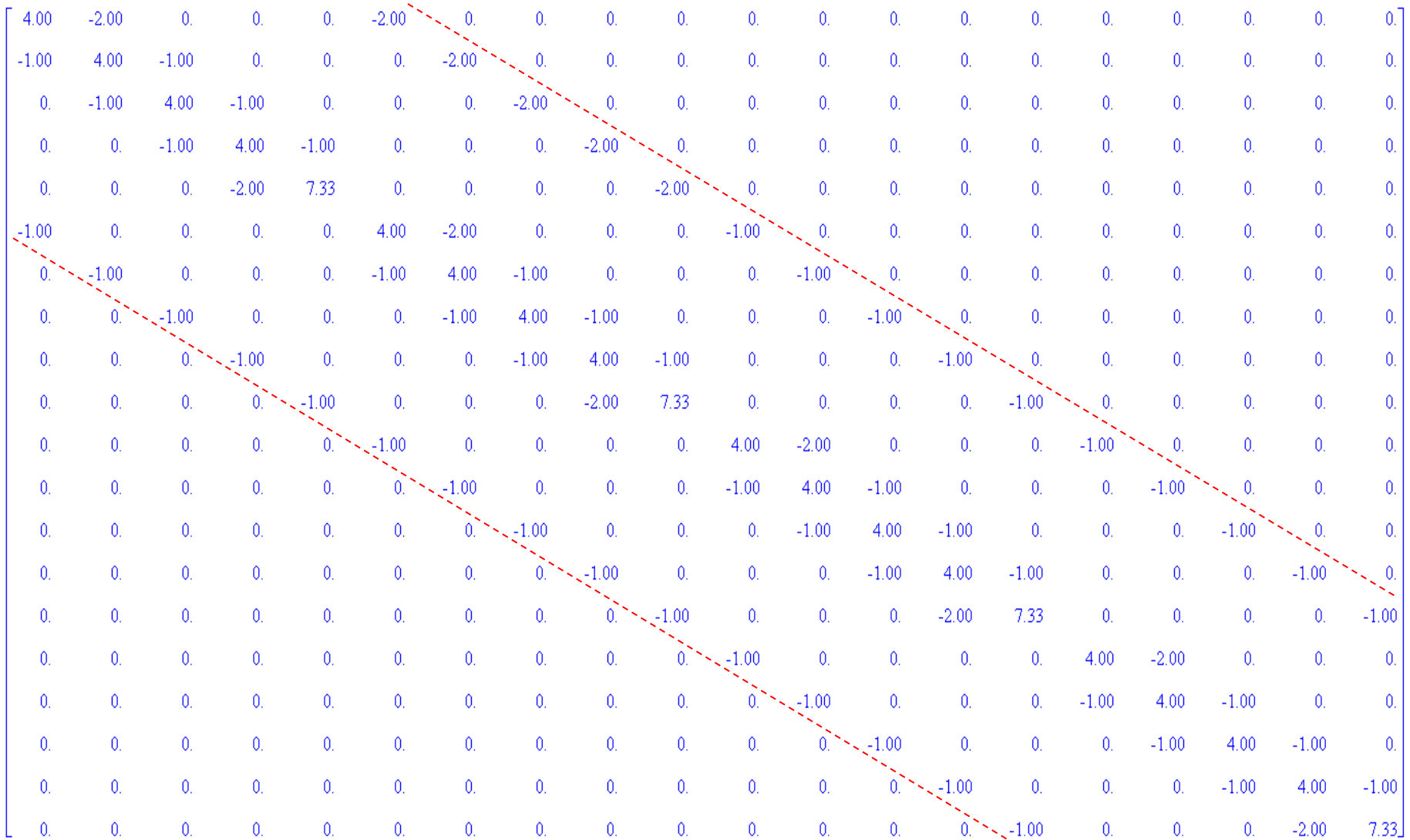
$$H = \frac{h}{k}$$

Note: These finite difference equations (FDEs) have been generated using second order central differences for fictitious nodes. A different system would be generated if first order forward or backward differences were used.

Discrete Poisson equation: A

4.00	-2.00	0.	0.	0.	-2.00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
-1.00	4.00	-1.00	0.	0.	0.	-2.00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	-1.00	4.00	-1.00	0.	0.	0.	-2.00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	-1.00	4.00	-1.00	0.	0.	0.	-2.00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	-2.00	7.33	0.	0.	0.	0.	-2.00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
-1.00	0.	0.	0.	0.	4.00	-2.00	0.	0.	0.	-1.00	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00	0.	0.	0.	-1.00	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00	0.	0.	0.	-1.00	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00	0.	0.	0.	-1.00	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	-1.00	0.	0.	0.	-2.00	7.33	0.	0.	0.	0.	-1.00	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	-1.00	0.	0.	0.	0.	4.00	-2.00	0.	0.	0.	-1.00	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00	0.	0.	0.	-1.00	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00	0.	0.	0.	-1.00	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00	0.	0.	0.	-1.00	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	-2.00	7.33	0.	0.	0.	0.	-1.00
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	0.	4.00	-2.00	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	-2.00	7.33

Discrete Poisson equation: A



4.00	-2.00	0.	0.	0.	-2.00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
-1.00	4.00	-1.00	0.	0.	0.	-2.00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	-1.00	4.00	-1.00	0.	0.	0.	-2.00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	-1.00	4.00	-1.00	0.	0.	0.	-2.00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	-2.00	7.33	0.	0.	0.	0.	-2.00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
-1.00	0.	0.	0.	0.	4.00	-2.00	0.	0.	0.	-1.00	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00	0.	0.	0.	-1.00	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00	0.	0.	0.	-1.00	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00	0.	0.	0.	-1.00	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	-1.00	0.	0.	0.	-2.00	7.33	0.	0.	0.	0.	-1.00	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	-1.00	0.	0.	0.	0.	4.00	-2.00	0.	0.	0.	-1.00	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00	0.	0.	0.	-1.00	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00	0.	0.	0.	-1.00	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00	0.	0.	0.	-1.00	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	-2.00	7.33	0.	0.	0.	0.	-1.00
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	0.	4.00	-2.00	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	-2.00	7.33

Discrete Poisson equation: A

4.00	-2.00	0.	0.	0.	-2.00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
-1.00	4.00	-1.00	0.	0.	0.	-2.00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	-1.00	4.00	-1.00	0.	0.	0.	-2.00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	-1.00	4.00	-1.00	0.	0.	0.	-2.00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	-2.00	7.33	0.	0.	0.	0.	-2.00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
-1.00	0.	0.	0.	0.	4.00	-2.00	0.	0.	0.	-1.00	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00	0.	0.	0.	-1.00	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00	0.	0.	0.	-1.00	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00	0.	0.	0.	-1.00	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	-1.00	0.	0.	0.	-2.00	7.33	0.	0.	0.	0.	-1.00	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	-1.00	0.	0.	0.	0.	4.00	-2.00	0.	0.	0.	-1.00	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00	0.	0.	0.	-1.00	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00	0.	0.	0.	-1.00	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00	0.	0.	0.	-1.00	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	-2.00	7.33	0.	0.	0.	0.	-1.00
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	0.	4.00	-2.00	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	-1.00	4.00	-1.00
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	-1.00	0.	0.	0.	-2.00	7.33

Discrete Poisson equation: b

0.4167
0.4167
0.4167
0.4167
83.7500
0.4167
0.4167
0.4167
0.4167
83.7500
0.4167
0.4167
0.4167
0.4167
83.7500
200.4167
191.0417
162.9167
116.0417
133.7500

Analytical Solution

200.000	190.625	162.500	115.625	50.0000
158.149	150.619	128.493	93.6310	51.1706
131.081	124.983	107.293	79.9501	46.3005
115.982	110.743	95.6002	72.2595	43.3732
111.138	106.179	91.8575	69.7816	42.4199

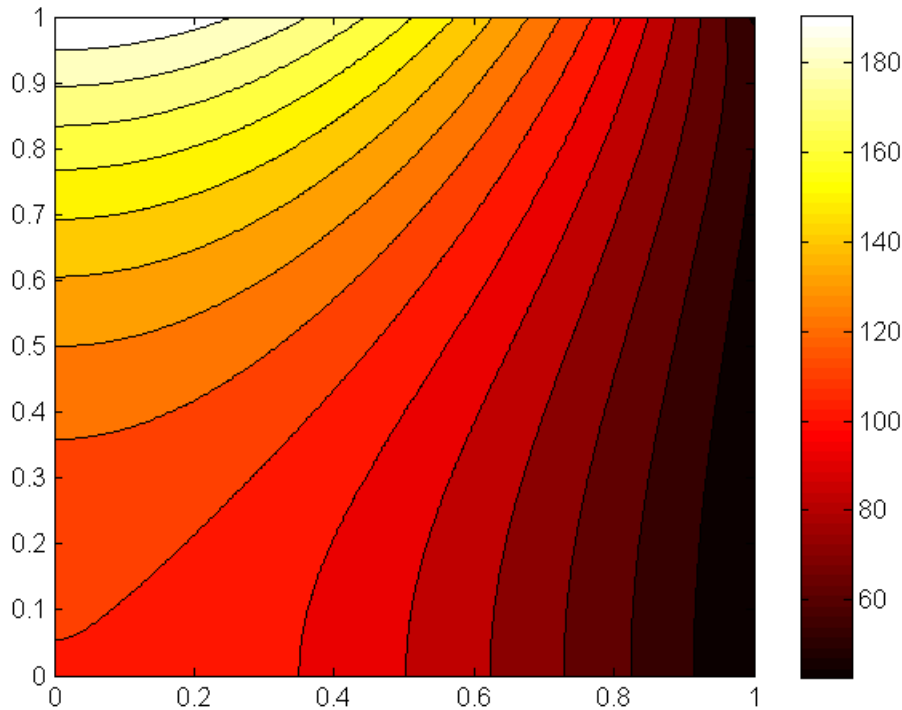
Numerical Solution

200.000	190.625	162.500	115.625	50.0000
158.542	151.014	128.873	93.7785	50.0865
131.725	125.598	107.784	80.1128	45.9941
116.745	111.452	96.1339	72.4782	43.2283
111.934	106.915	92.4052	70.0212	42.3067

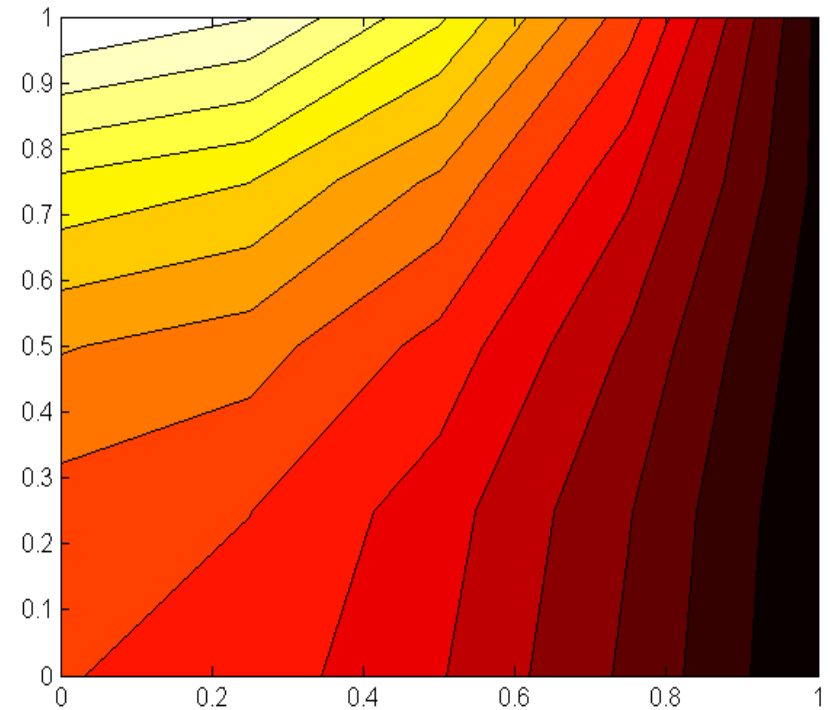
The physical parameters used for the computations are:

$$a = b = 1m, k = 3 \text{ W m}^{-1} \text{ }^{\circ}\text{C}^{-1}, h = 20 \text{ W m}^{-2} \text{ }^{\circ}\text{C}^{-1}, g_0 = 20 \text{ W m}^{-3}, T_{\infty} = 25 \text{ }^{\circ}\text{C}, f(x) = 200 - 150x^2$$

Analytical Solution



Numerical Solution



Higher accuracy could be obtained in the numerical solution by using a finer mesh (more nodes) .